PRELIMINARY HYDROLOGY AND HYDRAULIC STUDY FOR HEMET 30

RIVERSIDE COUNTY
CALIFORNIA

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This report has been prepared by or under the direction of the following registered civil engineer who attests to the technical information contained herein. The registered civil engineer has also judged the qualifications of any technical specialists providing engineering data upon which recommendations, conclusions, and decisions are based.



Joseph L. Castaneda RCE 59835 Registered Civil Engineer	03/09/2021 Date	Seal

Table of Contents

I. INTRODUCTION **1**
II. PROJECT SITE AND DRAINAGE AREA OVERVIEW **1**
III. HYDROLOGY ANALYSIS **2**
IV. HYDRAULIC ANALYSIS **3**
V. ONSITE BASIN ROUTING ANALYSIS **4**
VI. OFFSITE CHANNEL ANALYSES **4**
VII. CONCLUSIONS **6**
VIII. REFERENCES **6**

FIGURES

FIGURE 1 VICINITY MAP

APPENDICES

APPENDIX A: **PRE-PROJECT CONDITION RATIONAL METHOD HYDROLOGY**
APPENDIX A.1: AREA "A"
APPENDIX A.2: AREA "B"

APPENDIX B: **POST-PROJECT CONDITION RATIONAL METHOD HYDROLOGY**
APPENDIX B.1: AREA "A"
APPENDIX B.2: AREA "B"
APPENDIX B.3: AREA "C"
APPENDIX B.4: OFFSITE AREA "C" – EXISTING CONDITION OFFSITE AREA
APPENDIX B.5: OFFSITE AREA "C" – ULTIMATE CONDITION OFFSITE AREA

APPENDIX C: **PRE-PROJECT CONDITION UNIT HYDROGRAPH HYDROLOGY**
APPENDIX C.1: AREA "A" – ONSITE
APPENDIX C.2: AREA "C" – OFFSITE

APPENDIX D: **POST-PROJECT CONDITION UNIT HYDROGRAPH HYDROLOGY**
APPENDIX D.1: AREA "A" – ONSITE
APPENDIX D.2: AREA "C" – OFFSITE

APPENDIX E: **STREET CAPACITY CALCULATIONS**
APPENDIX E.1: HALF-STREET CAPACITY RATING TABLE

APPENDIX E.2: FULL STREET CAPACITY RATING TABLE

APPENDIX F: PRELIMINARY STORM DRAIN SIZING CALCULATIONS
APPENDIX F.1: LINE "A" STORM DRAIN AND LATERALS
APPENDIX F.2: LINE "B" STORM DRAIN AND LATERALS
APPENDIX F.3: LINE "C" STORM DRAIN
APPENDIX F.4: LINE "D" STORM DRAIN
APPENDIX F.5: LINE "E" STORM DRAIN
APPENDIX F.6: LINE "F" STORM DRAIN

APPENDIX G: ONSITE BASIN ROUTING ANALYSES
APPENDIX G.1: BASIN OUTFLOW CALCULATIONS
APPENDIX G.2: BASIN STORAGE VOLUME VS OUTFLOW TABLE
APPENDIX G.3: ONSITE BASIN ROUTING CALCULATIONS – 2-YEAR, 24-HOUR STORM DURATION
APPENDIX G.4: ONSITE BASIN ROUTING CALCULATIONS – 10-YEAR, 24-HOUR STORM DURATION
APPENDIX G.4: ONSITE BASIN ROUTING CALCULATIONS – 100-YEAR, 1-HOUR STORM DURATION

APPENDIX H: OFFSITE INTERIM CHANNEL ANALYSIS
APPENDIX H.1: COMBINED OFFSITE HYDROGRAPH AND ONSITE BASIN ROUTING CALCULATIONS – 100-YEAR, 1-HOUR STORM DURATION
APPENDIX H.2: PRE-PROJECT TWO DIMENSIONAL HEC-RAS WATER SURFACE ELEVATION PROFILE LINES
APPENDIX H.3: POST-PROJECT TWO DIMENSIONAL HEC-RAS WATER SURFACE ELEVATION PROFILE LINES
APPENDIX H.4: INTERIM CHANNEL STORAGE VOLUME CALCULATIONS
APPENDIX H.5: DRAWDOWN CALCULATIONS

EXCERPTS

EXCERPT A DRYWELL PERCOLATION TESTING – WILL BE PROVIDED

EXHIBITS

EXHIBIT A: EXISTING CONDITION RATIONAL METHOD HYDROLOGY MAP
EXHIBIT B: POST-PROJECT CONDITION RATIONAL METHOD HYDROLOGY MAP
EXHIBIT C: EXISTING CONDITION UNIT HYDROGRAPH HYDROLOGY MAP
EXHIBIT D: POST-PROJECT CONDITION UNIT HYDROGRAPH HYDROLOGY MAP
EXHIBIT E: DRAINAGE FACILITIES MAP
EXHIBIT F: HYDROLOGIC SOILS MAP
EXHIBIT G: RAINFALL MAPS
EXHIBIT H: SLOPE OF INTENSITY DURATION CURVES

EXHIBIT I: PRE-PROJECT TWO DIMENSIONAL HEC-RAS MAP
EXHIBIT J: POST-PROJECT TWO DIMENSIONAL HEC-RAS MAP

I. INTRODUCTION

Hemet 30 is a proposed residential development located in the unincorporated area of Hemet. The project proposes to construct 151 residential lots which are considered medium to medium high density residential lots. The project will also include a park area, a water quality/increased runoff mitigation basin, and a temporary channel fronting the project site for offsite flows.

The scope of this report will include the following:

- Perform hydrology analyses for the offsite and onsite areas for the pre-project and post-project conditions.
- Determine the necessary storm drain improvements to flood protect the project site
- Demonstrate that the proposed basin will adequately address increased runoff mitigation.
- Determine the necessary offsite drainage improvements that will adequately mimic the existing condition flow patterns
- Preparation of a preliminary hydrology and hydraulics report which summarizes the calculations and findings.

II. PROJECT SITE AND DRAINAGE OVERVIEW

Hemet 30 is a proposed residential development that will construct residential homes, subsurface storm drain, a bioretention basin, a temporary channel, a park area and utility infrastructure. The project will collect onsite flows via subsurface storm drain and discharge into the onsite Bioretention Basin where flows will be treated for water quality purposes (consistent with the Water Quality Management Plan) and mitigate for increased runoff. The project site is approximately 30 acres (including the temporary channel), and is roughly bounded by Joel Drive to the east, Highway 74 to the north, and undeveloped area to the south and west. The project is located in Section 14 of Township 5 South, Range 2 West. See Figure 1 – Vicinity Map.

There is currently no drainage infrastructure immediately downstream of the project site. An existing development just east of the project site has constructed a portion of Joel Road at the south east corner of the project. The project will extend Donald Street into the project. An interim channel will be constructed along Highway 74 that will collect the offsite flows. Flows will then pond at the downstream end for 2 feet until flows overtop and sheet flow easterly to mimic the existing drainage conditions. A two dimensional HEC-RAS model was prepared for the tributary pre-project and post-project conditions.

III. HYDROLOGY ANALYSIS

The RCFC & WCD Hydrology Manual (Reference 1) was used to develop the hydrological parameters for the rational method and unit hydrograph method. The calculations were performed using the computer program developed by Civil Cadd/Civil Design.

The existing soil classification for the area consists of Hydrologic Soil Type "A", "B", "C", and "D", as shown on Exhibit F. Exhibit F is a hydrologic soils map that was obtained from the United States Department of Agriculture, Natural Resources Conservation Service (NRCS). As recommended by the County of Riverside, an Antecedent Moisture Condition (AMC) I was utilized for the 2-year storm event and AMC II was utilized for the 10-year and 100-year storm events.

The following rainfall depths were obtained from the RCFC & WCD Hydrology Manual's Isohyetal Maps.

Storm Event	1-hour (in)	3-hour (in)	6-hour (in)	24-hour (in)
2-Year	0.50	0.80	1.20	1.80
100-Year	1.20	1.80	2.50	4.50

The slope value used for the rational method value is 0.50. The rainfall maps have been included as Exhibit G, and the slope of intensity duration curves have been included as Exhibit H.

The existing condition hydrology analyzed two watershed areas designated as Area "A" and Area "B". Area "A" is the offsite westerly watershed area, as well as the majority of the onsite area, that is tributary to the south east corner of the project site. Area "B" is the north easterly onsite area, as well as a small portion of offsite area immediately north of the project site. Since Area "B" is also tributary to the easterly property, there is no diversion between these two watershed areas. The existing condition was analyzed as undeveloped – poor cover land use.

The post project condition analyzed was analyzed for onsite area only, and then the onsite area plus the offsite area. The onsite area was analyzed as four watershed areas designated as Area "A", Area "B" and Area "C. Area "A" is the onsite area tributary to the onsite Bioretention Basin, and was analyzed as condominium, commercial and turf land use. Area "B" is the offsite area and small portion of onsite street area that drains to the south east corner of the project site. Area "C" is a small area of proposed street and slope area that drains to an existing low point at the boundary with the easterly project.

The offsite areas will not comingle with onsite flows (with the exception of Onsite Area B and C discussed above) prior to being treated for water quality purposes and increased runoff mitigation. The offsite rational method analyses analyzed one area designated as Area "C", and included the onsite area as area C6. Area C was analyzed for the existing

condition offsite area, and the ultimate condition offsite area (as defined by the Ultimate Condition Land Use included as Exhibit I).

The pre-project condition onsite unit hydrograph calculations utilized undeveloped – poor cover land use and runoff index numbers, as well as an impervious fraction of 0. The post-project condition utilized the resulting runoff index number and impervious fraction indicated by the post-project condition rational method calculations for Area A1. The unit hydrographs for the pre-project were analyzed for the 2-year, 24-hour and 10-year, 24-hour storm durations, and the post-project condition was analyzed for the 2-year, 24-hour, 10-year, 24-hour and 100-year, 1-hour storm durations. The 100-year, 1-hour storm duration was computed in order to perform 100-year, 1-hour basin routing calculations that are utilized in the combined hydrograph analyses with the offsite unit hydrograph. The offsite unit hydrograph was only analyzed for the 100-year, 1-hour storm duration. The pre-project offsite unit hydrograph included the onsite and offsite areas. The post-project offsite unit hydrograph did not include the onsite area, since this was used in the combined hydrograph analyses.

The pre-project rational method calculations have been included in Appendix A, and the pre-project rational method hydrology map has been included as Exhibit A. The pre-project unit hydrograph hydrology calculations have been included in Appendix C, and the pre-project unit hydrograph hydrology map has been included as Exhibit C. The post-project condition rational method hydrology calculations have been included in Appendix B, and the post-project condition rational method hydrology map has been included as Exhibit B. The post-project condition onsite unit hydrograph hydrology calculations have been included in Appendix D, and the post-project condition unit hydrograph hydrology map has been included as Exhibit D.

IV. HYDRAULIC ANALYSIS

The project site will incorporate subsurface storm drain, a bioretention basin and an interim channel to convey the onsite and offsite flows. The offsite flows will not comingle with the onsite flows. The offsite flows to the west are tributary to the proposed 6’ wide by 3’ high box crossing the entrance road, and then discharge into the interim channel. The small offsite area to the south of the project will be conveyed to the east where it will discharge into the street. The onsite areas will be conveyed to the onsite basin for water quality treatment and increased runoff mitigation.

Street capacity calculations were performed to determine the limits of storm drain based upon 100-year flows being contained within the right-of-way and 10-year flows being contained within the top of curb elevation. Since the top of curb elevation is at the right-of-way, only the 100-year capacity was analyzed.

During the preliminary stages, the onsite storm drain systems were sized using friction slope calculations. The downstream starting water surface elevation for the systems discharging into the basin was obtained from the 100-year, 1-hour basin routing analysis of 1530.43 (1.43 feet plus 1529.00 used as the bottom for the basin routing analysis).

Line D, Line E and Line F utilized soffit control as the starting water surface elevation. During final engineering, detailed inlet calculations and Water Surface Profile Gradient Program calculations will be performed.

The street capacity calculations have been included in Appendix E and the friction slope pipe sizing calculations have been included in Appendix F. The Drainage Facilities Map has been included as Exhibit E.

V. ONSITE BASIN ROUTING ANALYSES

Basin routing calculations were performed for the onsite basin in order to demonstrate that the project mitigates for increased runoff. The project routed the 2-year, 24-hour and 10-year, 24-hour storm durations.

Biofiltration Basin "A" was routed for the volume above the water quality volume. Since the first 0.5 feet of the basin are reserved for the water quality volume, and must infiltrate through the soil media, outflow was not calculated below elevation 1529.50. The basin outlet structure includes a 1" orifice hole at elevation 1529.50, and a 5' wide by 1' high weir opening at elevation 1531.00. The outflow calculations were calculated using a combination of orifice and weir equations, and are summarized on the table included in Appendix G. Table 1A calculates the flow through the 1" orifice, Table 2A calculates the flow through the weir using the weir equation, and then once flows exceed the top of the weir elevation (elevation 1532.00), the flows are calculated through the weir as an orifice due to the submerged condition (shown on Table 2B). Table 3 is the total basin outflow.

Based upon the basin routing results, the basin will adequately mitigate for increased runoff, as summarized below:

Condition	2-Year, 24-Hour	10-Year, 24-Hour
Pre-Project	0.53 ft^3/s	1.73 ft^3/s
Post-Project	3.00 ft^3/s	4.74 ft^3/s
Routed	0.27 ft^3/s	0.30 ft^3/s

VI. OFFSITE CHANNEL ANALYSES

An analyses was performed for the interim offsite channel, in conjunction with the onsite tributary routed flows to demonstrate that the project will adequately mimic the existing condition flooding. Currently, flows are tributary to the north easterly boundary from the westerly offsite area, and sheet flow through the northerly portion of the project site, and ultimately sheet flow across the easterly project boundary. An interim channel and collection culvert have been designed to intercept the offsite flows from the west. A triple 6' wide by 3' high box culvert will convey flows under the Highway 74 Connector entrance to the interim channel. The interim channel has a maximum depth of 2 feet of containment. Flows in the interim channel will pond due to the lack of an outlet, and once

the flows reach elevation 1525.00, the flows will sheet flow into the easterly property and mimic the existing condition.

A combined hydrograph analysis was prepared for the onsite routed condition and the offsite unit hydrograph for the 100-year, 1-hour storm duration to obtain a total flow rate at the downstream end of the project, as well as a hydrograph file that could be utilized in the two dimensional HEC-RAS analysis. The two dimensional analyses was utilized due to the shallow flooding and the sheet flow condition.

A 2 foot depression will be utilized that will allow flows to infiltrate. Flows in excess of 2 feet (elevation 1525.00) will overtop and sheet flow to the east. Infiltration testing for a drywell will be included in Excerpt A once this has been completed. Based upon email correspondence with the geotechnical engineer, an percolation rate of 3.5 inches per minute was observed 30 feet below ground. Using a 60" diameter drywell and assuming 10 feet of storage and 20 feet of infiltration depth, the surface area is 314.2 sq. ft. (for the 20 foot infiltration depth). The resulting flow rate when multiplying 3.5 in/min by the surface area of 314.2 sq. ft. (and the applicable conversion factors) is 1.53 ft^3/s. Using a safety factor of 3, the flow rate is 0.51 ft^3/s. The total volume within the interim channel is 79, 266 cu. ft. within the first two feet of depth. Dividing this volume by the flow rate of 0.51 ft^3/s, and converting to hours, the resulting drawdown time is 43.17 hours.

A pre-project and post-project two dimensional HEC-RAS analyses were performed. The following parameters were utilized in the analyses:

- Boundary conditions equal to normal depth for the outflow and the combined offsite and onsite routed flow hydrograph as the inflow
- A Manning's "n" value of 0.035
- Breaklines to define the following:
    - North bank (pre-project only)
    - South bank (pre-project only)
    - Centerline of Highway 74
    - Top of Curb of Highway 74 – north side
    - Top of Curb of Highway 74 – south side
    - Centerline of a swale adjacent to Highway 74 (pre-project) / Highway 74 Channel (post-project
    - Top of basin adjacent to Highway 74 (post-project only)
- Profile lines at the following locations:
    - 25 feet west of the property line
    - 50 feet east of the property line
    - Easterly property line
    - Westerly property line
    - Entry Road Centerline (post-project only)

The breaklines summarized above were utilized to define high points, low points and/or ridges in the model. The post-project condition modeled the proposed triple 6' wide by 3' high box culvert, which it modeled as an open rectangular channel. Since the flows do

no exceed 3 feet through the box system, analyzing the culverts in this manner is an accurate representation.

Water Surface Elevation Profile Line Plots have been included in Appendix H. Based upon the results, the maximum increase in water surface elevation in the post-project condition is 0.11 feet at 25 feet west of the property line, which is considered negligible. The table below summarizes the maximum water surface elevations at the four comparative profile lines:

Location	Pre-Project WSE	Post-Project WSE	Post-Pre WSE
25 ft West of PL	1532.53	1532.68	0.15
50 ft East of PL	1525.00	1525.00	0.00
Easterly PL	1525.84	1525.89	0.05
Westerly PL	1533.90	1533.90	0.00

The combined unit hydrograph routing calculations have been included in Appendix H. pre-project and post-project two dimensional exhibits have been included as Exhibits I and J, respectively.

VII. CONCLUSIONS

Preliminary hydrology and hydraulic analyses were performed for the project site. Based upon the results, the following can be concluded:

1. The proposed storm drain will adequately convey the peak 100-year flow rate.
2. The catch basins are located such that street capacity criteria will not be exceeded.
3. The onsite bioretention basin will adequately mitigate the onsite flows for increased runoff.
4. The interim channel will adequately mimic the existing condition flooding downstream of the project site.

VIII. REFERENCES

1. Riverside County Flood Control and Water Conservation District Hydrology Manual, April 1978.

FIGURES

FIGURE 1 VICINITY MAP



HEMET 30
VICINITY MAP

N

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FIGURE 1

Drawing Name: C:\Users\jcarver\Documents\Drawing1.dwg
Last Opened: Mar 09, 2021 – 3:11pm by jcarver

APPENDICES

APPENDIX A: PRE-PROJECT CONDITION RATIONAL METHOD HYDROLOGY

APPENDIX A.1: AREA "A"

100-YEAR

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 08/23/19 File:ARAEX100.out

HEMET 30 EXISTING CONDITION HYDROLOGY
RATIONAL METHOD ANALYSIS, 100-YEAR STORM EVENT
FILENAME: ARAEX100

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.200(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.200(In/Hr)
Slope of intensity duration curve = 0.5000

++

Process from Point/Station 101.000 to Point/Station 102.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 999.000(Ft.)
Top (of initial area) elevation = 2028.000(Ft.)
Bottom (of initial area) elevation = 1656.000(Ft.)
Difference in elevation = 372.000(Ft.)
Slope = 0.37237 s(percent)= 37.24
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 10.231 min.
Rainfall intensity = 2.906(In/Hr) for a 100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.837
Decimal fraction soil group A = 0.020
Decimal fraction soil group B = 0.210
Decimal fraction soil group C = 0.100
Decimal fraction soil group D = 0.670
RI index for soil(AMC 2) = 85.95
Pervious area fraction = 1.000; Impervious fraction = 0.000
Initial subarea runoff = 15.084(CFS)
Total initial stream area = 6.200(Ac.)
Pervious area fraction = 1.000

++

Process from Point/Station 102.000 to Point/Station 103.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****

Top of natural channel elevation = 1656.000(Ft.)
End of natural channel elevation = 1588.000(Ft.)
Length of natural channel = 777.000(Ft.)

```
Estimated mean flow rate at midpoint of channel =     26.824(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.60(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0875
Corrected/adjusted channel slope =  0.0875
Travel time =    1.35 min.     TC =   11.58  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.812
Decimal fraction soil group A = 0.160
Decimal fraction soil group B = 0.310
Decimal fraction soil group C = 0.060
Decimal fraction soil group D = 0.470
RI index for soil(AMC 2)  =  81.89
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.732(In/Hr) for a   100.0 year storm
Subarea runoff =     21.413(CFS) for      9.650(Ac.)
Total runoff =     36.497(CFS)        Total area =      15.850(Ac.)


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Process from Point/Station      103.000 to Point/Station      104.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1588.000(Ft.)
End of natural channel elevation =   1564.000(Ft.)
Length of natural channel  =   759.000(Ft.)
Estimated mean flow rate at midpoint of channel =     80.455(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.91(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0316
Corrected/adjusted channel slope =  0.0316
Travel time =    1.60 min.     TC =   13.18  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.807
Decimal fraction soil group A = 0.160
Decimal fraction soil group B = 0.310
Decimal fraction soil group C = 0.060
Decimal fraction soil group D = 0.470
RI index for soil(AMC 2)  =  81.89
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.561(In/Hr) for a   100.0 year storm
Subarea runoff =     78.898(CFS) for     38.180(Ac.)
Total runoff =    115.395(CFS)        Total area =      54.030(Ac.)


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Process from Point/Station      104.000 to Point/Station      105.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1564.000(Ft.)
End of natural channel elevation =   1540.000(Ft.)
Length of natural channel  =  1301.000(Ft.)
Estimated mean flow rate at midpoint of channel =    150.561(CFS)
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Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.30(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0184
Corrected/adjusted channel slope =  0.0184
Travel time =    2.97 min.     TC =   16.15  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.776
Decimal fraction soil group A = 0.420
Decimal fraction soil group B = 0.090
Decimal fraction soil group C = 0.150
Decimal fraction soil group D = 0.340
RI index for soil(AMC 2)  =  78.32
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.313(In/Hr) for a   100.0 year storm
Subarea runoff =     59.118(CFS) for     32.930(Ac.)
Total runoff =    174.513(CFS)        Total area =      86.960(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      105.000 to Point/Station      106.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
________________________________________________________________________
Top of natural channel elevation =   1540.000(Ft.)
End of natural channel elevation =   1532.000(Ft.)
Length of natural channel  =   878.000(Ft.)
Estimated mean flow rate at midpoint of channel =    237.567(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   5.91(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0091
Corrected/adjusted channel slope =  0.0091
Travel time =    2.48 min.     TC =   18.63  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.798
Decimal fraction soil group A = 0.210
Decimal fraction soil group B = 0.040
Decimal fraction soil group C = 0.370
Decimal fraction soil group D = 0.380
RI index for soil(AMC 2)  =  82.83
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.154(In/Hr) for a   100.0 year storm
Subarea runoff =    107.951(CFS) for     62.840(Ac.)
Total runoff =    282.464(CFS)        Total area =     149.800(Ac.)


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Process from Point/Station      106.000 to Point/Station      107.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
________________________________________________________________________
Top of natural channel elevation =   1532.000(Ft.)
End of natural channel elevation =   1525.000(Ft.)
Length of natural channel  =   993.000(Ft.)
Estimated mean flow rate at midpoint of channel =    307.298(CFS)
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Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   5.63(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0070
Corrected/adjusted channel slope =  0.0070
Travel time =    2.94 min.     TC =   21.57  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.760
Decimal fraction soil group A = 0.400
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.600
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  78.40
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.002(In/Hr) for a   100.0 year storm
Subarea runoff =     40.092(CFS) for     26.340(Ac.)
Total runoff =    322.556(CFS)       Total area =     176.140(Ac.)
End of computations, total study area =          176.14 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 1.000
Area averaged RI index number =  81.2
```

10-YEAR

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 02/16/21 File:ARAEX10.out

HEMET 30 EXISTING CONDITION HYDROLOGY
RATIONAL METHOD ANALYSIS, 10-YEAR STORM EVENT
FILENAME: ARAEX10

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 10.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.200(In.)

Storm event year = 10.0
Calculated rainfall intensity data:
1 hour intensity = 0.788(In/Hr)
Slope of intensity duration curve = 0.5000

++

Process from Point/Station 101.000 to Point/Station 102.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 999.000(Ft.)
Top (of initial area) elevation = 2028.000(Ft.)
Bottom (of initial area) elevation = 1656.000(Ft.)
Difference in elevation = 372.000(Ft.)
Slope = 0.37237 s(percent)= 37.24
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 10.231 min.
Rainfall intensity = 1.908(In/Hr) for a 10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.808
Decimal fraction soil group A = 0.020
Decimal fraction soil group B = 0.210
Decimal fraction soil group C = 0.100
Decimal fraction soil group D = 0.670
RI index for soil(AMC 2) = 85.95
Pervious area fraction = 1.000; Impervious fraction = 0.000
Initial subarea runoff = 9.557(CFS)
Total initial stream area = 6.200(Ac.)
Pervious area fraction = 1.000

++

Process from Point/Station 102.000 to Point/Station 103.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****

Top of natural channel elevation = 1656.000(Ft.)
End of natural channel elevation = 1588.000(Ft.)
Length of natural channel = 777.000(Ft.)

```
Estimated mean flow rate at midpoint of channel =     16.994(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.49(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0875
Corrected/adjusted channel slope =  0.0875
Travel time =    1.53 min.     TC =   11.76  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.772
Decimal fraction soil group A = 0.160
Decimal fraction soil group B = 0.310
Decimal fraction soil group C = 0.060
Decimal fraction soil group D = 0.470
RI index for soil(AMC 2)  =  81.89
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.780(In/Hr) for a    10.0 year storm
Subarea runoff =     13.263(CFS) for      9.650(Ac.)
Total runoff =     22.820(CFS)        Total area =      15.850(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      103.000 to Point/Station      104.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1588.000(Ft.)
End of natural channel elevation =   1564.000(Ft.)
Length of natural channel  =   759.000(Ft.)
Estimated mean flow rate at midpoint of channel =     50.305(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   6.89(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0316
Corrected/adjusted channel slope =  0.0316
Travel time =    1.83 min.     TC =   13.59  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.764
Decimal fraction soil group A = 0.160
Decimal fraction soil group B = 0.310
Decimal fraction soil group C = 0.060
Decimal fraction soil group D = 0.470
RI index for soil(AMC 2)  =  81.89
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.656(In/Hr) for a    10.0 year storm
Subarea runoff =     48.290(CFS) for     38.180(Ac.)
Total runoff =     71.110(CFS)        Total area =      54.030(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      104.000 to Point/Station      105.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1564.000(Ft.)
End of natural channel elevation =   1540.000(Ft.)
Length of natural channel  =  1301.000(Ft.)
Estimated mean flow rate at midpoint of channel =     92.780(CFS)
```

```
Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   6.30(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0184
Corrected/adjusted channel slope =  0.0184
Travel time =    3.44 min.     TC =   17.03  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.720
Decimal fraction soil group A = 0.420
Decimal fraction soil group B = 0.090
Decimal fraction soil group C = 0.150
Decimal fraction soil group D = 0.340
RI index for soil(AMC 2)  =  78.32
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.479(In/Hr) for a    10.0 year storm
Subarea runoff =     35.079(CFS) for     32.930(Ac.)
Total runoff =    106.189(CFS)        Total area =      86.960(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      105.000 to Point/Station      106.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
________________________________________________________________________
Top of natural channel elevation =   1540.000(Ft.)
End of natural channel elevation =   1532.000(Ft.)
Length of natural channel  =   878.000(Ft.)
Estimated mean flow rate at midpoint of channel =    144.557(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   5.07(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0091
Corrected/adjusted channel slope =  0.0091
Travel time =    2.89 min.     TC =   19.92  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.749
Decimal fraction soil group A = 0.210
Decimal fraction soil group B = 0.040
Decimal fraction soil group C = 0.370
Decimal fraction soil group D = 0.380
RI index for soil(AMC 2)  =  82.83
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.368(In/Hr) for a    10.0 year storm
Subarea runoff =     64.341(CFS) for     62.840(Ac.)
Total runoff =    170.530(CFS)        Total area =     149.800(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      106.000 to Point/Station      107.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
________________________________________________________________________
Top of natural channel elevation =   1532.000(Ft.)
End of natural channel elevation =   1525.000(Ft.)
Length of natural channel  =   993.000(Ft.)
Estimated mean flow rate at midpoint of channel =    185.523(CFS)
```

```
Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   4.81(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0070
Corrected/adjusted channel slope =  0.0070
Travel time =    3.44 min.     TC =   23.36  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.697
Decimal fraction soil group A = 0.400
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.600
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  78.40
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.263(In/Hr) for a    10.0 year storm
Subarea runoff =     23.191(CFS) for     26.340(Ac.)
Total runoff =    193.722(CFS)       Total area =     176.140(Ac.)
End of computations, total study area =          176.14 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 1.000
Area averaged RI index number =  81.2
```

APPENDIX A.2: AREA "B"

100-YEAR

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 08/23/19 File:ARBEX100.out

HEMET 30 EXISTING CONDITION HYDROLOGY
RATIONAL METHOD ANALYSIS, 100-YEAR STORM EVENT
FILENAME: ARBEX100

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.200(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.200(In/Hr)
Slope of intensity duration curve = 0.5000

++

Process from Point/Station 201.000 to Point/Station 202.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 727.000(Ft.)
Top (of initial area) elevation = 1572.000(Ft.)
Bottom (of initial area) elevation = 1534.000(Ft.)
Difference in elevation = 38.000(Ft.)
Slope = 0.05227 s(percent)= 5.23
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 13.343 min.
Rainfall intensity = 2.545(In/Hr) for a 100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.811
Decimal fraction soil group A = 0.170
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.830
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 82.77
Pervious area fraction = 1.000; Impervious fraction = 0.000
Initial subarea runoff = 6.463(CFS)
Total initial stream area = 3.130(Ac.)
Pervious area fraction = 1.000

++

Process from Point/Station 202.000 to Point/Station 203.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****

Top of natural channel elevation = 1534.000(Ft.)
End of natural channel elevation = 1528.000(Ft.)
Length of natural channel = 547.000(Ft.)

```
Estimated mean flow rate at midpoint of channel =     12.576(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   2.78(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0110
Corrected/adjusted channel slope =  0.0110
Travel time =    3.28 min.     TC =   16.63  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.839
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.010
Decimal fraction soil group D = 0.990
RI index for soil(AMC 2)  =  88.97
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.280(In/Hr) for a   100.0 year storm
Subarea runoff =     11.324(CFS) for      5.920(Ac.)
Total runoff =     17.788(CFS)        Total area =       9.050(Ac.)
End of computations, total study area =            9.05 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 1.000
Area averaged RI index number =  86.8
```

10-YEAR

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 02/16/21 File:ARBEX10.out

HEMET 30 EXISTING CONDITION HYDROLOGY
RATIONAL METHOD ANALYSIS, 10-YEAR STORM EVENT
FILENAME: ARBEX10

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 10.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.200(In.)

Storm event year = 10.0
Calculated rainfall intensity data:
1 hour intensity = 0.788(In/Hr)
Slope of intensity duration curve = 0.5000

++

Process from Point/Station 201.000 to Point/Station 202.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 727.000(Ft.)
Top (of initial area) elevation = 1572.000(Ft.)
Bottom (of initial area) elevation = 1534.000(Ft.)
Difference in elevation = 38.000(Ft.)
Slope = 0.05227 s(percent)= 5.23
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 13.343 min.
Rainfall intensity = 1.671(In/Hr) for a 10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.772
Decimal fraction soil group A = 0.170
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.830
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 82.77
Pervious area fraction = 1.000; Impervious fraction = 0.000
Initial subarea runoff = 4.037(CFS)
Total initial stream area = 3.130(Ac.)
Pervious area fraction = 1.000

++

Process from Point/Station 202.000 to Point/Station 203.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****

Top of natural channel elevation = 1534.000(Ft.)
End of natural channel elevation = 1528.000(Ft.)
Length of natural channel = 547.000(Ft.)

```
Estimated mean flow rate at midpoint of channel =      7.854(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   2.46(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0110
Corrected/adjusted channel slope =  0.0110
Travel time =    3.70 min.     TC =   17.04  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.809
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.010
Decimal fraction soil group D = 0.990
RI index for soil(AMC 2)  =  88.97
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.479(In/Hr) for a    10.0 year storm
Subarea runoff =      7.085(CFS) for      5.920(Ac.)
Total runoff =     11.122(CFS)        Total area =       9.050(Ac.)
End of computations, total study area =            9.05 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 1.000
Area averaged RI index number =  86.8
```

APPENDIX B: POST-PROJECT CONDITION RATIONAL METHOD HYDROLOGY

APPENDIX B.1: AREA "A"

100-YEAR

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2001 Version 6.4
Rational Hydrology Study Date: 10/23/21 File:ARA100.out

150.10.18
100-YEAR RATIONAL TABLING METHOD FOR AREA A
POST-PROJECT CONDITION
FN: ARA100.RRV

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

TRI-8 Builders - S/N 615

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.200(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.200(In/Hr)
Slope of intensity duration curve = 0.5000

++

Process from Point/Station 101.000 to Point/Station 102.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 802.000(Ft.)
Top (of initial area) elevation = 1563.000(Ft.)
Bottom (of initial area) elevation = 1537.000(Ft.)
Difference in elevation = 26.000(Ft.)
Slope = 0.03242 s(percent)= 3.24
TC = k(0.370)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 10.659 min.
Rainfall intensity = 2.847(In/Hr) for a 100.0 year storm
CONDOMINIUM subarea type
Runoff Coefficient = 0.842
Decimal fraction soil group A = 0.040
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.960
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 67.52
Pervious area fraction = 0.350; Impervious fraction = 0.650
Initial subarea runoff = 4.963(CFS)
Total initial stream area = 2.070(Ac.)
Pervious area fraction = 0.350

++

Process from Point/Station 102.000 to Point/Station 102.100
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1531.300(Ft.)
Downstream point/station elevation = 1531.200(Ft.)
Pipe length = 22.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 4.963(CFS)
Nearest computed pipe diameter = 18.00(In.)
Calculated individual pipe flow = 4.963(CFS)

```
Normal flow depth in pipe =   11.11(In.)
Flow top width inside pipe =   17.50(In.)
Critical Depth =   10.28(In.)
Pipe flow velocity =      4.34(Ft/s)
Travel time through pipe =    0.08 min.
Time of concentration (TC) =    10.74 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      102.100 to Point/Station      102.100
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
CONDOMINIUM subarea type
Runoff Coefficient = 0.845
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.350; Impervious fraction =  0.650
Time of concentration =    10.74 min.
Rainfall intensity =      2.836(In/Hr) for a   100.0 year storm
Subarea runoff =      0.312(CFS) for      0.130(Ac.)
Total runoff =      5.274(CFS)        Total area =       2.200(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      102.100 to Point/Station      105.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1531.200(Ft.)
Downstream point/station elevation =  1530.300(Ft.)
Pipe length  =   205.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     5.274(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =     5.274(CFS)
Normal flow depth in pipe =   11.72(In.)
Flow top width inside pipe =   17.16(In.)
Critical Depth =   10.62(In.)
Pipe flow velocity =      4.33(Ft/s)
Travel time through pipe =    0.79 min.
Time of concentration (TC) =    11.53 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      102.100 to Point/Station      105.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      2.200(Ac.)
Runoff from this stream =      5.274(CFS)
Time of concentration =   11.53 min.
Rainfall intensity =     2.737(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      103.000 to Point/Station      104.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   735.000(Ft.)
Top (of initial area) elevation =  1554.300(Ft.)
Bottom (of initial area) elevation =  1537.000(Ft.)
Difference in elevation =    17.300(Ft.)
Slope =    0.02354  s(percent)=       2.35
TC = k(0.370)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   10.974 min.
Rainfall intensity =      2.806(In/Hr) for a   100.0 year storm
CONDOMINIUM subarea type
Runoff Coefficient = 0.845
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
```

```
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.350; Impervious fraction =  0.650
Initial subarea runoff =      3.839(CFS)
Total initial stream area =        1.620(Ac.)
Pervious area fraction = 0.350


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      104.000 to Point/Station      104.100
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
________________________________________________________________________
Top of street segment elevation =  1537.000(Ft.)
End of street segment elevation =  1536.000(Ft.)
Length of street segment  =   248.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  22.000(Ft.)
Distance from crown to crossfall grade break  =  18.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.053
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      7.737(CFS)
Depth of flow =   0.567(Ft.), Average velocity =   1.964(Ft/s)
Warning: depth of flow exceeds top of curb
Distance that curb overflow reaches into property =    3.35(Ft.)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  18.714(Ft.)
Flow velocity =   1.96(Ft/s)
Travel time =    2.10 min.     TC =   13.08  min.
 Adding area flow to street
CONDOMINIUM subarea type
Runoff Coefficient = 0.840
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.350; Impervious fraction =  0.650
Rainfall intensity =      2.570(In/Hr) for a   100.0 year storm
Subarea runoff =      7.107(CFS) for      3.290(Ac.)
Total runoff =     10.946(CFS)        Total area =       4.910(Ac.)
Street flow at end of street =     10.946(CFS)
Half street flow at end of street =     10.946(CFS)
Depth of flow =   0.621(Ft.), Average velocity =   2.070(Ft/s)
Warning: depth of flow exceeds top of curb
Distance that curb overflow reaches into property =    6.07(Ft.)
Flow width (from curb towards crown)=  21.437(Ft.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      104.100 to Point/Station      105.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1530.400(Ft.)
Downstream point/station elevation =  1530.300(Ft.)
Pipe length  =    12.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    10.946(CFS)
Nearest computed pipe diameter  =     21.00(In.)
Calculated individual pipe flow  =    10.946(CFS)
Normal flow depth in pipe =   13.66(In.)
Flow top width inside pipe =   20.02(In.)
Critical Depth =   14.80(In.)
Pipe flow velocity =      6.61(Ft/s)
```

```
Travel time through pipe =    0.03 min.
Time of concentration (TC) =    13.11 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      105.000 to Point/Station      105.000
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
CONDOMINIUM subarea type
Runoff Coefficient = 0.840
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.350; Impervious fraction =  0.650
Time of concentration =    13.11 min.
Rainfall intensity =      2.567(In/Hr) for a   100.0 year storm
Subarea runoff =      2.136(CFS) for      0.990(Ac.)
Total runoff =     13.082(CFS)        Total area =       5.900(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      105.000 to Point/Station      105.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      5.900(Ac.)
Runoff from this stream =     13.082(CFS)
Time of concentration =   13.11 min.
Rainfall intensity =     2.567(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        5.274     11.53                2.737
2       13.082     13.11                2.567
Largest stream flow has longer time of concentration
Qp =     13.082 + sum of
          Qb         Ia/Ib
           5.274 *    0.938 =      4.947
Qp =     18.029

Total of 2 streams to confluence:
Flow rates before confluence point:
       5.274      13.082
Area of streams before confluence:
        2.200        5.900
Results of confluence:
Total flow rate =     18.029(CFS)
Time of concentration =    13.108 min.
Effective stream area after confluence =      8.100(Ac.)


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Process from Point/Station      105.000 to Point/Station      107.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1530.300(Ft.)
Downstream point/station elevation =  1529.700(Ft.)
Pipe length  =   230.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    18.029(CFS)
Nearest computed pipe diameter  =     30.00(In.)
Calculated individual pipe flow  =    18.029(CFS)
Normal flow depth in pipe =   21.47(In.)
Flow top width inside pipe =   27.07(In.)
Critical Depth =   17.25(In.)
Pipe flow velocity =      4.80(Ft/s)
Travel time through pipe =    0.80 min.
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Time of concentration (TC) =    13.91 min.


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Process from Point/Station      105.000 to Point/Station      107.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      8.100(Ac.)
Runoff from this stream =     18.029(CFS)
Time of concentration =   13.91 min.
Rainfall intensity =     2.493(In/Hr)


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Process from Point/Station      106.000 to Point/Station      106.100
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   734.000(Ft.)
Top (of initial area) elevation =  1544.300(Ft.)
Bottom (of initial area) elevation =  1536.000(Ft.)
Difference in elevation =     8.300(Ft.)
Slope =    0.01131  s(percent)=       1.13
TC = k(0.370)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   12.700 min.
Rainfall intensity =      2.608(In/Hr) for a   100.0 year storm
CONDOMINIUM subarea type
Runoff Coefficient = 0.841
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.350; Impervious fraction =  0.650
Initial subarea runoff =      5.770(CFS)
Total initial stream area =        2.630(Ac.)
Pervious area fraction = 0.350


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Process from Point/Station      106.100 to Point/Station      107.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1529.800(Ft.)
Downstream point/station elevation =  1529.700(Ft.)
Pipe length  =    14.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     5.770(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =     5.770(CFS)
Normal flow depth in pipe =   10.57(In.)
Flow top width inside pipe =   17.72(In.)
Critical Depth =   11.12(In.)
Pipe flow velocity =      5.35(Ft/s)
Travel time through pipe =    0.04 min.
Time of concentration (TC) =    12.74 min.


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Process from Point/Station      107.000 to Point/Station      107.000
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
CONDOMINIUM subarea type
Runoff Coefficient = 0.832
Decimal fraction soil group A = 0.110
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.890
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  64.93
Pervious area fraction =  0.350; Impervious fraction =  0.650
Time of concentration =    12.74 min.
Rainfall intensity =      2.604(In/Hr) for a   100.0 year storm
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Subarea runoff =      1.321(CFS) for      0.610(Ac.)
Total runoff =      7.091(CFS)        Total area =       3.240(Ac.)


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Process from Point/Station      107.000 to Point/Station      107.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      3.240(Ac.)
Runoff from this stream =      7.091(CFS)
Time of concentration =   12.74 min.
Rainfall intensity =     2.604(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       18.029     13.91                2.493
2        7.091     12.74                2.604
Largest stream flow has longer time of concentration
Qp =     18.029 + sum of
          Qb         Ia/Ib
           7.091 *    0.957 =      6.788
Qp =     24.818

Total of 2 streams to confluence:
Flow rates before confluence point:
      18.029       7.091
Area of streams before confluence:
        8.100        3.240
Results of confluence:
Total flow rate =     24.818(CFS)
Time of concentration =    13.907 min.
Effective stream area after confluence =     11.340(Ac.)


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Process from Point/Station      107.000 to Point/Station      109.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1529.700(Ft.)
Downstream point/station elevation =  1528.000(Ft.)
Pipe length  =   252.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    24.818(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    24.818(CFS)
Normal flow depth in pipe =   21.56(In.)
Flow top width inside pipe =   21.66(In.)
Critical Depth =   20.90(In.)
Pipe flow velocity =      7.29(Ft/s)
Travel time through pipe =    0.58 min.
Time of concentration (TC) =    14.48 min.


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Process from Point/Station      107.000 to Point/Station      109.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =     11.340(Ac.)
Runoff from this stream =     24.818(CFS)
Time of concentration =   14.48 min.
Rainfall intensity =     2.442(In/Hr)


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Process from Point/Station      108.000 to Point/Station      108.100
**** INITIAL AREA EVALUATION ****
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Initial area flow distance =   232.000(Ft.)
Top (of initial area) elevation =  1538.900(Ft.)
Bottom (of initial area) elevation =  1536.000(Ft.)
Difference in elevation =     2.900(Ft.)
Slope =    0.01250  s(percent)=       1.25
TC = k(0.370)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    7.853 min.
Rainfall intensity =      3.317(In/Hr) for a   100.0 year storm
CONDOMINIUM subarea type
Runoff Coefficient = 0.850
Decimal fraction soil group A = 0.030
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.970
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  67.89
Pervious area fraction =  0.350; Impervious fraction =  0.650
Initial subarea runoff =      1.691(CFS)
Total initial stream area =        0.600(Ac.)
Pervious area fraction = 0.350


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Process from Point/Station      108.100 to Point/Station      108.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1529.100(Ft.)
Downstream point/station elevation =  1529.000(Ft.)
Pipe length  =    38.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     1.691(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     1.691(CFS)
Normal flow depth in pipe =    9.12(In.)
Flow top width inside pipe =   10.25(In.)
Critical Depth =    6.63(In.)
Pipe flow velocity =      2.64(Ft/s)
Travel time through pipe =    0.24 min.
Time of concentration (TC) =     8.09 min.


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Process from Point/Station      108.200 to Point/Station      108.200
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
CONDOMINIUM subarea type
Runoff Coefficient = 0.829
Decimal fraction soil group A = 0.290
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.710
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  58.27
Pervious area fraction =  0.350; Impervious fraction =  0.650
Time of concentration =     8.09 min.
Rainfall intensity =      3.268(In/Hr) for a   100.0 year storm
Subarea runoff =      2.979(CFS) for      1.100(Ac.)
Total runoff =      4.670(CFS)        Total area =       1.700(Ac.)


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Process from Point/Station      108.200 to Point/Station      109.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1529.000(Ft.)
Downstream point/station elevation =  1528.900(Ft.)
Pipe length  =     7.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     4.670(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =     4.670(CFS)
Normal flow depth in pipe =    8.41(In.)
Flow top width inside pipe =   14.89(In.)
Critical Depth =   10.51(In.)
Pipe flow velocity =      6.59(Ft/s)
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Travel time through pipe =    0.02 min.
Time of concentration (TC) =     8.11 min.


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Process from Point/Station      108.200 to Point/Station      108.200
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      1.700(Ac.)
Runoff from this stream =      4.670(CFS)
Time of concentration =    8.11 min.
Rainfall intensity =     3.264(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       24.818     14.48                2.442
2        4.670      8.11                3.264
Largest stream flow has longer time of concentration
Qp =     24.818 + sum of
          Qb         Ia/Ib
           4.670 *    0.748 =      3.495
Qp =     28.312

Total of 2 streams to confluence:
Flow rates before confluence point:
      24.818       4.670
Area of streams before confluence:
       11.340        1.700
Results of confluence:
Total flow rate =     28.312(CFS)
Time of concentration =    14.483 min.
Effective stream area after confluence =     13.040(Ac.)


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Process from Point/Station      109.000 to Point/Station      118.100
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1528.900(Ft.)
Downstream point/station elevation =  1528.500(Ft.)
Pipe length  =   117.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    28.312(CFS)
Nearest computed pipe diameter  =     33.00(In.)
Calculated individual pipe flow  =    28.312(CFS)
Normal flow depth in pipe =   24.84(In.)
Flow top width inside pipe =   28.47(In.)
Critical Depth =   21.22(In.)
Pipe flow velocity =      5.90(Ft/s)
Travel time through pipe =    0.33 min.
Time of concentration (TC) =    14.81 min.


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Process from Point/Station      109.000 to Point/Station      118.100
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =     13.040(Ac.)
Runoff from this stream =     28.312(CFS)
Time of concentration =   14.81 min.
Rainfall intensity =     2.415(In/Hr)
Program is now starting with Main Stream No. 2


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Process from Point/Station      110.000 to Point/Station      110.100
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**** INITIAL AREA EVALUATION ****
_____________________________________________________________________
Initial area flow distance =   614.000(Ft.)
Top (of initial area) elevation =  1569.000(Ft.)
Bottom (of initial area) elevation =  1545.000(Ft.)
Difference in elevation =    24.000(Ft.)
Slope =    0.03909  s(percent)=       3.91
TC = k(0.370)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    9.227 min.
Rainfall intensity =      3.060(In/Hr) for a   100.0 year storm
CONDOMINIUM subarea type
Runoff Coefficient = 0.848
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.350; Impervious fraction =  0.650
Initial subarea runoff =      4.855(CFS)
Total initial stream area =        1.870(Ac.)
Pervious area fraction = 0.350


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Process from Point/Station      110.100 to Point/Station      111.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
_____________________________________________________________________
Top of street segment elevation =  1545.000(Ft.)
End of street segment elevation =  1541.000(Ft.)
Length of street segment  =   162.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  22.000(Ft.)
Distance from crown to crossfall grade break  =  18.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.053
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      5.712(CFS)
Depth of flow =   0.402(Ft.), Average velocity =   4.009(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  10.488(Ft.)
Flow velocity =   4.01(Ft/s)
Travel time =    0.67 min.     TC =    9.90  min.
 Adding area flow to street
CONDOMINIUM subarea type
Runoff Coefficient = 0.847
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.350; Impervious fraction =  0.650
Rainfall intensity =      2.954(In/Hr) for a   100.0 year storm
Subarea runoff =      1.651(CFS) for      0.660(Ac.)
Total runoff =      6.506(CFS)       Total area =       2.530(Ac.)
Street flow at end of street =      6.506(CFS)
Half street flow at end of street =      6.506(CFS)
Depth of flow =   0.417(Ft.), Average velocity =   4.114(Ft/s)
Flow width (from curb towards crown)=  11.210(Ft.)


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Process from Point/Station      111.000 to Point/Station      112.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
_____________________________________________________________________
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Upstream point/station elevation =  1529.800(Ft.)
Downstream point/station elevation =  1529.700(Ft.)
Pipe length  =    45.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     6.506(CFS)
Nearest computed pipe diameter  =     21.00(In.)
Calculated individual pipe flow  =     6.506(CFS)
Normal flow depth in pipe =   15.16(In.)
Flow top width inside pipe =   18.81(In.)
Critical Depth =   11.30(In.)
Pipe flow velocity =      3.50(Ft/s)
Travel time through pipe =    0.21 min.
Time of concentration (TC) =    10.11 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      111.000 to Point/Station      112.200
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =      2.530(Ac.)
Runoff from this stream =      6.506(CFS)
Time of concentration =   10.11 min.
Rainfall intensity =     2.923(In/Hr)


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Process from Point/Station      112.000 to Point/Station      112.100
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   337.000(Ft.)
Top (of initial area) elevation =  1548.100(Ft.)
Bottom (of initial area) elevation =  1541.000(Ft.)
Difference in elevation =     7.100(Ft.)
Slope =    0.02107  s(percent)=       2.11
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    6.660 min.
Rainfall intensity =      3.602(In/Hr) for a   100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.887
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      0.735(CFS)
Total initial stream area =        0.230(Ac.)
Pervious area fraction = 0.100


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Process from Point/Station      112.100 to Point/Station      112.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1529.900(Ft.)
Downstream point/station elevation =  1529.700(Ft.)
Pipe length  =    60.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     0.735(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     0.735(CFS)
Normal flow depth in pipe =    5.92(In.)
Flow top width inside pipe =    8.54(In.)
Critical Depth =    4.69(In.)
Pipe flow velocity =      2.38(Ft/s)
Travel time through pipe =    0.42 min.
Time of concentration (TC) =     7.08 min.


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Process from Point/Station      112.100 to Point/Station      112.200
**** CONFLUENCE OF MINOR STREAMS ****
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_____________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =      0.230(Ac.)
Runoff from this stream =      0.735(CFS)
Time of concentration =    7.08 min.
Rainfall intensity =     3.494(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        6.506     10.11                2.923
2        0.735      7.08                3.494
Largest stream flow has longer time of concentration
Qp =      6.506 + sum of
          Qb         Ia/Ib
           0.735 *    0.837 =      0.615
Qp =      7.121

Total of 2 streams to confluence:
Flow rates before confluence point:
       6.506       0.735
Area of streams before confluence:
        2.530        0.230
Results of confluence:
Total flow rate =      7.121(CFS)
Time of concentration =    10.115 min.
Effective stream area after confluence =      2.760(Ac.)


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Process from Point/Station      112.200 to Point/Station      114.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
_____________________________________________________________________________
Upstream point/station elevation =  1529.700(Ft.)
Downstream point/station elevation =  1528.900(Ft.)
Pipe length  =   260.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     7.121(CFS)
Nearest computed pipe diameter  =     21.00(In.)
Calculated individual pipe flow  =     7.121(CFS)
Normal flow depth in pipe =   14.34(In.)
Flow top width inside pipe =   19.54(In.)
Critical Depth =   11.85(In.)
Pipe flow velocity =      4.07(Ft/s)
Travel time through pipe =    1.06 min.
Time of concentration (TC) =    11.18 min.


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Process from Point/Station      112.200 to Point/Station      114.200
**** CONFLUENCE OF MINOR STREAMS ****
_____________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =      2.760(Ac.)
Runoff from this stream =      7.121(CFS)
Time of concentration =   11.18 min.
Rainfall intensity =     2.780(In/Hr)


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Process from Point/Station      113.000 to Point/Station      114.000
**** INITIAL AREA EVALUATION ****
_____________________________________________________________________________
Initial area flow distance =   439.000(Ft.)
Top (of initial area) elevation =  1544.100(Ft.)
Bottom (of initial area) elevation =  1536.400(Ft.)
Difference in elevation =     7.700(Ft.)
Slope =    0.01754  s(percent)=       1.75
TC = k(0.370)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    9.471 min.
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Rainfall intensity =      3.020(In/Hr) for a   100.0 year storm
CONDOMINIUM subarea type
Runoff Coefficient = 0.848
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.350; Impervious fraction =  0.650
Initial subarea runoff =      3.201(CFS)
Total initial stream area =        1.250(Ac.)
Pervious area fraction = 0.350


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Process from Point/Station      114.000 to Point/Station      114.100
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of street segment elevation =  1536.400(Ft.)
End of street segment elevation =  1536.000(Ft.)
Length of street segment  =    72.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  22.000(Ft.)
Distance from crown to crossfall grade break  =  18.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.053
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      4.033(CFS)
Depth of flow =   0.448(Ft.), Average velocity =   2.064(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  12.766(Ft.)
Flow velocity =   2.06(Ft/s)
Travel time =    0.58 min.     TC =   10.05  min.
 Adding area flow to street
CONDOMINIUM subarea type
Runoff Coefficient = 0.847
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.350; Impervious fraction =  0.650
Rainfall intensity =      2.932(In/Hr) for a   100.0 year storm
Subarea runoff =      1.613(CFS) for      0.650(Ac.)
Total runoff =      4.814(CFS)        Total area =       1.900(Ac.)
Street flow at end of street =      4.814(CFS)
Half street flow at end of street =      4.814(CFS)
Depth of flow =   0.470(Ft.), Average velocity =   2.145(Ft/s)
Flow width (from curb towards crown)=  13.856(Ft.)


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Process from Point/Station      114.100 to Point/Station      114.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1529.000(Ft.)
Downstream point/station elevation =  1528.900(Ft.)
Pipe length  =    19.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     4.814(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =     4.814(CFS)
Normal flow depth in pipe =   10.38(In.)
Flow top width inside pipe =   17.79(In.)
Critical Depth =   10.11(In.)
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Pipe flow velocity =      4.56(Ft/s)
Travel time through pipe =    0.07 min.
Time of concentration (TC) =    10.12 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      114.100 to Point/Station      114.200
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =      1.900(Ac.)
Runoff from this stream =      4.814(CFS)
Time of concentration =   10.12 min.
Rainfall intensity =     2.922(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        7.121     11.18                2.780
2        4.814     10.12                2.922
Largest stream flow has longer time of concentration
Qp =      7.121 + sum of
          Qb         Ia/Ib
           4.814 *    0.951 =      4.581
Qp =     11.702

Total of 2 streams to confluence:
Flow rates before confluence point:
       7.121       4.814
Area of streams before confluence:
        2.760        1.900
Results of confluence:
Total flow rate =     11.702(CFS)
Time of concentration =    11.180 min.
Effective stream area after confluence =      4.660(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      114.200 to Point/Station      115.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1528.900(Ft.)
Downstream point/station elevation =  1528.800(Ft.)
Pipe length  =    29.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    11.702(CFS)
Nearest computed pipe diameter  =     24.00(In.)
Calculated individual pipe flow  =    11.702(CFS)
Normal flow depth in pipe =   17.48(In.)
Flow top width inside pipe =   21.35(In.)
Critical Depth =   14.74(In.)
Pipe flow velocity =      4.77(Ft/s)
Travel time through pipe =    0.10 min.
Time of concentration (TC) =    11.28 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      114.200 to Point/Station      115.200
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =      4.660(Ac.)
Runoff from this stream =     11.702(CFS)
Time of concentration =   11.28 min.
Rainfall intensity =     2.767(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      115.000 to Point/Station      115.100
**** INITIAL AREA EVALUATION ****
```

```
Initial area flow distance =   448.000(Ft.)
Top (of initial area) elevation =  1540.500(Ft.)
Bottom (of initial area) elevation =  1536.000(Ft.)
Difference in elevation =     4.500(Ft.)
Slope =    0.01004  s(percent)=       1.00
TC = k(0.370)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   10.674 min.
Rainfall intensity =      2.845(In/Hr) for a   100.0 year storm
CONDOMINIUM subarea type
Runoff Coefficient = 0.798
Decimal fraction soil group A = 0.530
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.470
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  49.39
Pervious area fraction =  0.350; Impervious fraction =  0.650
Initial subarea runoff =      3.745(CFS)
Total initial stream area =        1.650(Ac.)
Pervious area fraction = 0.350


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      115.100 to Point/Station      115.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
----------------------------------------------------------------------
Upstream point/station elevation =  1528.900(Ft.)
Downstream point/station elevation =  1528.800(Ft.)
Pipe length  =     7.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     3.745(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     3.745(CFS)
Normal flow depth in pipe =    8.73(In.)
Flow top width inside pipe =   10.69(In.)
Critical Depth =    9.89(In.)
Pipe flow velocity =      6.12(Ft/s)
Travel time through pipe =    0.02 min.
Time of concentration (TC) =    10.69 min.


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Process from Point/Station      115.100 to Point/Station      115.200
**** CONFLUENCE OF MINOR STREAMS ****
----------------------------------------------------------------------
Along Main Stream number: 2 in normal stream number 2
Stream flow area =      1.650(Ac.)
Runoff from this stream =      3.745(CFS)
Time of concentration =   10.69 min.
Rainfall intensity =     2.843(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       11.702     11.28                2.767
2        3.745     10.69                2.843
Largest stream flow has longer time of concentration
Qp =     11.702 + sum of
          Qb         Ia/Ib
           3.745 *    0.974 =      3.646
Qp =     15.348

Total of 2 streams to confluence:
Flow rates before confluence point:
      11.702       3.745
Area of streams before confluence:
        4.660        1.650
Results of confluence:
Total flow rate =     15.348(CFS)
Time of concentration =    11.281 min.
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Effective stream area after confluence =      6.310(Ac.)


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Process from Point/Station      115.200 to Point/Station      118.100
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1528.800(Ft.)
Downstream point/station elevation =  1528.500(Ft.)
Pipe length  =   107.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    15.348(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    15.348(CFS)
Normal flow depth in pipe =   20.72(In.)
Flow top width inside pipe =   22.82(In.)
Critical Depth =   16.39(In.)
Pipe flow velocity =      4.69(Ft/s)
Travel time through pipe =    0.38 min.
Time of concentration (TC) =    11.66 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      115.200 to Point/Station      118.100
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =      6.310(Ac.)
Runoff from this stream =     15.348(CFS)
Time of concentration =   11.66 min.
Rainfall intensity =     2.722(In/Hr)
Program is now starting with Main Stream No. 3


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      116.000 to Point/Station      118.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   531.000(Ft.)
Top (of initial area) elevation =  1544.100(Ft.)
Bottom (of initial area) elevation =  1534.300(Ft.)
Difference in elevation =     9.800(Ft.)
Slope =    0.01846  s(percent)=       1.85
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    8.202 min.
Rainfall intensity =      3.246(In/Hr) for a   100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.874
Decimal fraction soil group A = 0.490
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.510
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  50.87
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      1.504(CFS)
Total initial stream area =        0.530(Ac.)
Pervious area fraction = 0.100


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Process from Point/Station      116.000 to Point/Station      118.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 3 in normal stream number 1
Stream flow area =      0.530(Ac.)
Runoff from this stream =      1.504(CFS)
Time of concentration =    8.20 min.
Rainfall intensity =     3.246(In/Hr)


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Process from Point/Station      117.000 to Point/Station      117.100
**** INITIAL AREA EVALUATION ****
----------------------------------------------------------------------------
Initial area flow distance =   462.000(Ft.)
Top (of initial area) elevation =  1543.600(Ft.)
Bottom (of initial area) elevation =  1534.300(Ft.)
Difference in elevation =     9.300(Ft.)
Slope =    0.02013  s(percent)=       2.01
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    7.624 min.
Rainfall intensity =      3.366(In/Hr) for a   100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.869
Decimal fraction soil group A = 0.690
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.310
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  43.47
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      0.380(CFS)
Total initial stream area =        0.130(Ac.)
Pervious area fraction = 0.100


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      117.100 to Point/Station      118.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
----------------------------------------------------------------------------
Upstream point/station elevation =  1528.700(Ft.)
Downstream point/station elevation =  1528.600(Ft.)
Pipe length  =    33.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     0.380(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     0.380(CFS)
Normal flow depth in pipe =    4.05(In.)
Flow top width inside pipe =    8.96(In.)
Critical Depth =    3.32(In.)
Pipe flow velocity =      1.97(Ft/s)
Travel time through pipe =    0.28 min.
Time of concentration (TC) =     7.90 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      117.100 to Point/Station      118.000
**** CONFLUENCE OF MINOR STREAMS ****
----------------------------------------------------------------------------
Along Main Stream number: 3 in normal stream number 2
Stream flow area =      0.130(Ac.)
Runoff from this stream =      0.380(CFS)
Time of concentration =    7.90 min.
Rainfall intensity =     3.306(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        1.504      8.20                3.246
2        0.380      7.90                3.306
Largest stream flow has longer time of concentration
Qp =      1.504 + sum of
          Qb         Ia/Ib
           0.380 *    0.982 =      0.373
Qp =      1.878

Total of 2 streams to confluence:
Flow rates before confluence point:
       1.504       0.380
Area of streams before confluence:
        0.530        0.130
Results of confluence:
```

```
Total flow rate =      1.878(CFS)
Time of concentration =     8.202 min.
Effective stream area after confluence =      0.660(Ac.)


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Process from Point/Station      118.000 to Point/Station      118.100
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1528.600(Ft.)
Downstream point/station elevation =  1528.500(Ft.)
Pipe length  =    43.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     1.878(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =     1.878(CFS)
Normal flow depth in pipe =    8.40(In.)
Flow top width inside pipe =   14.89(In.)
Critical Depth =    6.54(In.)
Pipe flow velocity =      2.66(Ft/s)
Travel time through pipe =    0.27 min.
Time of concentration (TC) =     8.47 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      118.000 to Point/Station      118.100
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 3
Stream flow area =      0.660(Ac.)
Runoff from this stream =      1.878(CFS)
Time of concentration =    8.47 min.
Rainfall intensity =     3.193(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       28.312     14.81               2.415
2       15.348     11.66               2.722
3        1.878      8.47               3.193
Largest stream flow has longer time of concentration
Qp =     28.312 + sum of
          Qb         Ia/Ib
          15.348 *    0.887 =     13.618
          Qb         Ia/Ib
           1.878 *    0.756 =      1.420
Qp =     43.350

Total of 3 main streams to confluence:
Flow rates before confluence point:
      28.312      15.348       1.878
Area of streams before confluence:
       13.040        6.310        0.660


Results of confluence:
Total flow rate =     43.350(CFS)
Time of concentration =    14.813 min.
Effective stream area after confluence  =     20.010(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      118.100 to Point/Station      118.100
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
UNDEVELOPED (good cover) subarea
Runoff Coefficient = 0.536
Decimal fraction soil group A = 0.810
Decimal fraction soil group B = 0.000
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Decimal fraction soil group C = 0.190
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  44.84
Pervious area fraction =  1.000; Impervious fraction =  0.000
Time of concentration =    14.81 min.
Rainfall intensity =      2.415(In/Hr) for a   100.0 year storm
Subarea runoff =      3.832(CFS) for      2.960(Ac.)
Total runoff =     47.181(CFS)        Total area =      22.970(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      118.100 to Point/Station      121.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1528.500(Ft.)
Downstream point/station elevation =  1523.000(Ft.)
Pipe length  =    55.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    47.181(CFS)
Nearest computed pipe diameter  =     21.00(In.)
Calculated individual pipe flow  =    47.181(CFS)
Normal flow depth in pipe =   16.22(In.)
Flow top width inside pipe =   17.61(In.)
Critical depth could not be calculated.
Pipe flow velocity =     23.69(Ft/s)
Travel time through pipe =    0.04 min.
Time of concentration (TC) =    14.85 min.


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Process from Point/Station      118.100 to Point/Station      121.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =     22.970(Ac.)
Runoff from this stream =     47.181(CFS)
Time of concentration =   14.85 min.
Rainfall intensity =     2.412(In/Hr)
Program is now starting with Main Stream No. 2


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Process from Point/Station      119.000 to Point/Station      119.100
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   611.000(Ft.)
Top (of initial area) elevation =  1536.000(Ft.)
Bottom (of initial area) elevation =  1530.000(Ft.)
Difference in elevation =     6.000(Ft.)
Slope =    0.00982  s(percent)=       0.98
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    9.843 min.
Rainfall intensity =      2.963(In/Hr) for a   100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.856
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  32.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      2.257(CFS)
Total initial stream area =        0.890(Ac.)
Pervious area fraction = 0.100


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Process from Point/Station      119.100 to Point/Station      121.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1523.100(Ft.)
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Downstream point/station elevation =  1523.000(Ft.)
Pipe length  =    48.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     2.257(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =     2.257(CFS)
Normal flow depth in pipe =    9.83(In.)
Flow top width inside pipe =   14.26(In.)
Critical Depth =    7.21(In.)
Pipe flow velocity =      2.65(Ft/s)
Travel time through pipe =    0.30 min.
Time of concentration (TC) =    10.14 min.


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Process from Point/Station      119.100 to Point/Station      121.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =      0.890(Ac.)
Runoff from this stream =      2.257(CFS)
Time of concentration =   10.14 min.
Rainfall intensity =     2.918(In/Hr)
Program is now starting with Main Stream No. 3


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Process from Point/Station      120.000 to Point/Station      120.100
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   833.000(Ft.)
Top (of initial area) elevation =  1530.500(Ft.)
Bottom (of initial area) elevation =  1525.000(Ft.)
Difference in elevation =     5.500(Ft.)
Slope =    0.00660  s(percent)=       0.66
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   12.062 min.
Rainfall intensity =      2.676(In/Hr) for a   100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.854
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  32.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      3.930(CFS)
Total initial stream area =        1.720(Ac.)
Pervious area fraction = 0.100


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Process from Point/Station      120.100 to Point/Station      121.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1523.100(Ft.)
Downstream point/station elevation =  1523.000(Ft.)
Pipe length  =    37.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     3.930(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =     3.930(CFS)
Normal flow depth in pipe =   11.31(In.)
Flow top width inside pipe =   17.40(In.)
Critical Depth =    9.10(In.)
Pipe flow velocity =      3.36(Ft/s)
Travel time through pipe =    0.18 min.
Time of concentration (TC) =    12.25 min.


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Process from Point/Station      120.100 to Point/Station      121.000
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```
**** CONFLUENCE OF MAIN STREAMS ****
_____________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 3
Stream flow area =      1.720(Ac.)
Runoff from this stream =      3.930(CFS)
Time of concentration =   12.25 min.
Rainfall intensity =     2.656(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       47.181     14.85               2.412
2        2.257     10.14               2.918
3        3.930     12.25               2.656
Largest stream flow has longer time of concentration
Qp =     47.181 + sum of
          Qb         Ia/Ib
           2.257 *    0.826 =      1.866
          Qb         Ia/Ib
           3.930 *    0.908 =      3.568
Qp =     52.615

Total of 3 main streams to confluence:
Flow rates before confluence point:
      47.181       2.257       3.930
Area of streams before confluence:
       22.970        0.890        1.720


Results of confluence:
Total flow rate =     52.615(CFS)
Time of concentration =    14.852 min.
Effective stream area after confluence  =     25.580(Ac.)


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Process from Point/Station      121.000 to Point/Station      121.000
**** SUBAREA FLOW ADDITION ****
_____________________________________________________________________
UNDEVELOPED (good cover) subarea
Runoff Coefficient = 0.477
Decimal fraction soil group A = 0.990
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.010
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  38.36
Pervious area fraction =  1.000; Impervious fraction =  0.000
Time of concentration =    14.85 min.
Rainfall intensity =      2.412(In/Hr) for a   100.0 year storm
Subarea runoff =      3.495(CFS) for      3.040(Ac.)
Total runoff =     56.110(CFS)        Total area =      28.620(Ac.)
End of computations, total study area =           28.62 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.456
Area averaged RI index number =  57.7
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10-YEAR

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2001 Version 6.4
Rational Hydrology Study Date: 10/23/21 File:ARA10.out

150.10.18
10-YEAR RATIONAL TABLING METHOD FOR AREA A
POST-PROJECT CONDITION
FN: ARA10.RRV

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

TRI-8 Builders - S/N 615

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 10.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.200(In.)

Storm event year = 10.0
Calculated rainfall intensity data:
1 hour intensity = 0.788(In/Hr)
Slope of intensity duration curve = 0.5000

++

Process from Point/Station 101.000 to Point/Station 102.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 802.000(Ft.)
Top (of initial area) elevation = 1563.000(Ft.)
Bottom (of initial area) elevation = 1537.000(Ft.)
Difference in elevation = 26.000(Ft.)
Slope = 0.03242 s(percent)= 3.24
TC = k(0.370)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 10.659 min.
Rainfall intensity = 1.870(In/Hr) for a 10.0 year storm
CONDOMINIUM subarea type
Runoff Coefficient = 0.820
Decimal fraction soil group A = 0.040
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.960
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 67.52
Pervious area fraction = 0.350; Impervious fraction = 0.650
Initial subarea runoff = 3.172(CFS)
Total initial stream area = 2.070(Ac.)
Pervious area fraction = 0.350

++

Process from Point/Station 102.000 to Point/Station 102.100
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1531.300(Ft.)
Downstream point/station elevation = 1531.200(Ft.)
Pipe length = 22.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 3.172(CFS)
Nearest computed pipe diameter = 15.00(In.)
Calculated individual pipe flow = 3.172(CFS)

```
Normal flow depth in pipe =    9.49(In.)
Flow top width inside pipe =   14.46(In.)
Critical Depth =    8.61(In.)
Pipe flow velocity =      3.87(Ft/s)
Travel time through pipe =    0.09 min.
Time of concentration (TC) =    10.75 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      102.100 to Point/Station      102.100
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
CONDOMINIUM subarea type
Runoff Coefficient = 0.823
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.350; Impervious fraction =  0.650
Time of concentration =    10.75 min.
Rainfall intensity =      1.861(In/Hr) for a    10.0 year storm
Subarea runoff =      0.199(CFS) for      0.130(Ac.)
Total runoff =      3.371(CFS)        Total area =       2.200(Ac.)


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Process from Point/Station      102.100 to Point/Station      105.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1531.200(Ft.)
Downstream point/station elevation =  1530.300(Ft.)
Pipe length  =   205.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     3.371(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =     3.371(CFS)
Normal flow depth in pipe =   10.03(In.)
Flow top width inside pipe =   14.12(In.)
Critical Depth =    8.88(In.)
Pipe flow velocity =      3.86(Ft/s)
Travel time through pipe =    0.88 min.
Time of concentration (TC) =    11.64 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      102.100 to Point/Station      105.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      2.200(Ac.)
Runoff from this stream =      3.371(CFS)
Time of concentration =   11.64 min.
Rainfall intensity =     1.789(In/Hr)


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Process from Point/Station      103.000 to Point/Station      104.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   735.000(Ft.)
Top (of initial area) elevation =  1554.300(Ft.)
Bottom (of initial area) elevation =  1537.000(Ft.)
Difference in elevation =    17.300(Ft.)
Slope =    0.02354  s(percent)=       2.35
TC = k(0.370)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   10.974 min.
Rainfall intensity =      1.843(In/Hr) for a    10.0 year storm
CONDOMINIUM subarea type
Runoff Coefficient = 0.823
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
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Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.350; Impervious fraction =  0.650
Initial subarea runoff =      2.456(CFS)
Total initial stream area =        1.620(Ac.)
Pervious area fraction = 0.350


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      104.000 to Point/Station      104.100
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
________________________________________________________________________
Top of street segment elevation =  1537.000(Ft.)
End of street segment elevation =  1536.000(Ft.)
Length of street segment  =   248.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  22.000(Ft.)
Distance from crown to crossfall grade break  =  18.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.053
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      4.949(CFS)
Depth of flow =   0.494(Ft.), Average velocity =   1.905(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  15.076(Ft.)
Flow velocity =   1.91(Ft/s)
Travel time =    2.17 min.     TC =   13.14  min.
 Adding area flow to street
CONDOMINIUM subarea type
Runoff Coefficient = 0.817
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.350; Impervious fraction =  0.650
Rainfall intensity =      1.684(In/Hr) for a    10.0 year storm
Subarea runoff =      4.527(CFS) for      3.290(Ac.)
Total runoff =      6.983(CFS)        Total area =       4.910(Ac.)
Street flow at end of street =      6.983(CFS)
Half street flow at end of street =      6.983(CFS)
Depth of flow =   0.551(Ft.), Average velocity =   1.942(Ft/s)
Warning: depth of flow exceeds top of curb
Distance that curb overflow reaches into property =    2.54(Ft.)
Flow width (from curb towards crown)=  17.906(Ft.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      104.100 to Point/Station      105.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1530.400(Ft.)
Downstream point/station elevation =  1530.300(Ft.)
Pipe length  =    12.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     6.983(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =     6.983(CFS)
Normal flow depth in pipe =   11.39(In.)
Flow top width inside pipe =   17.35(In.)
Critical Depth =   12.28(In.)
Pipe flow velocity =      5.92(Ft/s)
Travel time through pipe =    0.03 min.
Time of concentration (TC) =    13.18 min.
```

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Process from Point/Station      105.000 to Point/Station      105.000
**** SUBAREA FLOW ADDITION ****
_____________________________________________________________________________
CONDOMINIUM subarea type
Runoff Coefficient = 0.817
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.350; Impervious fraction =  0.650
Time of concentration =    13.18 min.
Rainfall intensity =      1.681(In/Hr) for a    10.0 year storm
Subarea runoff =      1.360(CFS) for      0.990(Ac.)
Total runoff =      8.343(CFS)        Total area =       5.900(Ac.)


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Process from Point/Station      105.000 to Point/Station      105.000
**** CONFLUENCE OF MINOR STREAMS ****
_____________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      5.900(Ac.)
Runoff from this stream =      8.343(CFS)
Time of concentration =   13.18 min.
Rainfall intensity =     1.681(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        3.371     11.64                 1.789
2        8.343     13.18                 1.681
Largest stream flow has longer time of concentration
Qp =      8.343 + sum of
          Qb         Ia/Ib
           3.371 *    0.940 =      3.168
Qp =     11.511

Total of 2 streams to confluence:
Flow rates before confluence point:
       3.371       8.343
Area of streams before confluence:
        2.200        5.900
Results of confluence:
Total flow rate =     11.511(CFS)
Time of concentration =    13.177 min.
Effective stream area after confluence =      8.100(Ac.)


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Process from Point/Station      105.000 to Point/Station      107.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
_____________________________________________________________________________
Upstream point/station elevation =  1530.300(Ft.)
Downstream point/station elevation =  1529.700(Ft.)
Pipe length  =   230.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    11.511(CFS)
Nearest computed pipe diameter  =     24.00(In.)
Calculated individual pipe flow  =    11.511(CFS)
Normal flow depth in pipe =   19.59(In.)
Flow top width inside pipe =   18.58(In.)
Critical Depth =   14.61(In.)
Pipe flow velocity =      4.19(Ft/s)
Travel time through pipe =    0.91 min.
Time of concentration (TC) =    14.09 min.
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++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      105.000 to Point/Station      107.000
**** CONFLUENCE OF MINOR STREAMS ****
____________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      8.100(Ac.)
Runoff from this stream =     11.511(CFS)
Time of concentration =   14.09 min.
Rainfall intensity =     1.626(In/Hr)


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Process from Point/Station      106.000 to Point/Station      106.100
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =   734.000(Ft.)
Top (of initial area) elevation =  1544.300(Ft.)
Bottom (of initial area) elevation =  1536.000(Ft.)
Difference in elevation =     8.300(Ft.)
Slope =    0.01131  s(percent)=       1.13
TC = k(0.370)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   12.700 min.
Rainfall intensity =      1.713(In/Hr) for a    10.0 year storm
CONDOMINIUM subarea type
Runoff Coefficient = 0.818
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.350; Impervious fraction =  0.650
Initial subarea runoff =      3.686(CFS)
Total initial stream area =        2.630(Ac.)
Pervious area fraction = 0.350


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Process from Point/Station      106.100 to Point/Station      107.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
____________________________________________________________________________
Upstream point/station elevation =  1529.800(Ft.)
Downstream point/station elevation =  1529.700(Ft.)
Pipe length  =    14.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     3.686(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =     3.686(CFS)
Normal flow depth in pipe =    9.04(In.)
Flow top width inside pipe =   14.68(In.)
Critical Depth =    9.32(In.)
Pipe flow velocity =      4.78(Ft/s)
Travel time through pipe =    0.05 min.
Time of concentration (TC) =    12.75 min.


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Process from Point/Station      107.000 to Point/Station      107.000
**** SUBAREA FLOW ADDITION ****
____________________________________________________________________________
CONDOMINIUM subarea type
Runoff Coefficient = 0.807
Decimal fraction soil group A = 0.110
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.890
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  64.93
Pervious area fraction =  0.350; Impervious fraction =  0.650
Time of concentration =    12.75 min.
Rainfall intensity =      1.709(In/Hr) for a    10.0 year storm
Subarea runoff =      0.841(CFS) for      0.610(Ac.)
Total runoff =      4.528(CFS)        Total area =       3.240(Ac.)
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Process from Point/Station      107.000 to Point/Station      107.000
**** CONFLUENCE OF MINOR STREAMS ****
_____________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      3.240(Ac.)
Runoff from this stream =      4.528(CFS)
Time of concentration =   12.75 min.
Rainfall intensity =     1.709(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       11.511     14.09                 1.626
2        4.528     12.75                 1.709
Largest stream flow has longer time of concentration
Qp =     11.511 + sum of
          Qb         Ia/Ib
           4.528 *    0.951 =      4.306
Qp =     15.818

Total of 2 streams to confluence:
Flow rates before confluence point:
      11.511       4.528
Area of streams before confluence:
        8.100        3.240
Results of confluence:
Total flow rate =     15.818(CFS)
Time of concentration =    14.091 min.
Effective stream area after confluence =     11.340(Ac.)


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Process from Point/Station      107.000 to Point/Station      109.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
_____________________________________________________________________________
Upstream point/station elevation =  1529.700(Ft.)
Downstream point/station elevation =  1528.000(Ft.)
Pipe length  =   252.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    15.818(CFS)
Nearest computed pipe diameter  =     24.00(In.)
Calculated individual pipe flow  =    15.818(CFS)
Normal flow depth in pipe =   17.02(In.)
Flow top width inside pipe =   21.80(In.)
Critical Depth =   17.19(In.)
Pipe flow velocity =      6.64(Ft/s)
Travel time through pipe =    0.63 min.
Time of concentration (TC) =    14.72 min.


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Process from Point/Station      107.000 to Point/Station      109.000
**** CONFLUENCE OF MINOR STREAMS ****
_____________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =     11.340(Ac.)
Runoff from this stream =     15.818(CFS)
Time of concentration =   14.72 min.
Rainfall intensity =     1.591(In/Hr)


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Process from Point/Station      108.000 to Point/Station      108.100
**** INITIAL AREA EVALUATION ****
_____________________________________________________________________________
Initial area flow distance =   232.000(Ft.)
Top (of initial area) elevation =  1538.900(Ft.)
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Bottom (of initial area) elevation =  1536.000(Ft.)
Difference in elevation =     2.900(Ft.)
Slope =    0.01250  s(percent)=       1.25
TC = k(0.370)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    7.853 min.
Rainfall intensity =      2.178(In/Hr) for a    10.0 year storm
CONDOMINIUM subarea type
Runoff Coefficient = 0.829
Decimal fraction soil group A = 0.030
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.970
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  67.89
Pervious area fraction =  0.350; Impervious fraction =  0.650
Initial subarea runoff =      1.084(CFS)
Total initial stream area =        0.600(Ac.)
Pervious area fraction = 0.350


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      108.100 to Point/Station      108.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1529.100(Ft.)
Downstream point/station elevation =  1529.000(Ft.)
Pipe length  =    38.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     1.084(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     1.084(CFS)
Normal flow depth in pipe =    6.65(In.)
Flow top width inside pipe =   11.93(In.)
Critical Depth =    5.26(In.)
Pipe flow velocity =      2.43(Ft/s)
Travel time through pipe =    0.26 min.
Time of concentration (TC) =     8.11 min.


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Process from Point/Station      108.200 to Point/Station      108.200
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
CONDOMINIUM subarea type
Runoff Coefficient = 0.803
Decimal fraction soil group A = 0.290
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.710
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  58.27
Pervious area fraction =  0.350; Impervious fraction =  0.650
Time of concentration =     8.11 min.
Rainfall intensity =      2.143(In/Hr) for a    10.0 year storm
Subarea runoff =      1.893(CFS) for      1.100(Ac.)
Total runoff =      2.976(CFS)        Total area =       1.700(Ac.)


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Process from Point/Station      108.200 to Point/Station      109.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1529.000(Ft.)
Downstream point/station elevation =  1528.900(Ft.)
Pipe length  =     7.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     2.976(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     2.976(CFS)
Normal flow depth in pipe =    7.39(In.)
Flow top width inside pipe =   11.67(In.)
Critical Depth =    8.88(In.)
Pipe flow velocity =      5.87(Ft/s)
Travel time through pipe =    0.02 min.
Time of concentration (TC) =     8.13 min.
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Process from Point/Station      108.200 to Point/Station      108.200
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      1.700(Ac.)
Runoff from this stream =      2.976(CFS)
Time of concentration =    8.13 min.
Rainfall intensity =     2.140(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       15.818     14.72                 1.591
2        2.976      8.13                 2.140
Largest stream flow has longer time of concentration
Qp =     15.818 + sum of
          Qb         Ia/Ib
           2.976 *    0.743 =      2.212
Qp =     18.030

Total of 2 streams to confluence:
Flow rates before confluence point:
      15.818       2.976
Area of streams before confluence:
       11.340        1.700
Results of confluence:
Total flow rate =     18.030(CFS)
Time of concentration =    14.724 min.
Effective stream area after confluence =     13.040(Ac.)


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Process from Point/Station      109.000 to Point/Station      118.100
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1528.900(Ft.)
Downstream point/station elevation =  1528.500(Ft.)
Pipe length  =   117.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    18.030(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    18.030(CFS)
Normal flow depth in pipe =   22.03(In.)
Flow top width inside pipe =   20.93(In.)
Critical Depth =   17.82(In.)
Pipe flow velocity =      5.19(Ft/s)
Travel time through pipe =    0.38 min.
Time of concentration (TC) =    15.10 min.


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Process from Point/Station      109.000 to Point/Station      118.100
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =     13.040(Ac.)
Runoff from this stream =     18.030(CFS)
Time of concentration =   15.10 min.
Rainfall intensity =     1.571(In/Hr)
Program is now starting with Main Stream No. 2


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Process from Point/Station      110.000 to Point/Station      110.100
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
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Initial area flow distance =   614.000(Ft.)
Top (of initial area) elevation =  1569.000(Ft.)
Bottom (of initial area) elevation =  1545.000(Ft.)
Difference in elevation =    24.000(Ft.)
Slope =    0.03909  s(percent)=       3.91
TC = k(0.370)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    9.227 min.
Rainfall intensity =      2.009(In/Hr) for a    10.0 year storm
CONDOMINIUM subarea type
Runoff Coefficient = 0.828
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.350; Impervious fraction =  0.650
Initial subarea runoff =      3.110(CFS)
Total initial stream area =        1.870(Ac.)
Pervious area fraction = 0.350


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Process from Point/Station      110.100 to Point/Station      111.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of street segment elevation =  1545.000(Ft.)
End of street segment elevation =  1541.000(Ft.)
Length of street segment  =   162.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  22.000(Ft.)
Distance from crown to crossfall grade break  =  18.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.053
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      3.659(CFS)
Depth of flow =   0.356(Ft.), Average velocity =   3.704(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =   8.143(Ft.)
Flow velocity =   3.70(Ft/s)
Travel time =    0.73 min.     TC =    9.96  min.
 Adding area flow to street
CONDOMINIUM subarea type
Runoff Coefficient = 0.826
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.350; Impervious fraction =  0.650
Rainfall intensity =      1.934(In/Hr) for a    10.0 year storm
Subarea runoff =      1.054(CFS) for      0.660(Ac.)
Total runoff =      4.164(CFS)        Total area =       2.530(Ac.)
Street flow at end of street =      4.164(CFS)
Half street flow at end of street =      4.164(CFS)
Depth of flow =   0.369(Ft.), Average velocity =   3.783(Ft/s)
Flow width (from curb towards crown)=   8.810(Ft.)


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Process from Point/Station      111.000 to Point/Station      112.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1529.800(Ft.)
Downstream point/station elevation =  1529.700(Ft.)
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```
Pipe length  =    45.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     4.164(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =     4.164(CFS)
Normal flow depth in pipe =   12.63(In.)
Flow top width inside pipe =   16.47(In.)
Critical Depth =    9.38(In.)
Pipe flow velocity =      3.14(Ft/s)
Travel time through pipe =    0.24 min.
Time of concentration (TC) =    10.19 min.


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Process from Point/Station      111.000 to Point/Station      112.200
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =      2.530(Ac.)
Runoff from this stream =      4.164(CFS)
Time of concentration =   10.19 min.
Rainfall intensity =     1.912(In/Hr)


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Process from Point/Station      112.000 to Point/Station      112.100
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   337.000(Ft.)
Top (of initial area) elevation =  1548.100(Ft.)
Bottom (of initial area) elevation =  1541.000(Ft.)
Difference in elevation =     7.100(Ft.)
Slope =    0.02107  s(percent)=       2.11
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    6.660 min.
Rainfall intensity =      2.365(In/Hr) for a    10.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.882
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      0.480(CFS)
Total initial stream area =        0.230(Ac.)
Pervious area fraction = 0.100


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Process from Point/Station      112.100 to Point/Station      112.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1529.900(Ft.)
Downstream point/station elevation =  1529.700(Ft.)
Pipe length  =    60.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     0.480(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     0.480(CFS)
Normal flow depth in pipe =    4.51(In.)
Flow top width inside pipe =    9.00(In.)
Critical Depth =    3.75(In.)
Pipe flow velocity =      2.16(Ft/s)
Travel time through pipe =    0.46 min.
Time of concentration (TC) =     7.12 min.


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Process from Point/Station      112.100 to Point/Station      112.200
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
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Stream flow area =      0.230(Ac.)
Runoff from this stream =      0.480(CFS)
Time of concentration =    7.12 min.
Rainfall intensity =     2.287(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        4.164     10.19                 1.912
2        0.480      7.12                 2.287
Largest stream flow has longer time of concentration
Qp =      4.164 + sum of
          Qb         Ia/Ib
           0.480 *    0.836 =      0.401
Qp =      4.565

Total of 2 streams to confluence:
Flow rates before confluence point:
       4.164       0.480
Area of streams before confluence:
        2.530        0.230
Results of confluence:
Total flow rate =      4.565(CFS)
Time of concentration =    10.195 min.
Effective stream area after confluence =      2.760(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      112.200 to Point/Station      114.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1529.700(Ft.)
Downstream point/station elevation =  1528.900(Ft.)
Pipe length  =   260.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     4.565(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =     4.565(CFS)
Normal flow depth in pipe =   12.00(In.)
Flow top width inside pipe =   16.97(In.)
Critical Depth =    9.84(In.)
Pipe flow velocity =      3.65(Ft/s)
Travel time through pipe =    1.19 min.
Time of concentration (TC) =    11.38 min.


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Process from Point/Station      112.200 to Point/Station      114.200
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =      2.760(Ac.)
Runoff from this stream =      4.565(CFS)
Time of concentration =   11.38 min.
Rainfall intensity =     1.809(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      113.000 to Point/Station      114.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   439.000(Ft.)
Top (of initial area) elevation =  1544.100(Ft.)
Bottom (of initial area) elevation =  1536.400(Ft.)
Difference in elevation =     7.700(Ft.)
Slope =    0.01754  s(percent)=       1.75
TC = k(0.370)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    9.471 min.
Rainfall intensity =      1.983(In/Hr) for a    10.0 year storm
CONDOMINIUM subarea type
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Runoff Coefficient = 0.827
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.350; Impervious fraction =  0.650
Initial subarea runoff =      2.050(CFS)
Total initial stream area =        1.250(Ac.)
Pervious area fraction = 0.350


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Process from Point/Station      114.000 to Point/Station      114.100
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of street segment elevation =  1536.400(Ft.)
End of street segment elevation =  1536.000(Ft.)
Length of street segment  =    72.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  22.000(Ft.)
Distance from crown to crossfall grade break  =  18.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.053
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      2.583(CFS)
Depth of flow =   0.397(Ft.), Average velocity =   1.884(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  10.229(Ft.)
Flow velocity =   1.88(Ft/s)
Travel time =    0.64 min.     TC =   10.11  min.
 Adding area flow to street
CONDOMINIUM subarea type
Runoff Coefficient = 0.825
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.350; Impervious fraction =  0.650
Rainfall intensity =      1.920(In/Hr) for a    10.0 year storm
Subarea runoff =      1.030(CFS) for      0.650(Ac.)
Total runoff =      3.080(CFS)        Total area =       1.900(Ac.)
Street flow at end of street =      3.080(CFS)
Half street flow at end of street =      3.080(CFS)
Depth of flow =   0.417(Ft.), Average velocity =   1.951(Ft/s)
Flow width (from curb towards crown)=  11.199(Ft.)


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Process from Point/Station      114.100 to Point/Station      114.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1529.000(Ft.)
Downstream point/station elevation =  1528.900(Ft.)
Pipe length  =    19.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     3.080(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =     3.080(CFS)
Normal flow depth in pipe =    8.87(In.)
Flow top width inside pipe =   14.75(In.)
Critical Depth =    8.47(In.)
Pipe flow velocity =      4.08(Ft/s)
Travel time through pipe =    0.08 min.
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Time of concentration (TC) =    10.19 min.


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Process from Point/Station      114.100 to Point/Station      114.200
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =      1.900(Ac.)
Runoff from this stream =      3.080(CFS)
Time of concentration =   10.19 min.
Rainfall intensity =     1.913(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        4.565     11.38                 1.809
2        3.080     10.19                 1.913
Largest stream flow has longer time of concentration
Qp =      4.565 + sum of
          Qb         Ia/Ib
           3.080 *    0.946 =      2.913
Qp =      7.478

Total of 2 streams to confluence:
Flow rates before confluence point:
       4.565       3.080
Area of streams before confluence:
        2.760        1.900
Results of confluence:
Total flow rate =      7.478(CFS)
Time of concentration =    11.382 min.
Effective stream area after confluence =      4.660(Ac.)


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Process from Point/Station      114.200 to Point/Station      115.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1528.900(Ft.)
Downstream point/station elevation =  1528.800(Ft.)
Pipe length  =    29.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     7.478(CFS)
Nearest computed pipe diameter  =     21.00(In.)
Calculated individual pipe flow  =     7.478(CFS)
Normal flow depth in pipe =   14.25(In.)
Flow top width inside pipe =   19.62(In.)
Critical Depth =   12.16(In.)
Pipe flow velocity =      4.30(Ft/s)
Travel time through pipe =    0.11 min.
Time of concentration (TC) =    11.49 min.


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Process from Point/Station      114.200 to Point/Station      115.200
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =      4.660(Ac.)
Runoff from this stream =      7.478(CFS)
Time of concentration =   11.49 min.
Rainfall intensity =     1.800(In/Hr)


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Process from Point/Station      115.000 to Point/Station      115.100
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   448.000(Ft.)
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Top (of initial area) elevation =  1540.500(Ft.)
Bottom (of initial area) elevation =  1536.000(Ft.)
Difference in elevation =     4.500(Ft.)
Slope =    0.01004  s(percent)=       1.00
TC = k(0.370)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   10.674 min.
Rainfall intensity =      1.868(In/Hr) for a    10.0 year storm
CONDOMINIUM subarea type
Runoff Coefficient = 0.767
Decimal fraction soil group A = 0.530
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.470
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  49.39
Pervious area fraction =  0.350; Impervious fraction =  0.650
Initial subarea runoff =      2.364(CFS)
Total initial stream area =        1.650(Ac.)
Pervious area fraction = 0.350


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Process from Point/Station      115.100 to Point/Station      115.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1528.900(Ft.)
Downstream point/station elevation =  1528.800(Ft.)
Pipe length  =     7.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     2.364(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     2.364(CFS)
Normal flow depth in pipe =    6.39(In.)
Flow top width inside pipe =   11.98(In.)
Critical Depth =    7.90(In.)
Pipe flow velocity =      5.56(Ft/s)
Travel time through pipe =    0.02 min.
Time of concentration (TC) =    10.69 min.


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Process from Point/Station      115.100 to Point/Station      115.200
**** CONFLUENCE OF MINOR STREAMS ****
________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =      1.650(Ac.)
Runoff from this stream =      2.364(CFS)
Time of concentration =   10.69 min.
Rainfall intensity =     1.866(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        7.478     11.49                 1.800
2        2.364     10.69                 1.866
Largest stream flow has longer time of concentration
Qp =      7.478 + sum of
          Qb         Ia/Ib
           2.364 *    0.965 =      2.280
Qp =      9.759

Total of 2 streams to confluence:
Flow rates before confluence point:
       7.478       2.364
Area of streams before confluence:
        4.660        1.650
Results of confluence:
Total flow rate =      9.759(CFS)
Time of concentration =    11.494 min.
Effective stream area after confluence =      6.310(Ac.)
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Process from Point/Station      115.200 to Point/Station      118.100
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1528.800(Ft.)
Downstream point/station elevation =  1528.500(Ft.)
Pipe length  =   107.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     9.759(CFS)
Nearest computed pipe diameter  =     24.00(In.)
Calculated individual pipe flow  =     9.759(CFS)
Normal flow depth in pipe =   16.45(In.)
Flow top width inside pipe =   22.29(In.)
Critical Depth =   13.41(In.)
Pipe flow velocity =      4.25(Ft/s)
Travel time through pipe =    0.42 min.
Time of concentration (TC) =    11.91 min.


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Process from Point/Station      115.200 to Point/Station      118.100
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =      6.310(Ac.)
Runoff from this stream =      9.759(CFS)
Time of concentration =   11.91 min.
Rainfall intensity =     1.768(In/Hr)
Program is now starting with Main Stream No. 3


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Process from Point/Station      116.000 to Point/Station      118.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   531.000(Ft.)
Top (of initial area) elevation =  1544.100(Ft.)
Bottom (of initial area) elevation =  1534.300(Ft.)
Difference in elevation =     9.800(Ft.)
Slope =    0.01846  s(percent)=       1.85
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    8.202 min.
Rainfall intensity =      2.131(In/Hr) for a    10.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.866
Decimal fraction soil group A = 0.490
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.510
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  50.87
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      0.978(CFS)
Total initial stream area =        0.530(Ac.)
Pervious area fraction = 0.100


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Process from Point/Station      116.000 to Point/Station      118.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 3 in normal stream number 1
Stream flow area =      0.530(Ac.)
Runoff from this stream =      0.978(CFS)
Time of concentration =    8.20 min.
Rainfall intensity =     2.131(In/Hr)


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Process from Point/Station      117.000 to Point/Station      117.100
**** INITIAL AREA EVALUATION ****
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Initial area flow distance =   462.000(Ft.)
Top (of initial area) elevation =  1543.600(Ft.)
Bottom (of initial area) elevation =  1534.300(Ft.)
Difference in elevation =     9.300(Ft.)
Slope =    0.02013  s(percent)=       2.01
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    7.624 min.
Rainfall intensity =      2.210(In/Hr) for a    10.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.860
Decimal fraction soil group A = 0.690
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.310
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  43.47
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      0.247(CFS)
Total initial stream area =        0.130(Ac.)
Pervious area fraction = 0.100


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Process from Point/Station      117.100 to Point/Station      118.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------
Upstream point/station elevation =  1528.700(Ft.)
Downstream point/station elevation =  1528.600(Ft.)
Pipe length  =    33.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     0.247(CFS)
Nearest computed pipe diameter  =      6.00(In.)
Calculated individual pipe flow  =     0.247(CFS)
Normal flow depth in pipe =    4.05(In.)
Flow top width inside pipe =    5.62(In.)
Critical Depth =    3.00(In.)
Pipe flow velocity =      1.75(Ft/s)
Travel time through pipe =    0.31 min.
Time of concentration (TC) =     7.94 min.


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Process from Point/Station      117.100 to Point/Station      118.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------
Along Main Stream number: 3 in normal stream number 2
Stream flow area =      0.130(Ac.)
Runoff from this stream =      0.247(CFS)
Time of concentration =    7.94 min.
Rainfall intensity =     2.166(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        0.978      8.20                2.131
2        0.247      7.94                2.166
Largest stream flow has longer time of concentration
Qp =      0.978 + sum of
          Qb         Ia/Ib
           0.247 *    0.984 =      0.243
Qp =      1.222

Total of 2 streams to confluence:
Flow rates before confluence point:
       0.978       0.247
Area of streams before confluence:
        0.530        0.130
Results of confluence:
Total flow rate =      1.222(CFS)
Time of concentration =     8.202 min.
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Effective stream area after confluence =      0.660(Ac.)


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Process from Point/Station      118.000 to Point/Station      118.100
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1528.600(Ft.)
Downstream point/station elevation =  1528.500(Ft.)
Pipe length  =    43.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     1.222(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     1.222(CFS)
Normal flow depth in pipe =    7.48(In.)
Flow top width inside pipe =   11.63(In.)
Critical Depth =    5.60(In.)
Pipe flow velocity =      2.37(Ft/s)
Travel time through pipe =    0.30 min.
Time of concentration (TC) =     8.50 min.


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Process from Point/Station      118.000 to Point/Station      118.100
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 3
Stream flow area =      0.660(Ac.)
Runoff from this stream =      1.222(CFS)
Time of concentration =    8.50 min.
Rainfall intensity =     2.093(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                  (In/Hr)


1       18.030     15.10               1.571
2        9.759     11.91               1.768
3        1.222      8.50               2.093
Largest stream flow has longer time of concentration
Qp =     18.030 + sum of
          Qb          Ia/Ib
           9.759 *    0.888 =      8.668
          Qb          Ia/Ib
           1.222 *    0.750 =      0.917
Qp =     27.615

Total of 3 main streams to confluence:
Flow rates before confluence point:
      18.030       9.759       1.222
Area of streams before confluence:
       13.040        6.310        0.660


Results of confluence:
Total flow rate =     27.615(CFS)
Time of concentration =    15.099 min.
Effective stream area after confluence  =     20.010(Ac.)


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Process from Point/Station      118.100 to Point/Station      118.100
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
UNDEVELOPED (good cover) subarea
Runoff Coefficient = 0.440
Decimal fraction soil group A = 0.810
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.190
Decimal fraction soil group D = 0.000
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RI index for soil(AMC 2)  =  44.84
Pervious area fraction =  1.000; Impervious fraction =  0.000
Time of concentration =    15.10 min.
Rainfall intensity =      1.571(In/Hr) for a    10.0 year storm
Subarea runoff =      2.047(CFS) for      2.960(Ac.)
Total runoff =     29.662(CFS)        Total area =      22.970(Ac.)


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Process from Point/Station      118.100 to Point/Station      121.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1528.500(Ft.)
Downstream point/station elevation =  1523.000(Ft.)
Pipe length  =    55.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    29.662(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =    29.662(CFS)
Normal flow depth in pipe =   13.27(In.)
Flow top width inside pipe =   15.85(In.)
Critical depth could not be calculated.
Pipe flow velocity =     21.25(Ft/s)
Travel time through pipe =    0.04 min.
Time of concentration (TC) =    15.14 min.


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Process from Point/Station      118.100 to Point/Station      121.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =     22.970(Ac.)
Runoff from this stream =     29.662(CFS)
Time of concentration =   15.14 min.
Rainfall intensity =     1.569(In/Hr)
Program is now starting with Main Stream No. 2


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Process from Point/Station      119.000 to Point/Station      119.100
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   611.000(Ft.)
Top (of initial area) elevation =  1536.000(Ft.)
Bottom (of initial area) elevation =  1530.000(Ft.)
Difference in elevation =     6.000(Ft.)
Slope =    0.00982  s(percent)=       0.98
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    9.843 min.
Rainfall intensity =      1.946(In/Hr) for a    10.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.847
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  32.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      1.466(CFS)
Total initial stream area =        0.890(Ac.)
Pervious area fraction = 0.100


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Process from Point/Station      119.100 to Point/Station      121.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1523.100(Ft.)
Downstream point/station elevation =  1523.000(Ft.)
Pipe length  =    48.00(Ft.)   Manning's N = 0.013
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No. of pipes = 1  Required pipe flow  =     1.466(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     1.466(CFS)
Normal flow depth in pipe =    8.91(In.)
Flow top width inside pipe =   10.50(In.)
Critical Depth =    6.16(In.)
Pipe flow velocity =      2.34(Ft/s)
Travel time through pipe =    0.34 min.
Time of concentration (TC) =    10.18 min.


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Process from Point/Station      119.100 to Point/Station      121.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =      0.890(Ac.)
Runoff from this stream =      1.466(CFS)
Time of concentration =   10.18 min.
Rainfall intensity =     1.913(In/Hr)
Program is now starting with Main Stream No. 3


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Process from Point/Station      120.000 to Point/Station      120.100
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   833.000(Ft.)
Top (of initial area) elevation =  1530.500(Ft.)
Bottom (of initial area) elevation =  1525.000(Ft.)
Difference in elevation =     5.500(Ft.)
Slope =    0.00660  s(percent)=       0.66
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   12.062 min.
Rainfall intensity =      1.757(In/Hr) for a    10.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.844
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  32.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      2.553(CFS)
Total initial stream area =        1.720(Ac.)
Pervious area fraction = 0.100


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Process from Point/Station      120.100 to Point/Station      121.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1523.100(Ft.)
Downstream point/station elevation =  1523.000(Ft.)
Pipe length  =    37.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     2.553(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =     2.553(CFS)
Normal flow depth in pipe =    9.79(In.)
Flow top width inside pipe =   14.29(In.)
Critical Depth =    7.68(In.)
Pipe flow velocity =      3.01(Ft/s)
Travel time through pipe =    0.20 min.
Time of concentration (TC) =    12.27 min.


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Process from Point/Station      120.100 to Point/Station      121.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
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The following data inside Main Stream is listed:
In Main Stream number: 3
Stream flow area =      1.720(Ac.)
Runoff from this stream =      2.553(CFS)
Time of concentration =   12.27 min.
Rainfall intensity =     1.743(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       29.662     15.14                1.569
2        1.466     10.18                1.913
3        2.553     12.27                1.743
Largest stream flow has longer time of concentration
Qp =     29.662 + sum of
          Qb         Ia/Ib
           1.466 *    0.820 =      1.202
          Qb         Ia/Ib
           2.553 *    0.900 =      2.297
Qp =     33.162

Total of 3 main streams to confluence:
Flow rates before confluence point:
      29.662       1.466       2.553
Area of streams before confluence:
       22.970        0.890        1.720


Results of confluence:
Total flow rate =     33.162(CFS)
Time of concentration =    15.143 min.
Effective stream area after confluence  =     25.580(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      121.000 to Point/Station      121.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
UNDEVELOPED (good cover) subarea
Runoff Coefficient = 0.380
Decimal fraction soil group A = 0.990
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.010
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  38.36
Pervious area fraction =  1.000; Impervious fraction =  0.000
Time of concentration =    15.14 min.
Rainfall intensity =      1.569(In/Hr) for a    10.0 year storm
Subarea runoff =      1.814(CFS) for      3.040(Ac.)
Total runoff =     34.976(CFS)        Total area =      28.620(Ac.)
End of computations, total study area =           28.62 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.456
Area averaged RI index number =  57.7
```

APPENDIX B.2: AREA "B"

100-YEAR

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2001 Version 6.4
Rational Hydrology Study Date: 10/23/21 File:ARB100.out

150.10.18
100-YEAR RATIONAL TABLING METHOD FOR AREA B
POST-PROJECT CONDITION
FN: ARB100.RRV

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

TRI-8 Builders - S/N 615

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.200(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.200(In/Hr)
Slope of intensity duration curve = 0.5000

++

Process from Point/Station 201.000 to Point/Station 202.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 470.000(Ft.)
Top (of initial area) elevation = 1577.300(Ft.)
Bottom (of initial area) elevation = 1558.000(Ft.)
Difference in elevation = 19.300(Ft.)
Slope = 0.04106 s(percent)= 4.11
TC = k(0.710)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 15.755 min.
Rainfall intensity = 2.342(In/Hr) for a 100.0 year storm
UNDEVELOPED (fair cover) subarea
Runoff Coefficient = 0.643
Decimal fraction soil group A = 0.700
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.300
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 58.70
Pervious area fraction = 1.000; Impervious fraction = 0.000
Initial subarea runoff = 1.099(CFS)
Total initial stream area = 0.730(Ac.)
Pervious area fraction = 1.000

++

Process from Point/Station 202.000 to Point/Station 203.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****

Top of natural channel elevation = 1558.000(Ft.)
End of natural channel elevation = 1530.000(Ft.)
Length of natural channel = 633.000(Ft.)
Estimated mean flow rate at midpoint of channel = 1.640(CFS)

Natural valley channel type used

```
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   3.47(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0442
Corrected/adjusted channel slope =  0.0442
Travel time =    3.04 min.     TC =   18.79  min.


 Adding area flow to channel
UNDEVELOPED (fair cover) subarea
Runoff Coefficient = 0.773
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.990
Decimal fraction soil group D = 0.010
RI index for soil(AMC 2)  =  79.05
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.144(In/Hr) for a   100.0 year storm
Subarea runoff =      1.193(CFS) for      0.720(Ac.)
Total runoff =      2.291(CFS)        Total area =       1.450(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      203.000 to Point/Station      203.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
USER INPUT of soil data for subarea
Runoff Coefficient = 0.862
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.860
Decimal fraction soil group D = 0.140
RI index for soil(AMC 2)  =  69.84
Pervious area fraction =  0.200; Impervious fraction =  0.800
Time of concentration =    18.79 min.
Rainfall intensity =      2.144(In/Hr) for a   100.0 year storm
Subarea runoff =      0.536(CFS) for      0.290(Ac.)
Total runoff =      2.827(CFS)        Total area =       1.740(Ac.)
End of computations, total study area =            1.74 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.867
Area averaged RI index number =  69.0
```

10-YEAR

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2001 Version 6.4
Rational Hydrology Study Date: 10/23/21 File:ARB10.out

150.10.18
10-YEAR RATIONAL TABLING METHOD FOR AREA B
POST-PROJECT CONDITION
FN: ARB10.RRV

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

TRI-8 Builders - S/N 615

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 10.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.200(In.)

Storm event year = 10.0
Calculated rainfall intensity data:
1 hour intensity = 0.788(In/Hr)
Slope of intensity duration curve = 0.5000

++

Process from Point/Station 201.000 to Point/Station 202.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 470.000(Ft.)
Top (of initial area) elevation = 1577.300(Ft.)
Bottom (of initial area) elevation = 1558.000(Ft.)
Difference in elevation = 19.300(Ft.)
Slope = 0.04106 s(percent)= 4.11
TC = k(0.710)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 15.755 min.
Rainfall intensity = 1.538(In/Hr) for a 10.0 year storm
UNDEVELOPED (fair cover) subarea
Runoff Coefficient = 0.559
Decimal fraction soil group A = 0.700
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.300
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2) = 58.70
Pervious area fraction = 1.000; Impervious fraction = 0.000
Initial subarea runoff = 0.628(CFS)
Total initial stream area = 0.730(Ac.)
Pervious area fraction = 1.000

++

Process from Point/Station 202.000 to Point/Station 203.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****

Top of natural channel elevation = 1558.000(Ft.)
End of natural channel elevation = 1530.000(Ft.)
Length of natural channel = 633.000(Ft.)
Estimated mean flow rate at midpoint of channel = 0.937(CFS)

Natural valley channel type used

```
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   3.12(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0442
Corrected/adjusted channel slope =  0.0442
Travel time =    3.39 min.     TC =   19.14  min.


 Adding area flow to channel
UNDEVELOPED (fair cover) subarea
Runoff Coefficient = 0.718
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.990
Decimal fraction soil group D = 0.010
RI index for soil(AMC 2)  =  79.05
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.395(In/Hr) for a    10.0 year storm
Subarea runoff =      0.721(CFS) for      0.720(Ac.)
Total runoff =      1.349(CFS)        Total area =       1.450(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      203.000 to Point/Station      203.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
USER INPUT of soil data for subarea
Runoff Coefficient = 0.847
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.860
Decimal fraction soil group D = 0.140
RI index for soil(AMC 2)  =  69.84
Pervious area fraction =  0.200; Impervious fraction =  0.800
Time of concentration =    19.14 min.
Rainfall intensity =      1.395(In/Hr) for a    10.0 year storm
Subarea runoff =      0.343(CFS) for      0.290(Ac.)
Total runoff =      1.692(CFS)        Total area =       1.740(Ac.)
End of computations, total study area =            1.74 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.867
Area averaged RI index number =  69.0
```

APPENDIX B.3: AREA "C"

100-YEAR

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2001 Version 6.4
Rational Hydrology Study Date: 10/23/21 File:ARC100.out

150.10.18
100-YEAR RATIONAL TABLING METHOD FOR AREA C
POST-PROJECT CONDITION
FN: ARC100.RRV

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

TRI-8 Builders - S/N 615

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.200(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.200(In/Hr)
Slope of intensity duration curve = 0.5000

++

Process from Point/Station 301.000 to Point/Station 302.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 207.000(Ft.)
Top (of initial area) elevation = 1538.000(Ft.)
Bottom (of initial area) elevation = 1529.000(Ft.)
Difference in elevation = 9.000(Ft.)
Slope = 0.04348 s(percent)= 4.35
TC = k(0.370)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 5.847 min.
Rainfall intensity = 3.844(In/Hr) for a 100.0 year storm
CONDOMINIUM subarea type
Runoff Coefficient = 0.859
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.860
Decimal fraction soil group D = 0.140
RI index for soil(AMC 2) = 69.84
Pervious area fraction = 0.350; Impervious fraction = 0.650
Initial subarea runoff = 0.693(CFS)
Total initial stream area = 0.210(Ac.)
Pervious area fraction = 0.350
End of computations, total study area = 0.21 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.350
Area averaged RI index number = 69.8

10-YEAR

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 12/22/20 File:ARC10.out

HEMET 30 POST-PROJECT CONDITION OFFSITE HYDROLOGY
RATIONAL METHOD ANALYSIS, 10-YEAR STORM EVENT
FILENAME: ARC10

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 10.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.200(In.)

Storm event year = 10.0
Calculated rainfall intensity data:
1 hour intensity = 0.788(In/Hr)
Slope of intensity duration curve = 0.5000

++

Process from Point/Station 301.000 to Point/Station 302.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 999.000(Ft.)
Top (of initial area) elevation = 2028.000(Ft.)
Bottom (of initial area) elevation = 1656.000(Ft.)
Difference in elevation = 372.000(Ft.)
Slope = 0.37237 s(percent)= 37.24
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 10.231 min.
Rainfall intensity = 1.908(In/Hr) for a 10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.808
Decimal fraction soil group A = 0.020
Decimal fraction soil group B = 0.210
Decimal fraction soil group C = 0.100
Decimal fraction soil group D = 0.670
RI index for soil(AMC 2) = 85.95
Pervious area fraction = 1.000; Impervious fraction = 0.000
Initial subarea runoff = 9.557(CFS)
Total initial stream area = 6.200(Ac.)
Pervious area fraction = 1.000

++

Process from Point/Station 302.000 to Point/Station 303.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****

Top of natural channel elevation = 1656.000(Ft.)
End of natural channel elevation = 1588.000(Ft.)
Length of natural channel = 777.000(Ft.)

```
Estimated mean flow rate at midpoint of channel =     16.994(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.49(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0875
Corrected/adjusted channel slope =  0.0875
Travel time =    1.53 min.     TC =   11.76  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.772
Decimal fraction soil group A = 0.160
Decimal fraction soil group B = 0.310
Decimal fraction soil group C = 0.060
Decimal fraction soil group D = 0.470
RI index for soil(AMC 2)  =  81.89
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.780(In/Hr) for a    10.0 year storm
Subarea runoff =     13.263(CFS) for      9.650(Ac.)
Total runoff =     22.820(CFS)        Total area =      15.850(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      303.000 to Point/Station      304.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1588.000(Ft.)
End of natural channel elevation =   1564.000(Ft.)
Length of natural channel  =   759.000(Ft.)
Estimated mean flow rate at midpoint of channel =     50.305(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   6.89(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0316
Corrected/adjusted channel slope =  0.0316
Travel time =    1.83 min.     TC =   13.59  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.764
Decimal fraction soil group A = 0.160
Decimal fraction soil group B = 0.310
Decimal fraction soil group C = 0.060
Decimal fraction soil group D = 0.470
RI index for soil(AMC 2)  =  81.89
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.656(In/Hr) for a    10.0 year storm
Subarea runoff =     48.290(CFS) for     38.180(Ac.)
Total runoff =     71.110(CFS)        Total area =      54.030(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      304.000 to Point/Station      305.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1564.000(Ft.)
End of natural channel elevation =   1540.000(Ft.)
Length of natural channel  =  1301.000(Ft.)
Estimated mean flow rate at midpoint of channel =     92.780(CFS)
```

```
Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   6.30(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0184
Corrected/adjusted channel slope =  0.0184
Travel time =    3.44 min.     TC =   17.03  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.720
Decimal fraction soil group A = 0.420
Decimal fraction soil group B = 0.090
Decimal fraction soil group C = 0.150
Decimal fraction soil group D = 0.340
RI index for soil(AMC 2)  =  78.32
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.479(In/Hr) for a    10.0 year storm
Subarea runoff =     35.079(CFS) for     32.930(Ac.)
Total runoff =    106.189(CFS)        Total area =      86.960(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      305.000 to Point/Station      306.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
________________________________________________________________________
Top of natural channel elevation =   1540.000(Ft.)
End of natural channel elevation =   1532.000(Ft.)
Length of natural channel  =   878.000(Ft.)
Estimated mean flow rate at midpoint of channel =    147.762(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   5.10(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0091
Corrected/adjusted channel slope =  0.0091
Travel time =    2.87 min.     TC =   19.90  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.747
Decimal fraction soil group A = 0.220
Decimal fraction soil group B = 0.030
Decimal fraction soil group C = 0.400
Decimal fraction soil group D = 0.350
RI index for soil(AMC 2)  =  82.63
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.368(In/Hr) for a    10.0 year storm
Subarea runoff =     69.591(CFS) for     68.090(Ac.)
Total runoff =    175.780(CFS)        Total area =     155.050(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      306.000 to Point/Station      307.000
**** IMPROVED CHANNEL TRAVEL TIME ****
________________________________________________________________________
Upstream point elevation =  1532.000(Ft.)
Downstream point elevation =  1525.000(Ft.)
Channel length thru subarea  =   970.000(Ft.)
Channel base width     =   50.000(Ft.)
Slope or 'Z' of left channel bank =   2.000
```

```
Slope or 'Z' of right channel bank =   4.000
Estimated mean flow rate at midpoint of channel =    177.896(CFS)
Manning's 'N'    = 0.030
Maximum depth of channel  =    4.000(Ft.)
Flow(q) thru subarea =    177.896(CFS)
Depth of flow =   0.896(Ft.), Average velocity =   3.768(Ft/s)
Channel flow top width =   55.376(Ft.)
Flow Velocity =    3.77(Ft/s)
Travel time  =    4.29 min.
Time of concentration =   24.19 min.

Sub-Channel No. 1 Critical depth =      0.719(Ft.)
  '     '       '     Critical flow top width =     54.313(Ft.)
  '     '       '     Critical flow velocity=    4.745(Ft/s)
  '     '       '     Critical flow area =     37.487(Sq.Ft)

 Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.548
Decimal fraction soil group A = 0.930
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.070
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  41.64
Pervious area fraction =  0.650; Impervious fraction =  0.350
Rainfall intensity =      1.241(In/Hr) for a    10.0 year storm
Subarea runoff =      4.145(CFS) for      6.090(Ac.)
Total runoff =    179.925(CFS)        Total area =     161.140(Ac.)
Depth of flow =   0.902(Ft.), Average velocity =   3.785(Ft/s)

Sub-Channel No. 1 Critical depth =      0.727(Ft.)
  '     '       '     Critical flow top width =     54.359(Ft.)
  '     '       '     Critical flow velocity=    4.746(Ft/s)
  '     '       '     Critical flow area =     37.912(Sq.Ft)

End of computations, total study area =          161.14 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.987
Area averaged RI index number =  80.1
```

APPENDIX B.4: OFFSITE AREA "C" – EXISTING CONDITION OFFSITE AREA

100-YEAR

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 11/01/21 File:ARCEX100.out

150.10.18
100-YEAR RATIONAL TABLING METHOD FOR OFFSITE AREA C
EXISTING CONDITION
FN: ARA100.RRV

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.200(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.200(In/Hr)
Slope of intensity duration curve = 0.5000

++

Process from Point/Station 301.000 to Point/Station 302.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 999.000(Ft.)
Top (of initial area) elevation = 2028.000(Ft.)
Bottom (of initial area) elevation = 1656.000(Ft.)
Difference in elevation = 372.000(Ft.)
Slope = 0.37237 s(percent)= 37.24
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 10.231 min.
Rainfall intensity = 2.906(In/Hr) for a 100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.852
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
RI index for soil(AMC 2) = 89.00
Pervious area fraction = 1.000; Impervious fraction = 0.000
Initial subarea runoff = 15.346(CFS)
Total initial stream area = 6.200(Ac.)
Pervious area fraction = 1.000

++

Process from Point/Station 302.000 to Point/Station 303.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****

Top of natural channel elevation = 1656.000(Ft.)
End of natural channel elevation = 1588.000(Ft.)
Length of natural channel = 777.000(Ft.)

```
Estimated mean flow rate at midpoint of channel =     27.288(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.65(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0875
Corrected/adjusted channel slope =  0.0875
Travel time =    1.34 min.     TC =   11.57  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.834
Decimal fraction soil group A = 0.020
Decimal fraction soil group B = 0.210
Decimal fraction soil group C = 0.100
Decimal fraction soil group D = 0.670
RI index for soil(AMC 2)  =  85.95
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.732(In/Hr) for a   100.0 year storm
Subarea runoff =     21.977(CFS) for      9.650(Ac.)
Total runoff =     37.323(CFS)        Total area =      15.850(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      303.000 to Point/Station      304.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1588.000(Ft.)
End of natural channel elevation =   1564.000(Ft.)
Length of natural channel  =   759.000(Ft.)
Estimated mean flow rate at midpoint of channel =     82.276(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.96(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0316
Corrected/adjusted channel slope =  0.0316
Travel time =    1.59 min.     TC =   13.16  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.807
Decimal fraction soil group A = 0.160
Decimal fraction soil group B = 0.310
Decimal fraction soil group C = 0.060
Decimal fraction soil group D = 0.470
RI index for soil(AMC 2)  =  81.89
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.562(In/Hr) for a   100.0 year storm
Subarea runoff =     78.954(CFS) for     38.180(Ac.)
Total runoff =    116.277(CFS)        Total area =      54.030(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      304.000 to Point/Station      305.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1564.000(Ft.)
End of natural channel elevation =   1540.000(Ft.)
Length of natural channel  =  1301.000(Ft.)
Estimated mean flow rate at midpoint of channel =    151.712(CFS)
```

```
Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.32(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0184
Corrected/adjusted channel slope =  0.0184
Travel time =    2.96 min.     TC =   16.13  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.776
Decimal fraction soil group A = 0.420
Decimal fraction soil group B = 0.090
Decimal fraction soil group C = 0.150
Decimal fraction soil group D = 0.340
RI index for soil(AMC 2)  =  78.32
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.315(In/Hr) for a   100.0 year storm
Subarea runoff =     59.168(CFS) for     32.930(Ac.)
Total runoff =    175.445(CFS)        Total area =      86.960(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      305.000 to Point/Station      306.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
________________________________________________________________________
Top of natural channel elevation =   1540.000(Ft.)
End of natural channel elevation =   1526.000(Ft.)
Length of natural channel  =   856.000(Ft.)
Estimated mean flow rate at midpoint of channel =    243.174(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.97(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0164
Corrected/adjusted channel slope =  0.0164
Travel time =    1.79 min.     TC =   17.92  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.800
Decimal fraction soil group A = 0.210
Decimal fraction soil group B = 0.030
Decimal fraction soil group C = 0.400
Decimal fraction soil group D = 0.360
RI index for soil(AMC 2)  =  82.85
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.196(In/Hr) for a   100.0 year storm
Subarea runoff =    117.884(CFS) for     67.140(Ac.)
Total runoff =    293.329(CFS)        Total area =     154.100(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      306.000 to Point/Station      307.000
**** IMPROVED CHANNEL TRAVEL TIME ****
________________________________________________________________________
Upstream point elevation =  1526.000(Ft.)
Downstream point elevation =  1523.000(Ft.)
Channel length thru subarea  =  1008.000(Ft.)
Channel base width     =   50.000(Ft.)
Slope or 'Z' of left channel bank =   2.000
```

```
Slope or 'Z' of right channel bank =   4.000
Estimated mean flow rate at midpoint of channel =    314.687(CFS)
Manning's 'N'    = 0.030
Maximum depth of channel  =    4.000(Ft.)
Flow(q) thru subarea =    314.687(CFS)
Depth of flow =   1.631(Ft.), Average velocity =   3.514(Ft/s)
Channel flow top width =   59.787(Ft.)
Flow Velocity =    3.51(Ft/s)
Travel time  =    4.78 min.
Time of concentration =   22.70 min.

Sub-Channel No. 1 Critical depth =      1.047(Ft.)
  '     '       '     Critical flow top width =     56.281(Ft.)
  '     '       '     Critical flow velocity=    5.657(Ft/s)
  '     '       '     Critical flow area =     55.632(Sq.Ft)

 Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.763
Decimal fraction soil group A = 0.340
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.660
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  57.70
Pervious area fraction =  0.456; Impervious fraction =  0.544
Rainfall intensity =      1.951(In/Hr) for a   100.0 year storm
Subarea runoff =     42.623(CFS) for     28.630(Ac.)
Total runoff =    335.952(CFS)        Total area =     182.730(Ac.)
Depth of flow =   1.695(Ft.), Average velocity =   3.598(Ft/s)

Sub-Channel No. 1 Critical depth =      1.094(Ft.)
  '     '       '     Critical flow top width =     56.563(Ft.)
  '     '       '     Critical flow velocity=    5.765(Ft/s)
  '     '       '     Critical flow area =     58.276(Sq.Ft)

End of computations, total study area =          182.73 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.915
Area averaged RI index number =  78.3
```

10-YEAR

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 11/01/21 File:ARCEX10.out

150.10.18
10-YEAR RATIONAL TABLING METHOD FOR OFFSITE AREA C
EXISTING CONDITION
FN: ARA10.RRV

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 10.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.200(In.)

Storm event year = 10.0
Calculated rainfall intensity data:
1 hour intensity = 0.788(In/Hr)
Slope of intensity duration curve = 0.5000

++

Process from Point/Station 301.000 to Point/Station 302.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 999.000(Ft.)
Top (of initial area) elevation = 2028.000(Ft.)
Bottom (of initial area) elevation = 1656.000(Ft.)
Difference in elevation = 372.000(Ft.)
Slope = 0.37237 s(percent)= 37.24
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 10.231 min.
Rainfall intensity = 1.908(In/Hr) for a 10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.828
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
RI index for soil(AMC 2) = 89.00
Pervious area fraction = 1.000; Impervious fraction = 0.000
Initial subarea runoff = 9.802(CFS)
Total initial stream area = 6.200(Ac.)
Pervious area fraction = 1.000

++

Process from Point/Station 302.000 to Point/Station 303.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****

Top of natural channel elevation = 1656.000(Ft.)
End of natural channel elevation = 1588.000(Ft.)
Length of natural channel = 777.000(Ft.)

```
Estimated mean flow rate at midpoint of channel =     17.430(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.54(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0875
Corrected/adjusted channel slope =  0.0875
Travel time =    1.52 min.     TC =   11.75  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.802
Decimal fraction soil group A = 0.020
Decimal fraction soil group B = 0.210
Decimal fraction soil group C = 0.100
Decimal fraction soil group D = 0.670
RI index for soil(AMC 2)  =  85.95
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.781(In/Hr) for a    10.0 year storm
Subarea runoff =     13.781(CFS) for      9.650(Ac.)
Total runoff =     23.582(CFS)        Total area =      15.850(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      303.000 to Point/Station      304.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1588.000(Ft.)
End of natural channel elevation =   1564.000(Ft.)
Length of natural channel  =   759.000(Ft.)
Estimated mean flow rate at midpoint of channel =     51.985(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   6.96(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0316
Corrected/adjusted channel slope =  0.0316
Travel time =    1.82 min.     TC =   13.56  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.764
Decimal fraction soil group A = 0.160
Decimal fraction soil group B = 0.310
Decimal fraction soil group C = 0.060
Decimal fraction soil group D = 0.470
RI index for soil(AMC 2)  =  81.89
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.657(In/Hr) for a    10.0 year storm
Subarea runoff =     48.346(CFS) for     38.180(Ac.)
Total runoff =     71.929(CFS)        Total area =      54.030(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      304.000 to Point/Station      305.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1564.000(Ft.)
End of natural channel elevation =   1540.000(Ft.)
Length of natural channel  =  1301.000(Ft.)
Estimated mean flow rate at midpoint of channel =     93.848(CFS)
```

```
Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   6.33(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0184
Corrected/adjusted channel slope =  0.0184
Travel time =    3.43 min.     TC =   16.99  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.720
Decimal fraction soil group A = 0.420
Decimal fraction soil group B = 0.090
Decimal fraction soil group C = 0.150
Decimal fraction soil group D = 0.340
RI index for soil(AMC 2)  =  78.32
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.481(In/Hr) for a    10.0 year storm
Subarea runoff =     35.128(CFS) for     32.930(Ac.)
Total runoff =    107.057(CFS)        Total area =      86.960(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      305.000 to Point/Station      306.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
________________________________________________________________________
Top of natural channel elevation =   1540.000(Ft.)
End of natural channel elevation =   1526.000(Ft.)
Length of natural channel  =   856.000(Ft.)
Estimated mean flow rate at midpoint of channel =    148.385(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   6.84(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0164
Corrected/adjusted channel slope =  0.0164
Travel time =    2.09 min.     TC =   19.08  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.752
Decimal fraction soil group A = 0.210
Decimal fraction soil group B = 0.030
Decimal fraction soil group C = 0.400
Decimal fraction soil group D = 0.360
RI index for soil(AMC 2)  =  82.85
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.397(In/Hr) for a    10.0 year storm
Subarea runoff =     70.515(CFS) for     67.140(Ac.)
Total runoff =    177.572(CFS)        Total area =     154.100(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      306.000 to Point/Station      307.000
**** IMPROVED CHANNEL TRAVEL TIME ****
________________________________________________________________________
Upstream point elevation =  1526.000(Ft.)
Downstream point elevation =  1523.000(Ft.)
Channel length thru subarea  =  1008.000(Ft.)
Channel base width     =   50.000(Ft.)
Slope or 'Z' of left channel bank =   2.000
```

```
Slope or 'Z' of right channel bank =   4.000
Estimated mean flow rate at midpoint of channel =    190.193(CFS)
Manning's 'N'    = 0.030
Maximum depth of channel  =    4.000(Ft.)
Flow(q) thru subarea =    190.193(CFS)
Depth of flow =   1.212(Ft.), Average velocity =   2.926(Ft/s)
Channel flow top width =   57.272(Ft.)
Flow Velocity =    2.93(Ft/s)
Travel time  =    5.74 min.
Time of concentration =   24.82 min.

Sub-Channel No. 1 Critical depth =      0.750(Ft.)
  '     '       '     Critical flow top width =     54.500(Ft.)
  '     '       '     Critical flow velocity=    4.853(Ft/s)
  '     '       '     Critical flow area =     39.188(Sq.Ft)

 Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.718
Decimal fraction soil group A = 0.340
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.660
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  57.70
Pervious area fraction =  0.456; Impervious fraction =  0.544
Rainfall intensity =      1.225(In/Hr) for a    10.0 year storm
Subarea runoff =     25.181(CFS) for     28.630(Ac.)
Total runoff =    202.752(CFS)        Total area =     182.730(Ac.)
Depth of flow =   1.259(Ft.), Average velocity =   2.995(Ft/s)

Sub-Channel No. 1 Critical depth =      0.789(Ft.)
  '     '       '     Critical flow top width =     54.734(Ft.)
  '     '       '     Critical flow velocity=    4.907(Ft/s)
  '     '       '     Critical flow area =     41.321(Sq.Ft)

End of computations, total study area =          182.73 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.915
Area averaged RI index number =  78.3
```

APPENDIX B.5: OFFSITE AREA "C" – ULTIMATE CONDITION OFFSITE AREA

100-YEAR

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 11/01/21 File:ARCULT100.out

150.10.18
100-YEAR RATIONAL TABLING METHOD FOR OFFSITE AREA C
ULTIMATE CONDITION
FN: ARA100.RRV

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.200(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.200(In/Hr)
Slope of intensity duration curve = 0.5000

++
Process from Point/Station 301.000 to Point/Station 302.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 999.000(Ft.)
Top (of initial area) elevation = 2028.000(Ft.)
Bottom (of initial area) elevation = 1656.000(Ft.)
Difference in elevation = 372.000(Ft.)
Slope = 0.37237 s(percent)= 37.24
TC = k(-0.892)*[(length^3)/(elevation change)]^0.2
Warning: TC computed to be less than 5 min.; program is assuming the
time of concentration is 5 minutes.
Initial area time of concentration = 5.000 min.
Rainfall intensity = 4.157(In/Hr) for a 100.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.848
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
RI index for soil(AMC 2) = 82.16
Pervious area fraction = 0.890; Impervious fraction = 0.110
Initial subarea runoff = 21.851(CFS)
Total initial stream area = 6.200(Ac.)
Pervious area fraction = 0.890

++
Process from Point/Station 302.000 to Point/Station 303.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****

Top of natural channel elevation = 1656.000(Ft.)

```
End of natural channel elevation =   1588.000(Ft.)
Length of natural channel  =   777.000(Ft.)
Estimated mean flow rate at midpoint of channel =     38.857(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  10.65(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0875
Corrected/adjusted channel slope =  0.0875
Travel time =    1.22 min.     TC =    6.22  min.


 Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.848
Decimal fraction soil group A = 0.020
Decimal fraction soil group B = 0.210
Decimal fraction soil group C = 0.100
Decimal fraction soil group D = 0.670
RI index for soil(AMC 2)  =  70.16
Pervious area fraction =  0.440; Impervious fraction =  0.560
Rainfall intensity =      3.728(In/Hr) for a   100.0 year storm
Subarea runoff =     30.500(CFS) for      9.650(Ac.)
Total runoff =     52.351(CFS)       Total area =      15.850(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      303.000 to Point/Station      304.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1588.000(Ft.)
End of natural channel elevation =   1564.000(Ft.)
Length of natural channel  =   759.000(Ft.)
Estimated mean flow rate at midpoint of channel =    115.404(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.81(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0316
Corrected/adjusted channel slope =  0.0316
Travel time =    1.44 min.     TC =    7.65  min.


 Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.819
Decimal fraction soil group A = 0.160
Decimal fraction soil group B = 0.310
Decimal fraction soil group C = 0.060
Decimal fraction soil group D = 0.470
RI index for soil(AMC 2)  =  65.09
Pervious area fraction =  0.510; Impervious fraction =  0.490
Rainfall intensity =      3.360(In/Hr) for a   100.0 year storm
Subarea runoff =    105.139(CFS) for     38.180(Ac.)
Total runoff =    157.490(CFS)       Total area =      54.030(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      304.000 to Point/Station      305.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1564.000(Ft.)
End of natural channel elevation =   1540.000(Ft.)
```

```
Length of natural channel  =  1301.000(Ft.)
Estimated mean flow rate at midpoint of channel =    205.483(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.03(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0184
Corrected/adjusted channel slope =  0.0184
Travel time =    2.70 min.     TC =   10.35  min.


 Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.810
Decimal fraction soil group A = 0.420
Decimal fraction soil group B = 0.090
Decimal fraction soil group C = 0.150
Decimal fraction soil group D = 0.340
RI index for soil(AMC 2)  =  56.54
Pervious area fraction =  0.380; Impervious fraction =  0.620
Rainfall intensity =      2.889(In/Hr) for a   100.0 year storm
Subarea runoff =     77.108(CFS) for     32.930(Ac.)
Total runoff =    234.598(CFS)        Total area =      86.960(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      305.000 to Point/Station      306.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
________________________________________________________________________
Top of natural channel elevation =   1540.000(Ft.)
End of natural channel elevation =   1526.000(Ft.)
Length of natural channel  =   856.000(Ft.)
Estimated mean flow rate at midpoint of channel =    325.161(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.73(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0164
Corrected/adjusted channel slope =  0.0164
Travel time =    1.63 min.     TC =   11.98  min.


 Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.813
Decimal fraction soil group A = 0.210
Decimal fraction soil group B = 0.030
Decimal fraction soil group C = 0.400
Decimal fraction soil group D = 0.360
RI index for soil(AMC 2)  =  65.04
Pervious area fraction =  0.460; Impervious fraction =  0.540
Rainfall intensity =      2.685(In/Hr) for a   100.0 year storm
Subarea runoff =    146.524(CFS) for     67.140(Ac.)
Total runoff =    381.121(CFS)        Total area =     154.100(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      306.000 to Point/Station      307.000
**** IMPROVED CHANNEL TRAVEL TIME ****
________________________________________________________________________
Upstream point elevation =  1526.000(Ft.)
Downstream point elevation =  1523.000(Ft.)
Channel length thru subarea  =  1008.000(Ft.)
```

```
Channel base width     =   50.000(Ft.)
Slope or 'Z' of left channel bank =   2.000
Slope or 'Z' of right channel bank =   4.000
Estimated mean flow rate at midpoint of channel =    406.751(CFS)
Manning's 'N'    = 0.030
Maximum depth of channel  =    4.000(Ft.)
Flow(q) thru subarea =    406.751(CFS)
Depth of flow =   1.896(Ft.), Average velocity =   3.852(Ft/s)
Channel flow top width =   61.378(Ft.)
Flow Velocity =    3.85(Ft/s)
Travel time  =    4.36 min.
Time of concentration =   16.35 min.

Sub-Channel No. 1 Critical depth =      1.234(Ft.)
  '     '       '     Critical flow top width =     57.406(Ft.)
  '     '       '     Critical flow velocity=    6.136(Ft/s)
  '     '       '     Critical flow area =     66.290(Sq.Ft)

 Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.778
Decimal fraction soil group A = 0.340
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.660
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  57.70
Pervious area fraction =  0.456; Impervious fraction =  0.544
Rainfall intensity =      2.299(In/Hr) for a   100.0 year storm
Subarea runoff =     51.181(CFS) for     28.630(Ac.)
Total runoff =    432.303(CFS)        Total area =     182.730(Ac.)
Depth of flow =   1.965(Ft.), Average velocity =   3.936(Ft/s)

Sub-Channel No. 1 Critical depth =      1.281(Ft.)
  '     '       '     Critical flow top width =     57.688(Ft.)
  '     '       '     Critical flow velocity=    6.266(Ft/s)
  '     '       '     Critical flow area =     68.987(Sq.Ft)

End of computations, total study area =          182.73 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.469
Area averaged RI index number =  63.2
```

10-YEAR

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 11/01/21 File:ARCULT10.out

150.10.18
10-YEAR RATIONAL TABLING METHOD FOR OFFSITE AREA C
ULTIMATE CONDITION
FN: ARA10.RRV

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 10.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.500(In.)
100 year, 1 hour precipitation = 1.200(In.)

Storm event year = 10.0
Calculated rainfall intensity data:
1 hour intensity = 0.788(In/Hr)
Slope of intensity duration curve = 0.5000

++

Process from Point/Station 301.000 to Point/Station 302.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 999.000(Ft.)
Top (of initial area) elevation = 2028.000(Ft.)
Bottom (of initial area) elevation = 1656.000(Ft.)
Difference in elevation = 372.000(Ft.)
Slope = 0.37237 s(percent)= 37.24
TC = k(-0.892)*[(length^3)/(elevation change)]^0.2
Warning: TC computed to be less than 5 min.; program is assuming the
time of concentration is 5 minutes.
Initial area time of concentration = 5.000 min.
Rainfall intensity = 2.730(In/Hr) for a 10.0 year storm
USER INPUT of soil data for subarea
Runoff Coefficient = 0.823
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 1.000
RI index for soil(AMC 2) = 82.16
Pervious area fraction = 0.890; Impervious fraction = 0.110
Initial subarea runoff = 13.932(CFS)
Total initial stream area = 6.200(Ac.)
Pervious area fraction = 0.890

++

Process from Point/Station 302.000 to Point/Station 303.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****

Top of natural channel elevation = 1656.000(Ft.)

```
End of natural channel elevation =   1588.000(Ft.)
Length of natural channel  =   777.000(Ft.)
Estimated mean flow rate at midpoint of channel =     24.774(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.40(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0875
Corrected/adjusted channel slope =  0.0875
Travel time =    1.38 min.     TC =    6.38  min.


 Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.825
Decimal fraction soil group A = 0.020
Decimal fraction soil group B = 0.210
Decimal fraction soil group C = 0.100
Decimal fraction soil group D = 0.670
RI index for soil(AMC 2)  =  70.16
Pervious area fraction =  0.440; Impervious fraction =  0.560
Rainfall intensity =      2.417(In/Hr) for a    10.0 year storm
Subarea runoff =     19.235(CFS) for      9.650(Ac.)
Total runoff =     33.166(CFS)        Total area =      15.850(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      303.000 to Point/Station      304.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
________________________________________________________________________
Top of natural channel elevation =   1588.000(Ft.)
End of natural channel elevation =   1564.000(Ft.)
Length of natural channel  =   759.000(Ft.)
Estimated mean flow rate at midpoint of channel =     73.113(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.69(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0316
Corrected/adjusted channel slope =  0.0316
Travel time =    1.65 min.     TC =    8.02  min.


 Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.786
Decimal fraction soil group A = 0.160
Decimal fraction soil group B = 0.310
Decimal fraction soil group C = 0.060
Decimal fraction soil group D = 0.470
RI index for soil(AMC 2)  =  65.09
Pervious area fraction =  0.510; Impervious fraction =  0.490
Rainfall intensity =      2.155(In/Hr) for a    10.0 year storm
Subarea runoff =     64.635(CFS) for     38.180(Ac.)
Total runoff =     97.802(CFS)        Total area =      54.030(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      304.000 to Point/Station      305.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
________________________________________________________________________
Top of natural channel elevation =   1564.000(Ft.)
End of natural channel elevation =   1540.000(Ft.)
```

```
Length of natural channel  =  1301.000(Ft.)
Estimated mean flow rate at midpoint of channel =    127.606(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   6.94(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0184
Corrected/adjusted channel slope =  0.0184
Travel time =    3.12 min.     TC =   11.15  min.


 Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.777
Decimal fraction soil group A = 0.420
Decimal fraction soil group B = 0.090
Decimal fraction soil group C = 0.150
Decimal fraction soil group D = 0.340
RI index for soil(AMC 2)  =  56.54
Pervious area fraction =  0.380; Impervious fraction =  0.620
Rainfall intensity =      1.828(In/Hr) for a    10.0 year storm
Subarea runoff =     46.783(CFS) for     32.930(Ac.)
Total runoff =    144.584(CFS)        Total area =      86.960(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      305.000 to Point/Station      306.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
________________________________________________________________________
Top of natural channel elevation =   1540.000(Ft.)
End of natural channel elevation =   1526.000(Ft.)
Length of natural channel  =   856.000(Ft.)
Estimated mean flow rate at midpoint of channel =    200.400(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.50(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0164
Corrected/adjusted channel slope =  0.0164
Travel time =    1.90 min.     TC =   13.05  min.


 Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.777
Decimal fraction soil group A = 0.210
Decimal fraction soil group B = 0.030
Decimal fraction soil group C = 0.400
Decimal fraction soil group D = 0.360
RI index for soil(AMC 2)  =  65.04
Pervious area fraction =  0.460; Impervious fraction =  0.540
Rainfall intensity =      1.690(In/Hr) for a    10.0 year storm
Subarea runoff =     88.113(CFS) for     67.140(Ac.)
Total runoff =    232.697(CFS)        Total area =     154.100(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      306.000 to Point/Station      307.000
**** IMPROVED CHANNEL TRAVEL TIME ****
________________________________________________________________________
Upstream point elevation =  1526.000(Ft.)
Downstream point elevation =  1523.000(Ft.)
Channel length thru subarea  =  1008.000(Ft.)
```

```
Channel base width     =   50.000(Ft.)
Slope or 'Z' of left channel bank =   2.000
Slope or 'Z' of right channel bank =   4.000
Estimated mean flow rate at midpoint of channel =    247.716(CFS)
Manning's 'N'    = 0.030
Maximum depth of channel  =    4.000(Ft.)
Flow(q) thru subarea =    247.716(CFS)
Depth of flow =   1.417(Ft.), Average velocity =   3.223(Ft/s)
Channel flow top width =   58.501(Ft.)
Flow Velocity =    3.22(Ft/s)
Travel time  =    5.21 min.
Time of concentration =   18.26 min.

Sub-Channel No. 1 Critical depth =      0.898(Ft.)
  '     '       '     Critical flow top width =     55.391(Ft.)
  '     '       '     Critical flow velocity=    5.232(Ft/s)
  '     '       '     Critical flow area =     47.343(Sq.Ft)

 Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.733
Decimal fraction soil group A = 0.340
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.660
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  57.70
Pervious area fraction =  0.456; Impervious fraction =  0.544
Rainfall intensity =      1.428(In/Hr) for a    10.0 year storm
Subarea runoff =     29.985(CFS) for     28.630(Ac.)
Total runoff =    262.682(CFS)        Total area =     182.730(Ac.)
Depth of flow =   1.467(Ft.), Average velocity =   3.292(Ft/s)

Sub-Channel No. 1 Critical depth =      0.938(Ft.)
  '     '       '     Critical flow top width =     55.625(Ft.)
  '     '       '     Critical flow velocity=    5.305(Ft/s)
  '     '       '     Critical flow area =     49.512(Sq.Ft)

End of computations, total study area =          182.73 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.469
Area averaged RI index number =  63.2
```

APPENDIX C: PRE-PROJECT CONDITION UNIT HYDROGRAPH HYDROLOGY

APPENDIX C.1: AREA "A" – ONSITE

2-YEAR, 24-HOUR

U n i t H y d r o g r a p h A n a l y s i s

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Study date 10/23/21 File: ARA1PRE242.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

TRI-8 Builders - S/N 615

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

150.10.18
UNIT HYDROGRAPH FOR BASIN NODE 118.1
PRE-PROJECT CONDITION
FN: ARA1PRE.UNRIV

Drainage Area = 22.97(Ac.) = 0.036 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 22.97(Ac.) = 0.036 Sq. Mi.
Length along longest watercourse = 1744.00(Ft.)
Length along longest watercourse measured to centroid = 446.00(Ft.)
Length along longest watercourse = 0.330 Mi.
Length along longest watercourse measured to centroid = 0.084 Mi.
Difference in elevation = 40.50(Ft.)
Slope along watercourse = 122.6147 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.074 Hr.
Lag time = 4.45 Min.
25% of lag time = 1.11 Min.
40% of lag time = 1.78 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
22.97	1.70	39.05

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
22.97	4.25	97.62

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.700(In)
Area Averaged 100-Year Rainfall = 4.250(In)

Point rain (area averaged) = 1.700(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.700(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
22.970	71.40	0.000

Total Area Entered = 22.97(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
71.4	52.7	0.545	0.000	0.545	1.000	0.545
					Sum (F) =	0.545

Area averaged mean soil loss (F) (In/Hr) = 0.545
Minimum soil loss rate ((In/Hr)) = 0.272
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	112.454	22.974	5.318
2	0.167	224.909	48.849	11.308
3	0.250	337.363	14.032	3.248
4	0.333	449.817	6.419	1.486
5	0.417	562.272	3.567	0.826
6	0.500	674.726	2.182	0.505
7	0.583	787.180	1.287	0.298
8	0.667	899.635	0.690	0.160
			Sum = 100.000	Sum= 23.149

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.014	0.966	0.012	0.00
2	0.17	0.07	0.014	0.962	0.012	0.00
3	0.25	0.07	0.014	0.958	0.012	0.00
4	0.33	0.10	0.020	0.954	0.018	0.00
5	0.42	0.10	0.020	0.951	0.018	0.00
6	0.50	0.10	0.020	0.947	0.018	0.00
7	0.58	0.10	0.020	0.943	0.018	0.00
8	0.67	0.10	0.020	0.940	0.018	0.00
9	0.75	0.10	0.020	0.936	0.018	0.00
10	0.83	0.13	0.027	0.932	0.024	0.00
11	0.92	0.13	0.027	0.929	0.024	0.00
12	1.00	0.13	0.027	0.925	0.024	0.00
13	1.08	0.10	0.020	0.921	0.018	0.00
14	1.17	0.10	0.020	0.918	0.018	0.00
15	1.25	0.10	0.020	0.914	0.018	0.00
16	1.33	0.10	0.020	0.910	0.018	0.00
17	1.42	0.10	0.020	0.907	0.018	0.00
18	1.50	0.10	0.020	0.903	0.018	0.00
19	1.58	0.10	0.020	0.899	0.018	0.00
20	1.67	0.10	0.020	0.896	0.018	0.00
21	1.75	0.10	0.020	0.892	0.018	0.00
22	1.83	0.13	0.027	0.889	0.024	0.00
23	1.92	0.13	0.027	0.885	0.024	0.00
24	2.00	0.13	0.027	0.881	0.024	0.00
25	2.08	0.13	0.027	0.878	0.024	0.00
26	2.17	0.13	0.027	0.874	0.024	0.00
27	2.25	0.13	0.027	0.871	0.024	0.00
28	2.33	0.13	0.027	0.867	0.024	0.00
29	2.42	0.13	0.027	0.864	0.024	0.00
30	2.50	0.13	0.027	0.860	0.024	0.00
31	2.58	0.17	0.034	0.857	0.031	0.00
32	2.67	0.17	0.034	0.853	0.031	0.00
33	2.75	0.17	0.034	0.850	0.031	0.00
34	2.83	0.17	0.034	0.846	0.031	0.00
35	2.92	0.17	0.034	0.843	0.031	0.00
36	3.00	0.17	0.034	0.839	0.031	0.00
37	3.08	0.17	0.034	0.836	0.031	0.00
38	3.17	0.17	0.034	0.832	0.031	0.00

39	3.25	0.17	0.034	0.829	0.031	0.00
40	3.33	0.17	0.034	0.825	0.031	0.00
41	3.42	0.17	0.034	0.822	0.031	0.00
42	3.50	0.17	0.034	0.818	0.031	0.00
43	3.58	0.17	0.034	0.815	0.031	0.00
44	3.67	0.17	0.034	0.812	0.031	0.00
45	3.75	0.17	0.034	0.808	0.031	0.00
46	3.83	0.20	0.041	0.805	0.037	0.00
47	3.92	0.20	0.041	0.801	0.037	0.00
48	4.00	0.20	0.041	0.798	0.037	0.00
49	4.08	0.20	0.041	0.795	0.037	0.00
50	4.17	0.20	0.041	0.791	0.037	0.00
51	4.25	0.20	0.041	0.788	0.037	0.00
52	4.33	0.23	0.048	0.784	0.043	0.00
53	4.42	0.23	0.048	0.781	0.043	0.00
54	4.50	0.23	0.048	0.778	0.043	0.00
55	4.58	0.23	0.048	0.774	0.043	0.00
56	4.67	0.23	0.048	0.771	0.043	0.00
57	4.75	0.23	0.048	0.768	0.043	0.00
58	4.83	0.27	0.054	0.765	0.049	0.01
59	4.92	0.27	0.054	0.761	0.049	0.01
60	5.00	0.27	0.054	0.758	0.049	0.01
61	5.08	0.20	0.041	0.755	0.037	0.00
62	5.17	0.20	0.041	0.751	0.037	0.00
63	5.25	0.20	0.041	0.748	0.037	0.00
64	5.33	0.23	0.048	0.745	0.043	0.00
65	5.42	0.23	0.048	0.742	0.043	0.00
66	5.50	0.23	0.048	0.738	0.043	0.00
67	5.58	0.27	0.054	0.735	0.049	0.01
68	5.67	0.27	0.054	0.732	0.049	0.01
69	5.75	0.27	0.054	0.729	0.049	0.01
70	5.83	0.27	0.054	0.725	0.049	0.01
71	5.92	0.27	0.054	0.722	0.049	0.01
72	6.00	0.27	0.054	0.719	0.049	0.01
73	6.08	0.30	0.061	0.716	0.055	0.01
74	6.17	0.30	0.061	0.713	0.055	0.01
75	6.25	0.30	0.061	0.709	0.055	0.01
76	6.33	0.30	0.061	0.706	0.055	0.01
77	6.42	0.30	0.061	0.703	0.055	0.01
78	6.50	0.30	0.061	0.700	0.055	0.01
79	6.58	0.33	0.068	0.697	0.061	0.01
80	6.67	0.33	0.068	0.694	0.061	0.01
81	6.75	0.33	0.068	0.691	0.061	0.01
82	6.83	0.33	0.068	0.687	0.061	0.01
83	6.92	0.33	0.068	0.684	0.061	0.01
84	7.00	0.33	0.068	0.681	0.061	0.01
85	7.08	0.33	0.068	0.678	0.061	0.01
86	7.17	0.33	0.068	0.675	0.061	0.01
87	7.25	0.33	0.068	0.672	0.061	0.01
88	7.33	0.37	0.075	0.669	0.067	0.01
89	7.42	0.37	0.075	0.666	0.067	0.01
90	7.50	0.37	0.075	0.663	0.067	0.01
91	7.58	0.40	0.082	0.660	0.073	0.01
92	7.67	0.40	0.082	0.657	0.073	0.01
93	7.75	0.40	0.082	0.654	0.073	0.01
94	7.83	0.43	0.088	0.651	0.080	0.01
95	7.92	0.43	0.088	0.648	0.080	0.01
96	8.00	0.43	0.088	0.645	0.080	0.01
97	8.08	0.50	0.102	0.642	0.092	0.01
98	8.17	0.50	0.102	0.639	0.092	0.01
99	8.25	0.50	0.102	0.636	0.092	0.01
100	8.33	0.50	0.102	0.633	0.092	0.01
101	8.42	0.50	0.102	0.630	0.092	0.01
102	8.50	0.50	0.102	0.627	0.092	0.01
103	8.58	0.53	0.109	0.624	0.098	0.01
104	8.67	0.53	0.109	0.621	0.098	0.01
105	8.75	0.53	0.109	0.618	0.098	0.01
106	8.83	0.57	0.116	0.615	0.104	0.01
107	8.92	0.57	0.116	0.612	0.104	0.01
108	9.00	0.57	0.116	0.609	0.104	0.01
109	9.08	0.63	0.129	0.606	0.116	0.01

110	9.17	0.63	0.129	0.603	0.116	0.01
111	9.25	0.63	0.129	0.601	0.116	0.01
112	9.33	0.67	0.136	0.598	0.122	0.01
113	9.42	0.67	0.136	0.595	0.122	0.01
114	9.50	0.67	0.136	0.592	0.122	0.01
115	9.58	0.70	0.143	0.589	0.129	0.01
116	9.67	0.70	0.143	0.586	0.129	0.01
117	9.75	0.70	0.143	0.584	0.129	0.01
118	9.83	0.73	0.150	0.581	0.135	0.01
119	9.92	0.73	0.150	0.578	0.135	0.01
120	10.00	0.73	0.150	0.575	0.135	0.01
121	10.08	0.50	0.102	0.572	0.092	0.01
122	10.17	0.50	0.102	0.570	0.092	0.01
123	10.25	0.50	0.102	0.567	0.092	0.01
124	10.33	0.50	0.102	0.564	0.092	0.01
125	10.42	0.50	0.102	0.561	0.092	0.01
126	10.50	0.50	0.102	0.559	0.092	0.01
127	10.58	0.67	0.136	0.556	0.122	0.01
128	10.67	0.67	0.136	0.553	0.122	0.01
129	10.75	0.67	0.136	0.550	0.122	0.01
130	10.83	0.67	0.136	0.548	0.122	0.01
131	10.92	0.67	0.136	0.545	0.122	0.01
132	11.00	0.67	0.136	0.542	0.122	0.01
133	11.08	0.63	0.129	0.540	0.116	0.01
134	11.17	0.63	0.129	0.537	0.116	0.01
135	11.25	0.63	0.129	0.534	0.116	0.01
136	11.33	0.63	0.129	0.532	0.116	0.01
137	11.42	0.63	0.129	0.529	0.116	0.01
138	11.50	0.63	0.129	0.527	0.116	0.01
139	11.58	0.57	0.116	0.524	0.104	0.01
140	11.67	0.57	0.116	0.521	0.104	0.01
141	11.75	0.57	0.116	0.519	0.104	0.01
142	11.83	0.60	0.122	0.516	0.110	0.01
143	11.92	0.60	0.122	0.514	0.110	0.01
144	12.00	0.60	0.122	0.511	0.110	0.01
145	12.08	0.83	0.170	0.508	0.153	0.02
146	12.17	0.83	0.170	0.506	0.153	0.02
147	12.25	0.83	0.170	0.503	0.153	0.02
148	12.33	0.87	0.177	0.501	0.159	0.02
149	12.42	0.87	0.177	0.498	0.159	0.02
150	12.50	0.87	0.177	0.496	0.159	0.02
151	12.58	0.93	0.190	0.493	0.171	0.02
152	12.67	0.93	0.190	0.491	0.171	0.02
153	12.75	0.93	0.190	0.488	0.171	0.02
154	12.83	0.97	0.197	0.486	0.177	0.02
155	12.92	0.97	0.197	0.483	0.177	0.02
156	13.00	0.97	0.197	0.481	0.177	0.02
157	13.08	1.13	0.231	0.479	0.208	0.02
158	13.17	1.13	0.231	0.476	0.208	0.02
159	13.25	1.13	0.231	0.474	0.208	0.02
160	13.33	1.13	0.231	0.471	0.208	0.02
161	13.42	1.13	0.231	0.469	0.208	0.02
162	13.50	1.13	0.231	0.467	0.208	0.02
163	13.58	0.77	0.156	0.464	0.141	0.02
164	13.67	0.77	0.156	0.462	0.141	0.02
165	13.75	0.77	0.156	0.459	0.141	0.02
166	13.83	0.77	0.156	0.457	0.141	0.02
167	13.92	0.77	0.156	0.455	0.141	0.02
168	14.00	0.77	0.156	0.452	0.141	0.02
169	14.08	0.90	0.184	0.450	0.165	0.02
170	14.17	0.90	0.184	0.448	0.165	0.02
171	14.25	0.90	0.184	0.446	0.165	0.02
172	14.33	0.87	0.177	0.443	0.159	0.02
173	14.42	0.87	0.177	0.441	0.159	0.02
174	14.50	0.87	0.177	0.439	0.159	0.02
175	14.58	0.87	0.177	0.436	0.159	0.02
176	14.67	0.87	0.177	0.434	0.159	0.02
177	14.75	0.87	0.177	0.432	0.159	0.02
178	14.83	0.83	0.170	0.430	0.153	0.02
179	14.92	0.83	0.170	0.428	0.153	0.02
180	15.00	0.83	0.170	0.425	0.153	0.02

181	15.08	0.80	0.163	0.423	0.147	0.02
182	15.17	0.80	0.163	0.421	0.147	0.02
183	15.25	0.80	0.163	0.419	0.147	0.02
184	15.33	0.77	0.156	0.417	0.141	0.02
185	15.42	0.77	0.156	0.415	0.141	0.02
186	15.50	0.77	0.156	0.412	0.141	0.02
187	15.58	0.63	0.129	0.410	0.116	0.01
188	15.67	0.63	0.129	0.408	0.116	0.01
189	15.75	0.63	0.129	0.406	0.116	0.01
190	15.83	0.63	0.129	0.404	0.116	0.01
191	15.92	0.63	0.129	0.402	0.116	0.01
192	16.00	0.63	0.129	0.400	0.116	0.01
193	16.08	0.13	0.027	0.398	0.024	0.00
194	16.17	0.13	0.027	0.396	0.024	0.00
195	16.25	0.13	0.027	0.394	0.024	0.00
196	16.33	0.13	0.027	0.392	0.024	0.00
197	16.42	0.13	0.027	0.390	0.024	0.00
198	16.50	0.13	0.027	0.388	0.024	0.00
199	16.58	0.10	0.020	0.386	0.018	0.00
200	16.67	0.10	0.020	0.384	0.018	0.00
201	16.75	0.10	0.020	0.382	0.018	0.00
202	16.83	0.10	0.020	0.380	0.018	0.00
203	16.92	0.10	0.020	0.378	0.018	0.00
204	17.00	0.10	0.020	0.376	0.018	0.00
205	17.08	0.17	0.034	0.374	0.031	0.00
206	17.17	0.17	0.034	0.372	0.031	0.00
207	17.25	0.17	0.034	0.371	0.031	0.00
208	17.33	0.17	0.034	0.369	0.031	0.00
209	17.42	0.17	0.034	0.367	0.031	0.00
210	17.50	0.17	0.034	0.365	0.031	0.00
211	17.58	0.17	0.034	0.363	0.031	0.00
212	17.67	0.17	0.034	0.361	0.031	0.00
213	17.75	0.17	0.034	0.360	0.031	0.00
214	17.83	0.13	0.027	0.358	0.024	0.00
215	17.92	0.13	0.027	0.356	0.024	0.00
216	18.00	0.13	0.027	0.354	0.024	0.00
217	18.08	0.13	0.027	0.353	0.024	0.00
218	18.17	0.13	0.027	0.351	0.024	0.00
219	18.25	0.13	0.027	0.349	0.024	0.00
220	18.33	0.13	0.027	0.347	0.024	0.00
221	18.42	0.13	0.027	0.346	0.024	0.00
222	18.50	0.13	0.027	0.344	0.024	0.00
223	18.58	0.10	0.020	0.342	0.018	0.00
224	18.67	0.10	0.020	0.341	0.018	0.00
225	18.75	0.10	0.020	0.339	0.018	0.00
226	18.83	0.07	0.014	0.337	0.012	0.00
227	18.92	0.07	0.014	0.336	0.012	0.00
228	19.00	0.07	0.014	0.334	0.012	0.00
229	19.08	0.10	0.020	0.333	0.018	0.00
230	19.17	0.10	0.020	0.331	0.018	0.00
231	19.25	0.10	0.020	0.330	0.018	0.00
232	19.33	0.13	0.027	0.328	0.024	0.00
233	19.42	0.13	0.027	0.326	0.024	0.00
234	19.50	0.13	0.027	0.325	0.024	0.00
235	19.58	0.10	0.020	0.323	0.018	0.00
236	19.67	0.10	0.020	0.322	0.018	0.00
237	19.75	0.10	0.020	0.321	0.018	0.00
238	19.83	0.07	0.014	0.319	0.012	0.00
239	19.92	0.07	0.014	0.318	0.012	0.00
240	20.00	0.07	0.014	0.316	0.012	0.00
241	20.08	0.10	0.020	0.315	0.018	0.00
242	20.17	0.10	0.020	0.313	0.018	0.00
243	20.25	0.10	0.020	0.312	0.018	0.00
244	20.33	0.10	0.020	0.311	0.018	0.00
245	20.42	0.10	0.020	0.309	0.018	0.00
246	20.50	0.10	0.020	0.308	0.018	0.00
247	20.58	0.10	0.020	0.307	0.018	0.00
248	20.67	0.10	0.020	0.306	0.018	0.00
249	20.75	0.10	0.020	0.304	0.018	0.00
250	20.83	0.07	0.014	0.303	0.012	0.00
251	20.92	0.07	0.014	0.302	0.012	0.00

252	21.00	0.07	0.014	0.301	0.012	0.00
253	21.08	0.10	0.020	0.299	0.018	0.00
254	21.17	0.10	0.020	0.298	0.018	0.00
255	21.25	0.10	0.020	0.297	0.018	0.00
256	21.33	0.07	0.014	0.296	0.012	0.00
257	21.42	0.07	0.014	0.295	0.012	0.00
258	21.50	0.07	0.014	0.294	0.012	0.00
259	21.58	0.10	0.020	0.293	0.018	0.00
260	21.67	0.10	0.020	0.292	0.018	0.00
261	21.75	0.10	0.020	0.291	0.018	0.00
262	21.83	0.07	0.014	0.290	0.012	0.00
263	21.92	0.07	0.014	0.289	0.012	0.00
264	22.00	0.07	0.014	0.288	0.012	0.00
265	22.08	0.10	0.020	0.287	0.018	0.00
266	22.17	0.10	0.020	0.286	0.018	0.00
267	22.25	0.10	0.020	0.285	0.018	0.00
268	22.33	0.07	0.014	0.284	0.012	0.00
269	22.42	0.07	0.014	0.283	0.012	0.00
270	22.50	0.07	0.014	0.282	0.012	0.00
271	22.58	0.07	0.014	0.281	0.012	0.00
272	22.67	0.07	0.014	0.281	0.012	0.00
273	22.75	0.07	0.014	0.280	0.012	0.00
274	22.83	0.07	0.014	0.279	0.012	0.00
275	22.92	0.07	0.014	0.278	0.012	0.00
276	23.00	0.07	0.014	0.278	0.012	0.00
277	23.08	0.07	0.014	0.277	0.012	0.00
278	23.17	0.07	0.014	0.276	0.012	0.00
279	23.25	0.07	0.014	0.276	0.012	0.00
280	23.33	0.07	0.014	0.275	0.012	0.00
281	23.42	0.07	0.014	0.275	0.012	0.00
282	23.50	0.07	0.014	0.274	0.012	0.00
283	23.58	0.07	0.014	0.274	0.012	0.00
284	23.67	0.07	0.014	0.273	0.012	0.00
285	23.75	0.07	0.014	0.273	0.012	0.00
286	23.83	0.07	0.014	0.273	0.012	0.00
287	23.92	0.07	0.014	0.273	0.012	0.00
288	24.00	0.07	0.014	0.272	0.012	0.00
Sum =		100.0			Sum =	2.0

Flood volume = Effective rainfall 0.17(In)
times area 23.0(Ac.)/[(In)/(Ft.)] = 0.3(Ac.Ft)
Total soil loss = 1.53(In)
Total soil loss = 2.929(Ac.Ft)
Total rainfall = 1.70(In)
Flood volume = 14174.2 Cubic Feet
Total soil loss = 127567.4 Cubic Feet

Peak flow rate of this hydrograph = 0.534(CFS)

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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0000	0.01	Q	|	|	|	|
0+10	0.0002	0.02	Q	|	|	|	|
0+15	0.0004	0.03	Q	|	|	|	|
0+20	0.0006	0.03	Q	|	|	|	|
0+25	0.0009	0.04	Q	|	|	|	|
0+30	0.0012	0.04	Q	|	|	|	|
0+35	0.0015	0.05	Q	|	|	|	|
0+40	0.0018	0.05	Q	|	|	|	|
0+45	0.0022	0.05	Q	|	|	|	|
0+50	0.0025	0.05	Q	|	|	|	|
0+55	0.0029	0.06	Q	|	|	|	|
1+ 0	0.0033	0.06	Q	|	|	|	|
1+ 5	0.0037	0.06	Q	|	|	|	|
1+10	0.0041	0.05	Q	|	|	|	|

1+15	0.0044	0.05	Q	|	|	|	|
1+20	0.0048	0.05	Q	|	|	|	|
1+25	0.0051	0.05	Q	|	|	|	|
1+30	0.0054	0.05	Q	|	|	|	|
1+35	0.0057	0.05	Q	|	|	|	|
1+40	0.0061	0.05	Q	|	|	|	|
1+45	0.0064	0.05	Q	|	|	|	|
1+50	0.0067	0.05	Q	|	|	|	|
1+55	0.0072	0.06	Q	|	|	|	|
2+ 0	0.0076	0.06	Q	|	|	|	|
2+ 5	0.0080	0.06	Q	|	|	|	|
2+10	0.0084	0.06	QV	|	|	|	|
2+15	0.0089	0.06	QV	|	|	|	|
2+20	0.0093	0.06	QV	|	|	|	|
2+25	0.0097	0.06	QV	|	|	|	|
2+30	0.0102	0.06	QV	|	|	|	|
2+35	0.0106	0.07	QV	|	|	|	|
2+40	0.0111	0.07	QV	|	|	|	|
2+45	0.0117	0.08	QV	|	|	|	|
2+50	0.0122	0.08	QV	|	|	|	|
2+55	0.0127	0.08	QV	|	|	|	|
3+ 0	0.0133	0.08	QV	|	|	|	|
3+ 5	0.0138	0.08	QV	|	|	|	|
3+10	0.0144	0.08	QV	|	|	|	|
3+15	0.0149	0.08	QV	|	|	|	|
3+20	0.0154	0.08	QV	|	|	|	|
3+25	0.0160	0.08	QV	|	|	|	|
3+30	0.0165	0.08	Q V	|	|	|	|
3+35	0.0171	0.08	Q V	|	|	|	|
3+40	0.0176	0.08	Q V	|	|	|	|
3+45	0.0181	0.08	Q V	|	|	|	|
3+50	0.0187	0.08	Q V	|	|	|	|
3+55	0.0193	0.09	Q V	|	|	|	|
4+ 0	0.0200	0.09	Q V	|	|	|	|
4+ 5	0.0206	0.09	Q V	|	|	|	|
4+10	0.0213	0.09	Q V	|	|	|	|
4+15	0.0219	0.09	Q V	|	|	|	|
4+20	0.0226	0.10	Q V	|	|	|	|
4+25	0.0233	0.11	Q V	|	|	|	|
4+30	0.0241	0.11	Q V	|	|	|	|
4+35	0.0248	0.11	Q V	|	|	|	|
4+40	0.0256	0.11	Q V	|	|	|	|
4+45	0.0263	0.11	Q V	|	|	|	|
4+50	0.0271	0.11	Q V	|	|	|	|
4+55	0.0279	0.12	Q V	|	|	|	|
5+ 0	0.0288	0.12	Q V	|	|	|	|
5+ 5	0.0296	0.12	Q V	|	|	|	|
5+10	0.0303	0.10	Q V	|	|	|	|
5+15	0.0310	0.10	Q V	|	|	|	|
5+20	0.0317	0.10	Q V	|	|	|	|
5+25	0.0324	0.11	Q V	|	|	|	|
5+30	0.0332	0.11	Q V	|	|	|	|
5+35	0.0339	0.11	Q V	|	|	|	|
5+40	0.0348	0.12	Q V	|	|	|	|
5+45	0.0356	0.12	Q V	|	|	|	|
5+50	0.0365	0.12	Q V	|	|	|	|
5+55	0.0373	0.13	Q V	|	|	|	|
6+ 0	0.0382	0.13	Q V	|	|	|	|
6+ 5	0.0391	0.13	Q V	|	|	|	|
6+10	0.0400	0.14	Q V	|	|	|	|
6+15	0.0410	0.14	Q V	|	|	|	|
6+20	0.0420	0.14	Q V	|	|	|	|
6+25	0.0429	0.14	Q V	|	|	|	|
6+30	0.0439	0.14	Q V	|	|	|	|
6+35	0.0449	0.15	Q V	|	|	|	|
6+40	0.0460	0.15	Q V	|	|	|	|
6+45	0.0470	0.16	Q V	|	|	|	|
6+50	0.0481	0.16	Q V	|	|	|	|
6+55	0.0492	0.16	Q V	|	|	|	|
7+ 0	0.0503	0.16	Q V	|	|	|	|
7+ 5	0.0514	0.16	Q V	|	|	|	|

7+10	0.0525	0.16	Q	V	|	|	|	|
7+15	0.0535	0.16	Q	V	|	|	|	|
7+20	0.0546	0.16	Q	V	|	|	|	|
7+25	0.0558	0.17	Q	V	|	|	|	|
7+30	0.0570	0.17	Q	V	|	|	|	|
7+35	0.0582	0.18	Q	V	|	|	|	|
7+40	0.0595	0.18	Q	V	|	|	|	|
7+45	0.0607	0.19	Q	V	|	|	|	|
7+50	0.0621	0.19	Q	V	|	|	|	|
7+55	0.0634	0.20	Q	V	|	|	|	|
8+ 0	0.0648	0.20	Q	V	|	|	|	|
8+ 5	0.0663	0.21	Q	V	|	|	|	|
8+10	0.0678	0.23	Q	V	|	|	|	|
8+15	0.0694	0.23	Q	V	|	|	|	|
8+20	0.0710	0.23	Q	V	|	|	|	|
8+25	0.0727	0.23	Q	V	|	|	|	|
8+30	0.0743	0.24	Q	V	|	|	|	|
8+35	0.0759	0.24	Q	V	|	|	|	|
8+40	0.0776	0.25	Q	V	|	|	|	|
8+45	0.0794	0.25	Q	V	|	|	|	|
8+50	0.0811	0.25	|Q	V	|	|	|	|
8+55	0.0829	0.26	|Q	V	|	|	|	|
9+ 0	0.0848	0.27	|Q	V	|	|	|	|
9+ 5	0.0866	0.27	|Q	V	|	|	|	|
9+10	0.0886	0.29	|Q	V	|	|	|	|
9+15	0.0907	0.29	|Q	|V	|	|	|	|
9+20	0.0927	0.30	|Q	|V	|	|	|	|
9+25	0.0949	0.31	|Q	|V	|	|	|	|
9+30	0.0970	0.31	|Q	|V	|	|	|	|
9+35	0.0992	0.32	|Q	| V	|	|	|	|
9+40	0.1014	0.33	|Q	| V	|	|	|	|
9+45	0.1037	0.33	|Q	| V	|	|	|	|
9+50	0.1060	0.33	|Q	| V	|	|	|	|
9+55	0.1083	0.34	|Q	| V	|	|	|	|
10+ 0	0.1107	0.34	|Q	| V	|	|	|	|
10+ 5	0.1129	0.32	|Q	| V	|	|	|	|
10+10	0.1147	0.27	|Q	| V	|	|	|	|
10+15	0.1165	0.25	|Q	| V	|	|	|	|
10+20	0.1182	0.24	Q	| V	|	|	|	|
10+25	0.1198	0.24	Q	| V	|	|	|	|
10+30	0.1215	0.24	Q	| V	|	|	|	|
10+35	0.1232	0.26	|Q	| V	|	|	|	|
10+40	0.1252	0.29	|Q	| V	|	|	|	|
10+45	0.1273	0.30	|Q	| V	|	|	|	|
10+50	0.1295	0.31	|Q	| V	|	|	|	|
10+55	0.1316	0.31	|Q	| V	|	|	|	|
11+ 0	0.1338	0.31	|Q	| V	|	|	|	|
11+ 5	0.1359	0.31	|Q	| V	|	|	|	|
11+10	0.1380	0.30	|Q	| V	|	|	|	|
11+15	0.1401	0.30	|Q	| V	|	|	|	|
11+20	0.1421	0.30	|Q	| V	|	|	|	|
11+25	0.1442	0.30	|Q	| V	|	|	|	|
11+30	0.1463	0.30	|Q	| V	|	|	|	|
11+35	0.1483	0.29	|Q	| V	|	|	|	|
11+40	0.1502	0.28	|Q	| V	|	|	|	|
11+45	0.1521	0.27	|Q	| V	|	|	|	|
11+50	0.1539	0.27	|Q	| V	|	|	|	|
11+55	0.1559	0.28	|Q	| V	|	|	|	|
12+ 0	0.1578	0.28	|Q	| V	|	|	|	|
12+ 5	0.1599	0.31	|Q	| V	|	|	|	|
12+10	0.1624	0.36	|Q	| V	|	|	|	|
12+15	0.1650	0.38	|Q	| V	|	|	|	|
12+20	0.1677	0.39	|Q	| V	|	|	|	|
12+25	0.1705	0.40	|Q	| V	|	|	|	|
12+30	0.1733	0.41	|Q	| |V	|	|	|	|
12+35	0.1761	0.41	|Q	| |V	|	|	|	|
12+40	0.1791	0.43	|Q	| | V	|	|	|	|
12+45	0.1821	0.44	|Q	| | V	|	|	|	|
12+50	0.1851	0.44	|Q	| | V	|	|	|	|
12+55	0.1882	0.45	|Q	| | V	|	|	|	|
13+ 0	0.1914	0.45	|Q	| | V	|	|	|	|

13+ 5	0.1946	0.47	Q		V		
13+10	0.1982	0.51	Q		V		
13+15	0.2018	0.52	Q		V		
13+20	0.2054	0.53	Q		V		
13+25	0.2091	0.53	Q		V		
13+30	0.2128	0.53	Q		V		
13+35	0.2162	0.50	Q		V		
13+40	0.2190	0.41	Q		V		
13+45	0.2217	0.39	Q		V		
13+50	0.2242	0.38	Q		V		
13+55	0.2268	0.37	Q		V		
14+ 0	0.2293	0.37	Q		V		
14+ 5	0.2319	0.38	Q		V		
14+10	0.2347	0.41	Q		V		
14+15	0.2376	0.42	Q		V		
14+20	0.2405	0.42	Q		V		
14+25	0.2433	0.41	Q		V		
14+30	0.2461	0.41	Q		V		
14+35	0.2489	0.41	Q		V		
14+40	0.2518	0.41	Q		V		
14+45	0.2546	0.41	Q		V		
14+50	0.2574	0.41	Q		V		
14+55	0.2601	0.40	Q		V		
15+ 0	0.2629	0.40	Q		V		
15+ 5	0.2655	0.39	Q		V		
15+10	0.2682	0.38	Q		V		
15+15	0.2708	0.38	Q		V		
15+20	0.2734	0.38	Q		V		
15+25	0.2759	0.37	Q		V		
15+30	0.2784	0.36	Q		V		
15+35	0.2808	0.35	Q		V		
15+40	0.2830	0.32	Q		V		
15+45	0.2852	0.31	Q		V		
15+50	0.2872	0.30	Q		V		
15+55	0.2893	0.30	Q		V		
16+ 0	0.2914	0.30	Q		V		
16+ 5	0.2931	0.25	Q		V		
16+10	0.2940	0.13	Q		V		
16+15	0.2946	0.10	Q		V		
16+20	0.2952	0.08	Q		V		
16+25	0.2957	0.07	Q		V		
16+30	0.2962	0.07	Q		V		
16+35	0.2966	0.06	Q		V		
16+40	0.2969	0.05	Q		V		
16+45	0.2973	0.05	Q		V		
16+50	0.2976	0.05	Q		V		
16+55	0.2979	0.05	Q		V		
17+ 0	0.2983	0.05	Q		V		
17+ 5	0.2987	0.05	Q		V		
17+10	0.2991	0.07	Q		V		
17+15	0.2996	0.07	Q		V		
17+20	0.3002	0.08	Q		V		
17+25	0.3007	0.08	Q		V		
17+30	0.3012	0.08	Q		V		
17+35	0.3018	0.08	Q		V		
17+40	0.3023	0.08	Q		V		
17+45	0.3029	0.08	Q		V		
17+50	0.3034	0.08	Q		V		
17+55	0.3038	0.07	Q		V		
18+ 0	0.3043	0.07	Q		V		
18+ 5	0.3047	0.06	Q		V		
18+10	0.3052	0.06	Q		V		
18+15	0.3056	0.06	Q		V		
18+20	0.3060	0.06	Q		V		
18+25	0.3065	0.06	Q		V		
18+30	0.3069	0.06	Q		V		
18+35	0.3073	0.06	Q		V		
18+40	0.3077	0.05	Q		V		
18+45	0.3080	0.05	Q		V		
18+50	0.3083	0.04	Q		V		
18+55	0.3086	0.04	Q		V		

19+ 0	0.3088	0.03	Q				V
19+ 5	0.3091	0.04	Q				V
19+10	0.3094	0.04	Q				V
19+15	0.3097	0.05	Q				V
19+20	0.3100	0.05	Q				V
19+25	0.3104	0.06	Q				V
19+30	0.3108	0.06	Q				V
19+35	0.3112	0.06	Q				V
19+40	0.3116	0.05	Q				V
19+45	0.3119	0.05	Q				V
19+50	0.3122	0.04	Q				V
19+55	0.3125	0.04	Q				V
20+ 0	0.3127	0.03	Q				V
20+ 5	0.3130	0.04	Q				V
20+10	0.3133	0.04	Q				V
20+15	0.3136	0.05	Q				V
20+20	0.3139	0.05	Q				V
20+25	0.3142	0.05	Q				V
20+30	0.3145	0.05	Q				V
20+35	0.3149	0.05	Q				V
20+40	0.3152	0.05	Q				V
20+45	0.3155	0.05	Q				V
20+50	0.3158	0.04	Q				V
20+55	0.3161	0.04	Q				V
21+ 0	0.3163	0.03	Q				V
21+ 5	0.3166	0.04	Q				V
21+10	0.3169	0.04	Q				V
21+15	0.3172	0.05	Q				V
21+20	0.3175	0.04	Q				V
21+25	0.3177	0.04	Q				V
21+30	0.3179	0.03	Q				V
21+35	0.3182	0.04	Q				V
21+40	0.3185	0.04	Q				V
21+45	0.3188	0.05	Q				V
21+50	0.3191	0.04	Q				V
21+55	0.3193	0.04	Q				V
22+ 0	0.3196	0.03	Q				V
22+ 5	0.3198	0.04	Q				V
22+10	0.3201	0.04	Q				V
22+15	0.3204	0.05	Q				V
22+20	0.3207	0.04	Q				V
22+25	0.3210	0.04	Q				V
22+30	0.3212	0.03	Q				V
22+35	0.3214	0.03	Q				V
22+40	0.3216	0.03	Q				V
22+45	0.3218	0.03	Q				V
22+50	0.3221	0.03	Q				V
22+55	0.3223	0.03	Q				V
23+ 0	0.3225	0.03	Q				V
23+ 5	0.3227	0.03	Q				V
23+10	0.3229	0.03	Q				V
23+15	0.3232	0.03	Q				V
23+20	0.3234	0.03	Q				V
23+25	0.3236	0.03	Q				V
23+30	0.3238	0.03	Q				V
23+35	0.3240	0.03	Q				V
23+40	0.3242	0.03	Q				V
23+45	0.3245	0.03	Q				V
23+50	0.3247	0.03	Q				V
23+55	0.3249	0.03	Q				V
24+ 0	0.3251	0.03	Q				V
24+ 5	0.3253	0.02	Q				V
24+10	0.3253	0.01	Q				V
24+15	0.3254	0.00	Q				V
24+20	0.3254	0.00	Q				V
24+25	0.3254	0.00	Q				V
24+30	0.3254	0.00	Q				V
24+35	0.3254	0.00	Q				V

10-YEAR, 24-HOUR

U n i t H y d r o g r a p h A n a l y s i s

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Study date 10/23/21 File: ARA1PRE2410.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

TRI-8 Builders - S/N 615

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

150.10.18
UNIT HYDROGRAPH FOR BASIN NODE 118.1
PRE-PROJECT CONDITION
FN: ARA1PRE.UNRIV

Drainage Area = 22.97(Ac.) = 0.036 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 22.97(Ac.) = 0.036 Sq. Mi.
Length along longest watercourse = 1744.00(Ft.)
Length along longest watercourse measured to centroid = 446.00(Ft.)
Length along longest watercourse = 0.330 Mi.
Length along longest watercourse measured to centroid = 0.084 Mi.
Difference in elevation = 40.50(Ft.)
Slope along watercourse = 122.6147 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.074 Hr.
Lag time = 4.45 Min.
25% of lag time = 1.11 Min.
40% of lag time = 1.78 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
22.97	1.70	39.05

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
22.97	4.25	97.62

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.700(In)
Area Averaged 100-Year Rainfall = 4.250(In)

Point rain (area averaged) = 2.749(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 2.749(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
22.970	71.40	0.000

Total Area Entered = 22.97(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
71.4	71.4	0.345	0.000	0.345	1.000	0.345
					Sum (F) =	0.345

Area averaged mean soil loss (F) (In/Hr) = 0.345
Minimum soil loss rate ((In/Hr)) = 0.173
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	112.454	22.974	5.318
2	0.167	224.909	48.849	11.308
3	0.250	337.363	14.032	3.248
4	0.333	449.817	6.419	1.486
5	0.417	562.272	3.567	0.826
6	0.500	674.726	2.182	0.505
7	0.583	787.180	1.287	0.298
8	0.667	899.635	0.690	0.160
			Sum = 100.000	Sum= 23.149

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.022	0.612	0.020	0.00
2	0.17	0.07	0.022	0.610	0.020	0.00
3	0.25	0.07	0.022	0.608	0.020	0.00
4	0.33	0.10	0.033	0.605	0.030	0.00
5	0.42	0.10	0.033	0.603	0.030	0.00
6	0.50	0.10	0.033	0.601	0.030	0.00
7	0.58	0.10	0.033	0.598	0.030	0.00
8	0.67	0.10	0.033	0.596	0.030	0.00
9	0.75	0.10	0.033	0.594	0.030	0.00
10	0.83	0.13	0.044	0.591	0.040	0.00
11	0.92	0.13	0.044	0.589	0.040	0.00
12	1.00	0.13	0.044	0.587	0.040	0.00
13	1.08	0.10	0.033	0.584	0.030	0.00
14	1.17	0.10	0.033	0.582	0.030	0.00
15	1.25	0.10	0.033	0.580	0.030	0.00
16	1.33	0.10	0.033	0.577	0.030	0.00
17	1.42	0.10	0.033	0.575	0.030	0.00
18	1.50	0.10	0.033	0.573	0.030	0.00
19	1.58	0.10	0.033	0.571	0.030	0.00
20	1.67	0.10	0.033	0.568	0.030	0.00
21	1.75	0.10	0.033	0.566	0.030	0.00
22	1.83	0.13	0.044	0.564	0.040	0.00
23	1.92	0.13	0.044	0.561	0.040	0.00
24	2.00	0.13	0.044	0.559	0.040	0.00
25	2.08	0.13	0.044	0.557	0.040	0.00
26	2.17	0.13	0.044	0.555	0.040	0.00
27	2.25	0.13	0.044	0.552	0.040	0.00
28	2.33	0.13	0.044	0.550	0.040	0.00
29	2.42	0.13	0.044	0.548	0.040	0.00
30	2.50	0.13	0.044	0.546	0.040	0.00
31	2.58	0.17	0.055	0.543	0.049	0.01
32	2.67	0.17	0.055	0.541	0.049	0.01
33	2.75	0.17	0.055	0.539	0.049	0.01
34	2.83	0.17	0.055	0.537	0.049	0.01
35	2.92	0.17	0.055	0.535	0.049	0.01
36	3.00	0.17	0.055	0.532	0.049	0.01
37	3.08	0.17	0.055	0.530	0.049	0.01
38	3.17	0.17	0.055	0.528	0.049	0.01

39	3.25	0.17	0.055	0.526	0.049	0.01
40	3.33	0.17	0.055	0.524	0.049	0.01
41	3.42	0.17	0.055	0.521	0.049	0.01
42	3.50	0.17	0.055	0.519	0.049	0.01
43	3.58	0.17	0.055	0.517	0.049	0.01
44	3.67	0.17	0.055	0.515	0.049	0.01
45	3.75	0.17	0.055	0.513	0.049	0.01
46	3.83	0.20	0.066	0.510	0.059	0.01
47	3.92	0.20	0.066	0.508	0.059	0.01
48	4.00	0.20	0.066	0.506	0.059	0.01
49	4.08	0.20	0.066	0.504	0.059	0.01
50	4.17	0.20	0.066	0.502	0.059	0.01
51	4.25	0.20	0.066	0.500	0.059	0.01
52	4.33	0.23	0.077	0.498	0.069	0.01
53	4.42	0.23	0.077	0.495	0.069	0.01
54	4.50	0.23	0.077	0.493	0.069	0.01
55	4.58	0.23	0.077	0.491	0.069	0.01
56	4.67	0.23	0.077	0.489	0.069	0.01
57	4.75	0.23	0.077	0.487	0.069	0.01
58	4.83	0.27	0.088	0.485	0.079	0.01
59	4.92	0.27	0.088	0.483	0.079	0.01
60	5.00	0.27	0.088	0.481	0.079	0.01
61	5.08	0.20	0.066	0.479	0.059	0.01
62	5.17	0.20	0.066	0.477	0.059	0.01
63	5.25	0.20	0.066	0.474	0.059	0.01
64	5.33	0.23	0.077	0.472	0.069	0.01
65	5.42	0.23	0.077	0.470	0.069	0.01
66	5.50	0.23	0.077	0.468	0.069	0.01
67	5.58	0.27	0.088	0.466	0.079	0.01
68	5.67	0.27	0.088	0.464	0.079	0.01
69	5.75	0.27	0.088	0.462	0.079	0.01
70	5.83	0.27	0.088	0.460	0.079	0.01
71	5.92	0.27	0.088	0.458	0.079	0.01
72	6.00	0.27	0.088	0.456	0.079	0.01
73	6.08	0.30	0.099	0.454	0.089	0.01
74	6.17	0.30	0.099	0.452	0.089	0.01
75	6.25	0.30	0.099	0.450	0.089	0.01
76	6.33	0.30	0.099	0.448	0.089	0.01
77	6.42	0.30	0.099	0.446	0.089	0.01
78	6.50	0.30	0.099	0.444	0.089	0.01
79	6.58	0.33	0.110	0.442	0.099	0.01
80	6.67	0.33	0.110	0.440	0.099	0.01
81	6.75	0.33	0.110	0.438	0.099	0.01
82	6.83	0.33	0.110	0.436	0.099	0.01
83	6.92	0.33	0.110	0.434	0.099	0.01
84	7.00	0.33	0.110	0.432	0.099	0.01
85	7.08	0.33	0.110	0.430	0.099	0.01
86	7.17	0.33	0.110	0.428	0.099	0.01
87	7.25	0.33	0.110	0.426	0.099	0.01
88	7.33	0.37	0.121	0.424	0.109	0.01
89	7.42	0.37	0.121	0.422	0.109	0.01
90	7.50	0.37	0.121	0.420	0.109	0.01
91	7.58	0.40	0.132	0.418	0.119	0.01
92	7.67	0.40	0.132	0.417	0.119	0.01
93	7.75	0.40	0.132	0.415	0.119	0.01
94	7.83	0.43	0.143	0.413	0.129	0.01
95	7.92	0.43	0.143	0.411	0.129	0.01
96	8.00	0.43	0.143	0.409	0.129	0.01
97	8.08	0.50	0.165	0.407	0.148	0.02
98	8.17	0.50	0.165	0.405	0.148	0.02
99	8.25	0.50	0.165	0.403	0.148	0.02
100	8.33	0.50	0.165	0.401	0.148	0.02
101	8.42	0.50	0.165	0.399	0.148	0.02
102	8.50	0.50	0.165	0.398	0.148	0.02
103	8.58	0.53	0.176	0.396	0.158	0.02
104	8.67	0.53	0.176	0.394	0.158	0.02
105	8.75	0.53	0.176	0.392	0.158	0.02
106	8.83	0.57	0.187	0.390	0.168	0.02
107	8.92	0.57	0.187	0.388	0.168	0.02
108	9.00	0.57	0.187	0.386	0.168	0.02
109	9.08	0.63	0.209	0.385	0.188	0.02

110	9.17	0.63	0.209	0.383	0.188	0.02
111	9.25	0.63	0.209	0.381	0.188	0.02
112	9.33	0.67	0.220	0.379	0.198	0.02
113	9.42	0.67	0.220	0.377	0.198	0.02
114	9.50	0.67	0.220	0.376	0.198	0.02
115	9.58	0.70	0.231	0.374	0.208	0.02
116	9.67	0.70	0.231	0.372	0.208	0.02
117	9.75	0.70	0.231	0.370	0.208	0.02
118	9.83	0.73	0.242	0.368	0.218	0.02
119	9.92	0.73	0.242	0.367	0.218	0.02
120	10.00	0.73	0.242	0.365	0.218	0.02
121	10.08	0.50	0.165	0.363	0.148	0.02
122	10.17	0.50	0.165	0.361	0.148	0.02
123	10.25	0.50	0.165	0.360	0.148	0.02
124	10.33	0.50	0.165	0.358	0.148	0.02
125	10.42	0.50	0.165	0.356	0.148	0.02
126	10.50	0.50	0.165	0.354	0.148	0.02
127	10.58	0.67	0.220	0.353	0.198	0.02
128	10.67	0.67	0.220	0.351	0.198	0.02
129	10.75	0.67	0.220	0.349	0.198	0.02
130	10.83	0.67	0.220	0.347	0.198	0.02
131	10.92	0.67	0.220	0.346	0.198	0.02
132	11.00	0.67	0.220	0.344	0.198	0.02
133	11.08	0.63	0.209	0.342	0.188	0.02
134	11.17	0.63	0.209	0.341	0.188	0.02
135	11.25	0.63	0.209	0.339	0.188	0.02
136	11.33	0.63	0.209	0.337	0.188	0.02
137	11.42	0.63	0.209	0.336	0.188	0.02
138	11.50	0.63	0.209	0.334	0.188	0.02
139	11.58	0.57	0.187	0.332	0.168	0.02
140	11.67	0.57	0.187	0.331	0.168	0.02
141	11.75	0.57	0.187	0.329	0.168	0.02
142	11.83	0.60	0.198	0.327	0.178	0.02
143	11.92	0.60	0.198	0.326	0.178	0.02
144	12.00	0.60	0.198	0.324	0.178	0.02
145	12.08	0.83	0.275	0.322	0.247	0.03
146	12.17	0.83	0.275	0.321	0.247	0.03
147	12.25	0.83	0.275	0.319	0.247	0.03
148	12.33	0.87	0.286	0.318	0.257	0.03
149	12.42	0.87	0.286	0.316	0.257	0.03
150	12.50	0.87	0.286	0.314	0.257	0.03
151	12.58	0.93	0.308	0.313	0.277	0.03
152	12.67	0.93	0.308	0.311	0.277	0.03
153	12.75	0.93	0.308	0.310	0.277	0.03
154	12.83	0.97	0.319	0.308	---	0.01
155	12.92	0.97	0.319	0.307	---	0.01
156	13.00	0.97	0.319	0.305	---	0.01
157	13.08	1.13	0.374	0.304	---	0.07
158	13.17	1.13	0.374	0.302	---	0.07
159	13.25	1.13	0.374	0.300	---	0.07
160	13.33	1.13	0.374	0.299	---	0.07
161	13.42	1.13	0.374	0.297	---	0.08
162	13.50	1.13	0.374	0.296	---	0.08
163	13.58	0.77	0.253	0.294	0.228	0.03
164	13.67	0.77	0.253	0.293	0.228	0.03
165	13.75	0.77	0.253	0.291	0.228	0.03
166	13.83	0.77	0.253	0.290	0.228	0.03
167	13.92	0.77	0.253	0.288	0.228	0.03
168	14.00	0.77	0.253	0.287	0.228	0.03
169	14.08	0.90	0.297	0.286	---	0.01
170	14.17	0.90	0.297	0.284	---	0.01
171	14.25	0.90	0.297	0.283	---	0.01
172	14.33	0.87	0.286	0.281	---	0.00
173	14.42	0.87	0.286	0.280	---	0.01
174	14.50	0.87	0.286	0.278	---	0.01
175	14.58	0.87	0.286	0.277	---	0.01
176	14.67	0.87	0.286	0.275	---	0.01
177	14.75	0.87	0.286	0.274	---	0.01
178	14.83	0.83	0.275	0.273	---	0.00
179	14.92	0.83	0.275	0.271	---	0.00
180	15.00	0.83	0.275	0.270	---	0.01

181	15.08	0.80	0.264	0.268	0.238	0.03
182	15.17	0.80	0.264	0.267	0.238	0.03
183	15.25	0.80	0.264	0.266	0.238	0.03
184	15.33	0.77	0.253	0.264	0.228	0.03
185	15.42	0.77	0.253	0.263	0.228	0.03
186	15.50	0.77	0.253	0.262	0.228	0.03
187	15.58	0.63	0.209	0.260	0.188	0.02
188	15.67	0.63	0.209	0.259	0.188	0.02
189	15.75	0.63	0.209	0.258	0.188	0.02
190	15.83	0.63	0.209	0.256	0.188	0.02
191	15.92	0.63	0.209	0.255	0.188	0.02
192	16.00	0.63	0.209	0.254	0.188	0.02
193	16.08	0.13	0.044	0.252	0.040	0.00
194	16.17	0.13	0.044	0.251	0.040	0.00
195	16.25	0.13	0.044	0.250	0.040	0.00
196	16.33	0.13	0.044	0.249	0.040	0.00
197	16.42	0.13	0.044	0.247	0.040	0.00
198	16.50	0.13	0.044	0.246	0.040	0.00
199	16.58	0.10	0.033	0.245	0.030	0.00
200	16.67	0.10	0.033	0.244	0.030	0.00
201	16.75	0.10	0.033	0.242	0.030	0.00
202	16.83	0.10	0.033	0.241	0.030	0.00
203	16.92	0.10	0.033	0.240	0.030	0.00
204	17.00	0.10	0.033	0.239	0.030	0.00
205	17.08	0.17	0.055	0.237	0.049	0.01
206	17.17	0.17	0.055	0.236	0.049	0.01
207	17.25	0.17	0.055	0.235	0.049	0.01
208	17.33	0.17	0.055	0.234	0.049	0.01
209	17.42	0.17	0.055	0.233	0.049	0.01
210	17.50	0.17	0.055	0.232	0.049	0.01
211	17.58	0.17	0.055	0.230	0.049	0.01
212	17.67	0.17	0.055	0.229	0.049	0.01
213	17.75	0.17	0.055	0.228	0.049	0.01
214	17.83	0.13	0.044	0.227	0.040	0.00
215	17.92	0.13	0.044	0.226	0.040	0.00
216	18.00	0.13	0.044	0.225	0.040	0.00
217	18.08	0.13	0.044	0.224	0.040	0.00
218	18.17	0.13	0.044	0.223	0.040	0.00
219	18.25	0.13	0.044	0.221	0.040	0.00
220	18.33	0.13	0.044	0.220	0.040	0.00
221	18.42	0.13	0.044	0.219	0.040	0.00
222	18.50	0.13	0.044	0.218	0.040	0.00
223	18.58	0.10	0.033	0.217	0.030	0.00
224	18.67	0.10	0.033	0.216	0.030	0.00
225	18.75	0.10	0.033	0.215	0.030	0.00
226	18.83	0.07	0.022	0.214	0.020	0.00
227	18.92	0.07	0.022	0.213	0.020	0.00
228	19.00	0.07	0.022	0.212	0.020	0.00
229	19.08	0.10	0.033	0.211	0.030	0.00
230	19.17	0.10	0.033	0.210	0.030	0.00
231	19.25	0.10	0.033	0.209	0.030	0.00
232	19.33	0.13	0.044	0.208	0.040	0.00
233	19.42	0.13	0.044	0.207	0.040	0.00
234	19.50	0.13	0.044	0.206	0.040	0.00
235	19.58	0.10	0.033	0.205	0.030	0.00
236	19.67	0.10	0.033	0.204	0.030	0.00
237	19.75	0.10	0.033	0.203	0.030	0.00
238	19.83	0.07	0.022	0.202	0.020	0.00
239	19.92	0.07	0.022	0.202	0.020	0.00
240	20.00	0.07	0.022	0.201	0.020	0.00
241	20.08	0.10	0.033	0.200	0.030	0.00
242	20.17	0.10	0.033	0.199	0.030	0.00
243	20.25	0.10	0.033	0.198	0.030	0.00
244	20.33	0.10	0.033	0.197	0.030	0.00
245	20.42	0.10	0.033	0.196	0.030	0.00
246	20.50	0.10	0.033	0.195	0.030	0.00
247	20.58	0.10	0.033	0.195	0.030	0.00
248	20.67	0.10	0.033	0.194	0.030	0.00
249	20.75	0.10	0.033	0.193	0.030	0.00
250	20.83	0.07	0.022	0.192	0.020	0.00
251	20.92	0.07	0.022	0.191	0.020	0.00

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252  21.00     0.07      0.022         0.191     0.020         0.00
253  21.08     0.10      0.033         0.190     0.030         0.00
254  21.17     0.10      0.033         0.189     0.030         0.00
255  21.25     0.10      0.033         0.188     0.030         0.00
256  21.33     0.07      0.022         0.188     0.020         0.00
257  21.42     0.07      0.022         0.187     0.020         0.00
258  21.50     0.07      0.022         0.186     0.020         0.00
259  21.58     0.10      0.033         0.186     0.030         0.00
260  21.67     0.10      0.033         0.185     0.030         0.00
261  21.75     0.10      0.033         0.184     0.030         0.00
262  21.83     0.07      0.022         0.184     0.020         0.00
263  21.92     0.07      0.022         0.183     0.020         0.00
264  22.00     0.07      0.022         0.182     0.020         0.00
265  22.08     0.10      0.033         0.182     0.030         0.00
266  22.17     0.10      0.033         0.181     0.030         0.00
267  22.25     0.10      0.033         0.181     0.030         0.00
268  22.33     0.07      0.022         0.180     0.020         0.00
269  22.42     0.07      0.022         0.180     0.020         0.00
270  22.50     0.07      0.022         0.179     0.020         0.00
271  22.58     0.07      0.022         0.178     0.020         0.00
272  22.67     0.07      0.022         0.178     0.020         0.00
273  22.75     0.07      0.022         0.177     0.020         0.00
274  22.83     0.07      0.022         0.177     0.020         0.00
275  22.92     0.07      0.022         0.177     0.020         0.00
276  23.00     0.07      0.022         0.176     0.020         0.00
277  23.08     0.07      0.022         0.176     0.020         0.00
278  23.17     0.07      0.022         0.175     0.020         0.00
279  23.25     0.07      0.022         0.175     0.020         0.00
280  23.33     0.07      0.022         0.175     0.020         0.00
281  23.42     0.07      0.022         0.174     0.020         0.00
282  23.50     0.07      0.022         0.174     0.020         0.00
283  23.58     0.07      0.022         0.174     0.020         0.00
284  23.67     0.07      0.022         0.173     0.020         0.00
285  23.75     0.07      0.022         0.173     0.020         0.00
286  23.83     0.07      0.022         0.173     0.020         0.00
287  23.92     0.07      0.022         0.173     0.020         0.00
288  24.00     0.07      0.022         0.173     0.020         0.00
    Sum =     100.0                                 Sum =      3.2
      Flood volume = Effective rainfall      0.27(In)
       times area      23.0(Ac.)/[(In)/(Ft.)] =       0.5(Ac.Ft)
      Total soil loss =      2.48(In)
      Total soil loss =     4.749(Ac.Ft)
      Total rainfall =      2.75(In)
      Flood volume =       22351.2 Cubic Feet
      Total soil loss =      206860.7 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      1.733(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ------------------------------------------------------------------------
   0+ 5       0.0001      0.01  Q         |         |         |         |
   0+10       0.0003      0.04  Q         |         |         |         |
   0+15       0.0006      0.04  Q         |         |         |         |
   0+20       0.0010      0.05  Q         |         |         |         |
   0+25       0.0015      0.07  Q         |         |         |         |
   0+30       0.0020      0.07  Q         |         |         |         |
   0+35       0.0025      0.07  Q         |         |         |         |
   0+40       0.0030      0.08  Q         |         |         |         |
   0+45       0.0035      0.08  Q         |         |         |         |
   0+50       0.0041      0.08  Q         |         |         |         |
   0+55       0.0047      0.09  Q         |         |         |         |
   1+ 0       0.0054      0.10  Q         |         |         |         |
   1+ 5       0.0060      0.09  Q         |         |         |         |
   1+10       0.0066      0.08  Q         |         |         |         |
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1+15	0.0072	0.08	Q	|	|	|	|
1+20	0.0077	0.08	Q	|	|	|	|
1+25	0.0082	0.08	Q	|	|	|	|
1+30	0.0088	0.08	Q	|	|	|	|
1+35	0.0093	0.08	Q	|	|	|	|
1+40	0.0098	0.08	Q	|	|	|	|
1+45	0.0103	0.08	Q	|	|	|	|
1+50	0.0109	0.08	Q	|	|	|	|
1+55	0.0116	0.09	Q	|	|	|	|
2+ 0	0.0122	0.10	Q	|	|	|	|
2+ 5	0.0129	0.10	QV	|	|	|	|
2+10	0.0136	0.10	QV	|	|	|	|
2+15	0.0143	0.10	QV	|	|	|	|
2+20	0.0150	0.10	QV	|	|	|	|
2+25	0.0157	0.10	QV	|	|	|	|
2+30	0.0164	0.10	QV	|	|	|	|
2+35	0.0172	0.11	QV	|	|	|	|
2+40	0.0180	0.12	QV	|	|	|	|
2+45	0.0188	0.12	QV	|	|	|	|
2+50	0.0197	0.13	QV	|	|	|	|
2+55	0.0206	0.13	QV	|	|	|	|
3+ 0	0.0215	0.13	QV	|	|	|	|
3+ 5	0.0223	0.13	QV	|	|	|	|
3+10	0.0232	0.13	QV	|	|	|	|
3+15	0.0241	0.13	QV	|	|	|	|
3+20	0.0250	0.13	QV	|	|	|	|
3+25	0.0258	0.13	Q V	|	|	|	|
3+30	0.0267	0.13	Q V	|	|	|	|
3+35	0.0276	0.13	Q V	|	|	|	|
3+40	0.0285	0.13	Q V	|	|	|	|
3+45	0.0293	0.13	Q V	|	|	|	|
3+50	0.0303	0.13	Q V	|	|	|	|
3+55	0.0313	0.15	Q V	|	|	|	|
4+ 0	0.0323	0.15	Q V	|	|	|	|
4+ 5	0.0333	0.15	Q V	|	|	|	|
4+10	0.0344	0.15	Q V	|	|	|	|
4+15	0.0354	0.15	Q V	|	|	|	|
4+20	0.0365	0.16	Q V	|	|	|	|
4+25	0.0377	0.17	Q V	|	|	|	|
4+30	0.0389	0.17	Q V	|	|	|	|
4+35	0.0401	0.18	Q V	|	|	|	|
4+40	0.0413	0.18	Q V	|	|	|	|
4+45	0.0426	0.18	Q V	|	|	|	|
4+50	0.0438	0.18	Q V	|	|	|	|
4+55	0.0452	0.20	Q V	|	|	|	|
5+ 0	0.0466	0.20	Q V	|	|	|	|
5+ 5	0.0479	0.19	Q V	|	|	|	|
5+10	0.0490	0.17	Q V	|	|	|	|
5+15	0.0501	0.16	Q V	|	|	|	|
5+20	0.0512	0.16	Q V	|	|	|	|
5+25	0.0524	0.17	Q V	|	|	|	|
5+30	0.0536	0.18	Q V	|	|	|	|
5+35	0.0549	0.18	Q V	|	|	|	|
5+40	0.0562	0.20	Q V	|	|	|	|
5+45	0.0576	0.20	Q V	|	|	|	|
5+50	0.0590	0.20	Q V	|	|	|	|
5+55	0.0604	0.20	Q V	|	|	|	|
6+ 0	0.0618	0.20	Q V	|	|	|	|
6+ 5	0.0632	0.21	Q V	|	|	|	|
6+10	0.0648	0.22	Q V	|	|	|	|
6+15	0.0663	0.23	Q V	|	|	|	|
6+20	0.0679	0.23	Q V	|	|	|	|
6+25	0.0695	0.23	Q V	|	|	|	|
6+30	0.0710	0.23	Q V	|	|	|	|
6+35	0.0726	0.23	Q V	|	|	|	|
6+40	0.0744	0.25	Q V	|	|	|	|
6+45	0.0761	0.25	|Q V	|	|	|	|
6+50	0.0778	0.25	|Q V	|	|	|	|
6+55	0.0796	0.25	|Q V	|	|	|	|
7+ 0	0.0813	0.25	|Q V	|	|	|	|
7+ 5	0.0831	0.25	|Q V	|	|	|	|

7+10	0.0848	0.25	Q V				
7+15	0.0866	0.25	Q V				
7+20	0.0884	0.26	Q V				
7+25	0.0903	0.27	Q V				
7+30	0.0922	0.28	Q V				
7+35	0.0941	0.28	Q V				
7+40	0.0962	0.30	Q V				
7+45	0.0982	0.30	Q V				
7+50	0.1004	0.31	Q V				
7+55	0.1026	0.32	Q V				
8+ 0	0.1048	0.33	Q V				
8+ 5	0.1072	0.34	Q V				
8+10	0.1097	0.37	Q V				
8+15	0.1123	0.37	Q V				
8+20	0.1149	0.38	Q V				
8+25	0.1175	0.38	Q V				
8+30	0.1201	0.38	Q V				
8+35	0.1228	0.39	Q V				
8+40	0.1256	0.40	Q V				
8+45	0.1283	0.40	Q V				
8+50	0.1312	0.41	Q V				
8+55	0.1341	0.42	Q V				
9+ 0	0.1371	0.43	Q V				
9+ 5	0.1401	0.44	Q V				
9+10	0.1433	0.47	Q V				
9+15	0.1466	0.48	Q V				
9+20	0.1500	0.49	Q V				
9+25	0.1534	0.50	Q V				
9+30	0.1569	0.50	Q V				
9+35	0.1604	0.51	Q V				
9+40	0.1640	0.53	Q V				
9+45	0.1677	0.53	Q V				
9+50	0.1714	0.54	Q V				
9+55	0.1752	0.55	Q V				
10+ 0	0.1790	0.56	Q V				
10+ 5	0.1826	0.52	Q V				
10+10	0.1856	0.43	Q V				
10+15	0.1884	0.41	Q V				
10+20	0.1911	0.40	Q V				
10+25	0.1938	0.39	Q V				
10+30	0.1964	0.39	Q V				
10+35	0.1993	0.41	Q V				
10+40	0.2025	0.47	Q V				
10+45	0.2059	0.49	Q V				
10+50	0.2093	0.50	Q V				
10+55	0.2128	0.50	Q V				
11+ 0	0.2163	0.51	Q V				
11+ 5	0.2198	0.50	Q V				
11+10	0.2232	0.49	Q V				
11+15	0.2265	0.49	Q V				
11+20	0.2299	0.49	Q V				
11+25	0.2332	0.48	Q V				
11+30	0.2365	0.48	Q V				
11+35	0.2398	0.47	Q V				
11+40	0.2429	0.45	Q V				
11+45	0.2459	0.44	Q V				
11+50	0.2489	0.44	Q V				
11+55	0.2521	0.45	Q V				
12+ 0	0.2552	0.46	Q V				
12+ 5	0.2586	0.50	Q V				
12+10	0.2627	0.59	Q V				
12+15	0.2669	0.61	Q V				
12+20	0.2712	0.63	Q V				
12+25	0.2757	0.65	Q V				
12+30	0.2802	0.66	Q V				
12+35	0.2848	0.67	Q V				
12+40	0.2896	0.70	Q V				
12+45	0.2945	0.71	Q V				
12+50	0.2986	0.60	Q V				
12+55	0.3013	0.38	Q V				
13+ 0	0.3036	0.35	Q V				

13+ 5	0.3081	0.64	| Q |	|	| V |	|
13+10	0.3169	1.28	| Q |	|	| V |	|
13+15	0.3271	1.48	| Q |	|	| V |	|
13+20	0.3380	1.59	| Q |	|	| V |	|
13+25	0.3496	1.67	| Q |	|	| V |	|
13+30	0.3615	1.73	| Q |	|	| V |	|
13+35	0.3718	1.50	| Q |	|	| V |	|
13+40	0.3781	0.92	| Q |	|	| V|	|
13+45	0.3833	0.75	| Q |	|	| V|	|
13+50	0.3880	0.68	| Q |	|	| V |	|
13+55	0.3924	0.64	| Q |	|	| V |	|
14+ 0	0.3966	0.61	| Q |	|	| V |	|
14+ 5	0.4001	0.52	| Q |	|	| |V |	|
14+10	0.4026	0.36	|Q |	|	| |V |	|
14+15	0.4050	0.34	|Q |	|	| |V |	|
14+20	0.4070	0.29	|Q |	|	| |V |	|
14+25	0.4083	0.19	Q |	|	| |V |	|
14+30	0.4095	0.18	Q |	|	| |V |	|
14+35	0.4108	0.19	Q |	|	| V |	|
14+40	0.4122	0.21	Q |	|	| V |	|
14+45	0.4138	0.24	Q |	|	| V |	|
14+50	0.4152	0.21	Q |	|	| V |	|
14+55	0.4160	0.11	Q |	|	| V |	|
15+ 0	0.4168	0.11	Q |	|	| V |	|
15+ 5	0.4184	0.23	Q |	|	| V |	|
15+10	0.4216	0.47	|Q |	|	| V |	|
15+15	0.4254	0.54	| Q |	|	| V |	|
15+20	0.4293	0.57	| Q |	|	| V |	|
15+25	0.4332	0.57	| Q |	|	| V |	|
15+30	0.4372	0.58	| Q |	|	| V |	|
15+35	0.4411	0.56	| Q |	|	| V |	|
15+40	0.4446	0.51	| Q |	|	| V |	|
15+45	0.4480	0.50	|Q |	|	| V |	|
15+50	0.4514	0.49	|Q |	|	| V |	|
15+55	0.4548	0.49	|Q |	|	| V |	|
16+ 0	0.4581	0.49	|Q |	|	| V |	|
16+ 5	0.4609	0.40	|Q |	|	| V |	|
16+10	0.4623	0.21	Q |	|	| V |	|
16+15	0.4634	0.16	Q |	|	| V |	|
16+20	0.4643	0.13	Q |	|	| V |	|
16+25	0.4651	0.12	Q |	|	| V |	|
16+30	0.4659	0.11	Q |	|	| V |	|
16+35	0.4665	0.10	Q |	|	| V |	|
16+40	0.4671	0.08	Q |	|	| V |	|
16+45	0.4677	0.08	Q |	|	| V |	|
16+50	0.4682	0.08	Q |	|	| V |	|
16+55	0.4687	0.08	Q |	|	| V |	|
17+ 0	0.4693	0.08	Q |	|	| V |	|
17+ 5	0.4699	0.09	Q |	|	| V |	|
17+10	0.4706	0.11	Q |	|	| V |	|
17+15	0.4715	0.12	Q |	|	| V |	|
17+20	0.4723	0.12	Q |	|	| V |	|
17+25	0.4732	0.13	Q |	|	| V |	|
17+30	0.4741	0.13	Q |	|	| V |	|
17+35	0.4749	0.13	Q |	|	| V |	|
17+40	0.4758	0.13	Q |	|	| V |	|
17+45	0.4767	0.13	Q |	|	| V |	|
17+50	0.4775	0.12	Q |	|	| V |	|
17+55	0.4783	0.11	Q |	|	| V |	|
18+ 0	0.4790	0.11	Q |	|	| V |	|
18+ 5	0.4797	0.10	Q |	|	| V |	|
18+10	0.4804	0.10	Q |	|	| V |	|
18+15	0.4811	0.10	Q |	|	| V |	|
18+20	0.4818	0.10	Q |	|	| V |	|
18+25	0.4825	0.10	Q |	|	| V |	|
18+30	0.4832	0.10	Q |	|	| V |	|
18+35	0.4839	0.10	Q |	|	| V |	|
18+40	0.4845	0.08	Q |	|	| V |	|
18+45	0.4850	0.08	Q |	|	| V |	|
18+50	0.4855	0.07	Q |	|	| V |	|
18+55	0.4859	0.06	Q |	|	| V |	|

19+ 0	0.4863	0.06	Q				V
19+ 5	0.4867	0.06	Q				V
19+10	0.4872	0.07	Q				V
19+15	0.4877	0.07	Q				V
19+20	0.4883	0.08	Q				V
19+25	0.4889	0.09	Q				V
19+30	0.4896	0.10	Q				V
19+35	0.4902	0.09	Q				V
19+40	0.4908	0.08	Q				V
19+45	0.4913	0.08	Q				V
19+50	0.4918	0.07	Q				V
19+55	0.4922	0.06	Q				V
20+ 0	0.4926	0.06	Q				V
20+ 5	0.4930	0.06	Q				V
20+10	0.4935	0.07	Q				V
20+15	0.4940	0.07	Q				V
20+20	0.4945	0.07	Q				V
20+25	0.4950	0.08	Q				V
20+30	0.4956	0.08	Q				V
20+35	0.4961	0.08	Q				V
20+40	0.4966	0.08	Q				V
20+45	0.4971	0.08	Q				V
20+50	0.4976	0.07	Q				V
20+55	0.4980	0.06	Q				V
21+ 0	0.4984	0.05	Q				V
21+ 5	0.4988	0.06	Q				V
21+10	0.4993	0.07	Q				V
21+15	0.4998	0.07	Q				V
21+20	0.5003	0.07	Q				V
21+25	0.5007	0.06	Q				V
21+30	0.5010	0.05	Q				V
21+35	0.5014	0.06	Q				V
21+40	0.5019	0.07	Q				V
21+45	0.5024	0.07	Q				V
21+50	0.5029	0.07	Q				V
21+55	0.5033	0.06	Q				V
22+ 0	0.5037	0.05	Q				V
22+ 5	0.5041	0.06	Q				V
22+10	0.5046	0.07	Q				V
22+15	0.5051	0.07	Q				V
22+20	0.5055	0.07	Q				V
22+25	0.5059	0.06	Q				V
22+30	0.5063	0.05	Q				V
22+35	0.5067	0.05	Q				V
22+40	0.5070	0.05	Q				V
22+45	0.5074	0.05	Q				V
22+50	0.5077	0.05	Q				V
22+55	0.5081	0.05	Q				V
23+ 0	0.5084	0.05	Q				V
23+ 5	0.5088	0.05	Q				V
23+10	0.5091	0.05	Q				V
23+15	0.5095	0.05	Q				V
23+20	0.5098	0.05	Q				V
23+25	0.5102	0.05	Q				V
23+30	0.5105	0.05	Q				V
23+35	0.5109	0.05	Q				V
23+40	0.5112	0.05	Q				V
23+45	0.5116	0.05	Q				V
23+50	0.5119	0.05	Q				V
23+55	0.5123	0.05	Q				V
24+ 0	0.5126	0.05	Q				V
24+ 5	0.5129	0.04	Q				V
24+10	0.5130	0.01	Q				V
24+15	0.5131	0.01	Q				V
24+20	0.5131	0.00	Q				V
24+25	0.5131	0.00	Q				V
24+30	0.5131	0.00	Q				V
24+35	0.5131	0.00	Q				V

APPENDIX C.2: AREA "C" – OFFSITE

100-YEAR, 1-HOUR

U n i t H y d r o g r a p h A n a l y s i s

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Study date 11/16/20 File: ARAEX1100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6279

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

HEMET 30 EXISTING CONDITION HYDROLOGY
UNIT HYDROGRAPH ANALYSIS, 100-YEAR STORM EVENT
FILENAME: ARAEX

Drainage Area = 176.14(Ac.) = 0.275 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 176.14(Ac.) = 0.275 Sq. Mi.
USER Entry of lag time in hours
Lag time = 0.288 Hr.
Lag time = 17.26 Min.
25% of lag time = 4.31 Min.
40% of lag time = 6.90 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
176.14	0.50	88.07

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
176.14	1.20	211.37

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 0.500(In)
Area Averaged 100-Year Rainfall = 1.200(In)

Point rain (area averaged) = 1.200(In)
Areal adjustment factor = 99.84 %
Adjusted average point rain = 1.198(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
176.140	81.20	0.000

Total Area Entered = 176.14(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
81.2	81.2	0.230	0.000	0.230	1.000	0.230
					Sum (F) =	0.230

Area averaged mean soil loss (F) (In/Hr) = 0.230
Minimum soil loss rate ((In/Hr)) = 0.115
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

Slope of intensity-duration curve for a 1 hour storm =0.5300

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	28.975	2.769	4.915
2	0.167	57.951	9.976	17.709
3	0.250	86.926	17.568	31.187
4	0.333	115.902	19.860	35.254
5	0.417	144.877	13.403	23.792
6	0.500	173.853	7.782	13.814
7	0.583	202.828	4.913	8.721
8	0.667	231.803	3.792	6.731
9	0.750	260.779	3.043	5.402
10	0.833	289.754	2.558	4.541
11	0.917	318.730	2.069	3.674
12	1.000	347.705	1.760	3.125
13	1.083	376.681	1.542	2.737
14	1.167	405.656	1.270	2.254
15	1.250	434.631	1.040	1.846
16	1.333	463.607	0.921	1.635
17	1.417	492.582	0.877	1.558
18	1.500	521.558	0.805	1.429
19	1.583	550.533	0.645	1.145
20	1.667	579.509	0.577	1.025
21	1.750	608.484	0.517	0.917
22	1.833	637.459	0.435	0.772
23	1.917	666.435	0.387	0.687
24	2.000	695.410	0.301	0.534
25	2.083	724.386	0.290	0.514
26	2.167	753.361	0.290	0.514
27	2.250	782.337	0.290	0.514
28	2.333	811.312	0.322	0.571
			Sum = 100.000	Sum= 177.516

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.40	0.489	0.230	(0.440)	0.258
2	0.17	4.70	0.676	0.230	(0.608)	0.445
3	0.25	4.70	0.676	0.230	(0.608)	0.445
4	0.33	5.10	0.733	0.230	(0.660)	0.503
5	0.42	5.80	0.834	0.230	(0.750)	0.604
6	0.50	5.90	0.848	0.230	(0.763)	0.618
7	0.58	7.10	1.021	0.230	(0.919)	0.790
8	0.67	8.70	1.251	0.230	(1.126)	1.020
9	0.75	13.20	1.898	0.230	(1.708)	1.667
10	0.83	29.70	4.270	0.230	(3.843)	4.040
11	0.92	7.70	1.107	0.230	(0.996)	0.877
12	1.00	4.00	0.575	0.230	(0.518)	0.345
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	11.6

Flood volume = Effective rainfall 0.97(In)
times area 176.1(Ac.)/[(In)/(Ft.)] = 14.2(Ac.Ft)
Total soil loss = 0.23(In)
Total soil loss = 3.381(Ac.Ft)

```
      Total rainfall =      1.20(In)
      Flood volume =      618777.2 Cubic Feet
      Total soil loss =      147263.9 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =    253.953(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          1 - H O U R    S T O R M
                     R u n o f f     H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0       75.0     150.0     225.0     300.0
 ---------------------------------------------------------------------------
   0+ 5       0.0088      1.27  Q         |         |         |         |
   0+10       0.0554      6.77  Q         |         |         |         |
   0+15       0.1804     18.15  V Q       |         |         |         |
   0+20       0.4103     33.38  |V  Q     |         |         |         |
   0+25       0.7384     47.64  | V   Q   |         |         |         |
   0+30       1.1468     59.31  |  V   Q  |         |         |         |
   0+35       1.6318     70.42  |   V    Q|         |         |         |
   0+40       2.2058     83.35  |     V   |Q        |         |         |
   0+45       2.9107    102.34  |       V |  Q      |         |         |
   0+50       3.8966    143.15  |         V       Q|         |         |
   0+55       5.3105    205.30  |         |   V     |      Q  |         |
   1+ 0       7.0595    253.95  |         |        V|         |  Q      |
   1+ 5       8.7819    250.09  |         |         |   V     |  Q      |
   1+10      10.0645    186.24  |         |         |   Q   V |         |
   1+15      10.9175    123.86  |         |     Q   |         V         |
   1+20      11.4939     83.69  |         |Q        |         | V       |
   1+25      11.9268     62.85  |       Q |         |         |  V      |
   1+30      12.2733     50.32  |     Q   |         |         |   V     |
   1+35      12.5616     41.86  |    Q    |         |         |    V    |
   1+40      12.8013     34.81  |   Q     |         |         |     V   |
   1+45      13.0053     29.62  |  Q      |         |         |     V   |
   1+50      13.1808     25.48  |  Q      |         |         |      V  |
   1+55      13.3295     21.59  | Q       |         |         |      V  |
   2+ 0      13.4562     18.41  | Q       |         |         |      V  |
   2+ 5      13.5679     16.22  | Q       |         |         |       V |
   2+10      13.6692     14.71  |Q        |         |         |       V |
   2+15      13.7597     13.14  |Q        |         |         |       V |
   2+20      13.8374     11.29  |Q        |         |         |       V |
   2+25      13.9055      9.88  |Q        |         |         |        V|
   2+30      13.9644      8.55  |Q        |         |         |        V|
   2+35      14.0146      7.29  Q         |         |         |        V|
   2+40      14.0577      6.25  Q         |         |         |        V|
   2+45      14.0933      5.17  Q         |         |         |        V|
   2+50      14.1251      4.62  Q         |         |         |        V|
   2+55      14.1537      4.15  Q         |         |         |        V|
   3+ 0      14.1789      3.66  Q         |         |         |        V|
   3+ 5      14.1991      2.94  Q         |         |         |        V|
   3+10      14.2038      0.68  Q         |         |         |        V|
   3+15      14.2052      0.20  Q         |         |         |         V
---------------------------------------------------------------------------
```

APPENDIX D: POST-PROJECT CONDITION UNIT HYDROGRAPH HYDROLOGY

APPENDIX D.1: AREA "A" – ONSITE

2-YEAR, 24-HOUR

U n i t H y d r o g r a p h A n a l y s i s

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Study date 10/23/21 File: ARA1POST242.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

TRI-8 Builders - S/N 615

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

150.10.18
UNIT HYDROGRAPH FOR BASIN NODE 118.1
POST-PROJECT CONDITION
FN: ARA1POST.UNRIV

Drainage Area = 22.97(Ac.) = 0.036 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 22.97(Ac.) = 0.036 Sq. Mi.
Length along longest watercourse = 1744.00(Ft.)
Length along longest watercourse measured to centroid = 446.00(Ft.)
Length along longest watercourse = 0.330 Mi.
Length along longest watercourse measured to centroid = 0.084 Mi.
Difference in elevation = 40.50(Ft.)
Slope along watercourse = 122.6147 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.037 Hr.
Lag time = 2.22 Min.
25% of lag time = 0.56 Min.
40% of lag time = 0.89 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
22.97	1.70	39.05

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
22.97	4.25	97.62

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.700(In)
Area Averaged 100-Year Rainfall = 4.250(In)

Point rain (area averaged) = 1.700(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.700(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
22.970	63.10	0.576

Total Area Entered = 22.97(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
63.1	43.1	0.640	0.576	0.308	1.000	0.308
					Sum (F) =	0.308

Area averaged mean soil loss (F) (In/Hr) = 0.308
Minimum soil loss rate ((In/Hr)) = 0.154
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.439

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	224.909	47.399	10.973
2	0.167	449.817	41.666	9.645
3	0.250	674.726	7.867	1.821
4	0.333	899.635	3.068	0.710
			Sum = 100.000	Sum= 23.149

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.014	0.546	0.006	0.01
2	0.17	0.07	0.014	0.544	0.006	0.01
3	0.25	0.07	0.014	0.542	0.006	0.01
4	0.33	0.10	0.020	0.540	0.009	0.01
5	0.42	0.10	0.020	0.538	0.009	0.01
6	0.50	0.10	0.020	0.536	0.009	0.01
7	0.58	0.10	0.020	0.533	0.009	0.01
8	0.67	0.10	0.020	0.531	0.009	0.01
9	0.75	0.10	0.020	0.529	0.009	0.01
10	0.83	0.13	0.027	0.527	0.012	0.02
11	0.92	0.13	0.027	0.525	0.012	0.02
12	1.00	0.13	0.027	0.523	0.012	0.02
13	1.08	0.10	0.020	0.521	0.009	0.01
14	1.17	0.10	0.020	0.519	0.009	0.01
15	1.25	0.10	0.020	0.517	0.009	0.01
16	1.33	0.10	0.020	0.515	0.009	0.01
17	1.42	0.10	0.020	0.513	0.009	0.01
18	1.50	0.10	0.020	0.511	0.009	0.01
19	1.58	0.10	0.020	0.509	0.009	0.01
20	1.67	0.10	0.020	0.507	0.009	0.01
21	1.75	0.10	0.020	0.505	0.009	0.01
22	1.83	0.13	0.027	0.503	0.012	0.02
23	1.92	0.13	0.027	0.501	0.012	0.02
24	2.00	0.13	0.027	0.499	0.012	0.02
25	2.08	0.13	0.027	0.497	0.012	0.02
26	2.17	0.13	0.027	0.495	0.012	0.02
27	2.25	0.13	0.027	0.493	0.012	0.02
28	2.33	0.13	0.027	0.490	0.012	0.02
29	2.42	0.13	0.027	0.488	0.012	0.02
30	2.50	0.13	0.027	0.487	0.012	0.02
31	2.58	0.17	0.034	0.485	0.015	0.02
32	2.67	0.17	0.034	0.483	0.015	0.02
33	2.75	0.17	0.034	0.481	0.015	0.02
34	2.83	0.17	0.034	0.479	0.015	0.02
35	2.92	0.17	0.034	0.477	0.015	0.02
36	3.00	0.17	0.034	0.475	0.015	0.02
37	3.08	0.17	0.034	0.473	0.015	0.02
38	3.17	0.17	0.034	0.471	0.015	0.02
39	3.25	0.17	0.034	0.469	0.015	0.02
40	3.33	0.17	0.034	0.467	0.015	0.02
41	3.42	0.17	0.034	0.465	0.015	0.02
42	3.50	0.17	0.034	0.463	0.015	0.02

43	3.58	0.17	0.034	0.461	0.015	0.02
44	3.67	0.17	0.034	0.459	0.015	0.02
45	3.75	0.17	0.034	0.457	0.015	0.02
46	3.83	0.20	0.041	0.455	0.018	0.02
47	3.92	0.20	0.041	0.453	0.018	0.02
48	4.00	0.20	0.041	0.451	0.018	0.02
49	4.08	0.20	0.041	0.449	0.018	0.02
50	4.17	0.20	0.041	0.447	0.018	0.02
51	4.25	0.20	0.041	0.446	0.018	0.02
52	4.33	0.23	0.048	0.444	0.021	0.03
53	4.42	0.23	0.048	0.442	0.021	0.03
54	4.50	0.23	0.048	0.440	0.021	0.03
55	4.58	0.23	0.048	0.438	0.021	0.03
56	4.67	0.23	0.048	0.436	0.021	0.03
57	4.75	0.23	0.048	0.434	0.021	0.03
58	4.83	0.27	0.054	0.432	0.024	0.03
59	4.92	0.27	0.054	0.431	0.024	0.03
60	5.00	0.27	0.054	0.429	0.024	0.03
61	5.08	0.20	0.041	0.427	0.018	0.02
62	5.17	0.20	0.041	0.425	0.018	0.02
63	5.25	0.20	0.041	0.423	0.018	0.02
64	5.33	0.23	0.048	0.421	0.021	0.03
65	5.42	0.23	0.048	0.419	0.021	0.03
66	5.50	0.23	0.048	0.418	0.021	0.03
67	5.58	0.27	0.054	0.416	0.024	0.03
68	5.67	0.27	0.054	0.414	0.024	0.03
69	5.75	0.27	0.054	0.412	0.024	0.03
70	5.83	0.27	0.054	0.410	0.024	0.03
71	5.92	0.27	0.054	0.408	0.024	0.03
72	6.00	0.27	0.054	0.407	0.024	0.03
73	6.08	0.30	0.061	0.405	0.027	0.03
74	6.17	0.30	0.061	0.403	0.027	0.03
75	6.25	0.30	0.061	0.401	0.027	0.03
76	6.33	0.30	0.061	0.399	0.027	0.03
77	6.42	0.30	0.061	0.398	0.027	0.03
78	6.50	0.30	0.061	0.396	0.027	0.03
79	6.58	0.33	0.068	0.394	0.030	0.04
80	6.67	0.33	0.068	0.392	0.030	0.04
81	6.75	0.33	0.068	0.391	0.030	0.04
82	6.83	0.33	0.068	0.389	0.030	0.04
83	6.92	0.33	0.068	0.387	0.030	0.04
84	7.00	0.33	0.068	0.385	0.030	0.04
85	7.08	0.33	0.068	0.383	0.030	0.04
86	7.17	0.33	0.068	0.382	0.030	0.04
87	7.25	0.33	0.068	0.380	0.030	0.04
88	7.33	0.37	0.075	0.378	0.033	0.04
89	7.42	0.37	0.075	0.377	0.033	0.04
90	7.50	0.37	0.075	0.375	0.033	0.04
91	7.58	0.40	0.082	0.373	0.036	0.05
92	7.67	0.40	0.082	0.371	0.036	0.05
93	7.75	0.40	0.082	0.370	0.036	0.05
94	7.83	0.43	0.088	0.368	0.039	0.05
95	7.92	0.43	0.088	0.366	0.039	0.05
96	8.00	0.43	0.088	0.365	0.039	0.05
97	8.08	0.50	0.102	0.363	0.045	0.06
98	8.17	0.50	0.102	0.361	0.045	0.06
99	8.25	0.50	0.102	0.359	0.045	0.06
100	8.33	0.50	0.102	0.358	0.045	0.06
101	8.42	0.50	0.102	0.356	0.045	0.06
102	8.50	0.50	0.102	0.354	0.045	0.06
103	8.58	0.53	0.109	0.353	0.048	0.06
104	8.67	0.53	0.109	0.351	0.048	0.06
105	8.75	0.53	0.109	0.349	0.048	0.06
106	8.83	0.57	0.116	0.348	0.051	0.06
107	8.92	0.57	0.116	0.346	0.051	0.06
108	9.00	0.57	0.116	0.345	0.051	0.06
109	9.08	0.63	0.129	0.343	0.057	0.07
110	9.17	0.63	0.129	0.341	0.057	0.07
111	9.25	0.63	0.129	0.340	0.057	0.07
112	9.33	0.67	0.136	0.338	0.060	0.08
113	9.42	0.67	0.136	0.336	0.060	0.08

114	9.50	0.67	0.136	0.335	0.060	0.08
115	9.58	0.70	0.143	0.333	0.063	0.08
116	9.67	0.70	0.143	0.332	0.063	0.08
117	9.75	0.70	0.143	0.330	0.063	0.08
118	9.83	0.73	0.150	0.328	0.066	0.08
119	9.92	0.73	0.150	0.327	0.066	0.08
120	10.00	0.73	0.150	0.325	0.066	0.08
121	10.08	0.50	0.102	0.324	0.045	0.06
122	10.17	0.50	0.102	0.322	0.045	0.06
123	10.25	0.50	0.102	0.321	0.045	0.06
124	10.33	0.50	0.102	0.319	0.045	0.06
125	10.42	0.50	0.102	0.317	0.045	0.06
126	10.50	0.50	0.102	0.316	0.045	0.06
127	10.58	0.67	0.136	0.314	0.060	0.08
128	10.67	0.67	0.136	0.313	0.060	0.08
129	10.75	0.67	0.136	0.311	0.060	0.08
130	10.83	0.67	0.136	0.310	0.060	0.08
131	10.92	0.67	0.136	0.308	0.060	0.08
132	11.00	0.67	0.136	0.307	0.060	0.08
133	11.08	0.63	0.129	0.305	0.057	0.07
134	11.17	0.63	0.129	0.304	0.057	0.07
135	11.25	0.63	0.129	0.302	0.057	0.07
136	11.33	0.63	0.129	0.301	0.057	0.07
137	11.42	0.63	0.129	0.299	0.057	0.07
138	11.50	0.63	0.129	0.298	0.057	0.07
139	11.58	0.57	0.116	0.296	0.051	0.06
140	11.67	0.57	0.116	0.295	0.051	0.06
141	11.75	0.57	0.116	0.293	0.051	0.06
142	11.83	0.60	0.122	0.292	0.054	0.07
143	11.92	0.60	0.122	0.290	0.054	0.07
144	12.00	0.60	0.122	0.289	0.054	0.07
145	12.08	0.83	0.170	0.288	0.075	0.10
146	12.17	0.83	0.170	0.286	0.075	0.10
147	12.25	0.83	0.170	0.285	0.075	0.10
148	12.33	0.87	0.177	0.283	0.078	0.10
149	12.42	0.87	0.177	0.282	0.078	0.10
150	12.50	0.87	0.177	0.280	0.078	0.10
151	12.58	0.93	0.190	0.279	0.084	0.11
152	12.67	0.93	0.190	0.278	0.084	0.11
153	12.75	0.93	0.190	0.276	0.084	0.11
154	12.83	0.97	0.197	0.275	0.087	0.11
155	12.92	0.97	0.197	0.273	0.087	0.11
156	13.00	0.97	0.197	0.272	0.087	0.11
157	13.08	1.13	0.231	0.271	0.102	0.13
158	13.17	1.13	0.231	0.269	0.102	0.13
159	13.25	1.13	0.231	0.268	0.102	0.13
160	13.33	1.13	0.231	0.267	0.102	0.13
161	13.42	1.13	0.231	0.265	0.102	0.13
162	13.50	1.13	0.231	0.264	0.102	0.13
163	13.58	0.77	0.156	0.263	0.069	0.09
164	13.67	0.77	0.156	0.261	0.069	0.09
165	13.75	0.77	0.156	0.260	0.069	0.09
166	13.83	0.77	0.156	0.259	0.069	0.09
167	13.92	0.77	0.156	0.257	0.069	0.09
168	14.00	0.77	0.156	0.256	0.069	0.09
169	14.08	0.90	0.184	0.255	0.081	0.10
170	14.17	0.90	0.184	0.253	0.081	0.10
171	14.25	0.90	0.184	0.252	0.081	0.10
172	14.33	0.87	0.177	0.251	0.078	0.10
173	14.42	0.87	0.177	0.249	0.078	0.10
174	14.50	0.87	0.177	0.248	0.078	0.10
175	14.58	0.87	0.177	0.247	0.078	0.10
176	14.67	0.87	0.177	0.246	0.078	0.10
177	14.75	0.87	0.177	0.244	0.078	0.10
178	14.83	0.83	0.170	0.243	0.075	0.10
179	14.92	0.83	0.170	0.242	0.075	0.10
180	15.00	0.83	0.170	0.241	0.075	0.10
181	15.08	0.80	0.163	0.239	0.072	0.09
182	15.17	0.80	0.163	0.238	0.072	0.09
183	15.25	0.80	0.163	0.237	0.072	0.09
184	15.33	0.77	0.156	0.236	0.069	0.09

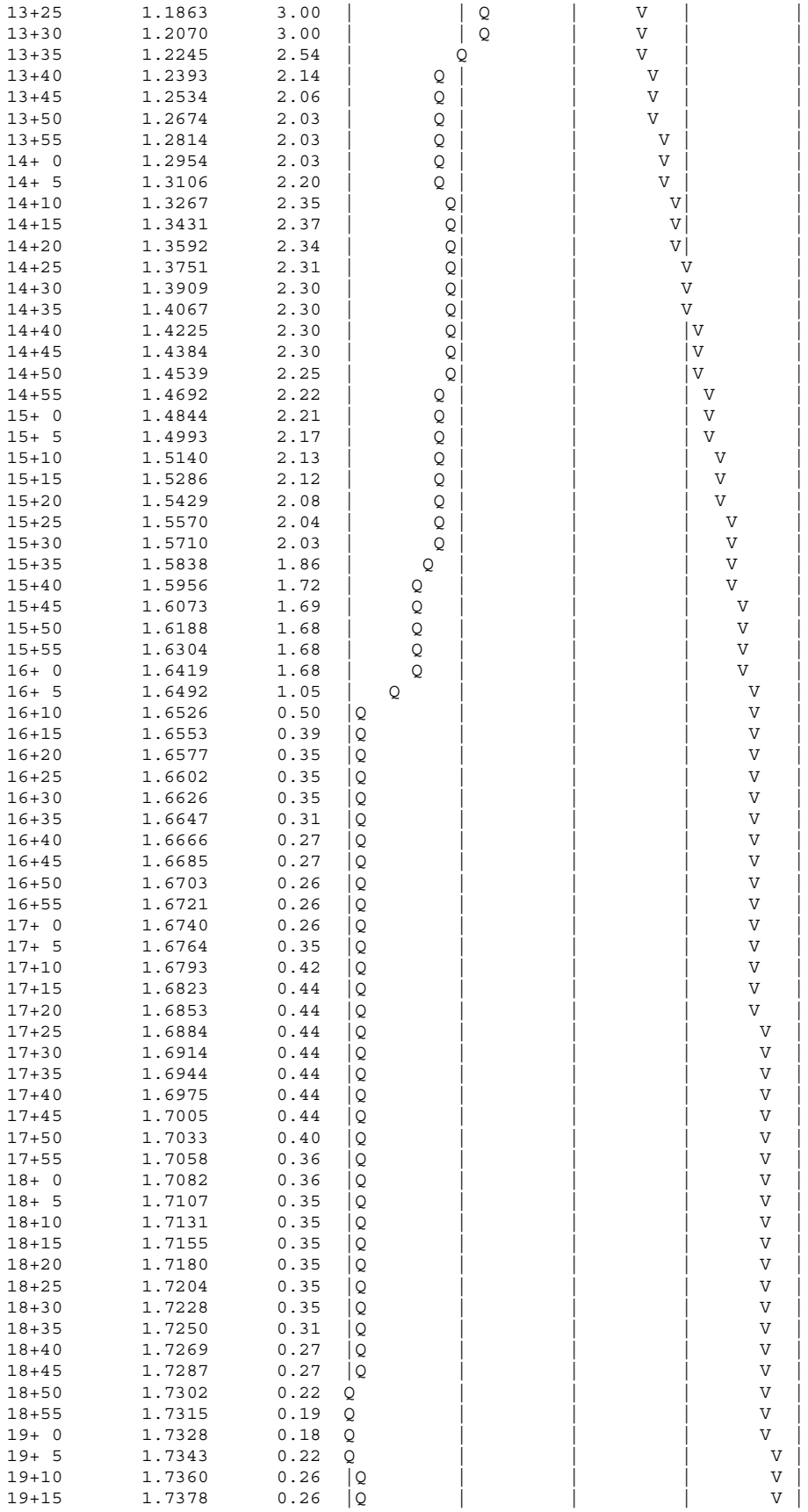
185	15.42	0.77	0.156	0.234	0.069	0.09
186	15.50	0.77	0.156	0.233	0.069	0.09
187	15.58	0.63	0.129	0.232	0.057	0.07
188	15.67	0.63	0.129	0.231	0.057	0.07
189	15.75	0.63	0.129	0.230	0.057	0.07
190	15.83	0.63	0.129	0.229	0.057	0.07
191	15.92	0.63	0.129	0.227	0.057	0.07
192	16.00	0.63	0.129	0.226	0.057	0.07
193	16.08	0.13	0.027	0.225	0.012	0.02
194	16.17	0.13	0.027	0.224	0.012	0.02
195	16.25	0.13	0.027	0.223	0.012	0.02
196	16.33	0.13	0.027	0.222	0.012	0.02
197	16.42	0.13	0.027	0.220	0.012	0.02
198	16.50	0.13	0.027	0.219	0.012	0.02
199	16.58	0.10	0.020	0.218	0.009	0.01
200	16.67	0.10	0.020	0.217	0.009	0.01
201	16.75	0.10	0.020	0.216	0.009	0.01
202	16.83	0.10	0.020	0.215	0.009	0.01
203	16.92	0.10	0.020	0.214	0.009	0.01
204	17.00	0.10	0.020	0.213	0.009	0.01
205	17.08	0.17	0.034	0.212	0.015	0.02
206	17.17	0.17	0.034	0.211	0.015	0.02
207	17.25	0.17	0.034	0.210	0.015	0.02
208	17.33	0.17	0.034	0.209	0.015	0.02
209	17.42	0.17	0.034	0.207	0.015	0.02
210	17.50	0.17	0.034	0.206	0.015	0.02
211	17.58	0.17	0.034	0.205	0.015	0.02
212	17.67	0.17	0.034	0.204	0.015	0.02
213	17.75	0.17	0.034	0.203	0.015	0.02
214	17.83	0.13	0.027	0.202	0.012	0.02
215	17.92	0.13	0.027	0.201	0.012	0.02
216	18.00	0.13	0.027	0.200	0.012	0.02
217	18.08	0.13	0.027	0.199	0.012	0.02
218	18.17	0.13	0.027	0.198	0.012	0.02
219	18.25	0.13	0.027	0.197	0.012	0.02
220	18.33	0.13	0.027	0.196	0.012	0.02
221	18.42	0.13	0.027	0.196	0.012	0.02
222	18.50	0.13	0.027	0.195	0.012	0.02
223	18.58	0.10	0.020	0.194	0.009	0.01
224	18.67	0.10	0.020	0.193	0.009	0.01
225	18.75	0.10	0.020	0.192	0.009	0.01
226	18.83	0.07	0.014	0.191	0.006	0.01
227	18.92	0.07	0.014	0.190	0.006	0.01
228	19.00	0.07	0.014	0.189	0.006	0.01
229	19.08	0.10	0.020	0.188	0.009	0.01
230	19.17	0.10	0.020	0.187	0.009	0.01
231	19.25	0.10	0.020	0.186	0.009	0.01
232	19.33	0.13	0.027	0.186	0.012	0.02
233	19.42	0.13	0.027	0.185	0.012	0.02
234	19.50	0.13	0.027	0.184	0.012	0.02
235	19.58	0.10	0.020	0.183	0.009	0.01
236	19.67	0.10	0.020	0.182	0.009	0.01
237	19.75	0.10	0.020	0.181	0.009	0.01
238	19.83	0.07	0.014	0.180	0.006	0.01
239	19.92	0.07	0.014	0.180	0.006	0.01
240	20.00	0.07	0.014	0.179	0.006	0.01
241	20.08	0.10	0.020	0.178	0.009	0.01
242	20.17	0.10	0.020	0.177	0.009	0.01
243	20.25	0.10	0.020	0.177	0.009	0.01
244	20.33	0.10	0.020	0.176	0.009	0.01
245	20.42	0.10	0.020	0.175	0.009	0.01
246	20.50	0.10	0.020	0.174	0.009	0.01
247	20.58	0.10	0.020	0.174	0.009	0.01
248	20.67	0.10	0.020	0.173	0.009	0.01
249	20.75	0.10	0.020	0.172	0.009	0.01
250	20.83	0.07	0.014	0.171	0.006	0.01
251	20.92	0.07	0.014	0.171	0.006	0.01
252	21.00	0.07	0.014	0.170	0.006	0.01
253	21.08	0.10	0.020	0.169	0.009	0.01
254	21.17	0.10	0.020	0.169	0.009	0.01
255	21.25	0.10	0.020	0.168	0.009	0.01

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256  21.33     0.07      0.014         0.167     0.006         0.01
257  21.42     0.07      0.014         0.167     0.006         0.01
258  21.50     0.07      0.014         0.166     0.006         0.01
259  21.58     0.10      0.020         0.166     0.009         0.01
260  21.67     0.10      0.020         0.165     0.009         0.01
261  21.75     0.10      0.020         0.164     0.009         0.01
262  21.83     0.07      0.014         0.164     0.006         0.01
263  21.92     0.07      0.014         0.163     0.006         0.01
264  22.00     0.07      0.014         0.163     0.006         0.01
265  22.08     0.10      0.020         0.162     0.009         0.01
266  22.17     0.10      0.020         0.162     0.009         0.01
267  22.25     0.10      0.020         0.161     0.009         0.01
268  22.33     0.07      0.014         0.161     0.006         0.01
269  22.42     0.07      0.014         0.160     0.006         0.01
270  22.50     0.07      0.014         0.160     0.006         0.01
271  22.58     0.07      0.014         0.159     0.006         0.01
272  22.67     0.07      0.014         0.159     0.006         0.01
273  22.75     0.07      0.014         0.158     0.006         0.01
274  22.83     0.07      0.014         0.158     0.006         0.01
275  22.92     0.07      0.014         0.157     0.006         0.01
276  23.00     0.07      0.014         0.157     0.006         0.01
277  23.08     0.07      0.014         0.157     0.006         0.01
278  23.17     0.07      0.014         0.156     0.006         0.01
279  23.25     0.07      0.014         0.156     0.006         0.01
280  23.33     0.07      0.014         0.156     0.006         0.01
281  23.42     0.07      0.014         0.155     0.006         0.01
282  23.50     0.07      0.014         0.155     0.006         0.01
283  23.58     0.07      0.014         0.155     0.006         0.01
284  23.67     0.07      0.014         0.155     0.006         0.01
285  23.75     0.07      0.014         0.154     0.006         0.01
286  23.83     0.07      0.014         0.154     0.006         0.01
287  23.92     0.07      0.014         0.154     0.006         0.01
288  24.00     0.07      0.014         0.154     0.006         0.01
    Sum =     100.0                                 Sum =     11.4
      Flood volume = Effective rainfall      0.95(In)
       times area      23.0(Ac.)/[(In)/(Ft.)] =       1.8(Ac.Ft)
      Total soil loss =      0.75(In)
      Total soil loss =     1.429(Ac.Ft)
      Total rainfall =      1.70(In)
      Flood volume =       79488.6 Cubic Feet
      Total soil loss =       62252.9 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      3.003(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ---------------------------------------------------------------------------
   0+ 5       0.0006      0.08  Q         |         |         |         |
   0+10       0.0017      0.16  Q         |         |         |         |
   0+15       0.0028      0.17  Q         |         |         |         |
   0+20       0.0043      0.22  Q         |         |         |         |
   0+25       0.0061      0.26  VQ        |         |         |         |
   0+30       0.0079      0.26  VQ        |         |         |         |
   0+35       0.0097      0.26  VQ        |         |         |         |
   0+40       0.0116      0.26  VQ        |         |         |         |
   0+45       0.0134      0.26  VQ        |         |         |         |
   0+50       0.0155      0.31  VQ        |         |         |         |
   0+55       0.0179      0.34  VQ        |         |         |         |
   1+ 0       0.0203      0.35  VQ        |         |         |         |
   1+ 5       0.0224      0.31  VQ        |         |         |         |
   1+10       0.0243      0.27  VQ        |         |         |         |
   1+15       0.0262      0.27  VQ        |         |         |         |
   1+20       0.0280      0.26  VQ        |         |         |         |
   1+25       0.0298      0.26  VQ        |         |         |         |
   1+30       0.0316      0.26  VQ        |         |         |         |
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1+35	0.0335	0.26	VQ	|	|	|	|
1+40	0.0353	0.26	VQ	|	|	|	|
1+45	0.0371	0.26	VQ	|	|	|	|
1+50	0.0392	0.31	VQ	|	|	|	|
1+55	0.0416	0.34	VQ	|	|	|	|
2+ 0	0.0440	0.35	VQ	|	|	|	|
2+ 5	0.0464	0.35	|Q	|	|	|	|
2+10	0.0489	0.35	|Q	|	|	|	|
2+15	0.0513	0.35	|Q	|	|	|	|
2+20	0.0537	0.35	|Q	|	|	|	|
2+25	0.0562	0.35	|Q	|	|	|	|
2+30	0.0586	0.35	|Q	|	|	|	|
2+35	0.0613	0.40	|Q	|	|	|	|
2+40	0.0643	0.43	|Q	|	|	|	|
2+45	0.0673	0.44	|Q	|	|	|	|
2+50	0.0704	0.44	|Q	|	|	|	|
2+55	0.0734	0.44	|Q	|	|	|	|
3+ 0	0.0764	0.44	|Q	|	|	|	|
3+ 5	0.0795	0.44	|Q	|	|	|	|
3+10	0.0825	0.44	|Q	|	|	|	|
3+15	0.0856	0.44	|Q	|	|	|	|
3+20	0.0886	0.44	|Q	|	|	|	|
3+25	0.0916	0.44	|QV	|	|	|	|
3+30	0.0947	0.44	|QV	|	|	|	|
3+35	0.0977	0.44	|QV	|	|	|	|
3+40	0.1008	0.44	|QV	|	|	|	|
3+45	0.1038	0.44	|QV	|	|	|	|
3+50	0.1071	0.48	|QV	|	|	|	|
3+55	0.1107	0.52	| Q	|	|	|	|
4+ 0	0.1144	0.53	| Q	|	|	|	|
4+ 5	0.1180	0.53	| Q	|	|	|	|
4+10	0.1217	0.53	| Q	|	|	|	|
4+15	0.1253	0.53	| Q	|	|	|	|
4+20	0.1292	0.57	| Q	|	|	|	|
4+25	0.1334	0.61	| Q	|	|	|	|
4+30	0.1377	0.62	| QV	|	|	|	|
4+35	0.1419	0.62	| QV	|	|	|	|
4+40	0.1462	0.62	| QV	|	|	|	|
4+45	0.1504	0.62	| QV	|	|	|	|
4+50	0.1550	0.66	| QV	|	|	|	|
4+55	0.1598	0.70	| QV	|	|	|	|
5+ 0	0.1646	0.70	| QV	|	|	|	|
5+ 5	0.1689	0.62	| QV	|	|	|	|
5+10	0.1727	0.55	| QV	|	|	|	|
5+15	0.1764	0.54	| QV	|	|	|	|
5+20	0.1803	0.57	| QV	|	|	|	|
5+25	0.1845	0.61	| Q V	|	|	|	|
5+30	0.1888	0.62	| Q V	|	|	|	|
5+35	0.1933	0.66	| Q V	|	|	|	|
5+40	0.1981	0.70	| Q V	|	|	|	|
5+45	0.2030	0.70	| Q V	|	|	|	|
5+50	0.2078	0.71	| Q V	|	|	|	|
5+55	0.2127	0.71	| Q V	|	|	|	|
6+ 0	0.2176	0.71	| Q V	|	|	|	|
6+ 5	0.2227	0.75	| Q V	|	|	|	|
6+10	0.2281	0.79	| Q V	|	|	|	|
6+15	0.2336	0.79	| Q V	|	|	|	|
6+20	0.2391	0.79	| Q V	|	|	|	|
6+25	0.2445	0.79	| Q V	|	|	|	|
6+30	0.2500	0.79	| Q V	|	|	|	|
6+35	0.2558	0.84	| Q V	|	|	|	|
6+40	0.2618	0.87	| Q V	|	|	|	|
6+45	0.2678	0.88	| Q V	|	|	|	|
6+50	0.2739	0.88	| Q V	|	|	|	|
6+55	0.2800	0.88	| Q V	|	|	|	|
7+ 0	0.2861	0.88	| Q V	|	|	|	|
7+ 5	0.2922	0.88	| Q V	|	|	|	|
7+10	0.2983	0.88	| Q V	|	|	|	|
7+15	0.3043	0.88	| Q V	|	|	|	|
7+20	0.3107	0.93	| Q V	|	|	|	|
7+25	0.3173	0.96	| Q V	|	|	|	|

7+30	0.3240	0.97	Q V				
7+35	0.3310	1.01	Q V				
7+40	0.3382	1.05	Q V				
7+45	0.3455	1.06	Q V				
7+50	0.3531	1.10	Q V				
7+55	0.3609	1.14	Q V				
8+ 0	0.3688	1.15	Q V				
8+ 5	0.3773	1.23	Q V				
8+10	0.3863	1.31	Q V				
8+15	0.3954	1.32	Q V				
8+20	0.4045	1.32	Q V				
8+25	0.4136	1.32	Q V				
8+30	0.4228	1.32	Q V				
8+35	0.4322	1.37	Q V				
8+40	0.4418	1.40	Q V				
8+45	0.4515	1.41	Q V				
8+50	0.4616	1.45	Q V				
8+55	0.4718	1.49	Q V				
9+ 0	0.4822	1.50	Q V				
9+ 5	0.4931	1.59	Q V				
9+10	0.5045	1.66	Q V				
9+15	0.5160	1.67	Q V				
9+20	0.5279	1.72	Q V				
9+25	0.5400	1.76	Q V				
9+30	0.5521	1.76	Q V				
9+35	0.5646	1.81	Q V				
9+40	0.5773	1.85	Q V				
9+45	0.5900	1.85	Q V				
9+50	0.6031	1.90	Q V				
9+55	0.6164	1.93	Q V				
10+ 0	0.6298	1.94	Q V				
10+ 5	0.6411	1.65	Q V				
10+10	0.6507	1.39	Q V				
10+15	0.6600	1.34	Q V				
10+20	0.6691	1.32	Q V				
10+25	0.6782	1.32	Q V				
10+30	0.6874	1.32	Q V				
10+35	0.6979	1.53	Q V				
10+40	0.7097	1.72	Q V				
10+45	0.7218	1.75	Q V				
10+50	0.7340	1.77	Q V				
10+55	0.7462	1.77	Q V				
11+ 0	0.7583	1.77	Q V				
11+ 5	0.7702	1.72	Q V				
11+10	0.7818	1.69	Q V				
11+15	0.7934	1.68	Q V				
11+20	0.8050	1.68	Q V				
11+25	0.8165	1.68	Q V				
11+30	0.8281	1.68	Q V				
11+35	0.8390	1.59	Q V				
11+40	0.8495	1.52	Q V				
11+45	0.8599	1.51	Q V				
11+50	0.8705	1.54	Q V				
11+55	0.8814	1.58	Q V				
12+ 0	0.8923	1.59	Q V				
12+ 5	0.9053	1.88	Q V				
12+10	0.9200	2.14	Q V				
12+15	0.9351	2.19	Q V				
12+20	0.9506	2.25	Q V				
12+25	0.9664	2.29	Q V				
12+30	0.9822	2.29	Q V				
12+35	0.9986	2.38	Q V				
12+40	1.0155	2.45	Q V				
12+45	1.0324	2.47	Q V				
12+50	1.0498	2.51	Q V				
12+55	1.0673	2.55	Q V				
13+ 0	1.0850	2.56	Q V				
13+ 5	1.1040	2.77	Q V				
13+10	1.1244	2.95	Q V				
13+15	1.1450	2.99	Q V				
13+20	1.1657	3.00	Q V				



13+25	1.1863	3.00	
13+30	1.2070	3.00	
13+35	1.2245	2.54	
13+40	1.2393	2.14	
13+45	1.2534	2.06	
13+50	1.2674	2.03	
13+55	1.2814	2.03	
14+ 0	1.2954	2.03	
14+ 5	1.3106	2.20	
14+10	1.3267	2.35	
14+15	1.3431	2.37	
14+20	1.3592	2.34	
14+25	1.3751	2.31	
14+30	1.3909	2.30	
14+35	1.4067	2.30	
14+40	1.4225	2.30	
14+45	1.4384	2.30	
14+50	1.4539	2.25	
14+55	1.4692	2.22	
15+ 0	1.4844	2.21	
15+ 5	1.4993	2.17	
15+10	1.5140	2.13	
15+15	1.5286	2.12	
15+20	1.5429	2.08	
15+25	1.5570	2.04	
15+30	1.5710	2.03	
15+35	1.5838	1.86	
15+40	1.5956	1.72	
15+45	1.6073	1.69	
15+50	1.6188	1.68	
15+55	1.6304	1.68	
16+ 0	1.6419	1.68	
16+ 5	1.6492	1.05	
16+10	1.6526	0.50	
16+15	1.6553	0.39	
16+20	1.6577	0.35	
16+25	1.6602	0.35	
16+30	1.6626	0.35	
16+35	1.6647	0.31	
16+40	1.6666	0.27	
16+45	1.6685	0.27	
16+50	1.6703	0.26	
16+55	1.6721	0.26	
17+ 0	1.6740	0.26	
17+ 5	1.6764	0.35	
17+10	1.6793	0.42	
17+15	1.6823	0.44	
17+20	1.6853	0.44	
17+25	1.6884	0.44	
17+30	1.6914	0.44	
17+35	1.6944	0.44	
17+40	1.6975	0.44	
17+45	1.7005	0.44	
17+50	1.7033	0.40	
17+55	1.7058	0.36	
18+ 0	1.7082	0.36	
18+ 5	1.7107	0.35	
18+10	1.7131	0.35	
18+15	1.7155	0.35	
18+20	1.7180	0.35	
18+25	1.7204	0.35	
18+30	1.7228	0.35	
18+35	1.7250	0.31	
18+40	1.7269	0.27	
18+45	1.7287	0.27	
18+50	1.7302	0.22	
18+55	1.7315	0.19	
19+ 0	1.7328	0.18	
19+ 5	1.7343	0.22	
19+10	1.7360	0.26	
19+15	1.7378	0.26	

19+20	1.7399	0.31	|Q	|	|	|	V |
19+25	1.7423	0.34	|Q	|	|	|	V |
19+30	1.7447	0.35	|Q	|	|	|	V |
19+35	1.7469	0.31	|Q	|	|	|	V |
19+40	1.7488	0.27	|Q	|	|	|	V |
19+45	1.7506	0.27	|Q	|	|	|	V |
19+50	1.7521	0.22	Q	|	|	|	V |
19+55	1.7534	0.19	Q	|	|	|	V |
20+ 0	1.7547	0.18	Q	|	|	|	V |
20+ 5	1.7562	0.22	Q	|	|	|	V |
20+10	1.7579	0.26	|Q	|	|	|	V |
20+15	1.7597	0.26	|Q	|	|	|	V |
20+20	1.7615	0.26	|Q	|	|	|	V |
20+25	1.7634	0.26	|Q	|	|	|	V |
20+30	1.7652	0.26	|Q	|	|	|	V |
20+35	1.7670	0.26	|Q	|	|	|	V |
20+40	1.7688	0.26	|Q	|	|	|	V |
20+45	1.7707	0.26	|Q	|	|	|	V |
20+50	1.7722	0.22	Q	|	|	|	V |
20+55	1.7735	0.19	Q	|	|	|	V |
21+ 0	1.7747	0.18	Q	|	|	|	V |
21+ 5	1.7762	0.22	Q	|	|	|	V |
21+10	1.7780	0.26	|Q	|	|	|	V |
21+15	1.7798	0.26	|Q	|	|	|	V|
21+20	1.7813	0.22	Q	|	|	|	V|
21+25	1.7826	0.19	Q	|	|	|	V|
21+30	1.7839	0.18	Q	|	|	|	V|
21+35	1.7854	0.22	Q	|	|	|	V|
21+40	1.7871	0.26	|Q	|	|	|	V|
21+45	1.7889	0.26	|Q	|	|	|	V|
21+50	1.7905	0.22	Q	|	|	|	V|
21+55	1.7917	0.19	Q	|	|	|	V|
22+ 0	1.7930	0.18	Q	|	|	|	V|
22+ 5	1.7945	0.22	Q	|	|	|	V|
22+10	1.7962	0.26	|Q	|	|	|	V|
22+15	1.7980	0.26	|Q	|	|	|	V|
22+20	1.7996	0.22	Q	|	|	|	V|
22+25	1.8009	0.19	Q	|	|	|	V|
22+30	1.8021	0.18	Q	|	|	|	V|
22+35	1.8033	0.18	Q	|	|	|	V|
22+40	1.8045	0.18	Q	|	|	|	V|
22+45	1.8057	0.18	Q	|	|	|	V|
22+50	1.8070	0.18	Q	|	|	|	V|
22+55	1.8082	0.18	Q	|	|	|	V|
23+ 0	1.8094	0.18	Q	|	|	|	V|
23+ 5	1.8106	0.18	Q	|	|	|	V|
23+10	1.8118	0.18	Q	|	|	|	V|
23+15	1.8130	0.18	Q	|	|	|	V|
23+20	1.8143	0.18	Q	|	|	|	V|
23+25	1.8155	0.18	Q	|	|	|	V|
23+30	1.8167	0.18	Q	|	|	|	V|
23+35	1.8179	0.18	Q	|	|	|	V|
23+40	1.8191	0.18	Q	|	|	|	V|
23+45	1.8203	0.18	Q	|	|	|	V|
23+50	1.8216	0.18	Q	|	|	|	V|
23+55	1.8228	0.18	Q	|	|	|	V|
24+ 0	1.8240	0.18	Q	|	|	|	V|
24+ 5	1.8246	0.09	Q	|	|	|	V|
24+10	1.8248	0.02	Q	|	|	|	V|
24+15	1.8248	0.01	Q	|	|	|	V|

10-YEAR, 24-HOUR

U n i t H y d r o g r a p h A n a l y s i s

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Study date 10/23/21 File: ARA1POST2410.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

TRI-8 Builders - S/N 615

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

150.10.18
UNIT HYDROGRAPH FOR BASIN NODE 118.1
POST-PROJECT CONDITION
FN: ARA1POST.UNRIV

Drainage Area = 22.97(Ac.) = 0.036 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 22.97(Ac.) = 0.036 Sq. Mi.
Length along longest watercourse = 1744.00(Ft.)
Length along longest watercourse measured to centroid = 446.00(Ft.)
Length along longest watercourse = 0.330 Mi.
Length along longest watercourse measured to centroid = 0.084 Mi.
Difference in elevation = 40.50(Ft.)
Slope along watercourse = 122.6147 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.037 Hr.
Lag time = 2.22 Min.
25% of lag time = 0.56 Min.
40% of lag time = 0.89 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
22.97	1.70	39.05

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
22.97	4.25	97.62

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.700(In)
Area Averaged 100-Year Rainfall = 4.250(In)

Point rain (area averaged) = 2.749(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 2.749(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
22.970	63.10	0.576

Total Area Entered = 22.97(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
63.1	63.1	0.437	0.576	0.210	1.000	0.210
					Sum (F) =	0.210

Area averaged mean soil loss (F) (In/Hr) = 0.210
Minimum soil loss rate ((In/Hr)) = 0.105
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.439

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	224.909	47.399	10.973
2	0.167	449.817	41.666	9.645
3	0.250	674.726	7.867	1.821
4	0.333	899.635	3.068	0.710
			Sum = 100.000	Sum= 23.149

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.022	0.373	0.010	0.01
2	0.17	0.07	0.022	0.371	0.010	0.01
3	0.25	0.07	0.022	0.370	0.010	0.01
4	0.33	0.10	0.033	0.368	0.014	0.02
5	0.42	0.10	0.033	0.367	0.014	0.02
6	0.50	0.10	0.033	0.365	0.014	0.02
7	0.58	0.10	0.033	0.364	0.014	0.02
8	0.67	0.10	0.033	0.363	0.014	0.02
9	0.75	0.10	0.033	0.361	0.014	0.02
10	0.83	0.13	0.044	0.360	0.019	0.02
11	0.92	0.13	0.044	0.358	0.019	0.02
12	1.00	0.13	0.044	0.357	0.019	0.02
13	1.08	0.10	0.033	0.356	0.014	0.02
14	1.17	0.10	0.033	0.354	0.014	0.02
15	1.25	0.10	0.033	0.353	0.014	0.02
16	1.33	0.10	0.033	0.351	0.014	0.02
17	1.42	0.10	0.033	0.350	0.014	0.02
18	1.50	0.10	0.033	0.349	0.014	0.02
19	1.58	0.10	0.033	0.347	0.014	0.02
20	1.67	0.10	0.033	0.346	0.014	0.02
21	1.75	0.10	0.033	0.344	0.014	0.02
22	1.83	0.13	0.044	0.343	0.019	0.02
23	1.92	0.13	0.044	0.342	0.019	0.02
24	2.00	0.13	0.044	0.340	0.019	0.02
25	2.08	0.13	0.044	0.339	0.019	0.02
26	2.17	0.13	0.044	0.337	0.019	0.02
27	2.25	0.13	0.044	0.336	0.019	0.02
28	2.33	0.13	0.044	0.335	0.019	0.02
29	2.42	0.13	0.044	0.333	0.019	0.02
30	2.50	0.13	0.044	0.332	0.019	0.02
31	2.58	0.17	0.055	0.331	0.024	0.03
32	2.67	0.17	0.055	0.329	0.024	0.03
33	2.75	0.17	0.055	0.328	0.024	0.03
34	2.83	0.17	0.055	0.327	0.024	0.03
35	2.92	0.17	0.055	0.325	0.024	0.03
36	3.00	0.17	0.055	0.324	0.024	0.03
37	3.08	0.17	0.055	0.323	0.024	0.03
38	3.17	0.17	0.055	0.321	0.024	0.03
39	3.25	0.17	0.055	0.320	0.024	0.03
40	3.33	0.17	0.055	0.319	0.024	0.03
41	3.42	0.17	0.055	0.317	0.024	0.03
42	3.50	0.17	0.055	0.316	0.024	0.03

43	3.58	0.17	0.055	0.315	0.024	0.03
44	3.67	0.17	0.055	0.313	0.024	0.03
45	3.75	0.17	0.055	0.312	0.024	0.03
46	3.83	0.20	0.066	0.311	0.029	0.04
47	3.92	0.20	0.066	0.309	0.029	0.04
48	4.00	0.20	0.066	0.308	0.029	0.04
49	4.08	0.20	0.066	0.307	0.029	0.04
50	4.17	0.20	0.066	0.305	0.029	0.04
51	4.25	0.20	0.066	0.304	0.029	0.04
52	4.33	0.23	0.077	0.303	0.034	0.04
53	4.42	0.23	0.077	0.302	0.034	0.04
54	4.50	0.23	0.077	0.300	0.034	0.04
55	4.58	0.23	0.077	0.299	0.034	0.04
56	4.67	0.23	0.077	0.298	0.034	0.04
57	4.75	0.23	0.077	0.296	0.034	0.04
58	4.83	0.27	0.088	0.295	0.039	0.05
59	4.92	0.27	0.088	0.294	0.039	0.05
60	5.00	0.27	0.088	0.293	0.039	0.05
61	5.08	0.20	0.066	0.291	0.029	0.04
62	5.17	0.20	0.066	0.290	0.029	0.04
63	5.25	0.20	0.066	0.289	0.029	0.04
64	5.33	0.23	0.077	0.287	0.034	0.04
65	5.42	0.23	0.077	0.286	0.034	0.04
66	5.50	0.23	0.077	0.285	0.034	0.04
67	5.58	0.27	0.088	0.284	0.039	0.05
68	5.67	0.27	0.088	0.282	0.039	0.05
69	5.75	0.27	0.088	0.281	0.039	0.05
70	5.83	0.27	0.088	0.280	0.039	0.05
71	5.92	0.27	0.088	0.279	0.039	0.05
72	6.00	0.27	0.088	0.277	0.039	0.05
73	6.08	0.30	0.099	0.276	0.043	0.06
74	6.17	0.30	0.099	0.275	0.043	0.06
75	6.25	0.30	0.099	0.274	0.043	0.06
76	6.33	0.30	0.099	0.273	0.043	0.06
77	6.42	0.30	0.099	0.271	0.043	0.06
78	6.50	0.30	0.099	0.270	0.043	0.06
79	6.58	0.33	0.110	0.269	0.048	0.06
80	6.67	0.33	0.110	0.268	0.048	0.06
81	6.75	0.33	0.110	0.267	0.048	0.06
82	6.83	0.33	0.110	0.265	0.048	0.06
83	6.92	0.33	0.110	0.264	0.048	0.06
84	7.00	0.33	0.110	0.263	0.048	0.06
85	7.08	0.33	0.110	0.262	0.048	0.06
86	7.17	0.33	0.110	0.261	0.048	0.06
87	7.25	0.33	0.110	0.259	0.048	0.06
88	7.33	0.37	0.121	0.258	0.053	0.07
89	7.42	0.37	0.121	0.257	0.053	0.07
90	7.50	0.37	0.121	0.256	0.053	0.07
91	7.58	0.40	0.132	0.255	0.058	0.07
92	7.67	0.40	0.132	0.253	0.058	0.07
93	7.75	0.40	0.132	0.252	0.058	0.07
94	7.83	0.43	0.143	0.251	0.063	0.08
95	7.92	0.43	0.143	0.250	0.063	0.08
96	8.00	0.43	0.143	0.249	0.063	0.08
97	8.08	0.50	0.165	0.248	0.072	0.09
98	8.17	0.50	0.165	0.246	0.072	0.09
99	8.25	0.50	0.165	0.245	0.072	0.09
100	8.33	0.50	0.165	0.244	0.072	0.09
101	8.42	0.50	0.165	0.243	0.072	0.09
102	8.50	0.50	0.165	0.242	0.072	0.09
103	8.58	0.53	0.176	0.241	0.077	0.10
104	8.67	0.53	0.176	0.240	0.077	0.10
105	8.75	0.53	0.176	0.239	0.077	0.10
106	8.83	0.57	0.187	0.237	0.082	0.10
107	8.92	0.57	0.187	0.236	0.082	0.10
108	9.00	0.57	0.187	0.235	0.082	0.10
109	9.08	0.63	0.209	0.234	0.092	0.12
110	9.17	0.63	0.209	0.233	0.092	0.12
111	9.25	0.63	0.209	0.232	0.092	0.12
112	9.33	0.67	0.220	0.231	0.097	0.12
113	9.42	0.67	0.220	0.230	0.097	0.12

114	9.50	0.67	0.220	0.229	0.097	0.12
115	9.58	0.70	0.231	0.227	---	0.00
116	9.67	0.70	0.231	0.226	---	0.00
117	9.75	0.70	0.231	0.225	---	0.01
118	9.83	0.73	0.242	0.224	---	0.02
119	9.92	0.73	0.242	0.223	---	0.02
120	10.00	0.73	0.242	0.222	---	0.02
121	10.08	0.50	0.165	0.221	0.072	0.09
122	10.17	0.50	0.165	0.220	0.072	0.09
123	10.25	0.50	0.165	0.219	0.072	0.09
124	10.33	0.50	0.165	0.218	0.072	0.09
125	10.42	0.50	0.165	0.217	0.072	0.09
126	10.50	0.50	0.165	0.216	0.072	0.09
127	10.58	0.67	0.220	0.215	---	0.01
128	10.67	0.67	0.220	0.214	---	0.01
129	10.75	0.67	0.220	0.212	---	0.01
130	10.83	0.67	0.220	0.211	---	0.01
131	10.92	0.67	0.220	0.210	---	0.01
132	11.00	0.67	0.220	0.209	---	0.01
133	11.08	0.63	0.209	0.208	---	0.00
134	11.17	0.63	0.209	0.207	---	0.00
135	11.25	0.63	0.209	0.206	---	0.00
136	11.33	0.63	0.209	0.205	---	0.00
137	11.42	0.63	0.209	0.204	---	0.00
138	11.50	0.63	0.209	0.203	---	0.01
139	11.58	0.57	0.187	0.202	0.082	0.10
140	11.67	0.57	0.187	0.201	0.082	0.10
141	11.75	0.57	0.187	0.200	0.082	0.10
142	11.83	0.60	0.198	0.199	0.087	0.11
143	11.92	0.60	0.198	0.198	0.087	0.11
144	12.00	0.60	0.198	0.197	---	0.00
145	12.08	0.83	0.275	0.196	---	0.08
146	12.17	0.83	0.275	0.195	---	0.08
147	12.25	0.83	0.275	0.194	---	0.08
148	12.33	0.87	0.286	0.193	---	0.09
149	12.42	0.87	0.286	0.192	---	0.09
150	12.50	0.87	0.286	0.191	---	0.09
151	12.58	0.93	0.308	0.190	---	0.12
152	12.67	0.93	0.308	0.189	---	0.12
153	12.75	0.93	0.308	0.188	---	0.12
154	12.83	0.97	0.319	0.188	---	0.13
155	12.92	0.97	0.319	0.187	---	0.13
156	13.00	0.97	0.319	0.186	---	0.13
157	13.08	1.13	0.374	0.185	---	0.19
158	13.17	1.13	0.374	0.184	---	0.19
159	13.25	1.13	0.374	0.183	---	0.19
160	13.33	1.13	0.374	0.182	---	0.19
161	13.42	1.13	0.374	0.181	---	0.19
162	13.50	1.13	0.374	0.180	---	0.19
163	13.58	0.77	0.253	0.179	---	0.07
164	13.67	0.77	0.253	0.178	---	0.07
165	13.75	0.77	0.253	0.177	---	0.08
166	13.83	0.77	0.253	0.176	---	0.08
167	13.92	0.77	0.253	0.176	---	0.08
168	14.00	0.77	0.253	0.175	---	0.08
169	14.08	0.90	0.297	0.174	---	0.12
170	14.17	0.90	0.297	0.173	---	0.12
171	14.25	0.90	0.297	0.172	---	0.12
172	14.33	0.87	0.286	0.171	---	0.11
173	14.42	0.87	0.286	0.170	---	0.12
174	14.50	0.87	0.286	0.169	---	0.12
175	14.58	0.87	0.286	0.168	---	0.12
176	14.67	0.87	0.286	0.168	---	0.12
177	14.75	0.87	0.286	0.167	---	0.12
178	14.83	0.83	0.275	0.166	---	0.11
179	14.92	0.83	0.275	0.165	---	0.11
180	15.00	0.83	0.275	0.164	---	0.11
181	15.08	0.80	0.264	0.163	---	0.10
182	15.17	0.80	0.264	0.163	---	0.10
183	15.25	0.80	0.264	0.162	---	0.10
184	15.33	0.77	0.253	0.161	---	0.09

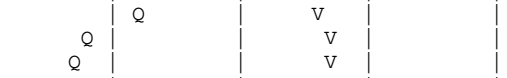
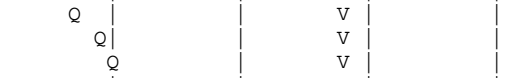
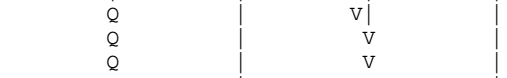
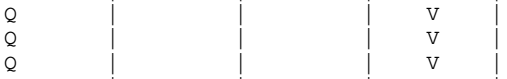
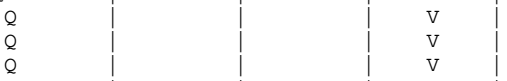
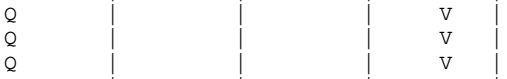
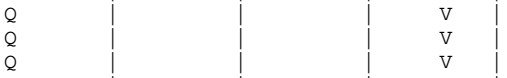
185	15.42	0.77	0.253	0.160	---	0.09
186	15.50	0.77	0.253	0.159	---	0.09
187	15.58	0.63	0.209	0.158	---	0.05
188	15.67	0.63	0.209	0.158	---	0.05
189	15.75	0.63	0.209	0.157	---	0.05
190	15.83	0.63	0.209	0.156	---	0.05
191	15.92	0.63	0.209	0.155	---	0.05
192	16.00	0.63	0.209	0.154	---	0.05
193	16.08	0.13	0.044	0.154	0.019	0.02
194	16.17	0.13	0.044	0.153	0.019	0.02
195	16.25	0.13	0.044	0.152	0.019	0.02
196	16.33	0.13	0.044	0.151	0.019	0.02
197	16.42	0.13	0.044	0.150	0.019	0.02
198	16.50	0.13	0.044	0.150	0.019	0.02
199	16.58	0.10	0.033	0.149	0.014	0.02
200	16.67	0.10	0.033	0.148	0.014	0.02
201	16.75	0.10	0.033	0.147	0.014	0.02
202	16.83	0.10	0.033	0.147	0.014	0.02
203	16.92	0.10	0.033	0.146	0.014	0.02
204	17.00	0.10	0.033	0.145	0.014	0.02
205	17.08	0.17	0.055	0.144	0.024	0.03
206	17.17	0.17	0.055	0.144	0.024	0.03
207	17.25	0.17	0.055	0.143	0.024	0.03
208	17.33	0.17	0.055	0.142	0.024	0.03
209	17.42	0.17	0.055	0.142	0.024	0.03
210	17.50	0.17	0.055	0.141	0.024	0.03
211	17.58	0.17	0.055	0.140	0.024	0.03
212	17.67	0.17	0.055	0.139	0.024	0.03
213	17.75	0.17	0.055	0.139	0.024	0.03
214	17.83	0.13	0.044	0.138	0.019	0.02
215	17.92	0.13	0.044	0.137	0.019	0.02
216	18.00	0.13	0.044	0.137	0.019	0.02
217	18.08	0.13	0.044	0.136	0.019	0.02
218	18.17	0.13	0.044	0.135	0.019	0.02
219	18.25	0.13	0.044	0.135	0.019	0.02
220	18.33	0.13	0.044	0.134	0.019	0.02
221	18.42	0.13	0.044	0.133	0.019	0.02
222	18.50	0.13	0.044	0.133	0.019	0.02
223	18.58	0.10	0.033	0.132	0.014	0.02
224	18.67	0.10	0.033	0.131	0.014	0.02
225	18.75	0.10	0.033	0.131	0.014	0.02
226	18.83	0.07	0.022	0.130	0.010	0.01
227	18.92	0.07	0.022	0.130	0.010	0.01
228	19.00	0.07	0.022	0.129	0.010	0.01
229	19.08	0.10	0.033	0.128	0.014	0.02
230	19.17	0.10	0.033	0.128	0.014	0.02
231	19.25	0.10	0.033	0.127	0.014	0.02
232	19.33	0.13	0.044	0.127	0.019	0.02
233	19.42	0.13	0.044	0.126	0.019	0.02
234	19.50	0.13	0.044	0.125	0.019	0.02
235	19.58	0.10	0.033	0.125	0.014	0.02
236	19.67	0.10	0.033	0.124	0.014	0.02
237	19.75	0.10	0.033	0.124	0.014	0.02
238	19.83	0.07	0.022	0.123	0.010	0.01
239	19.92	0.07	0.022	0.123	0.010	0.01
240	20.00	0.07	0.022	0.122	0.010	0.01
241	20.08	0.10	0.033	0.122	0.014	0.02
242	20.17	0.10	0.033	0.121	0.014	0.02
243	20.25	0.10	0.033	0.120	0.014	0.02
244	20.33	0.10	0.033	0.120	0.014	0.02
245	20.42	0.10	0.033	0.119	0.014	0.02
246	20.50	0.10	0.033	0.119	0.014	0.02
247	20.58	0.10	0.033	0.118	0.014	0.02
248	20.67	0.10	0.033	0.118	0.014	0.02
249	20.75	0.10	0.033	0.117	0.014	0.02
250	20.83	0.07	0.022	0.117	0.010	0.01
251	20.92	0.07	0.022	0.116	0.010	0.01
252	21.00	0.07	0.022	0.116	0.010	0.01
253	21.08	0.10	0.033	0.116	0.014	0.02
254	21.17	0.10	0.033	0.115	0.014	0.02
255	21.25	0.10	0.033	0.115	0.014	0.02

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256  21.33     0.07      0.022         0.114     0.010         0.01
257  21.42     0.07      0.022         0.114     0.010         0.01
258  21.50     0.07      0.022         0.113     0.010         0.01
259  21.58     0.10      0.033         0.113     0.014         0.02
260  21.67     0.10      0.033         0.113     0.014         0.02
261  21.75     0.10      0.033         0.112     0.014         0.02
262  21.83     0.07      0.022         0.112     0.010         0.01
263  21.92     0.07      0.022         0.111     0.010         0.01
264  22.00     0.07      0.022         0.111     0.010         0.01
265  22.08     0.10      0.033         0.111     0.014         0.02
266  22.17     0.10      0.033         0.110     0.014         0.02
267  22.25     0.10      0.033         0.110     0.014         0.02
268  22.33     0.07      0.022         0.110     0.010         0.01
269  22.42     0.07      0.022         0.109     0.010         0.01
270  22.50     0.07      0.022         0.109     0.010         0.01
271  22.58     0.07      0.022         0.109     0.010         0.01
272  22.67     0.07      0.022         0.108     0.010         0.01
273  22.75     0.07      0.022         0.108     0.010         0.01
274  22.83     0.07      0.022         0.108     0.010         0.01
275  22.92     0.07      0.022         0.107     0.010         0.01
276  23.00     0.07      0.022         0.107     0.010         0.01
277  23.08     0.07      0.022         0.107     0.010         0.01
278  23.17     0.07      0.022         0.107     0.010         0.01
279  23.25     0.07      0.022         0.106     0.010         0.01
280  23.33     0.07      0.022         0.106     0.010         0.01
281  23.42     0.07      0.022         0.106     0.010         0.01
282  23.50     0.07      0.022         0.106     0.010         0.01
283  23.58     0.07      0.022         0.106     0.010         0.01
284  23.67     0.07      0.022         0.106     0.010         0.01
285  23.75     0.07      0.022         0.105     0.010         0.01
286  23.83     0.07      0.022         0.105     0.010         0.01
287  23.92     0.07      0.022         0.105     0.010         0.01
288  24.00     0.07      0.022         0.105     0.010         0.01
    Sum =     100.0                                    Sum =    13.9
      Flood volume = Effective rainfall      1.16(In)
       times area      23.0(Ac.)/[(In)/(Ft.)] =       2.2(Ac.Ft)
      Total soil loss =      1.59(In)
      Total soil loss =     3.051(Ac.Ft)
      Total rainfall =      2.75(In)
      Flood volume =       96324.5 Cubic Feet
      Total soil loss =      132887.4 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      4.474(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f     H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ---------------------------------------------------------------------------
   0+ 5       0.0009      0.14  Q          |         |         |         |
   0+10       0.0027      0.25  VQ         |         |         |         |
   0+15       0.0046      0.28  VQ         |         |         |         |
   0+20       0.0070      0.35  VQ         |         |         |         |
   0+25       0.0099      0.41  VQ         |         |         |         |
   0+30       0.0128      0.42  VQ         |         |         |         |
   0+35       0.0157      0.43  VQ         |         |         |         |
   0+40       0.0187      0.43  VQ         |         |         |         |
   0+45       0.0216      0.43  VQ         |         |         |         |
   0+50       0.0251      0.50  VQ         |         |         |         |
   0+55       0.0289      0.56  V Q        |         |         |         |
   1+ 0       0.0328      0.57  V Q        |         |         |         |
   1+ 5       0.0363      0.50  V Q        |         |         |         |
   1+10       0.0393      0.44  VQ         |         |         |         |
   1+15       0.0423      0.43  VQ         |         |         |         |
   1+20       0.0452      0.43  VQ         |         |         |         |
   1+25       0.0482      0.43  VQ         |         |         |         |
   1+30       0.0512      0.43  VQ         |         |         |         |
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1+35	0.0541	0.43	VQ				
1+40	0.0571	0.43	|Q				
1+45	0.0600	0.43	|Q				
1+50	0.0634	0.50	|Q				
1+55	0.0672	0.56	|VQ				
2+ 0	0.0712	0.57	|VQ				
2+ 5	0.0751	0.57	|VQ				
2+10	0.0790	0.57	|VQ				
2+15	0.0830	0.57	|VQ				
2+20	0.0869	0.57	|VQ				
2+25	0.0908	0.57	|VQ				
2+30	0.0948	0.57	|VQ				
2+35	0.0992	0.64	|VQ				
2+40	0.1040	0.70	|VQ				
2+45	0.1089	0.71	|VQ				
2+50	0.1138	0.71	| Q				
2+55	0.1187	0.71	| Q				
3+ 0	0.1236	0.71	| Q				
3+ 5	0.1285	0.71	| Q				
3+10	0.1335	0.71	| Q				
3+15	0.1384	0.71	| Q				
3+20	0.1433	0.71	| Q				
3+25	0.1482	0.71	| Q				
3+30	0.1531	0.71	| Q				
3+35	0.1580	0.71	| Q				
3+40	0.1630	0.71	| Q				
3+45	0.1679	0.71	| QV				
3+50	0.1733	0.78	| Q				
3+55	0.1791	0.84	| Q				
4+ 0	0.1849	0.85	| Q				
4+ 5	0.1908	0.86	| Q				
4+10	0.1967	0.86	| Q				
4+15	0.2026	0.86	| Q				
4+20	0.2090	0.92	| Q				
4+25	0.2158	0.98	| Q				
4+30	0.2226	1.00	| QV				
4+35	0.2295	1.00	| QV				
4+40	0.2364	1.00	| QV				
4+45	0.2433	1.00	| QV				
4+50	0.2506	1.07	| Q				
4+55	0.2584	1.13	| Q				
5+ 0	0.2662	1.14	| Q				
5+ 5	0.2732	1.01	| Q				
5+10	0.2793	0.89	| Q V				
5+15	0.2853	0.87	| Q V				
5+20	0.2916	0.92	| Q V				
5+25	0.2984	0.98	| Q V				
5+30	0.3053	1.00	| Q V				
5+35	0.3126	1.07	| QV				
5+40	0.3204	1.13	| QV				
5+45	0.3282	1.14	| QV				
5+50	0.3361	1.14	| Q V				
5+55	0.3440	1.14	| Q V				
6+ 0	0.3518	1.14	| Q V				
6+ 5	0.3602	1.21	| Q V				
6+10	0.3689	1.27	| QV				
6+15	0.3777	1.28	| QV				
6+20	0.3866	1.29	| QV				
6+25	0.3954	1.29	| Q V				
6+30	0.4043	1.29	| Q V				
6+35	0.4136	1.35	| Q V				
6+40	0.4233	1.41	| Q V				
6+45	0.4331	1.42	| Q V				
6+50	0.4430	1.43	| Q V				
6+55	0.4528	1.43	| Q V				
7+ 0	0.4626	1.43	| Q V				
7+ 5	0.4725	1.43	| Q V				
7+10	0.4823	1.43	| Q V				
7+15	0.4922	1.43	| Q V				
7+20	0.5025	1.50	| Q V				
7+25	0.5132	1.56	| Q V				

7+30	0.5240	1.57	| Q V|	|	|	|	|
7+35	0.5352	1.64	| Q V|	|	|	|	|
7+40	0.5469	1.70	| Q V|	|	|	|	|
7+45	0.5587	1.71	| Q V	|	|	|	|
7+50	0.5710	1.78	| Q V	|	|	|	|
7+55	0.5837	1.84	| Q V	|	|	|	|
8+ 0	0.5964	1.85	| Q V	|	|	|	|
8+ 5	0.6101	1.99	| Q |V	|	|	|	|
8+10	0.6247	2.11	| Q |V	|	|	|	|
8+15	0.6394	2.13	| Q |V	|	|	|	|
8+20	0.6541	2.14	| Q |V	|	|	|	|
8+25	0.6689	2.14	| Q | V	|	|	|	|
8+30	0.6836	2.14	| Q | V	|	|	|	|
8+35	0.6989	2.21	| Q | V	|	|	|	|
8+40	0.7145	2.27	| Q| V	|	|	|	|
8+45	0.7302	2.28	| Q| V	|	|	|	|
8+50	0.7464	2.35	| Q| V	|	|	|	|
8+55	0.7630	2.41	| Q| V	|	|	|	|
9+ 0	0.7797	2.42	| Q| V	|	|	|	|
9+ 5	0.7974	2.56	| Q V	|	|	|	|
9+10	0.8158	2.68	| Q V	|	|	|	|
9+15	0.8345	2.70	| Q V	|	|	|	|
9+20	0.8536	2.78	| |Q V	|	|	|	|
9+25	0.8732	2.84	| |Q V	|	|	|	|
9+30	0.8928	2.85	| |Q V	|	|	|	|
9+35	0.9034	1.54	| Q | V	|	|	|	|
9+40	0.9062	0.40	|Q | V	|	|	|	|
9+45	0.9076	0.20	Q | V	|	|	|	|
9+50	0.9093	0.26	|Q | V	|	|	|	|
9+55	0.9120	0.39	|Q | V	|	|	|	|
10+ 0	0.9151	0.44	|Q | V	|	|	|	|
10+ 5	0.9237	1.25	| Q | V	|	|	|	|
10+10	0.9372	1.96	| Q | V	|	|	|	|
10+15	0.9516	2.09	| Q | V	|	|	|	|
10+20	0.9663	2.14	| Q | V	|	|	|	|
10+25	0.9811	2.14	| Q | V	|	|	|	|
10+30	0.9958	2.14	| Q | V	|	|	|	|
10+35	1.0040	1.19	| Q | V	|	|	|	|
10+40	1.0065	0.36	|Q | V	|	|	|	|
10+45	1.0080	0.22	Q | V	|	|	|	|
10+50	1.0092	0.18	Q | V	|	|	|	|
10+55	1.0106	0.20	Q | V	|	|	|	|
11+ 0	1.0122	0.23	Q | V	|	|	|	|
11+ 5	1.0131	0.13	Q | V	|	|	|	|
11+10	1.0134	0.05	Q | V	|	|	|	|
11+15	1.0138	0.05	Q | V	|	|	|	|
11+20	1.0143	0.07	Q | V	|	|	|	|
11+25	1.0149	0.09	Q | V	|	|	|	|
11+30	1.0157	0.12	Q | V	|	|	|	|
11+35	1.0241	1.22	| Q | V	|	|	|	|
11+40	1.0391	2.18	| Q | V	|	|	|	|
11+45	1.0553	2.36	| Q| V	|	|	|	|
11+50	1.0725	2.50	| Q| V	|	|	|	|
11+55	1.0901	2.56	| Q V	|	|	|	|
12+ 0	1.0995	1.36	| Q | V	|	|	|	|
12+ 5	1.1074	1.15	| Q | V	|	|	|	|
12+10	1.1192	1.71	| Q | V	|	|	|	|
12+15	1.1316	1.80	| Q | V	|	|	|	|
12+20	1.1453	2.00	| Q | V	|	|	|	|
12+25	1.1599	2.12	| Q | V	|	|	|	|
12+30	1.1749	2.17	| Q | V	|	|	|	|
12+35	1.1916	2.44	| Q| V	|	|	|	|
12+40	1.2101	2.67	| Q V	|	|	|	|
12+45	1.2289	2.73	| Q V	|	|	|	|
12+50	1.2488	2.89	| |Q V	|	|	|	|
12+55	1.2696	3.02	| | Q V	|	|	|	|
13+ 0	1.2907	3.06	| | Q V	|	|	|	|
13+ 5	1.3162	3.70	| | Q V	|	|	|	|
13+10	1.3454	4.25	| | Q V	|	|	|	|
13+15	1.3756	4.37	| | Q V	|	|	|	|
13+20	1.4061	4.43	| | Q V	|	|	|	|

13+25	1.4367	4.45	
13+30	1.4676	4.47	
13+35	1.4894	3.17	
13+40	1.5033	2.02	
13+45	1.5158	1.82	
13+50	1.5279	1.76	
13+55	1.5402	1.78	
14+ 0	1.5526	1.80	
14+ 5	1.5684	2.30	
14+10	1.5874	2.75	
14+15	1.6070	2.85	
14+20	1.6261	2.78	
14+25	1.6447	2.69	
14+30	1.6632	2.69	
14+35	1.6819	2.71	
14+40	1.7007	2.73	
14+45	1.7196	2.75	
14+50	1.7378	2.65	
14+55	1.7554	2.56	
15+ 0	1.7730	2.56	
15+ 5	1.7899	2.45	
15+10	1.8062	2.36	
15+15	1.8225	2.36	
15+20	1.8380	2.25	
15+25	1.8529	2.17	
15+30	1.8678	2.17	
15+35	1.8795	1.69	
15+40	1.8883	1.29	
15+45	1.8968	1.23	
15+50	1.9051	1.21	
15+55	1.9136	1.23	
16+ 0	1.9222	1.25	
16+ 5	1.9287	0.93	
16+10	1.9331	0.65	
16+15	1.9372	0.59	
16+20	1.9411	0.57	
16+25	1.9451	0.57	
16+30	1.9490	0.57	
16+35	1.9525	0.50	
16+40	1.9555	0.44	
16+45	1.9585	0.43	
16+50	1.9615	0.43	
16+55	1.9644	0.43	
17+ 0	1.9674	0.43	
17+ 5	1.9712	0.56	
17+10	1.9760	0.68	
17+15	1.9808	0.71	
17+20	1.9857	0.71	
17+25	1.9906	0.71	
17+30	1.9956	0.71	
17+35	2.0005	0.71	
17+40	2.0054	0.71	
17+45	2.0103	0.71	
17+50	2.0148	0.65	
17+55	2.0188	0.59	
18+ 0	2.0228	0.58	
18+ 5	2.0267	0.57	
18+10	2.0306	0.57	
18+15	2.0346	0.57	
18+20	2.0385	0.57	
18+25	2.0425	0.57	
18+30	2.0464	0.57	
18+35	2.0499	0.50	
18+40	2.0529	0.44	
18+45	2.0559	0.43	
18+50	2.0584	0.36	
18+55	2.0605	0.30	
19+ 0	2.0625	0.29	
19+ 5	2.0649	0.35	
19+10	2.0677	0.41	
19+15	2.0706	0.42	

```
   19+20       2.0741      0.50  |Q        |         |         |      V  |
   19+25       2.0779      0.56  | Q       |         |         |      V  |
   19+30       2.0818      0.57  | Q       |         |         |      V  |
   19+35       2.0853      0.50  | Q       |         |         |      V  |
   19+40       2.0883      0.44  |Q        |         |         |      V  |
   19+45       2.0913      0.43  |Q        |         |         |      V  |
   19+50       2.0938      0.36  |Q        |         |         |      V  |
   19+55       2.0959      0.30  |Q        |         |         |      V  |
   20+ 0       2.0979      0.29  |Q        |         |         |      V  |
   20+ 5       2.1003      0.35  |Q        |         |         |      V  |
   20+10       2.1031      0.41  |Q        |         |         |       V |
   20+15       2.1061      0.42  |Q        |         |         |       V |
   20+20       2.1090      0.43  |Q        |         |         |       V |
   20+25       2.1120      0.43  |Q        |         |         |       V |
   20+30       2.1149      0.43  |Q        |         |         |       V |
   20+35       2.1179      0.43  |Q        |         |         |       V |
   20+40       2.1208      0.43  |Q        |         |         |       V |
   20+45       2.1238      0.43  |Q        |         |         |       V |
   20+50       2.1262      0.36  |Q        |         |         |       V |
   20+55       2.1283      0.30  |Q        |         |         |       V |
   21+ 0       2.1303      0.29  |Q        |         |         |       V |
   21+ 5       2.1328      0.35  |Q        |         |         |       V |
   21+10       2.1356      0.41  |Q        |         |         |       V |
   21+15       2.1385      0.42  |Q        |         |         |       V |
   21+20       2.1410      0.36  |Q        |         |         |       V |
   21+25       2.1431      0.30  |Q        |         |         |       V |
   21+30       2.1451      0.29  |Q        |         |         |       V |
   21+35       2.1475      0.35  |Q        |         |         |       V |
   21+40       2.1504      0.41  |Q        |         |         |       V |
   21+45       2.1533      0.42  |Q        |         |         |       V |
   21+50       2.1558      0.36  |Q        |         |         |       V |
   21+55       2.1578      0.30  |Q        |         |         |        V|
   22+ 0       2.1598      0.29  |Q        |         |         |        V|
   22+ 5       2.1623      0.35  |Q        |         |         |        V|
   22+10       2.1651      0.41  |Q        |         |         |        V|
   22+15       2.1680      0.42  |Q        |         |         |        V|
   22+20       2.1705      0.36  |Q        |         |         |        V|
   22+25       2.1726      0.30  |Q        |         |         |        V|
   22+30       2.1746      0.29  |Q        |         |         |        V|
   22+35       2.1766      0.29  |Q        |         |         |        V|
   22+40       2.1785      0.29  |Q        |         |         |        V|
   22+45       2.1805      0.29  |Q        |         |         |        V|
   22+50       2.1825      0.29  |Q        |         |         |        V|
   22+55       2.1844      0.29  |Q        |         |         |        V|
   23+ 0       2.1864      0.29  |Q        |         |         |        V|
   23+ 5       2.1884      0.29  |Q        |         |         |        V|
   23+10       2.1903      0.29  |Q        |         |         |        V|
   23+15       2.1923      0.29  |Q        |         |         |        V|
   23+20       2.1943      0.29  |Q        |         |         |        V|
   23+25       2.1962      0.29  |Q        |         |         |        V|
   23+30       2.1982      0.29  |Q        |         |         |        V|
   23+35       2.2002      0.29  |Q        |         |         |        V|
   23+40       2.2021      0.29  |Q        |         |         |        V|
   23+45       2.2041      0.29  |Q        |         |         |        V|
   23+50       2.2061      0.29  |Q        |         |         |        V|
   23+55       2.2080      0.29  |Q        |         |         |        V|
   24+ 0       2.2100      0.29  |Q        |         |         |        V|
   24+ 5       2.2110      0.15  Q         |         |         |        V|
   24+10       2.2112      0.03  Q         |         |         |        V|
   24+15       2.2113      0.01  Q         |         |         |        V|
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100-YEAR, 1-HOUR

U n i t H y d r o g r a p h A n a l y s i s

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Study date 10/28/21 File: ARA1POST1100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6279

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

150.10.18
UNIT HYDROGRAPH FOR BASIN NODE 118.1
POST-PROJECT CONDITION
FN: ARA1POST.UNRIV

Drainage Area = 22.97(Ac.) = 0.036 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 22.97(Ac.) = 0.036 Sq. Mi.
Length along longest watercourse = 1744.00(Ft.)
Length along longest watercourse measured to centroid = 446.00(Ft.)
Length along longest watercourse = 0.330 Mi.
Length along longest watercourse measured to centroid = 0.084 Mi.
Difference in elevation = 40.50(Ft.)
Slope along watercourse = 122.6147 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.037 Hr.
Lag time = 2.22 Min.
25% of lag time = 0.56 Min.
40% of lag time = 0.89 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
22.97	0.50	11.48

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
22.97	1.20	27.56

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 0.500(In)
Area Averaged 100-Year Rainfall = 1.200(In)

Point rain (area averaged) = 1.200(In)
Areal adjustment factor = 99.98 %
Adjusted average point rain = 1.200(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
22.970	63.10	0.576

Total Area Entered = 22.97(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
63.1	63.1	0.437	0.576	0.210	1.000	0.210
					Sum (F) =	0.210

Area averaged mean soil loss (F) (In/Hr) = 0.210
Minimum soil loss rate ((In/Hr)) = 0.105
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.439

Slope of intensity-duration curve for a 1 hour storm =0.5000

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	224.909	47.399	10.973
2	0.167	449.817	41.666	9.645
3	0.250	674.726	7.867	1.821
4	0.333	899.635	3.068	0.710
		Sum = 100.000	Sum=	23.149

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.20	0.605	0.210	(0.266)	0.394

APPENDIX D.2: AREA "C" – OFFSITE

U n i t H y d r o g r a p h A n a l y s i s

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Study date 10/30/21 File: ARA1100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

TRI-8 Builders - S/N 615

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

150.10.18
UNIT HYDROGRAPH FOR OFFSITE AREA A
(EXCLUDING AREA A1 OF ONSITE AREA)
FN: ARA

Drainage Area = 159.75(Ac.) = 0.250 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 159.75(Ac.) = 0.250 Sq. Mi.
Length along longest watercourse = 5703.00(Ft.)
Length along longest watercourse measured to centroid = 3200.00(Ft.)
Length along longest watercourse = 1.080 Mi.
Length along longest watercourse measured to centroid = 0.606 Mi.
Difference in elevation = 505.00(Ft.)
Slope along watercourse = 467.5434 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.191 Hr.
Lag time = 11.44 Min.
25% of lag time = 2.86 Min.
40% of lag time = 4.57 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
159.75	0.50	79.88

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
159.75	1.20	191.70

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 0.500(In)
Area Averaged 100-Year Rainfall = 1.200(In)

Point rain (area averaged) = 1.200(In)
Areal adjustment factor = 99.86 %
Adjusted average point rain = 1.198(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
159.750	81.00	0.000

Total Area Entered = 159.75(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
81.0	81.0	0.233	0.000	0.233	1.000	0.233
					Sum (F) =	0.233

Area averaged mean soil loss (F) (In/Hr) = 0.233
Minimum soil loss rate ((In/Hr)) = 0.116
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

Slope of intensity-duration curve for a 1 hour storm =0.5000

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	43.720	4.986	8.027
2	0.167	87.440	20.879	33.614
3	0.250	131.159	28.297	45.557
4	0.333	174.879	15.620	25.148
5	0.417	218.599	7.625	12.277
6	0.500	262.319	5.109	8.226
7	0.583	306.038	3.811	6.135
8	0.667	349.758	2.847	4.584
9	0.750	393.478	2.277	3.666
10	0.833	437.198	1.734	2.791
11	0.917	480.918	1.383	2.227
12	1.000	524.637	1.260	2.028
13	1.083	568.357	0.980	1.577
14	1.167	612.077	0.810	1.304
15	1.250	655.797	0.656	1.057
16	1.333	699.516	0.503	0.810
17	1.417	743.236	0.437	0.704
18	1.500	786.956	0.437	0.704
19	1.583	830.676	0.349	0.562
			Sum = 100.000	Sum= 160.998

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	4.20	0.604	0.233	---	0.37
2	0.17	4.30	0.618	0.233	---	0.39
3	0.25	5.00	0.719	0.233	---	0.49
4	0.33	5.00	0.719	0.233	---	0.49
5	0.42	5.80	0.834	0.233	---	0.60
6	0.50	6.50	0.935	0.233	---	0.70
7	0.58	7.40	1.064	0.233	---	0.83
8	0.67	8.60	1.237	0.233	---	1.00
9	0.75	12.30	1.769	0.233	---	1.54
10	0.83	29.10	4.184	0.233	---	3.95
11	0.92	6.80	0.978	0.233	---	0.75
12	1.00	5.00	0.719	0.233	---	0.49
Sum =		100.0			Sum =	11.6

Flood volume = Effective rainfall 0.97(In)
times area 159.8(Ac.)/[(In)/(Ft.)] = 12.9(Ac.Ft)
Total soil loss = 0.23(In)
Total soil loss = 3.096(Ac.Ft)
Total rainfall = 1.20(In)
Flood volume = 559980.6 Cubic Feet
Total soil loss = 134883.0 Cubic Feet

Peak flow rate of this hydrograph = 278.737(CFS)

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1 - H O U R S T O R M

R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	75.0	150.0	225.0	300.0
0+ 5	0.0205	2.98	Q				
0+10	0.1279	15.59	V Q				
0+15	0.3607	33.80	V Q				
0+20	0.6857	47.19	V Q				
0+25	1.0825	57.62	V Q				
0+30	1.5513	68.06	V Q				
0+35	2.1116	81.37	V Q				
0+40	2.7811	97.21	V Q				
0+45	3.6018	119.17	V Q				
0+50	4.7817	171.32	V Q				
0+55	6.5707	259.77	V			Q	
1+ 0	8.4904	278.74	V			Q	
1+ 5	9.8074	191.22	Q	V			
1+10	10.6303	119.49	Q			V	
1+15	11.1603	76.95	Q			V	
1+20	11.5343	54.31	Q			V	
1+25	11.8173	41.09	Q			V	
1+30	12.0407	32.45	Q			V	
1+35	12.2166	25.54	Q			V	
1+40	12.3584	20.59	Q			V	
1+45	12.4773	17.26	Q			V	
1+50	12.5721	13.76	Q			V	
1+55	12.6490	11.17	Q			V	
2+ 0	12.7100	8.85	Q			V	
2+ 5	12.7573	6.88	Q			V	
2+10	12.7955	5.55	Q			V	
2+15	12.8270	4.57	Q			V	
2+20	12.8483	3.09	Q			V	
2+25	12.8535	0.76	Q			V	
2+30	12.8554	0.27	Q				V

100-YEAR, 1-HOUR

APPENDIX E: STREET CAPACITY CALCULATIONS

APPENDIX E.1: HALF-STREET CAPACITY RATING TABLE

Rating Table for Half In-Tract Street Capacity

Project Description

Friction Method	Manning Formula
Solve For	Discharge

Input Data

Channel Slope	0.00700	ft/ft
Normal Depth	0.48	ft

Section Definitions

Station (ft)	Elevation (ft)
0+00.000	0.50
0+00.125	0.00
0+02.125	0.13
0+02.125	0.16
0+18.125	0.48

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00.000, 0.50)	(0+18.125, 0.48)	0.015

Channel Slope (ft/ft)	Discharge (ft³/s)	Velocity (ft/s)	Flow Area (ft²)	Wetted Perimeter (ft)	Top Width (ft)
0.00500	7.76	2.27	3.42	18.53	18.12
0.00600	8.50	2.49	3.42	18.53	18.12
0.00700	9.18	2.69	3.42	18.53	18.12
0.00800	9.82	2.87	3.42	18.53	18.12
0.00900	10.41	3.05	3.42	18.53	18.12
0.01000	10.98	3.21	3.42	18.53	18.12
0.01100	11.51	3.37	3.42	18.53	18.12
0.01200	12.02	3.52	3.42	18.53	18.12
0.01300	12.51	3.66	3.42	18.53	18.12

Rating Table for Half In-Tract Street Capacity

Input Data

Channel Slope (ft/ft)	Discharge (ft³/s)	Velocity (ft/s)	Flow Area (ft²)	Wetted Perimeter (ft)	Top Width (ft)
0.01400	12.99	3.80	3.42	18.53	18.12
0.01500	13.44	3.93	3.42	18.53	18.12
0.01600	13.88	4.06	3.42	18.53	18.12
0.01700	14.31	4.19	3.42	18.53	18.12
0.01800	14.72	4.31	3.42	18.53	18.12
0.01900	15.13	4.42	3.42	18.53	18.12
0.02000	15.52	4.54	3.42	18.53	18.12
0.02100	15.90	4.65	3.42	18.53	18.12
0.02200	16.28	4.76	3.42	18.53	18.12
0.02300	16.64	4.87	3.42	18.53	18.12
0.02400	17.00	4.97	3.42	18.53	18.12
0.02500	17.35	5.08	3.42	18.53	18.12
0.02600	17.70	5.18	3.42	18.53	18.12
0.02700	18.03	5.27	3.42	18.53	18.12
0.02800	18.36	5.37	3.42	18.53	18.12
0.02900	18.69	5.47	3.42	18.53	18.12
0.03000	19.01	5.56	3.42	18.53	18.12
0.03100	19.32	5.65	3.42	18.53	18.12
0.03200	19.63	5.74	3.42	18.53	18.12
0.03300	19.94	5.83	3.42	18.53	18.12
0.03400	20.24	5.92	3.42	18.53	18.12
0.03500	20.53	6.01	3.42	18.53	18.12
0.03600	20.82	6.09	3.42	18.53	18.12
0.03700	21.11	6.17	3.42	18.53	18.12
0.03800	21.39	6.26	3.42	18.53	18.12
0.03900	21.67	6.34	3.42	18.53	18.12
0.04000	21.95	6.42	3.42	18.53	18.12
0.04100	22.22	6.50	3.42	18.53	18.12
0.04200	22.49	6.58	3.42	18.53	18.12
0.04300	22.76	6.66	3.42	18.53	18.12
0.04400	23.02	6.73	3.42	18.53	18.12
0.04500	23.28	6.81	3.42	18.53	18.12

APPENDIX E.2: FULL STREET CAPACITY RATING TABLE

Rating Table for Full In-Tract Street Capacity

Project Description

Friction Method	Manning Formula
Solve For	Discharge

Input Data

Channel Slope	0.00700	ft/ft
Normal Depth	0.50	ft

Section Definitions

Station (ft)	Elevation (ft)
0+00.000	0.50
0+00.125	0.00
0+02.125	0.13
0+02.125	0.16
0+18.125	0.48
0+34.125	0.16
0+34.125	0.13
0+36.125	0.00
0+36.250	0.50

Roughness Segment Definitions

Start Station	Ending Station	Roughness Coefficient
(0+00.000, 0.50)	(0+36.250, 0.50)	0.015

Channel Slope (ft/ft)	Discharge (ft³/s)	Velocity (ft/s)	Flow Area (ft²)	Wetted Perimeter (ft)	Top Width (ft)
0.00500	18.35	2.43	7.56	37.11	36.25
0.00600	20.10	2.66	7.56	37.11	36.25
0.00700	21.71	2.87	7.56	37.11	36.25
0.00800	23.21	3.07	7.56	37.11	36.25
0.00900	24.61	3.25	7.56	37.11	36.25

Rating Table for Full In-Tract Street Capacity

Input Data

Channel Slope (ft/ft)	Discharge (ft³/s)	Velocity (ft/s)	Flow Area (ft²)	Wetted Perimeter (ft)	Top Width (ft)
0.01000	25.94	3.43	7.56	37.11	36.25
0.01100	27.21	3.60	7.56	37.11	36.25
0.01200	28.42	3.76	7.56	37.11	36.25
0.01300	29.58	3.91	7.56	37.11	36.25
0.01400	30.70	4.06	7.56	37.11	36.25
0.01500	31.78	4.20	7.56	37.11	36.25
0.01600	32.82	4.34	7.56	37.11	36.25
0.01700	33.83	4.47	7.56	37.11	36.25
0.01800	34.81	4.60	7.56	37.11	36.25
0.01900	35.76	4.73	7.56	37.11	36.25
0.02000	36.69	4.85	7.56	37.11	36.25
0.02100	37.60	4.97	7.56	37.11	36.25
0.02200	38.48	5.09	7.56	37.11	36.25
0.02300	39.35	5.20	7.56	37.11	36.25
0.02400	40.19	5.31	7.56	37.11	36.25
0.02500	41.02	5.42	7.56	37.11	36.25
0.02600	41.83	5.53	7.56	37.11	36.25
0.02700	42.63	5.64	7.56	37.11	36.25
0.02800	43.41	5.74	7.56	37.11	36.25
0.02900	44.18	5.84	7.56	37.11	36.25
0.03000	44.94	5.94	7.56	37.11	36.25
0.03100	45.68	6.04	7.56	37.11	36.25
0.03200	46.41	6.14	7.56	37.11	36.25
0.03300	47.13	6.23	7.56	37.11	36.25
0.03400	47.84	6.33	7.56	37.11	36.25
0.03500	48.54	6.42	7.56	37.11	36.25
0.03600	49.23	6.51	7.56	37.11	36.25
0.03700	49.91	6.60	7.56	37.11	36.25
0.03800	50.58	6.69	7.56	37.11	36.25
0.03900	51.24	6.78	7.56	37.11	36.25
0.04000	51.89	6.86	7.56	37.11	36.25
0.04100	52.53	6.95	7.56	37.11	36.25
0.04200	53.17	7.03	7.56	37.11	36.25
0.04300	53.80	7.11	7.56	37.11	36.25
0.04400	54.42	7.20	7.56	37.11	36.25
0.04500	55.04	7.28	7.56	37.11	36.25

APPENDIX F: PRELIMINARY STORM DRAIN SIZING CALCULATIONS

APPENDIX F.1: LINE "A" STORM DRAIN AND LATERALS

LINE A

PIPE OUTFLOW (SOFFIT CONTROL)														
DS WSE	SYSTEM	PIPE DIA.	PIPE LENGTH	Q (cfs)	K	PIPE SLOPE	DS INVERT	US INVERT	FRICTION SLOPE	VELOCITY	VELOCITY HEAD	LOSS COEFFICIENT	LOSSES	US WSE
1530.43	LINE A	30	116.10	28.31	410.2	0.0030	1528.50	1528.85	0.0048	5.7748	0.5169	0.50	0.2585	1531.24
1531.24	LINE A	30	252.31	24.82	410.2	0.0030	1528.85	1529.61	0.0037	5.0629	0.3973	0.50	0.1987	1532.36
1532.36	LINE A	24	229.69	18.03	226.2	0.0030	1529.61	1530.29	0.0064	5.7466	0.5119	0.50	0.2559	1534.08
1534.08	LINE A	18	294.72	5.27	105.0	0.0030	1530.29	1531.18	0.0025	2.9861	0.1382	0.50	0.0691	1534.89
1534.89	LINE A	18	48.63	0.31	105.0	0.0030	1531.18	1531.32	0.0000	0.1757	0.0005	0.50	0.0002	1534.89

LAT A-1

PIPE OUTFLOW (SOFFIT CONTROL)														
DS WSE	SYSTEM	PIPE DIA.	PIPE LENGTH	Q (cfs)	K	PIPE SLOPE	DS INVERT	US INVERT	FRICTION SLOPE	VELOCITY	VELOCITY HEAD	LOSS COEFFICIENT	LOSSES	US WSE
1531.24	LAT A-1	18	7.69	2.98	105.0	0.0200	1528.85	1529.00	0.0008	1.6885	0.0442	1.50	0.0663	1531.31
1531.31	LAT A-3	18	37.06	1.69	105.0	0.0300	1529.00	1530.11	0.0003	0.9576	0.0142	1.50	0.0213	1531.34

LAT A-2

PIPE OUTFLOW (SOFFIT CONTROL)														
DS WSE	SYSTEM	PIPE DIA.	PIPE LENGTH	Q (cfs)	K	PIPE SLOPE	DS INVERT	US INVERT	FRICTION SLOPE	VELOCITY	VELOCITY HEAD	LOSS COEFFICIENT	LOSSES	US WSE
1532.36	LAT A-2	18	13.54	5.77	105.0	0.0200	1529.61	1529.88	0.0030	3.2694	0.1657	1.50	0.2485	1532.65

LAT A-3

PIPE OUTFLOW (SOFFIT CONTROL)														
DS WSE	SYSTEM	PIPE DIA.	PIPE LENGTH	Q (cfs)	K	PIPE SLOPE	DS INVERT	US INVERT	FRICTION SLOPE	VELOCITY	VELOCITY HEAD	LOSS COEFFICIENT	LOSSES	US WSE
1532.36	LAT A-3	18	25.04	1.32	105.0	0.0200	1529.61	1530.11	0.0002	0.7479	0.0087	1.50	0.0130	1532.38

LAT A-4

PIPE OUTFLOW (SOFFIT CONTROL)														
DS WSE	SYSTEM	PIPE DIA.	PIPE LENGTH	Q (cfs)	K	PIPE SLOPE	DS INVERT	US INVERT	FRICTION SLOPE	VELOCITY	VELOCITY HEAD	LOSS COEFFICIENT	LOSSES	US WSE
1534.08	LAT A-4	18	13.86	10.95	105.0	0.0200	1530.29	1530.57	0.0109	6.2045	0.5967	1.50	0.8950	1535.12

LAT A-5

PIPE OUTFLOW (SOFFIT CONTROL)														
DS WSE	SYSTEM	PIPE DIA.	PIPE LENGTH	Q (cfs)	K	PIPE SLOPE	DS INVERT	US INVERT	FRICTION SLOPE	VELOCITY	VELOCITY HEAD	LOSS COEFFICIENT	LOSSES	US WSE
1534.08	LAT A-5	18	32.00	2.14	105.0	0.0200	1530.29	1530.93	0.0004	1.2126	0.0228	1.50	0.0342	1534.13

LAT A-6

PIPE OUTFLOW (SOFFIT CONTROL)														
DS WSE	SYSTEM	PIPE DIA.	PIPE LENGTH	Q (cfs)	K	PIPE SLOPE	DS INVERT	US INVERT	FRICTION SLOPE	VELOCITY	VELOCITY HEAD	LOSS COEFFICIENT	LOSSES	US WSE
1534.89	LAT A-6	18	21.28	4.96	105.0	0.0200	1531.18	1531.60	0.0022	2.8105	0.1224	1.50	0.1836	1535.12

APPENDIX F.2: LINE "B" STORM DRAIN AND LATERALS

LINE B

PIPE OUTFLOW (SOFFIT CONTROL)														
DS WSE	SYSTEM	PIPE DIA.	PIPE LENGTH	Q (cfs)	K	PIPE SLOPE	DS INVERT	US INVERT	FRICTION SLOPE	VELOCITY	VELOCITY HEAD	LOSS COEFFICIENT	LOSSES	US WSE
1530.43	LINE B	24	107.15	15.35	226.2	0.0030	1528.50	1528.82	0.0046	4.8924	0.3710	1.50	0.5565	1531.48
1531.48	LINE B	18	26.70	11.70	105.0	0.0030	1528.82	1528.90	0.0124	6.6295	0.6812	1.50	1.0218	1532.83
1532.83	LINE B	18	261.70	7.12	105.0	0.0100	1528.90	1531.52	0.0046	4.0344	0.2523	1.50	0.3784	1534.41
1534.41	LINE B	18	58.71	0.74	105.0	0.0100	1531.52	1532.11	0.0000	0.4193	0.0027	1.50	0.0041	1534.42

LAT B-1

PIPE OUTFLOW (SOFFIT CONTROL)														
DS WSE	SYSTEM	PIPE DIA.	PIPE LENGTH	Q (cfs)	K	PIPE SLOPE	DS INVERT	US INVERT	FRICTION SLOPE	VELOCITY	VELOCITY HEAD	LOSS COEFFICIENT	LOSSES	US WSE
1531.48	LAT B-1	18	14.79	3.75	105.0	0.0030	1528.82	1528.87	0.0013	2.1248	0.0700	1.50	0.1050	1531.60

LAT B-2

PIPE OUTFLOW (SOFFIT CONTROL)														
DS WSE	SYSTEM	PIPE DIA.	PIPE LENGTH	Q (cfs)	K	PIPE SLOPE	DS INVERT	US INVERT	FRICTION SLOPE	VELOCITY	VELOCITY HEAD	LOSS COEFFICIENT	LOSSES	US WSE
1531.48	LAT B-2	18	24.81	4.81	105.0	0.0030	1528.82	1528.90	0.0021	2.7255	0.1151	1.50	0.1727	1531.70

LAT B-3

PIPE OUTFLOW (SOFFIT CONTROL)														
DS WSE	SYSTEM	PIPE DIA.	PIPE LENGTH	Q (cfs)	K	PIPE SLOPE	DS INVERT	US INVERT	FRICTION SLOPE	VELOCITY	VELOCITY HEAD	LOSS COEFFICIENT	LOSSES	US WSE
1531.48	LAT B-3	18	24.81	6.51	105.0	0.0030	1528.82	1528.90	0.0038	3.6887	0.2109	1.50	0.3164	1531.89
1531.89	LAT A-3	18	37.06	6.51	105.0	0.0300	1528.90	1530.01	0.0038	3.6887	0.2109	1.50	0.3164	1532.35

APPENDIX F.3: LINE "C" STORM DRAIN

LINE C

PIPE OUTFLOW (SOFFIT CONTROL)														
DS WSE	SYSTEM	PIPE DIA.	PIPE LENGTH	Q (cfs)	K	PIPE SLOPE	DS INVERT	US INVERT	FRICTION SLOPE	VELOCITY	VELOCITY HEAD	LOSS COEFFICIENT	LOSSES	US WSE
1530.43	LINE C	18	42.20	1.88	105.0	0.0030	1329.00	1329.13	0.0003	1.0653	0.0176	1.50	0.0264	1530.47
1530.47	LINE C	18	33.04	0.38	105.0	0.0030	1329.13	1329.23	0.0000	0.2153	0.0007	1.50	0.0011	1530.47

APPENDIX F.4: LINE "D" STORM DRAIN

LINE D

PIPE OUTFLOW (SOFFIT CONTROL)

DS WSE	SYSTEM	PIPE DIA.	PIPE LENGTH	Q (cfs)	K	PIPE SLOPE	DS INVERT	US INVERT	FRICTION SLOPE	VELOCITY	VELOCITY HEAD	LOSS COEFFICIENT	LOSSES	US WSE
1525.30	LINE D	36	54.45	47.18	667.0	0.0125	1523.90	1524.58	0.0050	6.6833	0.6923	1.50	1.0385	1526.61

APPENDIX F.5: LINE "E" STORM DRAIN

LINE E

PIPE OUTFLOW (SOFFIT CONTROL)

DS WSE	SYSTEM	PIPE DIA.	PIPE LENGTH	Q (cfs)	K	PIPE SLOPE	DS INVERT	US INVERT	FRICTION SLOPE	VELOCITY	VELOCITY HEAD	LOSS COEFFICIENT	LOSSES	US WSE
1524.55	LINE E	18	47.29	43.52	105.0	0.0125	1523.90	1524.49	0.1717	24.6595	9.4254	1.50	14.1381	1546.81

APPENDIX F.6: LINE "F" STORM DRAIN

LINE F

PIPE OUTFLOW (SOFFIT CONTROL)														
DS WSE	SYSTEM	PIPE DIA.	PIPE LENGTH	Q (cfs)	K	PIPE SLOPE	DS INVERT	US INVERT	FRICTION SLOPE	VELOCITY	VELOCITY HEAD	LOSS COEFFICIENT	LOSSES	US WSE
1524.55	LINE F	18	36.39	3.93	105.0	0.0125	1523.90	1524.35	0.0014	2.2268	0.0769	1.50	0.1153	1524.72

APPENDIX G: ONSITE BASIN ROUTING ANALYSES

APPENDIX G.1: BASIN OUTFLOW CALCULATIONS

BASIN A

TABLE 1A - Basin Underdrain

Orfice Equation $Q = CA(2gh)^{0.5}$

Diameter of Holes	1.5	inches
Area of Hole	0.049087	sq ft
Number of Holes per Row	1	
Area of Holes per Row	0.049087	
Orfice Coeffcient	0.66	
Invert Elevation of Outlet	1529.5	

Q_{TOTAL}	Q_1	WSE	H	h1
0.1720	0.1720	1530.00	0.50	0.44
0.3117	0.3117	1531.00	1.50	1.44
0.4059	0.4059	1532.00	2.50	2.44
0.4820	0.4820	1533.00	3.50	3.44

TABLE 2A - OUTLET STRUCTURE WEIR

Weir Equation $Q = CLH^{3/2}$

Length of Opening (Weir 1)	5
Length of Opening (Weir 2)	0
Length of Opening (Weir 3)	0
Weir Coeffcient	3
Invert Elevation of Weir 1	1531
Invert Elevation of Weir 2	0
Invert Elevation of Weir 3	0

Q_{TOTAL}	Q_1	WSE	H1
15.00	15.00	1532.00	1.00

TABLE 2B - OUTLET STRUCTURE WEIR SUBMERGED

Orfice Equation $Q = CA(2gh)^{0.5}$

Length of Opening (Weir 1)	5
Height of Opening (Weir 1)	1.00
Length of Opening (Weir 2)	0
Height of Opening (Weir 2)	0
Length of Opening (Weir 3)	0
Height of Opening (Weir 3)	0
Area of Opening (Weir 1)	5
Area of Opening (Weir 2)	0
Area of Opening (Weir 3)	0
Orfice Coeffcient	0.66
Invert of Opening (Weir 1)	1531
Invert of Opening (Weir 2)	0
Invert of Opening (Weir 3)	0

Q_{TOTAL}	Q_1	WSE	H1	h1
37.45	37.45	1533.00	2.00	1.50

TABLE 3 - TOTAL BASIN OUTFLOW

Total Flow Rate for Basin Structure

WSE	$Q_{Orifice}$	Q_{WEIR}	$Q_{WEIR-ORIFICE}$	Q_{TOTAL}
1530.00	0.172	0.000	0.000	0.172
1531.00	0.312	0.000	0.000	0.312
1532.00	0.406	15.000	0.000	15.406
1533.00	0.482	0.000	37.452	37.934

APPENDIX G.2: BASIN STORAGE VOLUME VS OUTFLOW TABLE

Onsite Basin A

Contour Elevation	Contour Area (sf)	Contour Area (ac)	Contour Interval Volume (ac-ft)	Total Basin Volume (ac-ft)	Total Basin Volume (ft^3)	Outflow (cfs)
1529.50	51182.06	1.175		0.0000		0
0.50			0.616			
1530.00	56219.60	1.291		0.6162	26840.56	0.1720
1.50			1.349			
1531.00	61337.57	1.408		1.9651	85600.57	0.3117
2.50			1.467			
1532.00	66534.80	1.527		3.4325	149519.15	15.4059
3.50			1.588			
1533.00	71811.29	1.649		5.0201	218675.42	37.9338

APPENDIX G.3: ONSITE BASIN ROUTING CALCULATIONS – 2-YEAR, 24-HOUR STORM DURATION

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014
Study date: 10/28/21

HEMET 30 ONSITE BASIN A ROUTING
2-YEAR, 24-HOUR ROUTING ANALYSIS
FILENAME: BASINA242

Program License Serial Number 6279

********** HYDROGRAPH INFORMATION **********

From study/file name: ARA1POST242.rte
**********HYDROGRAPH DATA**********
Number of intervals = 291
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 3.003 (CFS)
Total volume = 1.825 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****
_____

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 291
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.500	0.616	0.172	0.615	0.617
1.500	1.965	0.312	1.964	1.966
2.500	3.433	15.406	3.380	3.486
3.500	5.020	37.934	4.889	5.151

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.8	1.50	2.25	3.00	Depth (Ft.)
0.083	0.08	0.00	0.000	O	|	|	|	|	0.00
0.167	0.16	0.00	0.001	OI	|	|	|	|	0.00

0.250	0.17	0.00	0.002	OI	|	|	|	0.00
0.333	0.22	0.00	0.004	O I	|	|	|	0.00
0.417	0.26	0.00	0.005	O I	|	|	|	0.00
0.500	0.26	0.00	0.007	O I	|	|	|	0.01
0.583	0.26	0.00	0.009	O I	|	|	|	0.01
0.667	0.26	0.00	0.011	O I	|	|	|	0.01
0.750	0.26	0.00	0.012	O I	|	|	|	0.01
0.833	0.31	0.00	0.014	O I	|	|	|	0.01
0.917	0.34	0.00	0.017	O I	|	|	|	0.01
1.000	0.35	0.01	0.019	O I	|	|	|	0.02
1.083	0.31	0.01	0.021	O I	|	|	|	0.02
1.167	0.27	0.01	0.023	O I	|	|	|	0.02
1.250	0.27	0.01	0.025	O I	|	|	|	0.02
1.333	0.26	0.01	0.027	O I	|	|	|	0.02
1.417	0.26	0.01	0.028	O I	|	|	|	0.02
1.500	0.26	0.01	0.030	O I	|	|	|	0.02
1.583	0.26	0.01	0.032	O I	|	|	|	0.03
1.667	0.26	0.01	0.034	O I	|	|	|	0.03
1.750	0.26	0.01	0.036	O I	|	|	|	0.03
1.833	0.31	0.01	0.037	O I	|	|	|	0.03
1.917	0.34	0.01	0.040	O I	|	|	|	0.03
2.000	0.35	0.01	0.042	O I	|	|	|	0.03
2.083	0.35	0.01	0.044	O I	|	|	|	0.04
2.167	0.35	0.01	0.047	O I	|	|	|	0.04
2.250	0.35	0.01	0.049	O I	|	|	|	0.04
2.333	0.35	0.01	0.051	O I	|	|	|	0.04
2.417	0.35	0.01	0.054	O I	|	|	|	0.04
2.500	0.35	0.02	0.056	O I	|	|	|	0.05
2.583	0.40	0.02	0.058	O I	|	|	|	0.05
2.667	0.43	0.02	0.061	O I	|	|	|	0.05
2.750	0.44	0.02	0.064	O I	|	|	|	0.05
2.833	0.44	0.02	0.067	O I	|	|	|	0.05
2.917	0.44	0.02	0.070	O I	|	|	|	0.06
3.000	0.44	0.02	0.073	O I	|	|	|	0.06
3.083	0.44	0.02	0.076	O I	|	|	|	0.06
3.167	0.44	0.02	0.079	O I	|	|	|	0.06
3.250	0.44	0.02	0.081	O I	|	|	|	0.07
3.333	0.44	0.02	0.084	O I	|	|	|	0.07
3.417	0.44	0.02	0.087	O I	|	|	|	0.07
3.500	0.44	0.03	0.090	O I	|	|	|	0.07
3.583	0.44	0.03	0.093	O I	|	|	|	0.08
3.667	0.44	0.03	0.096	O I	|	|	|	0.08
3.750	0.44	0.03	0.099	O I	|	|	|	0.08
3.833	0.48	0.03	0.102	O I	|	|	|	0.08
3.917	0.52	0.03	0.105	O I	|	|	|	0.09
4.000	0.53	0.03	0.108	O I	|	|	|	0.09
4.083	0.53	0.03	0.112	O I	|	|	|	0.09
4.167	0.53	0.03	0.115	O I	|	|	|	0.09
4.250	0.53	0.03	0.119	O I	|	|	|	0.10
4.333	0.57	0.03	0.122	O I	|	|	|	0.10
4.417	0.61	0.04	0.126	O I	|	|	|	0.10
4.500	0.62	0.04	0.130	O I	|	|	|	0.11
4.583	0.62	0.04	0.134	O I	|	|	|	0.11
4.667	0.62	0.04	0.138	O I	|	|	|	0.11
4.750	0.62	0.04	0.142	O I	|	|	|	0.12
4.833	0.66	0.04	0.146	O I	|	|	|	0.12
4.917	0.70	0.04	0.150	O I	|	|	|	0.12
5.000	0.70	0.04	0.155	O I	|	|	|	0.13
5.083	0.62	0.04	0.159	O I	|	|	|	0.13
5.167	0.55	0.05	0.163	O I	|	|	|	0.13
5.250	0.54	0.05	0.166	O I	|	|	|	0.14
5.333	0.57	0.05	0.170	O I	|	|	|	0.14
5.417	0.61	0.05	0.174	O I	|	|	|	0.14
5.500	0.62	0.05	0.177	O I	|	|	|	0.14
5.583	0.66	0.05	0.182	O I	|	|	|	0.15
5.667	0.70	0.05	0.186	O I	|	|	|	0.15
5.750	0.70	0.05	0.190	O I	|	|	|	0.15
5.833	0.71	0.05	0.195	O I	|	|	|	0.16
5.917	0.71	0.06	0.199	O I	|	|	|	0.16
6.000	0.71	0.06	0.204	O I	|	|	|	0.17
6.083	0.75	0.06	0.208	O I	|	|	|	0.17

6.167	0.79	0.06	0.213	O	I	|	|	|	0.17
6.250	0.79	0.06	0.218	O	I	|	|	|	0.18
6.333	0.79	0.06	0.223	O	I	|	|	|	0.18
6.417	0.79	0.06	0.228	O	I	|	|	|	0.19
6.500	0.79	0.07	0.233	O	I	|	|	|	0.19
6.583	0.84	0.07	0.239	O	I	|	|	|	0.19
6.667	0.87	0.07	0.244	O	|I	|	|	|	0.20
6.750	0.88	0.07	0.250	O	|I	|	|	|	0.20
6.833	0.88	0.07	0.255	O	|I	|	|	|	0.21
6.917	0.88	0.07	0.261	O	|I	|	|	|	0.21
7.000	0.88	0.07	0.266	O	|I	|	|	|	0.22
7.083	0.88	0.08	0.272	O	|I	|	|	|	0.22
7.167	0.88	0.08	0.277	O	|I	|	|	|	0.23
7.250	0.88	0.08	0.283	O	|I	|	|	|	0.23
7.333	0.93	0.08	0.289	O	|I	|	|	|	0.23
7.417	0.96	0.08	0.295	O	| I	|	|	|	0.24
7.500	0.97	0.08	0.301	O	| I	|	|	|	0.24
7.583	1.01	0.09	0.307	O	| I	|	|	|	0.25
7.667	1.05	0.09	0.313	O	| I	|	|	|	0.25
7.750	1.06	0.09	0.320	O	| I	|	|	|	0.26
7.833	1.10	0.09	0.327	O	| I	|	|	|	0.27
7.917	1.14	0.09	0.334	O	| I	|	|	|	0.27
8.000	1.15	0.10	0.341	|O	| I	|	|	|	0.28
8.083	1.23	0.10	0.349	|O	| I	|	|	|	0.28
8.167	1.31	0.10	0.357	|O	| I	|	|	|	0.29
8.250	1.32	0.10	0.365	|O	| I	|	|	|	0.30
8.333	1.32	0.10	0.373	|O	| I	|	|	|	0.30
8.417	1.32	0.11	0.382	|O	| I	|	|	|	0.31
8.500	1.32	0.11	0.390	|O	| I	|	|	|	0.32
8.583	1.37	0.11	0.399	|O	| I	|	|	|	0.32
8.667	1.40	0.11	0.408	|O	| I	|	|	|	0.33
8.750	1.41	0.12	0.416	|O	| I|	|	|	0.34
8.833	1.45	0.12	0.425	|O	| I|	|	|	0.35
8.917	1.49	0.12	0.435	|O	| I|	|	|	0.35
9.000	1.50	0.12	0.444	|O	| I|	|	|	0.36
9.083	1.59	0.13	0.454	|O	| I	|	|	0.37
9.167	1.66	0.13	0.464	|O	| |I	|	|	0.38
9.250	1.67	0.13	0.475	|O	| |I	|	|	0.39
9.333	1.72	0.14	0.486	|O	| | I	|	|	0.39
9.417	1.76	0.14	0.497	|O	| | I	|	|	0.40
9.500	1.76	0.14	0.508	|O	| | I	|	|	0.41
9.583	1.81	0.14	0.519	|O	| | I	|	|	0.42
9.667	1.85	0.15	0.531	|O	| | I	|	|	0.43
9.750	1.85	0.15	0.542	|O	| | I	|	|	0.44
9.833	1.90	0.15	0.554	|O	| | I	|	|	0.45
9.917	1.93	0.16	0.566	|O	| | I	|	|	0.46
10.000	1.94	0.16	0.579	|O	| | I	|	|	0.47
10.083	1.65	0.16	0.590	|O	| |I	|	|	0.48
10.167	1.39	0.17	0.599	|O	| I |	|	|	0.49
10.250	1.34	0.17	0.607	|O	| I |	|	|	0.49
10.333	1.32	0.17	0.615	|O	| I |	|	|	0.50
10.417	1.32	0.17	0.623	|O	| I |	|	|	0.51
10.500	1.32	0.17	0.631	|O	| I |	|	|	0.51
10.583	1.53	0.17	0.640	|O	| I	|	|	0.52
10.667	1.72	0.18	0.650	|O	| | I	|	|	0.53
10.750	1.75	0.18	0.661	|O	| | I	|	|	0.53
10.833	1.77	0.18	0.672	|O	| | I	|	|	0.54
10.917	1.77	0.18	0.683	|O	| | I	|	|	0.55
11.000	1.77	0.18	0.693	|O	| | I	|	|	0.56
11.083	1.72	0.18	0.704	|O	| | I	|	|	0.57
11.167	1.69	0.18	0.715	|O	| |I	|	|	0.57
11.250	1.68	0.18	0.725	|O	| |I	|	|	0.58
11.333	1.68	0.18	0.735	|O	| |I	|	|	0.59
11.417	1.68	0.19	0.746	|O	| |I	|	|	0.60
11.500	1.68	0.19	0.756	|O	| |I	|	|	0.60
11.583	1.59	0.19	0.766	|O	| I	|	|	0.61
11.667	1.52	0.19	0.775	| O	| I	|	|	0.62
11.750	1.51	0.19	0.784	| O	| I	|	|	0.62
11.833	1.54	0.19	0.794	| O	| I	|	|	0.63
11.917	1.58	0.19	0.803	| O	| I	|	|	0.64
12.000	1.59	0.19	0.813	| O	| I	|	|	0.65

12.083	1.88	0.19	0.823	O		I		0.65
12.167	2.14	0.19	0.836	O		I		0.66
12.250	2.19	0.20	0.849	O		I		0.67
12.333	2.25	0.20	0.863	O		I		0.68
12.417	2.29	0.20	0.878	O		I		0.69
12.500	2.29	0.20	0.892	O		I		0.70
12.583	2.38	0.20	0.907	O		I		0.72
12.667	2.45	0.20	0.922	O		I		0.73
12.750	2.47	0.21	0.937	O		I		0.74
12.833	2.51	0.21	0.953	O		I		0.75
12.917	2.55	0.21	0.969	O		I		0.76
13.000	2.56	0.21	0.985	O		I		0.77
13.083	2.77	0.21	1.002	O		I		0.79
13.167	2.95	0.21	1.020	O		I		0.80
13.250	2.99	0.22	1.039	O		I		0.81
13.333	3.00	0.22	1.059	O		I		0.83
13.417	3.00	0.22	1.078	O		I		0.84
13.500	3.00	0.22	1.097	O		I		0.86
13.583	2.54	0.22	1.115	O		I		0.87
13.667	2.14	0.23	1.129	O		I		0.88
13.750	2.06	0.23	1.142	O		I		0.89
13.833	2.03	0.23	1.155	O		I		0.90
13.917	2.03	0.23	1.167	O		I		0.91
14.000	2.03	0.23	1.179	O		I		0.92
14.083	2.20	0.23	1.192	O		I		0.93
14.167	2.35	0.23	1.206	O		I		0.94
14.250	2.37	0.23	1.221	O		I		0.95
14.333	2.34	0.24	1.236	O		I		0.96
14.417	2.31	0.24	1.250	O		I		0.97
14.500	2.30	0.24	1.264	O		I		0.98
14.583	2.30	0.24	1.278	O		I		0.99
14.667	2.30	0.24	1.293	O		I		1.00
14.750	2.30	0.24	1.307	O		I		1.01
14.833	2.25	0.25	1.321	O		I		1.02
14.917	2.22	0.25	1.334	O		I		1.03
15.000	2.21	0.25	1.348	O		I		1.04
15.083	2.17	0.25	1.361	O		I		1.05
15.167	2.13	0.25	1.374	O		I		1.06
15.250	2.12	0.25	1.387	O		I		1.07
15.333	2.08	0.25	1.400	O		I		1.08
15.417	2.04	0.25	1.412	O		I		1.09
15.500	2.03	0.26	1.425	O		I		1.10
15.583	1.86	0.26	1.436	O		I		1.11
15.667	1.72	0.26	1.447	O		I		1.12
15.750	1.69	0.26	1.457	O		I		1.12
15.833	1.68	0.26	1.467	O		I		1.13
15.917	1.68	0.26	1.476	O		I		1.14
16.000	1.68	0.26	1.486	O		I		1.15
16.083	1.05	0.26	1.494	O	I			1.15
16.167	0.50	0.26	1.497	O I				1.15
16.250	0.39	0.26	1.499	O I				1.15
16.333	0.35	0.26	1.499	OI				1.15
16.417	0.35	0.26	1.500	OI				1.16
16.500	0.35	0.26	1.501	OI				1.16
16.583	0.31	0.26	1.501	OI				1.16
16.667	0.27	0.26	1.501	O				1.16
16.750	0.27	0.26	1.501	O				1.16
16.833	0.26	0.26	1.501	O				1.16
16.917	0.26	0.26	1.501	O				1.16
17.000	0.26	0.26	1.501	O				1.16
17.083	0.35	0.26	1.502	OI				1.16
17.167	0.42	0.26	1.502	O I				1.16
17.250	0.44	0.26	1.504	O I				1.16
17.333	0.44	0.26	1.505	O I				1.16
17.417	0.44	0.26	1.506	O I				1.16
17.500	0.44	0.26	1.507	O I				1.16
17.583	0.44	0.26	1.508	O I				1.16
17.667	0.44	0.26	1.510	O I				1.16
17.750	0.44	0.26	1.511	O I				1.16
17.833	0.40	0.26	1.512	O I				1.16
17.917	0.36	0.27	1.513	OI				1.16

18.000	0.36	0.27	1.513	OI				1.17
18.083	0.35	0.27	1.514	OI				1.17
18.167	0.35	0.27	1.515	OI				1.17
18.250	0.35	0.27	1.515	OI				1.17
18.333	0.35	0.27	1.516	OI				1.17
18.417	0.35	0.27	1.516	OI				1.17
18.500	0.35	0.27	1.517	OI				1.17
18.583	0.31	0.27	1.517	OI				1.17
18.667	0.27	0.27	1.518	O				1.17
18.750	0.27	0.27	1.518	O				1.17
18.833	0.22	0.27	1.518	O				1.17
18.917	0.19	0.27	1.517	IO				1.17
19.000	0.18	0.27	1.517	IO				1.17
19.083	0.22	0.27	1.516	O				1.17
19.167	0.26	0.27	1.516	O				1.17
19.250	0.26	0.27	1.516	O				1.17
19.333	0.31	0.27	1.516	OI				1.17
19.417	0.34	0.27	1.516	OI				1.17
19.500	0.35	0.27	1.517	OI				1.17
19.583	0.31	0.27	1.517	OI				1.17
19.667	0.27	0.27	1.518	O				1.17
19.750	0.27	0.27	1.518	O				1.17
19.833	0.22	0.27	1.518	O				1.17
19.917	0.19	0.27	1.517	IO				1.17
20.000	0.18	0.27	1.517	IO				1.17
20.083	0.22	0.27	1.516	O				1.17
20.167	0.26	0.27	1.516	O				1.17
20.250	0.26	0.27	1.516	O				1.17
20.333	0.26	0.27	1.516	O				1.17
20.417	0.26	0.27	1.516	O				1.17
20.500	0.26	0.27	1.516	O				1.17
20.583	0.26	0.27	1.516	O				1.17
20.667	0.26	0.27	1.516	O				1.17
20.750	0.26	0.27	1.516	O				1.17
20.833	0.22	0.27	1.516	O				1.17
20.917	0.19	0.27	1.515	IO				1.17
21.000	0.18	0.27	1.515	IO				1.17
21.083	0.22	0.27	1.514	O				1.17
21.167	0.26	0.27	1.514	O				1.17
21.250	0.26	0.27	1.514	O				1.17
21.333	0.22	0.27	1.514	O				1.17
21.417	0.19	0.27	1.513	IO				1.17
21.500	0.18	0.27	1.513	IO				1.16
21.583	0.22	0.27	1.512	O				1.16
21.667	0.26	0.27	1.512	O				1.16
21.750	0.26	0.27	1.512	O				1.16
21.833	0.22	0.26	1.512	O				1.16
21.917	0.19	0.26	1.512	IO				1.16
22.000	0.18	0.26	1.511	IO				1.16
22.083	0.22	0.26	1.511	O				1.16
22.167	0.26	0.26	1.510	O				1.16
22.250	0.26	0.26	1.510	O				1.16
22.333	0.22	0.26	1.510	O				1.16
22.417	0.19	0.26	1.510	IO				1.16
22.500	0.18	0.26	1.509	IO				1.16
22.583	0.18	0.26	1.509	IO				1.16
22.667	0.18	0.26	1.508	IO				1.16
22.750	0.18	0.26	1.507	IO				1.16
22.833	0.18	0.26	1.507	IO				1.16
22.917	0.18	0.26	1.506	IO				1.16
23.000	0.18	0.26	1.506	IO				1.16
23.083	0.18	0.26	1.505	IO				1.16
23.167	0.18	0.26	1.504	IO				1.16
23.250	0.18	0.26	1.504	IO				1.16
23.333	0.18	0.26	1.503	IO				1.16
23.417	0.18	0.26	1.503	IO				1.16
23.500	0.18	0.26	1.502	IO				1.16
23.583	0.18	0.26	1.501	IO				1.16
23.667	0.18	0.26	1.501	IO				1.16
23.750	0.18	0.26	1.500	IO				1.16
23.833	0.18	0.26	1.500	IO				1.15

23.917	0.18	0.26	1.499	|IO	|	|	|	1.15
24.000	0.18	0.26	1.498	|IO	|	|	|	1.15
24.083	0.09	0.26	1.497	I O	|	|	|	1.15
24.167	0.02	0.26	1.496	I O	|	|	|	1.15
24.250	0.01	0.26	1.494	I O	|	|	|	1.15
24.333	0.00	0.26	1.493	I O	|	|	|	1.15
24.417	0.00	0.26	1.491	I O	|	|	|	1.15
24.500	0.00	0.26	1.489	I O	|	|	|	1.15
24.583	0.00	0.26	1.487	I O	|	|	|	1.15
24.667	0.00	0.26	1.485	I O	|	|	|	1.14
24.750	0.00	0.26	1.483	I O	|	|	|	1.14
24.833	0.00	0.26	1.482	I O	|	|	|	1.14
24.917	0.00	0.26	1.480	I O	|	|	|	1.14
25.000	0.00	0.26	1.478	I O	|	|	|	1.14
25.083	0.00	0.26	1.476	I O	|	|	|	1.14
25.167	0.00	0.26	1.474	I O	|	|	|	1.14
25.250	0.00	0.26	1.473	I O	|	|	|	1.14
25.333	0.00	0.26	1.471	I O	|	|	|	1.13
25.417	0.00	0.26	1.469	I O	|	|	|	1.13
25.500	0.00	0.26	1.467	I O	|	|	|	1.13
25.583	0.00	0.26	1.466	I O	|	|	|	1.13
25.667	0.00	0.26	1.464	I O	|	|	|	1.13
25.750	0.00	0.26	1.462	I O	|	|	|	1.13
25.833	0.00	0.26	1.460	I O	|	|	|	1.13
25.917	0.00	0.26	1.458	I O	|	|	|	1.12
26.000	0.00	0.26	1.457	I O	|	|	|	1.12
26.083	0.00	0.26	1.455	I O	|	|	|	1.12
26.167	0.00	0.26	1.453	I O	|	|	|	1.12
26.250	0.00	0.26	1.451	I O	|	|	|	1.12
26.333	0.00	0.26	1.449	I O	|	|	|	1.12
26.417	0.00	0.26	1.448	I O	|	|	|	1.12
26.500	0.00	0.26	1.446	I O	|	|	|	1.12
26.583	0.00	0.26	1.444	I O	|	|	|	1.11
26.667	0.00	0.26	1.442	I O	|	|	|	1.11
26.750	0.00	0.26	1.441	I O	|	|	|	1.11
26.833	0.00	0.26	1.439	I O	|	|	|	1.11
26.917	0.00	0.26	1.437	I O	|	|	|	1.11
27.000	0.00	0.26	1.435	I O	|	|	|	1.11
27.083	0.00	0.26	1.433	I O	|	|	|	1.11
27.167	0.00	0.26	1.432	I O	|	|	|	1.10
27.250	0.00	0.26	1.430	I O	|	|	|	1.10
27.333	0.00	0.26	1.428	I O	|	|	|	1.10
27.417	0.00	0.26	1.426	I O	|	|	|	1.10
27.500	0.00	0.26	1.425	I O	|	|	|	1.10
27.583	0.00	0.26	1.423	I O	|	|	|	1.10
27.667	0.00	0.26	1.421	I O	|	|	|	1.10
27.750	0.00	0.26	1.419	I O	|	|	|	1.10
27.833	0.00	0.26	1.418	I O	|	|	|	1.09
27.917	0.00	0.26	1.416	I O	|	|	|	1.09
28.000	0.00	0.25	1.414	I O	|	|	|	1.09
28.083	0.00	0.25	1.412	I O	|	|	|	1.09
28.167	0.00	0.25	1.411	I O	|	|	|	1.09
28.250	0.00	0.25	1.409	I O	|	|	|	1.09
28.333	0.00	0.25	1.407	I O	|	|	|	1.09
28.417	0.00	0.25	1.405	I O	|	|	|	1.09
28.500	0.00	0.25	1.404	I O	|	|	|	1.08
28.583	0.00	0.25	1.402	I O	|	|	|	1.08
28.667	0.00	0.25	1.400	I O	|	|	|	1.08
28.750	0.00	0.25	1.398	I O	|	|	|	1.08
28.833	0.00	0.25	1.397	I O	|	|	|	1.08
28.917	0.00	0.25	1.395	I O	|	|	|	1.08
29.000	0.00	0.25	1.393	I O	|	|	|	1.08
29.083	0.00	0.25	1.391	I O	|	|	|	1.07
29.167	0.00	0.25	1.390	I O	|	|	|	1.07
29.250	0.00	0.25	1.388	I O	|	|	|	1.07
29.333	0.00	0.25	1.386	I O	|	|	|	1.07
29.417	0.00	0.25	1.384	I O	|	|	|	1.07
29.500	0.00	0.25	1.383	I O	|	|	|	1.07
29.583	0.00	0.25	1.381	I O	|	|	|	1.07
29.667	0.00	0.25	1.379	I O	|	|	|	1.07
29.750	0.00	0.25	1.377	I O	|	|	|	1.06

29.833	0.00	0.25	1.376	I	O				1.06
29.917	0.00	0.25	1.374	I	O				1.06
30.000	0.00	0.25	1.372	I	O				1.06
30.083	0.00	0.25	1.371	I	O				1.06
30.167	0.00	0.25	1.369	I	O				1.06
30.250	0.00	0.25	1.367	I	O				1.06
30.333	0.00	0.25	1.365	I	O				1.06
30.417	0.00	0.25	1.364	I	O				1.05
30.500	0.00	0.25	1.362	I	O				1.05
30.583	0.00	0.25	1.360	I	O				1.05
30.667	0.00	0.25	1.359	I	O				1.05
30.750	0.00	0.25	1.357	I	O				1.05
30.833	0.00	0.25	1.355	I	O				1.05
30.917	0.00	0.25	1.353	I	O				1.05
31.000	0.00	0.25	1.352	I	O				1.05
31.083	0.00	0.25	1.350	I	O				1.04
31.167	0.00	0.25	1.348	I	O				1.04
31.250	0.00	0.25	1.347	I	O				1.04
31.333	0.00	0.25	1.345	I	O				1.04
31.417	0.00	0.25	1.343	I	O				1.04
31.500	0.00	0.25	1.341	I	O				1.04
31.583	0.00	0.25	1.340	I	O				1.04
31.667	0.00	0.25	1.338	I	O				1.04
31.750	0.00	0.25	1.336	I	O				1.03
31.833	0.00	0.25	1.335	I	O				1.03
31.917	0.00	0.25	1.333	I	O				1.03
32.000	0.00	0.25	1.331	I	O				1.03
32.083	0.00	0.25	1.330	I	O				1.03
32.167	0.00	0.25	1.328	I	O				1.03
32.250	0.00	0.25	1.326	I	O				1.03
32.333	0.00	0.25	1.324	I	O				1.03
32.417	0.00	0.25	1.323	I	O				1.02
32.500	0.00	0.25	1.321	I	O				1.02
32.583	0.00	0.25	1.319	I	O				1.02
32.667	0.00	0.24	1.318	I	O				1.02
32.750	0.00	0.24	1.316	I	O				1.02
32.833	0.00	0.24	1.314	I	O				1.02
32.917	0.00	0.24	1.313	I	O				1.02
33.000	0.00	0.24	1.311	I	O				1.02
33.083	0.00	0.24	1.309	I	O				1.01
33.167	0.00	0.24	1.308	I	O				1.01
33.250	0.00	0.24	1.306	I	O				1.01
33.333	0.00	0.24	1.304	I	O				1.01
33.417	0.00	0.24	1.303	I	O				1.01
33.500	0.00	0.24	1.301	I	O				1.01
33.583	0.00	0.24	1.299	I	O				1.01
33.667	0.00	0.24	1.298	I	O				1.01
33.750	0.00	0.24	1.296	I	O				1.00
33.833	0.00	0.24	1.294	I	O				1.00
33.917	0.00	0.24	1.293	I	O				1.00
34.000	0.00	0.24	1.291	I	O				1.00
34.083	0.00	0.24	1.289	I	O				1.00
34.167	0.00	0.24	1.288	I	O				1.00
34.250	0.00	0.24	1.286	I	O				1.00
34.333	0.00	0.24	1.284	I	O				1.00
34.417	0.00	0.24	1.283	I	O				0.99
34.500	0.00	0.24	1.281	I	O				0.99
34.583	0.00	0.24	1.279	I	O				0.99
34.667	0.00	0.24	1.278	I	O				0.99
34.750	0.00	0.24	1.276	I	O				0.99
34.833	0.00	0.24	1.274	I	O				0.99
34.917	0.00	0.24	1.273	I	O				0.99
35.000	0.00	0.24	1.271	I	O				0.99
35.083	0.00	0.24	1.269	I	O				0.98
35.167	0.00	0.24	1.268	I	O				0.98
35.250	0.00	0.24	1.266	I	O				0.98
35.333	0.00	0.24	1.264	I	O				0.98
35.417	0.00	0.24	1.263	I	O				0.98
35.500	0.00	0.24	1.261	I	O				0.98
35.583	0.00	0.24	1.259	I	O				0.98
35.667	0.00	0.24	1.258	I	O				0.98

35.750	0.00	0.24	1.256	I	O				0.97
35.833	0.00	0.24	1.255	I	O				0.97
35.917	0.00	0.24	1.253	I	O				0.97
36.000	0.00	0.24	1.251	I	O				0.97
36.083	0.00	0.24	1.250	I	O				0.97
36.167	0.00	0.24	1.248	I	O				0.97
36.250	0.00	0.24	1.246	I	O				0.97
36.333	0.00	0.24	1.245	I	O				0.97
36.417	0.00	0.24	1.243	I	O				0.96
36.500	0.00	0.24	1.241	I	O				0.96
36.583	0.00	0.24	1.240	I	O				0.96
36.667	0.00	0.24	1.238	I	O				0.96
36.750	0.00	0.24	1.237	I	O				0.96
36.833	0.00	0.24	1.235	I	O				0.96
36.917	0.00	0.24	1.233	I	O				0.96
37.000	0.00	0.24	1.232	I	O				0.96
37.083	0.00	0.24	1.230	I	O				0.96
37.167	0.00	0.24	1.228	I	O				0.95
37.250	0.00	0.24	1.227	I	O				0.95
37.333	0.00	0.24	1.225	I	O				0.95
37.417	0.00	0.24	1.224	I	O				0.95
37.500	0.00	0.23	1.222	I	O				0.95
37.583	0.00	0.23	1.220	I	O				0.95
37.667	0.00	0.23	1.219	I	O				0.95
37.750	0.00	0.23	1.217	I	O				0.95
37.833	0.00	0.23	1.215	I	O				0.94
37.917	0.00	0.23	1.214	I	O				0.94
38.000	0.00	0.23	1.212	I	O				0.94
38.083	0.00	0.23	1.211	I	O				0.94
38.167	0.00	0.23	1.209	I	O				0.94
38.250	0.00	0.23	1.207	I	O				0.94
38.333	0.00	0.23	1.206	I	O				0.94
38.417	0.00	0.23	1.204	I	O				0.94
38.500	0.00	0.23	1.203	I	O				0.93
38.583	0.00	0.23	1.201	I	O				0.93
38.667	0.00	0.23	1.199	I	O				0.93
38.750	0.00	0.23	1.198	I	O				0.93
38.833	0.00	0.23	1.196	I	O				0.93
38.917	0.00	0.23	1.195	I	O				0.93
39.000	0.00	0.23	1.193	I	O				0.93
39.083	0.00	0.23	1.191	I	O				0.93
39.167	0.00	0.23	1.190	I	O				0.93
39.250	0.00	0.23	1.188	I	O				0.92
39.333	0.00	0.23	1.187	I	O				0.92
39.417	0.00	0.23	1.185	I	O				0.92
39.500	0.00	0.23	1.183	I	O				0.92
39.583	0.00	0.23	1.182	I	O				0.92
39.667	0.00	0.23	1.180	I	O				0.92
39.750	0.00	0.23	1.179	I	O				0.92
39.833	0.00	0.23	1.177	I	O				0.92
39.917	0.00	0.23	1.176	I	O				0.91
40.000	0.00	0.23	1.174	I	O				0.91
40.083	0.00	0.23	1.172	I	O				0.91
40.167	0.00	0.23	1.171	I	O				0.91
40.250	0.00	0.23	1.169	I	O				0.91
40.333	0.00	0.23	1.168	I	O				0.91
40.417	0.00	0.23	1.166	I	O				0.91
40.500	0.00	0.23	1.164	I	O				0.91
40.583	0.00	0.23	1.163	I	O				0.91
40.667	0.00	0.23	1.161	I	O				0.90
40.750	0.00	0.23	1.160	I	O				0.90
40.833	0.00	0.23	1.158	I	O				0.90
40.917	0.00	0.23	1.157	I	O				0.90
41.000	0.00	0.23	1.155	I	O				0.90
41.083	0.00	0.23	1.153	I	O				0.90
41.167	0.00	0.23	1.152	I	O				0.90
41.250	0.00	0.23	1.150	I	O				0.90
41.333	0.00	0.23	1.149	I	O				0.89
41.417	0.00	0.23	1.147	I	O				0.89
41.500	0.00	0.23	1.146	I	O				0.89
41.583	0.00	0.23	1.144	I	O				0.89

41.667	0.00	0.23	1.142	I	O	|	|	|	| 0.89
41.750	0.00	0.23	1.141	I	O	|	|	|	| 0.89
41.833	0.00	0.23	1.139	I	O	|	|	|	| 0.89
41.917	0.00	0.23	1.138	I	O	|	|	|	| 0.89
42.000	0.00	0.23	1.136	I	O	|	|	|	| 0.89
42.083	0.00	0.23	1.135	I	O	|	|	|	| 0.88
42.167	0.00	0.23	1.133	I	O	|	|	|	| 0.88
42.250	0.00	0.23	1.132	I	O	|	|	|	| 0.88
42.333	0.00	0.23	1.130	I	O	|	|	|	| 0.88
42.417	0.00	0.23	1.128	I	O	|	|	|	| 0.88
42.500	0.00	0.23	1.127	I	O	|	|	|	| 0.88
42.583	0.00	0.22	1.125	I	O	|	|	|	| 0.88
42.667	0.00	0.22	1.124	I	O	|	|	|	| 0.88
42.750	0.00	0.22	1.122	I	O	|	|	|	| 0.88
42.833	0.00	0.22	1.121	I	O	|	|	|	| 0.87
42.917	0.00	0.22	1.119	I	O	|	|	|	| 0.87
43.000	0.00	0.22	1.118	I	O	|	|	|	| 0.87
43.083	0.00	0.22	1.116	I	O	|	|	|	| 0.87
43.167	0.00	0.22	1.115	I	O	|	|	|	| 0.87
43.250	0.00	0.22	1.113	I	O	|	|	|	| 0.87
43.333	0.00	0.22	1.111	I	O	|	|	|	| 0.87
43.417	0.00	0.22	1.110	I	O	|	|	|	| 0.87
43.500	0.00	0.22	1.108	I	O	|	|	|	| 0.87
43.583	0.00	0.22	1.107	I	O	|	|	|	| 0.86
43.667	0.00	0.22	1.105	I	O	|	|	|	| 0.86
43.750	0.00	0.22	1.104	I	O	|	|	|	| 0.86
43.833	0.00	0.22	1.102	I	O	|	|	|	| 0.86
43.917	0.00	0.22	1.101	I	O	|	|	|	| 0.86
44.000	0.00	0.22	1.099	I	O	|	|	|	| 0.86
44.083	0.00	0.22	1.098	I	O	|	|	|	| 0.86
44.167	0.00	0.22	1.096	I	O	|	|	|	| 0.86
44.250	0.00	0.22	1.095	I	O	|	|	|	| 0.85
44.333	0.00	0.22	1.093	I	O	|	|	|	| 0.85
44.417	0.00	0.22	1.092	I	O	|	|	|	| 0.85
44.500	0.00	0.22	1.090	I	O	|	|	|	| 0.85
44.583	0.00	0.22	1.089	I	O	|	|	|	| 0.85
44.667	0.00	0.22	1.087	I	O	|	|	|	| 0.85
44.750	0.00	0.22	1.085	I	O	|	|	|	| 0.85
44.833	0.00	0.22	1.084	I	O	|	|	|	| 0.85
44.917	0.00	0.22	1.082	I	O	|	|	|	| 0.85
45.000	0.00	0.22	1.081	I	O	|	|	|	| 0.84
45.083	0.00	0.22	1.079	I	O	|	|	|	| 0.84
45.167	0.00	0.22	1.078	I	O	|	|	|	| 0.84
45.250	0.00	0.22	1.076	I	O	|	|	|	| 0.84
45.333	0.00	0.22	1.075	I	O	|	|	|	| 0.84
45.417	0.00	0.22	1.073	I	O	|	|	|	| 0.84
45.500	0.00	0.22	1.072	I	O	|	|	|	| 0.84
45.583	0.00	0.22	1.070	I	O	|	|	|	| 0.84
45.667	0.00	0.22	1.069	I	O	|	|	|	| 0.84
45.750	0.00	0.22	1.067	I	O	|	|	|	| 0.83
45.833	0.00	0.22	1.066	I	O	|	|	|	| 0.83
45.917	0.00	0.22	1.064	I	O	|	|	|	| 0.83
46.000	0.00	0.22	1.063	I	O	|	|	|	| 0.83
46.083	0.00	0.22	1.061	I	O	|	|	|	| 0.83
46.167	0.00	0.22	1.060	I	O	|	|	|	| 0.83
46.250	0.00	0.22	1.058	I	O	|	|	|	| 0.83
46.333	0.00	0.22	1.057	I	O	|	|	|	| 0.83
46.417	0.00	0.22	1.055	I	O	|	|	|	| 0.83
46.500	0.00	0.22	1.054	I	O	|	|	|	| 0.82
46.583	0.00	0.22	1.052	I	O	|	|	|	| 0.82
46.667	0.00	0.22	1.051	I	O	|	|	|	| 0.82
46.750	0.00	0.22	1.049	I	O	|	|	|	| 0.82
46.833	0.00	0.22	1.048	I	O	|	|	|	| 0.82
46.917	0.00	0.22	1.046	I	O	|	|	|	| 0.82
47.000	0.00	0.22	1.045	I	O	|	|	|	| 0.82
47.083	0.00	0.22	1.043	I	O	|	|	|	| 0.82
47.167	0.00	0.22	1.042	I	O	|	|	|	| 0.82
47.250	0.00	0.22	1.040	I	O	|	|	|	| 0.81
47.333	0.00	0.22	1.039	I	O	|	|	|	| 0.81
47.417	0.00	0.22	1.037	I	O	|	|	|	| 0.81
47.500	0.00	0.22	1.036	I	O	|	|	|	| 0.81

47.583	0.00	0.22	1.034	I	O	|	|	|	| 0.81
47.667	0.00	0.22	1.033	I	O	|	|	|	| 0.81
47.750	0.00	0.22	1.031	I	O	|	|	|	| 0.81
47.833	0.00	0.21	1.030	I	O	|	|	|	| 0.81
47.917	0.00	0.21	1.029	I	O	|	|	|	| 0.81
48.000	0.00	0.21	1.027	I	O	|	|	|	| 0.80
48.083	0.00	0.21	1.026	I	O	|	|	|	| 0.80
48.167	0.00	0.21	1.024	I	O	|	|	|	| 0.80
48.250	0.00	0.21	1.023	I	O	|	|	|	| 0.80
48.333	0.00	0.21	1.021	I	O	|	|	|	| 0.80
48.417	0.00	0.21	1.020	I	O	|	|	|	| 0.80
48.500	0.00	0.21	1.018	I	O	|	|	|	| 0.80
48.583	0.00	0.21	1.017	I	O	|	|	|	| 0.80
48.667	0.00	0.21	1.015	I	O	|	|	|	| 0.80
48.750	0.00	0.21	1.014	I	O	|	|	|	| 0.79
48.833	0.00	0.21	1.012	I	O	|	|	|	| 0.79
48.917	0.00	0.21	1.011	I	O	|	|	|	| 0.79
49.000	0.00	0.21	1.009	I	O	|	|	|	| 0.79
49.083	0.00	0.21	1.008	I	O	|	|	|	| 0.79
49.167	0.00	0.21	1.006	I	O	|	|	|	| 0.79
49.250	0.00	0.21	1.005	I	O	|	|	|	| 0.79
49.333	0.00	0.21	1.004	I	O	|	|	|	| 0.79
49.417	0.00	0.21	1.002	I	O	|	|	|	| 0.79
49.500	0.00	0.21	1.001	I	O	|	|	|	| 0.79
49.583	0.00	0.21	0.999	I	O	|	|	|	| 0.78
49.667	0.00	0.21	0.998	I	O	|	|	|	| 0.78
49.750	0.00	0.21	0.996	I	O	|	|	|	| 0.78
49.833	0.00	0.21	0.995	I	O	|	|	|	| 0.78
49.917	0.00	0.21	0.993	I	O	|	|	|	| 0.78
50.000	0.00	0.21	0.992	I	O	|	|	|	| 0.78
50.083	0.00	0.21	0.990	I	O	|	|	|	| 0.78
50.167	0.00	0.21	0.989	I	O	|	|	|	| 0.78
50.250	0.00	0.21	0.987	I	O	|	|	|	| 0.78
50.333	0.00	0.21	0.986	I	O	|	|	|	| 0.77
50.417	0.00	0.21	0.985	I	O	|	|	|	| 0.77
50.500	0.00	0.21	0.983	I	O	|	|	|	| 0.77
50.583	0.00	0.21	0.982	I	O	|	|	|	| 0.77
50.667	0.00	0.21	0.980	I	O	|	|	|	| 0.77
50.750	0.00	0.21	0.979	I	O	|	|	|	| 0.77
50.833	0.00	0.21	0.977	I	O	|	|	|	| 0.77
50.917	0.00	0.21	0.976	I	O	|	|	|	| 0.77
51.000	0.00	0.21	0.974	I	O	|	|	|	| 0.77
51.083	0.00	0.21	0.973	I	O	|	|	|	| 0.76
51.167	0.00	0.21	0.972	I	O	|	|	|	| 0.76
51.250	0.00	0.21	0.970	I	O	|	|	|	| 0.76
51.333	0.00	0.21	0.969	I	O	|	|	|	| 0.76
51.417	0.00	0.21	0.967	I	O	|	|	|	| 0.76
51.500	0.00	0.21	0.966	I	O	|	|	|	| 0.76
51.583	0.00	0.21	0.964	I	O	|	|	|	| 0.76
51.667	0.00	0.21	0.963	I	O	|	|	|	| 0.76
51.750	0.00	0.21	0.962	I	O	|	|	|	| 0.76
51.833	0.00	0.21	0.960	I	O	|	|	|	| 0.76
51.917	0.00	0.21	0.959	I	O	|	|	|	| 0.75
52.000	0.00	0.21	0.957	I	O	|	|	|	| 0.75
52.083	0.00	0.21	0.956	I	O	|	|	|	| 0.75
52.167	0.00	0.21	0.954	I	O	|	|	|	| 0.75
52.250	0.00	0.21	0.953	I	O	|	|	|	| 0.75
52.333	0.00	0.21	0.952	I	O	|	|	|	| 0.75
52.417	0.00	0.21	0.950	I	O	|	|	|	| 0.75
52.500	0.00	0.21	0.949	I	O	|	|	|	| 0.75
52.583	0.00	0.21	0.947	I	O	|	|	|	| 0.75
52.667	0.00	0.21	0.946	I	O	|	|	|	| 0.74
52.750	0.00	0.21	0.944	I	O	|	|	|	| 0.74
52.833	0.00	0.21	0.943	I	O	|	|	|	| 0.74
52.917	0.00	0.21	0.942	I	O	|	|	|	| 0.74
53.000	0.00	0.21	0.940	I	O	|	|	|	| 0.74
53.083	0.00	0.21	0.939	I	O	|	|	|	| 0.74
53.167	0.00	0.21	0.937	I	O	|	|	|	| 0.74
53.250	0.00	0.21	0.936	I	O	|	|	|	| 0.74
53.333	0.00	0.21	0.935	I	O	|	|	|	| 0.74
53.417	0.00	0.20	0.933	I	O	|	|	|	| 0.74

53.500	0.00	0.20	0.932	I	O				0.73
53.583	0.00	0.20	0.930	I	O				0.73
53.667	0.00	0.20	0.929	I	O				0.73
53.750	0.00	0.20	0.927	I	O				0.73
53.833	0.00	0.20	0.926	I	O				0.73
53.917	0.00	0.20	0.925	I	O				0.73
54.000	0.00	0.20	0.923	I	O				0.73
54.083	0.00	0.20	0.922	I	O				0.73
54.167	0.00	0.20	0.920	I	O				0.73
54.250	0.00	0.20	0.919	I	O				0.72
54.333	0.00	0.20	0.918	I	O				0.72
54.417	0.00	0.20	0.916	I	O				0.72
54.500	0.00	0.20	0.915	I	O				0.72
54.583	0.00	0.20	0.913	I	O				0.72
54.667	0.00	0.20	0.912	I	O				0.72
54.750	0.00	0.20	0.911	I	O				0.72
54.833	0.00	0.20	0.909	I	O				0.72
54.917	0.00	0.20	0.908	I	O				0.72
55.000	0.00	0.20	0.906	I	O				0.72
55.083	0.00	0.20	0.905	I	O				0.71
55.167	0.00	0.20	0.904	I	O				0.71
55.250	0.00	0.20	0.902	I	O				0.71
55.333	0.00	0.20	0.901	I	O				0.71
55.417	0.00	0.20	0.900	I	O				0.71
55.500	0.00	0.20	0.898	I	O				0.71
55.583	0.00	0.20	0.897	I	O				0.71
55.667	0.00	0.20	0.895	I	O				0.71
55.750	0.00	0.20	0.894	I	O				0.71
55.833	0.00	0.20	0.893	I	O				0.71
55.917	0.00	0.20	0.891	I	O				0.70
56.000	0.00	0.20	0.890	I	O				0.70
56.083	0.00	0.20	0.888	I	O				0.70
56.167	0.00	0.20	0.887	I	O				0.70
56.250	0.00	0.20	0.886	I	O				0.70
56.333	0.00	0.20	0.884	I	O				0.70
56.417	0.00	0.20	0.883	I	O				0.70
56.500	0.00	0.20	0.882	I	O				0.70
56.583	0.00	0.20	0.880	I	O				0.70
56.667	0.00	0.20	0.879	I	O				0.69
56.750	0.00	0.20	0.877	I	O				0.69
56.833	0.00	0.20	0.876	I	O				0.69
56.917	0.00	0.20	0.875	I	O				0.69
57.000	0.00	0.20	0.873	I	O				0.69
57.083	0.00	0.20	0.872	I	O				0.69
57.167	0.00	0.20	0.871	I	O				0.69
57.250	0.00	0.20	0.869	I	O				0.69
57.333	0.00	0.20	0.868	I	O				0.69
57.417	0.00	0.20	0.867	I	O				0.69
57.500	0.00	0.20	0.865	I	O				0.68
57.583	0.00	0.20	0.864	I	O				0.68
57.667	0.00	0.20	0.862	I	O				0.68
57.750	0.00	0.20	0.861	I	O				0.68
57.833	0.00	0.20	0.860	I	O				0.68
57.917	0.00	0.20	0.858	I	O				0.68
58.000	0.00	0.20	0.857	I	O				0.68
58.083	0.00	0.20	0.856	I	O				0.68
58.167	0.00	0.20	0.854	I	O				0.68
58.250	0.00	0.20	0.853	I	O				0.68
58.333	0.00	0.20	0.852	I	O				0.67
58.417	0.00	0.20	0.850	I	O				0.67
58.500	0.00	0.20	0.849	I	O				0.67
58.583	0.00	0.20	0.848	I	O				0.67
58.667	0.00	0.20	0.846	I	O				0.67
58.750	0.00	0.20	0.845	I	O				0.67
58.833	0.00	0.20	0.843	I	O				0.67
58.917	0.00	0.20	0.842	I	O				0.67
59.000	0.00	0.20	0.841	I	O				0.67
59.083	0.00	0.20	0.839	I	O				0.67
59.167	0.00	0.20	0.838	I	O				0.66
59.250	0.00	0.19	0.837	I	O				0.66
59.333	0.00	0.19	0.835	I	O				0.66

59.417	0.00	0.19	0.834	I O				0.66
59.500	0.00	0.19	0.833	I O				0.66
59.583	0.00	0.19	0.831	I O				0.66
59.667	0.00	0.19	0.830	I O				0.66
59.750	0.00	0.19	0.829	I O				0.66
59.833	0.00	0.19	0.827	I O				0.66
59.917	0.00	0.19	0.826	I O				0.66
60.000	0.00	0.19	0.825	I O				0.65
60.083	0.00	0.19	0.823	I O				0.65
60.167	0.00	0.19	0.822	I O				0.65
60.250	0.00	0.19	0.821	I O				0.65
60.333	0.00	0.19	0.819	I O				0.65
60.417	0.00	0.19	0.818	I O				0.65
60.500	0.00	0.19	0.817	I O				0.65
60.583	0.00	0.19	0.815	I O				0.65
60.667	0.00	0.19	0.814	I O				0.65
60.750	0.00	0.19	0.813	I O				0.65
60.833	0.00	0.19	0.811	I O				0.64
60.917	0.00	0.19	0.810	I O				0.64
61.000	0.00	0.19	0.809	I O				0.64
61.083	0.00	0.19	0.807	I O				0.64
61.167	0.00	0.19	0.806	I O				0.64
61.250	0.00	0.19	0.805	I O				0.64
61.333	0.00	0.19	0.804	I O				0.64
61.417	0.00	0.19	0.802	I O				0.64
61.500	0.00	0.19	0.801	I O				0.64
61.583	0.00	0.19	0.800	I O				0.64
61.667	0.00	0.19	0.798	I O				0.64
61.750	0.00	0.19	0.797	I O				0.63
61.833	0.00	0.19	0.796	I O				0.63
61.917	0.00	0.19	0.794	I O				0.63
62.000	0.00	0.19	0.793	I O				0.63
62.083	0.00	0.19	0.792	I O				0.63
62.167	0.00	0.19	0.790	I O				0.63
62.250	0.00	0.19	0.789	I O				0.63
62.333	0.00	0.19	0.788	I O				0.63
62.417	0.00	0.19	0.786	I O				0.63
62.500	0.00	0.19	0.785	I O				0.63
62.583	0.00	0.19	0.784	I O				0.62
62.667	0.00	0.19	0.783	I O				0.62
62.750	0.00	0.19	0.781	I O				0.62
62.833	0.00	0.19	0.780	I O				0.62
62.917	0.00	0.19	0.779	I O				0.62
63.000	0.00	0.19	0.777	I O				0.62
63.083	0.00	0.19	0.776	I O				0.62
63.167	0.00	0.19	0.775	I O				0.62
63.250	0.00	0.19	0.773	I O				0.62
63.333	0.00	0.19	0.772	I O				0.62
63.417	0.00	0.19	0.771	I O				0.61
63.500	0.00	0.19	0.770	I O				0.61
63.583	0.00	0.19	0.768	I O				0.61
63.667	0.00	0.19	0.767	IO				0.61
63.750	0.00	0.19	0.766	IO				0.61
63.833	0.00	0.19	0.764	IO				0.61
63.917	0.00	0.19	0.763	IO				0.61
64.000	0.00	0.19	0.762	IO				0.61
64.083	0.00	0.19	0.761	IO				0.61
64.167	0.00	0.19	0.759	IO				0.61
64.250	0.00	0.19	0.758	IO				0.61
64.333	0.00	0.19	0.757	IO				0.60
64.417	0.00	0.19	0.755	IO				0.60
64.500	0.00	0.19	0.754	IO				0.60
64.583	0.00	0.19	0.753	IO				0.60
64.667	0.00	0.19	0.752	IO				0.60
64.750	0.00	0.19	0.750	IO				0.60
64.833	0.00	0.19	0.749	IO				0.60
64.917	0.00	0.19	0.748	IO				0.60
65.000	0.00	0.19	0.746	IO				0.60
65.083	0.00	0.19	0.745	IO				0.60
65.167	0.00	0.19	0.744	IO				0.59
65.250	0.00	0.19	0.743	IO				0.59

65.333	0.00	0.19	0.741	IO				0.59
65.417	0.00	0.18	0.740	IO				0.59
65.500	0.00	0.18	0.739	IO				0.59
65.583	0.00	0.18	0.737	IO				0.59
65.667	0.00	0.18	0.736	IO				0.59
65.750	0.00	0.18	0.735	IO				0.59
65.833	0.00	0.18	0.734	IO				0.59
65.917	0.00	0.18	0.732	IO				0.59
66.000	0.00	0.18	0.731	IO				0.59
66.083	0.00	0.18	0.730	IO				0.58
66.167	0.00	0.18	0.729	IO				0.58
66.250	0.00	0.18	0.727	IO				0.58
66.333	0.00	0.18	0.726	IO				0.58
66.417	0.00	0.18	0.725	IO				0.58
66.500	0.00	0.18	0.724	IO				0.58
66.583	0.00	0.18	0.722	IO				0.58
66.667	0.00	0.18	0.721	IO				0.58
66.750	0.00	0.18	0.720	IO				0.58
66.833	0.00	0.18	0.719	IO				0.58
66.917	0.00	0.18	0.717	IO				0.58
67.000	0.00	0.18	0.716	IO				0.57
67.083	0.00	0.18	0.715	IO				0.57
67.167	0.00	0.18	0.713	IO				0.57
67.250	0.00	0.18	0.712	IO				0.57
67.333	0.00	0.18	0.711	IO				0.57
67.417	0.00	0.18	0.710	IO				0.57
67.500	0.00	0.18	0.708	IO				0.57
67.583	0.00	0.18	0.707	IO				0.57
67.667	0.00	0.18	0.706	IO				0.57
67.750	0.00	0.18	0.705	IO				0.57
67.833	0.00	0.18	0.703	IO				0.56
67.917	0.00	0.18	0.702	IO				0.56
68.000	0.00	0.18	0.701	IO				0.56
68.083	0.00	0.18	0.700	IO				0.56
68.167	0.00	0.18	0.698	IO				0.56
68.250	0.00	0.18	0.697	IO				0.56
68.333	0.00	0.18	0.696	IO				0.56
68.417	0.00	0.18	0.695	IO				0.56
68.500	0.00	0.18	0.694	IO				0.56
68.583	0.00	0.18	0.692	IO				0.56
68.667	0.00	0.18	0.691	IO				0.56
68.750	0.00	0.18	0.690	IO				0.55
68.833	0.00	0.18	0.689	IO				0.55
68.917	0.00	0.18	0.687	IO				0.55
69.000	0.00	0.18	0.686	IO				0.55
69.083	0.00	0.18	0.685	IO				0.55
69.167	0.00	0.18	0.684	IO				0.55
69.250	0.00	0.18	0.682	IO				0.55
69.333	0.00	0.18	0.681	IO				0.55
69.417	0.00	0.18	0.680	IO				0.55
69.500	0.00	0.18	0.679	IO				0.55
69.583	0.00	0.18	0.677	IO				0.55
69.667	0.00	0.18	0.676	IO				0.54
69.750	0.00	0.18	0.675	IO				0.54
69.833	0.00	0.18	0.674	IO				0.54
69.917	0.00	0.18	0.673	IO				0.54
70.000	0.00	0.18	0.671	IO				0.54
70.083	0.00	0.18	0.670	IO				0.54
70.167	0.00	0.18	0.669	IO				0.54
70.250	0.00	0.18	0.668	IO				0.54
70.333	0.00	0.18	0.666	IO				0.54
70.417	0.00	0.18	0.665	IO				0.54
70.500	0.00	0.18	0.664	IO				0.54
70.583	0.00	0.18	0.663	IO				0.53
70.667	0.00	0.18	0.662	IO				0.53
70.750	0.00	0.18	0.660	IO				0.53
70.833	0.00	0.18	0.659	IO				0.53
70.917	0.00	0.18	0.658	IO				0.53
71.000	0.00	0.18	0.657	IO				0.53
71.083	0.00	0.18	0.656	IO				0.53
71.167	0.00	0.18	0.654	IO				0.53

71.250	0.00	0.18	0.653	IO				0.53
71.333	0.00	0.18	0.652	IO				0.53
71.417	0.00	0.18	0.651	IO				0.53
71.500	0.00	0.18	0.649	IO				0.52
71.583	0.00	0.18	0.648	IO				0.52
71.667	0.00	0.18	0.647	IO				0.52
71.750	0.00	0.18	0.646	IO				0.52
71.833	0.00	0.17	0.645	IO				0.52
71.917	0.00	0.17	0.643	IO				0.52
72.000	0.00	0.17	0.642	IO				0.52
72.083	0.00	0.17	0.641	IO				0.52
72.167	0.00	0.17	0.640	IO				0.52
72.250	0.00	0.17	0.639	IO				0.52
72.333	0.00	0.17	0.637	IO				0.52
72.417	0.00	0.17	0.636	IO				0.51
72.500	0.00	0.17	0.635	IO				0.51
72.583	0.00	0.17	0.634	IO				0.51
72.667	0.00	0.17	0.633	IO				0.51
72.750	0.00	0.17	0.631	IO				0.51
72.833	0.00	0.17	0.630	IO				0.51
72.917	0.00	0.17	0.629	IO				0.51
73.000	0.00	0.17	0.628	IO				0.51
73.083	0.00	0.17	0.627	IO				0.51
73.167	0.00	0.17	0.625	IO				0.51
73.250	0.00	0.17	0.624	IO				0.51
73.333	0.00	0.17	0.623	IO				0.51
73.417	0.00	0.17	0.622	IO				0.50
73.500	0.00	0.17	0.621	IO				0.50
73.583	0.00	0.17	0.620	IO				0.50
73.667	0.00	0.17	0.618	IO				0.50
73.750	0.00	0.17	0.617	IO				0.50
73.833	0.00	0.17	0.616	IO				0.50
73.917	0.00	0.17	0.615	IO				0.50
74.000	0.00	0.17	0.614	IO				0.50
74.083	0.00	0.17	0.612	IO				0.50
74.167	0.00	0.17	0.611	IO				0.50
74.250	0.00	0.17	0.610	IO				0.50
74.333	0.00	0.17	0.609	IO				0.49
74.417	0.00	0.17	0.608	IO				0.49
74.500	0.00	0.17	0.607	IO				0.49
74.583	0.00	0.17	0.605	IO				0.49
74.667	0.00	0.17	0.604	IO				0.49
74.750	0.00	0.17	0.603	IO				0.49
74.833	0.00	0.17	0.602	IO				0.49
74.917	0.00	0.17	0.601	IO				0.49
75.000	0.00	0.17	0.600	IO				0.49
75.083	0.00	0.17	0.598	IO				0.49
75.167	0.00	0.17	0.597	IO				0.48
75.250	0.00	0.17	0.596	IO				0.48
75.333	0.00	0.17	0.595	IO				0.48
75.417	0.00	0.17	0.594	IO				0.48
75.500	0.00	0.17	0.593	IO				0.48
75.583	0.00	0.17	0.592	IO				0.48
75.667	0.00	0.16	0.590	IO				0.48
75.750	0.00	0.16	0.589	IO				0.48
75.833	0.00	0.16	0.588	IO				0.48
75.917	0.00	0.16	0.587	IO				0.48
76.000	0.00	0.16	0.586	IO				0.48
76.083	0.00	0.16	0.585	IO				0.47
76.167	0.00	0.16	0.584	IO				0.47
76.250	0.00	0.16	0.583	IO				0.47
76.333	0.00	0.16	0.581	IO				0.47
76.417	0.00	0.16	0.580	IO				0.47
76.500	0.00	0.16	0.579	IO				0.47
76.583	0.00	0.16	0.578	IO				0.47
76.667	0.00	0.16	0.577	IO				0.47
76.750	0.00	0.16	0.576	IO				0.47
76.833	0.00	0.16	0.575	IO				0.47
76.917	0.00	0.16	0.574	IO				0.47
77.000	0.00	0.16	0.573	IO				0.46
77.083	0.00	0.16	0.571	IO				0.46

77.167	0.00	0.16	0.570	IO				0.46
77.250	0.00	0.16	0.569	IO				0.46
77.333	0.00	0.16	0.568	IO				0.46
77.417	0.00	0.16	0.567	IO				0.46
77.500	0.00	0.16	0.566	IO				0.46
77.583	0.00	0.16	0.565	IO				0.46
77.667	0.00	0.16	0.564	IO				0.46
77.750	0.00	0.16	0.563	IO				0.46
77.833	0.00	0.16	0.562	IO				0.46
77.917	0.00	0.16	0.561	IO				0.46
78.000	0.00	0.16	0.559	IO				0.45
78.083	0.00	0.16	0.558	IO				0.45
78.167	0.00	0.16	0.557	IO				0.45
78.250	0.00	0.16	0.556	IO				0.45
78.333	0.00	0.16	0.555	IO				0.45
78.417	0.00	0.15	0.554	IO				0.45
78.500	0.00	0.15	0.553	IO				0.45
78.583	0.00	0.15	0.552	IO				0.45
78.667	0.00	0.15	0.551	IO				0.45
78.750	0.00	0.15	0.550	IO				0.45
78.833	0.00	0.15	0.549	IO				0.45
78.917	0.00	0.15	0.548	IO				0.44
79.000	0.00	0.15	0.547	IO				0.44
79.083	0.00	0.15	0.546	IO				0.44
79.167	0.00	0.15	0.545	IO				0.44
79.250	0.00	0.15	0.544	IO				0.44
79.333	0.00	0.15	0.543	IO				0.44
79.417	0.00	0.15	0.541	IO				0.44
79.500	0.00	0.15	0.540	IO				0.44
79.583	0.00	0.15	0.539	IO				0.44
79.667	0.00	0.15	0.538	IO				0.44
79.750	0.00	0.15	0.537	IO				0.44
79.833	0.00	0.15	0.536	IO				0.44
79.917	0.00	0.15	0.535	IO				0.43
80.000	0.00	0.15	0.534	IO				0.43
80.083	0.00	0.15	0.533	IO				0.43
80.167	0.00	0.15	0.532	IO				0.43
80.250	0.00	0.15	0.531	IO				0.43
80.333	0.00	0.15	0.530	IO				0.43
80.417	0.00	0.15	0.529	IO				0.43
80.500	0.00	0.15	0.528	IO				0.43
80.583	0.00	0.15	0.527	IO				0.43
80.667	0.00	0.15	0.526	IO				0.43
80.750	0.00	0.15	0.525	IO				0.43
80.833	0.00	0.15	0.524	IO				0.43
80.917	0.00	0.15	0.523	IO				0.42
81.000	0.00	0.15	0.522	IO				0.42
81.083	0.00	0.15	0.521	IO				0.42
81.167	0.00	0.15	0.520	IO				0.42
81.250	0.00	0.14	0.519	IO				0.42
81.333	0.00	0.14	0.518	IO				0.42
81.417	0.00	0.14	0.517	IO				0.42
81.500	0.00	0.14	0.516	IO				0.42
81.583	0.00	0.14	0.515	IO				0.42
81.667	0.00	0.14	0.514	IO				0.42
81.750	0.00	0.14	0.513	IO				0.42
81.833	0.00	0.14	0.512	IO				0.42
81.917	0.00	0.14	0.511	IO				0.41
82.000	0.00	0.14	0.510	IO				0.41
82.083	0.00	0.14	0.509	IO				0.41
82.167	0.00	0.14	0.508	IO				0.41
82.250	0.00	0.14	0.507	IO				0.41
82.333	0.00	0.14	0.506	IO				0.41
82.417	0.00	0.14	0.505	IO				0.41
82.500	0.00	0.14	0.504	IO				0.41
82.583	0.00	0.14	0.503	IO				0.41
82.667	0.00	0.14	0.502	IO				0.41
82.750	0.00	0.14	0.501	IO				0.41
82.833	0.00	0.14	0.500	IO				0.41
82.917	0.00	0.14	0.499	IO				0.41
83.000	0.00	0.14	0.499	IO				0.40

83.083	0.00	0.14	0.498	IO				0.40
83.167	0.00	0.14	0.497	IO				0.40
83.250	0.00	0.14	0.496	IO				0.40
83.333	0.00	0.14	0.495	IO				0.40
83.417	0.00	0.14	0.494	IO				0.40
83.500	0.00	0.14	0.493	IO				0.40
83.583	0.00	0.14	0.492	IO				0.40
83.667	0.00	0.14	0.491	IO				0.40
83.750	0.00	0.14	0.490	IO				0.40
83.833	0.00	0.14	0.489	IO				0.40
83.917	0.00	0.14	0.488	IO				0.40
84.000	0.00	0.14	0.487	IO				0.40
84.083	0.00	0.14	0.486	IO				0.39
84.167	0.00	0.14	0.485	IO				0.39
84.250	0.00	0.14	0.484	IO				0.39
84.333	0.00	0.13	0.483	IO				0.39
84.417	0.00	0.13	0.482	IO				0.39
84.500	0.00	0.13	0.482	IO				0.39
84.583	0.00	0.13	0.481	IO				0.39
84.667	0.00	0.13	0.480	IO				0.39
84.750	0.00	0.13	0.479	IO				0.39
84.833	0.00	0.13	0.478	IO				0.39
84.917	0.00	0.13	0.477	IO				0.39
85.000	0.00	0.13	0.476	IO				0.39
85.083	0.00	0.13	0.475	IO				0.39
85.167	0.00	0.13	0.474	IO				0.38
85.250	0.00	0.13	0.473	IO				0.38
85.333	0.00	0.13	0.472	IO				0.38
85.417	0.00	0.13	0.471	IO				0.38
85.500	0.00	0.13	0.471	IO				0.38
85.583	0.00	0.13	0.470	IO				0.38
85.667	0.00	0.13	0.469	IO				0.38
85.750	0.00	0.13	0.468	IO				0.38
85.833	0.00	0.13	0.467	IO				0.38
85.917	0.00	0.13	0.466	IO				0.38
86.000	0.00	0.13	0.465	IO				0.38
86.083	0.00	0.13	0.464	IO				0.38
86.167	0.00	0.13	0.463	IO				0.38
86.250	0.00	0.13	0.463	IO				0.38
86.333	0.00	0.13	0.462	IO				0.37
86.417	0.00	0.13	0.461	IO				0.37
86.500	0.00	0.13	0.460	IO				0.37
86.583	0.00	0.13	0.459	IO				0.37
86.667	0.00	0.13	0.458	IO				0.37
86.750	0.00	0.13	0.457	IO				0.37
86.833	0.00	0.13	0.456	IO				0.37
86.917	0.00	0.13	0.455	IO				0.37
87.000	0.00	0.13	0.455	IO				0.37
87.083	0.00	0.13	0.454	IO				0.37
87.167	0.00	0.13	0.453	IO				0.37
87.250	0.00	0.13	0.452	IO				0.37
87.333	0.00	0.13	0.451	IO				0.37
87.417	0.00	0.13	0.450	IO				0.37
87.500	0.00	0.13	0.449	IO				0.36
87.583	0.00	0.13	0.448	IO				0.36
87.667	0.00	0.12	0.448	IO				0.36
87.750	0.00	0.12	0.447	IO				0.36
87.833	0.00	0.12	0.446	IO				0.36
87.917	0.00	0.12	0.445	IO				0.36
88.000	0.00	0.12	0.444	IO				0.36
88.083	0.00	0.12	0.443	IO				0.36
88.167	0.00	0.12	0.442	IO				0.36
88.250	0.00	0.12	0.442	IO				0.36
88.333	0.00	0.12	0.441	IO				0.36
88.417	0.00	0.12	0.440	IO				0.36
88.500	0.00	0.12	0.439	IO				0.36
88.583	0.00	0.12	0.438	IO				0.36
88.667	0.00	0.12	0.437	IO				0.36
88.750	0.00	0.12	0.437	IO				0.35
88.833	0.00	0.12	0.436	IO				0.35
88.917	0.00	0.12	0.435	IO				0.35

89.000	0.00	0.12	0.434	IO				0.35
89.083	0.00	0.12	0.433	IO				0.35
89.167	0.00	0.12	0.432	IO				0.35
89.250	0.00	0.12	0.432	IO				0.35
89.333	0.00	0.12	0.431	IO				0.35
89.417	0.00	0.12	0.430	IO				0.35
89.500	0.00	0.12	0.429	IO				0.35
89.583	0.00	0.12	0.428	IO				0.35
89.667	0.00	0.12	0.427	IO				0.35
89.750	0.00	0.12	0.427	IO				0.35
89.833	0.00	0.12	0.426	IO				0.35
89.917	0.00	0.12	0.425	IO				0.34
90.000	0.00	0.12	0.424	IO				0.34
90.083	0.00	0.12	0.423	IO				0.34
90.167	0.00	0.12	0.423	IO				0.34
90.250	0.00	0.12	0.422	IO				0.34
90.333	0.00	0.12	0.421	IO				0.34
90.417	0.00	0.12	0.420	IO				0.34
90.500	0.00	0.12	0.419	IO				0.34
90.583	0.00	0.12	0.418	IO				0.34
90.667	0.00	0.12	0.418	IO				0.34
90.750	0.00	0.12	0.417	IO				0.34
90.833	0.00	0.12	0.416	IO				0.34
90.917	0.00	0.12	0.415	IO				0.34
91.000	0.00	0.12	0.414	IO				0.34
91.083	0.00	0.12	0.414	IO				0.34
91.167	0.00	0.12	0.413	IO				0.34
91.250	0.00	0.12	0.412	IO				0.33
91.333	0.00	0.11	0.411	IO				0.33
91.417	0.00	0.11	0.411	IO				0.33
91.500	0.00	0.11	0.410	IO				0.33
91.583	0.00	0.11	0.409	IO				0.33
91.667	0.00	0.11	0.408	IO				0.33
91.750	0.00	0.11	0.407	IO				0.33
91.833	0.00	0.11	0.407	IO				0.33
91.917	0.00	0.11	0.406	IO				0.33
92.000	0.00	0.11	0.405	IO				0.33
92.083	0.00	0.11	0.404	IO				0.33
92.167	0.00	0.11	0.403	IO				0.33
92.250	0.00	0.11	0.403	IO				0.33
92.333	0.00	0.11	0.402	IO				0.33
92.417	0.00	0.11	0.401	IO				0.33
92.500	0.00	0.11	0.400	IO				0.32
92.583	0.00	0.11	0.400	IO				0.32
92.667	0.00	0.11	0.399	IO				0.32
92.750	0.00	0.11	0.398	IO				0.32
92.833	0.00	0.11	0.397	IO				0.32
92.917	0.00	0.11	0.397	IO				0.32
93.000	0.00	0.11	0.396	IO				0.32
93.083	0.00	0.11	0.395	IO				0.32
93.167	0.00	0.11	0.394	IO				0.32
93.250	0.00	0.11	0.394	IO				0.32
93.333	0.00	0.11	0.393	IO				0.32
93.417	0.00	0.11	0.392	IO				0.32
93.500	0.00	0.11	0.391	IO				0.32
93.583	0.00	0.11	0.390	IO				0.32
93.667	0.00	0.11	0.390	IO				0.32
93.750	0.00	0.11	0.389	IO				0.32
93.833	0.00	0.11	0.388	IO				0.32
93.917	0.00	0.11	0.388	IO				0.31
94.000	0.00	0.11	0.387	IO				0.31
94.083	0.00	0.11	0.386	IO				0.31
94.167	0.00	0.11	0.385	IO				0.31
94.250	0.00	0.11	0.385	IO				0.31
94.333	0.00	0.11	0.384	IO				0.31
94.417	0.00	0.11	0.383	IO				0.31
94.500	0.00	0.11	0.382	IO				0.31
94.583	0.00	0.11	0.382	IO				0.31
94.667	0.00	0.11	0.381	IO				0.31
94.750	0.00	0.11	0.380	IO				0.31
94.833	0.00	0.11	0.379	IO				0.31

94.917	0.00	0.11	0.379	IO				0.31
95.000	0.00	0.11	0.378	IO				0.31
95.083	0.00	0.11	0.377	IO				0.31
95.167	0.00	0.11	0.376	IO				0.31
95.250	0.00	0.10	0.376	IO				0.31
95.333	0.00	0.10	0.375	IO				0.30
95.417	0.00	0.10	0.374	IO				0.30
95.500	0.00	0.10	0.374	IO				0.30
95.583	0.00	0.10	0.373	IO				0.30
95.667	0.00	0.10	0.372	IO				0.30
95.750	0.00	0.10	0.371	IO				0.30
95.833	0.00	0.10	0.371	IO				0.30
95.917	0.00	0.10	0.370	IO				0.30
96.000	0.00	0.10	0.369	IO				0.30
96.083	0.00	0.10	0.369	IO				0.30
96.167	0.00	0.10	0.368	IO				0.30
96.250	0.00	0.10	0.367	IO				0.30
96.333	0.00	0.10	0.366	IO				0.30
96.417	0.00	0.10	0.366	IO				0.30
96.500	0.00	0.10	0.365	IO				0.30
96.583	0.00	0.10	0.364	IO				0.30
96.667	0.00	0.10	0.364	IO				0.30
96.750	0.00	0.10	0.363	IO				0.29
96.833	0.00	0.10	0.362	IO				0.29
96.917	0.00	0.10	0.362	IO				0.29
97.000	0.00	0.10	0.361	IO				0.29
97.083	0.00	0.10	0.360	IO				0.29
97.167	0.00	0.10	0.360	IO				0.29
97.250	0.00	0.10	0.359	IO				0.29
97.333	0.00	0.10	0.358	IO				0.29
97.417	0.00	0.10	0.357	IO				0.29
97.500	0.00	0.10	0.357	IO				0.29
97.583	0.00	0.10	0.356	IO				0.29
97.667	0.00	0.10	0.355	IO				0.29
97.750	0.00	0.10	0.355	IO				0.29
97.833	0.00	0.10	0.354	IO				0.29
97.917	0.00	0.10	0.353	IO				0.29
98.000	0.00	0.10	0.353	IO				0.29
98.083	0.00	0.10	0.352	IO				0.29
98.167	0.00	0.10	0.351	IO				0.29
98.250	0.00	0.10	0.351	IO				0.28
98.333	0.00	0.10	0.350	IO				0.28
98.417	0.00	0.10	0.349	IO				0.28
98.500	0.00	0.10	0.349	IO				0.28
98.583	0.00	0.10	0.348	IO				0.28
98.667	0.00	0.10	0.347	IO				0.28
98.750	0.00	0.10	0.347	IO				0.28
98.833	0.00	0.10	0.346	IO				0.28
98.917	0.00	0.10	0.345	IO				0.28
99.000	0.00	0.10	0.345	IO				0.28
99.083	0.00	0.10	0.344	IO				0.28
99.167	0.00	0.10	0.343	IO				0.28
99.250	0.00	0.10	0.343	IO				0.28
99.333	0.00	0.10	0.342	IO				0.28
99.417	0.00	0.10	0.341	IO				0.28
99.500	0.00	0.10	0.341	IO				0.28
99.583	0.00	0.09	0.340	IO				0.28
99.667	0.00	0.09	0.339	IO				0.28
99.750	0.00	0.09	0.339	IO				0.27
99.833	0.00	0.09	0.338	IO				0.27
99.917	0.00	0.09	0.337	IO				0.27
100.000	0.00	0.09	0.337	IO				0.27
100.083	0.00	0.09	0.336	IO				0.27
100.167	0.00	0.09	0.335	O				0.27
100.250	0.00	0.09	0.335	O				0.27
100.333	0.00	0.09	0.334	O				0.27
100.417	0.00	0.09	0.334	O				0.27
100.500	0.00	0.09	0.333	O				0.27
100.583	0.00	0.09	0.332	O				0.27
100.667	0.00	0.09	0.332	O				0.27
100.750	0.00	0.09	0.331	O				0.27

100.833	0.00	0.09	0.330	O					0.27
100.917	0.00	0.09	0.330	O					0.27
101.000	0.00	0.09	0.329	O					0.27
101.083	0.00	0.09	0.328	O					0.27
101.167	0.00	0.09	0.328	O					0.27
101.250	0.00	0.09	0.327	O					0.27
101.333	0.00	0.09	0.327	O					0.27
101.417	0.00	0.09	0.326	O					0.26
101.500	0.00	0.09	0.325	O					0.26
101.583	0.00	0.09	0.325	O					0.26
101.667	0.00	0.09	0.324	O					0.26
101.750	0.00	0.09	0.323	O					0.26
101.833	0.00	0.09	0.323	O					0.26
101.917	0.00	0.09	0.322	O					0.26
102.000	0.00	0.09	0.322	O					0.26
102.083	0.00	0.09	0.321	O					0.26
102.167	0.00	0.09	0.320	O					0.26
102.250	0.00	0.09	0.320	O					0.26
102.333	0.00	0.09	0.319	O					0.26
102.417	0.00	0.09	0.318	O					0.26
102.500	0.00	0.09	0.318	O					0.26
102.583	0.00	0.09	0.317	O					0.26
102.667	0.00	0.09	0.317	O					0.26
102.750	0.00	0.09	0.316	O					0.26
102.833	0.00	0.09	0.315	O					0.26
102.917	0.00	0.09	0.315	O					0.26
103.000	0.00	0.09	0.314	O					0.26
103.083	0.00	0.09	0.314	O					0.25
103.167	0.00	0.09	0.313	O					0.25
103.250	0.00	0.09	0.312	O					0.25
103.333	0.00	0.09	0.312	O					0.25
103.417	0.00	0.09	0.311	O					0.25
103.500	0.00	0.09	0.311	O					0.25
103.583	0.00	0.09	0.310	O					0.25
103.667	0.00	0.09	0.309	O					0.25
103.750	0.00	0.09	0.309	O					0.25
103.833	0.00	0.09	0.308	O					0.25
103.917	0.00	0.09	0.308	O					0.25
104.000	0.00	0.09	0.307	O					0.25
104.083	0.00	0.09	0.306	O					0.25
104.167	0.00	0.09	0.306	O					0.25
104.250	0.00	0.09	0.305	O					0.25
104.333	0.00	0.09	0.305	O					0.25
104.417	0.00	0.08	0.304	O					0.25
104.500	0.00	0.08	0.304	O					0.25
104.583	0.00	0.08	0.303	O					0.25
104.667	0.00	0.08	0.302	O					0.25
104.750	0.00	0.08	0.302	O					0.24
104.833	0.00	0.08	0.301	O					0.24
104.917	0.00	0.08	0.301	O					0.24
105.000	0.00	0.08	0.300	O					0.24
105.083	0.00	0.08	0.299	O					0.24
105.167	0.00	0.08	0.299	O					0.24
105.250	0.00	0.08	0.298	O					0.24
105.333	0.00	0.08	0.298	O					0.24
105.417	0.00	0.08	0.297	O					0.24
105.500	0.00	0.08	0.297	O					0.24
105.583	0.00	0.08	0.296	O					0.24
105.667	0.00	0.08	0.295	O					0.24
105.750	0.00	0.08	0.295	O					0.24
105.833	0.00	0.08	0.294	O					0.24
105.917	0.00	0.08	0.294	O					0.24
106.000	0.00	0.08	0.293	O					0.24
106.083	0.00	0.08	0.293	O					0.24
106.167	0.00	0.08	0.292	O					0.24
106.250	0.00	0.08	0.292	O					0.24
106.333	0.00	0.08	0.291	O					0.24
106.417	0.00	0.08	0.290	O					0.24
106.500	0.00	0.08	0.290	O					0.24
106.583	0.00	0.08	0.289	O					0.23
106.667	0.00	0.08	0.289	O					0.23

106.750	0.00	0.08	0.288	O	|	|	|	|	0.23
106.833	0.00	0.08	0.288	O	|	|	|	|	0.23
106.917	0.00	0.08	0.287	O	|	|	|	|	0.23
107.000	0.00	0.08	0.287	O	|	|	|	|	0.23
107.083	0.00	0.08	0.286	O	|	|	|	|	0.23
107.167	0.00	0.08	0.285	O	|	|	|	|	0.23
107.250	0.00	0.08	0.285	O	|	|	|	|	0.23
107.333	0.00	0.08	0.284	O	|	|	|	|	0.23
107.417	0.00	0.08	0.284	O	|	|	|	|	0.23
107.500	0.00	0.08	0.283	O	|	|	|	|	0.23
107.583	0.00	0.08	0.283	O	|	|	|	|	0.23
107.667	0.00	0.08	0.282	O	|	|	|	|	0.23
107.750	0.00	0.08	0.282	O	|	|	|	|	0.23
107.833	0.00	0.08	0.281	O	|	|	|	|	0.23
107.917	0.00	0.08	0.281	O	|	|	|	|	0.23
108.000	0.00	0.08	0.280	O	|	|	|	|	0.23
108.083	0.00	0.08	0.279	O	|	|	|	|	0.23
108.167	0.00	0.08	0.279	O	|	|	|	|	0.23
108.250	0.00	0.08	0.278	O	|	|	|	|	0.23
108.333	0.00	0.08	0.278	O	|	|	|	|	0.23
108.417	0.00	0.08	0.277	O	|	|	|	|	0.23
108.500	0.00	0.08	0.277	O	|	|	|	|	0.22
108.583	0.00	0.08	0.276	O	|	|	|	|	0.22
108.667	0.00	0.08	0.276	O	|	|	|	|	0.22
108.750	0.00	0.08	0.275	O	|	|	|	|	0.22
108.833	0.00	0.08	0.275	O	|	|	|	|	0.22
108.917	0.00	0.08	0.274	O	|	|	|	|	0.22
109.000	0.00	0.08	0.274	O	|	|	|	|	0.22
109.083	0.00	0.08	0.273	O	|	|	|	|	0.22
109.167	0.00	0.08	0.273	O	|	|	|	|	0.22
109.250	0.00	0.08	0.272	O	|	|	|	|	0.22
109.333	0.00	0.08	0.272	O	|	|	|	|	0.22
109.417	0.00	0.08	0.271	O	|	|	|	|	0.22
109.500	0.00	0.08	0.270	O	|	|	|	|	0.22
109.583	0.00	0.08	0.270	O	|	|	|	|	0.22
109.667	0.00	0.08	0.269	O	|	|	|	|	0.22
109.750	0.00	0.08	0.269	O	|	|	|	|	0.22
109.833	0.00	0.07	0.268	O	|	|	|	|	0.22
109.917	0.00	0.07	0.268	O	|	|	|	|	0.22
110.000	0.00	0.07	0.267	O	|	|	|	|	0.22
110.083	0.00	0.07	0.267	O	|	|	|	|	0.22
110.167	0.00	0.07	0.266	O	|	|	|	|	0.22
110.250	0.00	0.07	0.266	O	|	|	|	|	0.22
110.333	0.00	0.07	0.265	O	|	|	|	|	0.22
110.417	0.00	0.07	0.265	O	|	|	|	|	0.21
110.500	0.00	0.07	0.264	O	|	|	|	|	0.21
110.583	0.00	0.07	0.264	O	|	|	|	|	0.21
110.667	0.00	0.07	0.263	O	|	|	|	|	0.21
110.750	0.00	0.07	0.263	O	|	|	|	|	0.21
110.833	0.00	0.07	0.262	O	|	|	|	|	0.21
110.917	0.00	0.07	0.262	O	|	|	|	|	0.21
111.000	0.00	0.07	0.261	O	|	|	|	|	0.21
111.083	0.00	0.07	0.261	O	|	|	|	|	0.21
111.167	0.00	0.07	0.260	O	|	|	|	|	0.21
111.250	0.00	0.07	0.260	O	|	|	|	|	0.21
111.333	0.00	0.07	0.259	O	|	|	|	|	0.21
111.417	0.00	0.07	0.259	O	|	|	|	|	0.21
111.500	0.00	0.07	0.258	O	|	|	|	|	0.21
111.583	0.00	0.07	0.258	O	|	|	|	|	0.21
111.667	0.00	0.07	0.257	O	|	|	|	|	0.21
111.750	0.00	0.07	0.257	O	|	|	|	|	0.21
111.833	0.00	0.07	0.256	O	|	|	|	|	0.21
111.917	0.00	0.07	0.256	O	|	|	|	|	0.21
112.000	0.00	0.07	0.255	O	|	|	|	|	0.21
112.083	0.00	0.07	0.255	O	|	|	|	|	0.21
112.167	0.00	0.07	0.254	O	|	|	|	|	0.21
112.250	0.00	0.07	0.254	O	|	|	|	|	0.21
112.333	0.00	0.07	0.253	O	|	|	|	|	0.21
112.417	0.00	0.07	0.253	O	|	|	|	|	0.21
112.500	0.00	0.07	0.252	O	|	|	|	|	0.20
112.583	0.00	0.07	0.252	O	|	|	|	|	0.20

112.667	0.00	0.07	0.251	O	|	|	|	|	0.20
112.750	0.00	0.07	0.251	O	|	|	|	|	0.20
112.833	0.00	0.07	0.250	O	|	|	|	|	0.20
112.917	0.00	0.07	0.250	O	|	|	|	|	0.20
113.000	0.00	0.07	0.249	O	|	|	|	|	0.20
113.083	0.00	0.07	0.249	O	|	|	|	|	0.20
113.167	0.00	0.07	0.249	O	|	|	|	|	0.20
113.250	0.00	0.07	0.248	O	|	|	|	|	0.20
113.333	0.00	0.07	0.248	O	|	|	|	|	0.20
113.417	0.00	0.07	0.247	O	|	|	|	|	0.20
113.500	0.00	0.07	0.247	O	|	|	|	|	0.20
113.583	0.00	0.07	0.246	O	|	|	|	|	0.20
113.667	0.00	0.07	0.246	O	|	|	|	|	0.20
113.750	0.00	0.07	0.245	O	|	|	|	|	0.20
113.833	0.00	0.07	0.245	O	|	|	|	|	0.20
113.917	0.00	0.07	0.244	O	|	|	|	|	0.20
114.000	0.00	0.07	0.244	O	|	|	|	|	0.20
114.083	0.00	0.07	0.243	O	|	|	|	|	0.20
114.167	0.00	0.07	0.243	O	|	|	|	|	0.20
114.250	0.00	0.07	0.242	O	|	|	|	|	0.20
114.333	0.00	0.07	0.242	O	|	|	|	|	0.20
114.417	0.00	0.07	0.241	O	|	|	|	|	0.20
114.500	0.00	0.07	0.241	O	|	|	|	|	0.20
114.583	0.00	0.07	0.241	O	|	|	|	|	0.20
114.667	0.00	0.07	0.240	O	|	|	|	|	0.19
114.750	0.00	0.07	0.240	O	|	|	|	|	0.19
114.833	0.00	0.07	0.239	O	|	|	|	|	0.19
114.917	0.00	0.07	0.239	O	|	|	|	|	0.19
115.000	0.00	0.07	0.238	O	|	|	|	|	0.19
115.083	0.00	0.07	0.238	O	|	|	|	|	0.19
115.167	0.00	0.07	0.237	O	|	|	|	|	0.19
115.250	0.00	0.07	0.237	O	|	|	|	|	0.19
115.333	0.00	0.07	0.236	O	|	|	|	|	0.19
115.417	0.00	0.07	0.236	O	|	|	|	|	0.19
115.500	0.00	0.07	0.235	O	|	|	|	|	0.19
115.583	0.00	0.07	0.235	O	|	|	|	|	0.19
115.667	0.00	0.07	0.235	O	|	|	|	|	0.19
115.750	0.00	0.07	0.234	O	|	|	|	|	0.19
115.833	0.00	0.07	0.234	O	|	|	|	|	0.19
115.917	0.00	0.07	0.233	O	|	|	|	|	0.19
116.000	0.00	0.06	0.233	O	|	|	|	|	0.19
116.083	0.00	0.06	0.232	O	|	|	|	|	0.19
116.167	0.00	0.06	0.232	O	|	|	|	|	0.19
116.250	0.00	0.06	0.231	O	|	|	|	|	0.19
116.333	0.00	0.06	0.231	O	|	|	|	|	0.19
116.417	0.00	0.06	0.231	O	|	|	|	|	0.19
116.500	0.00	0.06	0.230	O	|	|	|	|	0.19
116.583	0.00	0.06	0.230	O	|	|	|	|	0.19
116.667	0.00	0.06	0.229	O	|	|	|	|	0.19
116.750	0.00	0.06	0.229	O	|	|	|	|	0.19
116.833	0.00	0.06	0.228	O	|	|	|	|	0.19
116.917	0.00	0.06	0.228	O	|	|	|	|	0.18
117.000	0.00	0.06	0.227	O	|	|	|	|	0.18
117.083	0.00	0.06	0.227	O	|	|	|	|	0.18
117.167	0.00	0.06	0.227	O	|	|	|	|	0.18
117.250	0.00	0.06	0.226	O	|	|	|	|	0.18
117.333	0.00	0.06	0.226	O	|	|	|	|	0.18
117.417	0.00	0.06	0.225	O	|	|	|	|	0.18
117.500	0.00	0.06	0.225	O	|	|	|	|	0.18
117.583	0.00	0.06	0.224	O	|	|	|	|	0.18
117.667	0.00	0.06	0.224	O	|	|	|	|	0.18
117.750	0.00	0.06	0.224	O	|	|	|	|	0.18
117.833	0.00	0.06	0.223	O	|	|	|	|	0.18
117.917	0.00	0.06	0.223	O	|	|	|	|	0.18
118.000	0.00	0.06	0.222	O	|	|	|	|	0.18
118.083	0.00	0.06	0.222	O	|	|	|	|	0.18
118.167	0.00	0.06	0.221	O	|	|	|	|	0.18
118.250	0.00	0.06	0.221	O	|	|	|	|	0.18
118.333	0.00	0.06	0.221	O	|	|	|	|	0.18
118.417	0.00	0.06	0.220	O	|	|	|	|	0.18
118.500	0.00	0.06	0.220	O	|	|	|	|	0.18

118.583	0.00	0.06	0.219	O	|	|	|	|	0.18
118.667	0.00	0.06	0.219	O	|	|	|	|	0.18
118.750	0.00	0.06	0.218	O	|	|	|	|	0.18
118.833	0.00	0.06	0.218	O	|	|	|	|	0.18
118.917	0.00	0.06	0.218	O	|	|	|	|	0.18
119.000	0.00	0.06	0.217	O	|	|	|	|	0.18
119.083	0.00	0.06	0.217	O	|	|	|	|	0.18
119.167	0.00	0.06	0.216	O	|	|	|	|	0.18
119.250	0.00	0.06	0.216	O	|	|	|	|	0.18
119.333	0.00	0.06	0.216	O	|	|	|	|	0.17
119.417	0.00	0.06	0.215	O	|	|	|	|	0.17
119.500	0.00	0.06	0.215	O	|	|	|	|	0.17
119.583	0.00	0.06	0.214	O	|	|	|	|	0.17
119.667	0.00	0.06	0.214	O	|	|	|	|	0.17
119.750	0.00	0.06	0.213	O	|	|	|	|	0.17
119.833	0.00	0.06	0.213	O	|	|	|	|	0.17
119.917	0.00	0.06	0.213	O	|	|	|	|	0.17
120.000	0.00	0.06	0.212	O	|	|	|	|	0.17
120.083	0.00	0.06	0.212	O	|	|	|	|	0.17
120.167	0.00	0.06	0.211	O	|	|	|	|	0.17
120.250	0.00	0.06	0.211	O	|	|	|	|	0.17
120.333	0.00	0.06	0.211	O	|	|	|	|	0.17
120.417	0.00	0.06	0.210	O	|	|	|	|	0.17
120.500	0.00	0.06	0.210	O	|	|	|	|	0.17
120.583	0.00	0.06	0.209	O	|	|	|	|	0.17
120.667	0.00	0.06	0.209	O	|	|	|	|	0.17
120.750	0.00	0.06	0.209	O	|	|	|	|	0.17
120.833	0.00	0.06	0.208	O	|	|	|	|	0.17
120.917	0.00	0.06	0.208	O	|	|	|	|	0.17
121.000	0.00	0.06	0.207	O	|	|	|	|	0.17
121.083	0.00	0.06	0.207	O	|	|	|	|	0.17
121.167	0.00	0.06	0.207	O	|	|	|	|	0.17
121.250	0.00	0.06	0.206	O	|	|	|	|	0.17
121.333	0.00	0.06	0.206	O	|	|	|	|	0.17
121.417	0.00	0.06	0.205	O	|	|	|	|	0.17
121.500	0.00	0.06	0.205	O	|	|	|	|	0.17
121.583	0.00	0.06	0.205	O	|	|	|	|	0.17
121.667	0.00	0.06	0.204	O	|	|	|	|	0.17
121.750	0.00	0.06	0.204	O	|	|	|	|	0.17
121.833	0.00	0.06	0.203	O	|	|	|	|	0.17
121.917	0.00	0.06	0.203	O	|	|	|	|	0.16
122.000	0.00	0.06	0.203	O	|	|	|	|	0.16
122.083	0.00	0.06	0.202	O	|	|	|	|	0.16
122.167	0.00	0.06	0.202	O	|	|	|	|	0.16
122.250	0.00	0.06	0.202	O	|	|	|	|	0.16
122.333	0.00	0.06	0.201	O	|	|	|	|	0.16
122.417	0.00	0.06	0.201	O	|	|	|	|	0.16
122.500	0.00	0.06	0.200	O	|	|	|	|	0.16
122.583	0.00	0.06	0.200	O	|	|	|	|	0.16
122.667	0.00	0.06	0.200	O	|	|	|	|	0.16
122.750	0.00	0.06	0.199	O	|	|	|	|	0.16
122.833	0.00	0.06	0.199	O	|	|	|	|	0.16
122.917	0.00	0.06	0.198	O	|	|	|	|	0.16
123.000	0.00	0.06	0.198	O	|	|	|	|	0.16
123.083	0.00	0.06	0.198	O	|	|	|	|	0.16
123.167	0.00	0.06	0.197	O	|	|	|	|	0.16
123.250	0.00	0.05	0.197	O	|	|	|	|	0.16
123.333	0.00	0.05	0.197	O	|	|	|	|	0.16
123.417	0.00	0.05	0.196	O	|	|	|	|	0.16
123.500	0.00	0.05	0.196	O	|	|	|	|	0.16
123.583	0.00	0.05	0.195	O	|	|	|	|	0.16
123.667	0.00	0.05	0.195	O	|	|	|	|	0.16
123.750	0.00	0.05	0.195	O	|	|	|	|	0.16
123.833	0.00	0.05	0.194	O	|	|	|	|	0.16
123.917	0.00	0.05	0.194	O	|	|	|	|	0.16
124.000	0.00	0.05	0.194	O	|	|	|	|	0.16
124.083	0.00	0.05	0.193	O	|	|	|	|	0.16
124.167	0.00	0.05	0.193	O	|	|	|	|	0.16
124.250	0.00	0.05	0.192	O	|	|	|	|	0.16
124.333	0.00	0.05	0.192	O	|	|	|	|	0.16
124.417	0.00	0.05	0.192	O	|	|	|	|	0.16

124.500	0.00	0.05	0.191	O	|	|	|	|	0.16
124.583	0.00	0.05	0.191	O	|	|	|	|	0.16
124.667	0.00	0.05	0.191	O	|	|	|	|	0.15
124.750	0.00	0.05	0.190	O	|	|	|	|	0.15
124.833	0.00	0.05	0.190	O	|	|	|	|	0.15
124.917	0.00	0.05	0.189	O	|	|	|	|	0.15
125.000	0.00	0.05	0.189	O	|	|	|	|	0.15
125.083	0.00	0.05	0.189	O	|	|	|	|	0.15
125.167	0.00	0.05	0.188	O	|	|	|	|	0.15
125.250	0.00	0.05	0.188	O	|	|	|	|	0.15
125.333	0.00	0.05	0.188	O	|	|	|	|	0.15
125.417	0.00	0.05	0.187	O	|	|	|	|	0.15
125.500	0.00	0.05	0.187	O	|	|	|	|	0.15
125.583	0.00	0.05	0.187	O	|	|	|	|	0.15
125.667	0.00	0.05	0.186	O	|	|	|	|	0.15
125.750	0.00	0.05	0.186	O	|	|	|	|	0.15
125.833	0.00	0.05	0.186	O	|	|	|	|	0.15
125.917	0.00	0.05	0.185	O	|	|	|	|	0.15
126.000	0.00	0.05	0.185	O	|	|	|	|	0.15
126.083	0.00	0.05	0.184	O	|	|	|	|	0.15
126.167	0.00	0.05	0.184	O	|	|	|	|	0.15
126.250	0.00	0.05	0.184	O	|	|	|	|	0.15
126.333	0.00	0.05	0.183	O	|	|	|	|	0.15
126.417	0.00	0.05	0.183	O	|	|	|	|	0.15
126.500	0.00	0.05	0.183	O	|	|	|	|	0.15
126.583	0.00	0.05	0.182	O	|	|	|	|	0.15
126.667	0.00	0.05	0.182	O	|	|	|	|	0.15
126.750	0.00	0.05	0.182	O	|	|	|	|	0.15
126.833	0.00	0.05	0.181	O	|	|	|	|	0.15
126.917	0.00	0.05	0.181	O	|	|	|	|	0.15
127.000	0.00	0.05	0.181	O	|	|	|	|	0.15
127.083	0.00	0.05	0.180	O	|	|	|	|	0.15
127.167	0.00	0.05	0.180	O	|	|	|	|	0.15
127.250	0.00	0.05	0.180	O	|	|	|	|	0.15
127.333	0.00	0.05	0.179	O	|	|	|	|	0.15
127.417	0.00	0.05	0.179	O	|	|	|	|	0.15
127.500	0.00	0.05	0.179	O	|	|	|	|	0.14
127.583	0.00	0.05	0.178	O	|	|	|	|	0.14
127.667	0.00	0.05	0.178	O	|	|	|	|	0.14
127.750	0.00	0.05	0.178	O	|	|	|	|	0.14
127.833	0.00	0.05	0.177	O	|	|	|	|	0.14
127.917	0.00	0.05	0.177	O	|	|	|	|	0.14
128.000	0.00	0.05	0.176	O	|	|	|	|	0.14
128.083	0.00	0.05	0.176	O	|	|	|	|	0.14
128.167	0.00	0.05	0.176	O	|	|	|	|	0.14
128.250	0.00	0.05	0.175	O	|	|	|	|	0.14
128.333	0.00	0.05	0.175	O	|	|	|	|	0.14
128.417	0.00	0.05	0.175	O	|	|	|	|	0.14
128.500	0.00	0.05	0.174	O	|	|	|	|	0.14
128.583	0.00	0.05	0.174	O	|	|	|	|	0.14
128.667	0.00	0.05	0.174	O	|	|	|	|	0.14
128.750	0.00	0.05	0.173	O	|	|	|	|	0.14
128.833	0.00	0.05	0.173	O	|	|	|	|	0.14
128.917	0.00	0.05	0.173	O	|	|	|	|	0.14
129.000	0.00	0.05	0.172	O	|	|	|	|	0.14
129.083	0.00	0.05	0.172	O	|	|	|	|	0.14
129.167	0.00	0.05	0.172	O	|	|	|	|	0.14
129.250	0.00	0.05	0.171	O	|	|	|	|	0.14
129.333	0.00	0.05	0.171	O	|	|	|	|	0.14
129.417	0.00	0.05	0.171	O	|	|	|	|	0.14
129.500	0.00	0.05	0.170	O	|	|	|	|	0.14
129.583	0.00	0.05	0.170	O	|	|	|	|	0.14
129.667	0.00	0.05	0.170	O	|	|	|	|	0.14
129.750	0.00	0.05	0.169	O	|	|	|	|	0.14
129.833	0.00	0.05	0.169	O	|	|	|	|	0.14
129.917	0.00	0.05	0.169	O	|	|	|	|	0.14
130.000	0.00	0.05	0.169	O	|	|	|	|	0.14
130.083	0.00	0.05	0.168	O	|	|	|	|	0.14
130.167	0.00	0.05	0.168	O	|	|	|	|	0.14
130.250	0.00	0.05	0.168	O	|	|	|	|	0.14
130.333	0.00	0.05	0.167	O	|	|	|	|	0.14

130.417	0.00	0.05	0.167	O	|	|	|	|	0.14
130.500	0.00	0.05	0.167	O	|	|	|	|	0.14
130.583	0.00	0.05	0.166	O	|	|	|	|	0.13
130.667	0.00	0.05	0.166	O	|	|	|	|	0.13
130.750	0.00	0.05	0.166	O	|	|	|	|	0.13
130.833	0.00	0.05	0.165	O	|	|	|	|	0.13
130.917	0.00	0.05	0.165	O	|	|	|	|	0.13
131.000	0.00	0.05	0.165	O	|	|	|	|	0.13
131.083	0.00	0.05	0.164	O	|	|	|	|	0.13
131.167	0.00	0.05	0.164	O	|	|	|	|	0.13
131.250	0.00	0.05	0.164	O	|	|	|	|	0.13
131.333	0.00	0.05	0.163	O	|	|	|	|	0.13
131.417	0.00	0.05	0.163	O	|	|	|	|	0.13
131.500	0.00	0.05	0.163	O	|	|	|	|	0.13
131.583	0.00	0.05	0.162	O	|	|	|	|	0.13
131.667	0.00	0.05	0.162	O	|	|	|	|	0.13
131.750	0.00	0.05	0.162	O	|	|	|	|	0.13
131.833	0.00	0.05	0.162	O	|	|	|	|	0.13
131.917	0.00	0.05	0.161	O	|	|	|	|	0.13
132.000	0.00	0.04	0.161	O	|	|	|	|	0.13
132.083	0.00	0.04	0.161	O	|	|	|	|	0.13
132.167	0.00	0.04	0.160	O	|	|	|	|	0.13
132.250	0.00	0.04	0.160	O	|	|	|	|	0.13
132.333	0.00	0.04	0.160	O	|	|	|	|	0.13
132.417	0.00	0.04	0.159	O	|	|	|	|	0.13
132.500	0.00	0.04	0.159	O	|	|	|	|	0.13
132.583	0.00	0.04	0.159	O	|	|	|	|	0.13
132.667	0.00	0.04	0.158	O	|	|	|	|	0.13
132.750	0.00	0.04	0.158	O	|	|	|	|	0.13
132.833	0.00	0.04	0.158	O	|	|	|	|	0.13
132.917	0.00	0.04	0.158	O	|	|	|	|	0.13
133.000	0.00	0.04	0.157	O	|	|	|	|	0.13
133.083	0.00	0.04	0.157	O	|	|	|	|	0.13
133.167	0.00	0.04	0.157	O	|	|	|	|	0.13
133.250	0.00	0.04	0.156	O	|	|	|	|	0.13
133.333	0.00	0.04	0.156	O	|	|	|	|	0.13
133.417	0.00	0.04	0.156	O	|	|	|	|	0.13
133.500	0.00	0.04	0.155	O	|	|	|	|	0.13
133.583	0.00	0.04	0.155	O	|	|	|	|	0.13
133.667	0.00	0.04	0.155	O	|	|	|	|	0.13
133.750	0.00	0.04	0.155	O	|	|	|	|	0.13
133.833	0.00	0.04	0.154	O	|	|	|	|	0.13
133.917	0.00	0.04	0.154	O	|	|	|	|	0.12
134.000	0.00	0.04	0.154	O	|	|	|	|	0.12
134.083	0.00	0.04	0.153	O	|	|	|	|	0.12
134.167	0.00	0.04	0.153	O	|	|	|	|	0.12
134.250	0.00	0.04	0.153	O	|	|	|	|	0.12
134.333	0.00	0.04	0.152	O	|	|	|	|	0.12
134.417	0.00	0.04	0.152	O	|	|	|	|	0.12
134.500	0.00	0.04	0.152	O	|	|	|	|	0.12
134.583	0.00	0.04	0.152	O	|	|	|	|	0.12
134.667	0.00	0.04	0.151	O	|	|	|	|	0.12
134.750	0.00	0.04	0.151	O	|	|	|	|	0.12
134.833	0.00	0.04	0.151	O	|	|	|	|	0.12
134.917	0.00	0.04	0.150	O	|	|	|	|	0.12
135.000	0.00	0.04	0.150	O	|	|	|	|	0.12
135.083	0.00	0.04	0.150	O	|	|	|	|	0.12
135.167	0.00	0.04	0.150	O	|	|	|	|	0.12
135.250	0.00	0.04	0.149	O	|	|	|	|	0.12
135.333	0.00	0.04	0.149	O	|	|	|	|	0.12
135.417	0.00	0.04	0.149	O	|	|	|	|	0.12
135.500	0.00	0.04	0.148	O	|	|	|	|	0.12
135.583	0.00	0.04	0.148	O	|	|	|	|	0.12
135.667	0.00	0.04	0.148	O	|	|	|	|	0.12
135.750	0.00	0.04	0.148	O	|	|	|	|	0.12
135.833	0.00	0.04	0.147	O	|	|	|	|	0.12
135.917	0.00	0.04	0.147	O	|	|	|	|	0.12
136.000	0.00	0.04	0.147	O	|	|	|	|	0.12
136.083	0.00	0.04	0.146	O	|	|	|	|	0.12
136.167	0.00	0.04	0.146	O	|	|	|	|	0.12
136.250	0.00	0.04	0.146	O	|	|	|	|	0.12

136.333	0.00	0.04	0.146	O	|	|	|	|	0.12
136.417	0.00	0.04	0.145	O	|	|	|	|	0.12
136.500	0.00	0.04	0.145	O	|	|	|	|	0.12
136.583	0.00	0.04	0.145	O	|	|	|	|	0.12
136.667	0.00	0.04	0.144	O	|	|	|	|	0.12
136.750	0.00	0.04	0.144	O	|	|	|	|	0.12
136.833	0.00	0.04	0.144	O	|	|	|	|	0.12
136.917	0.00	0.04	0.144	O	|	|	|	|	0.12
137.000	0.00	0.04	0.143	O	|	|	|	|	0.12
137.083	0.00	0.04	0.143	O	|	|	|	|	0.12
137.167	0.00	0.04	0.143	O	|	|	|	|	0.12
137.250	0.00	0.04	0.143	O	|	|	|	|	0.12
137.333	0.00	0.04	0.142	O	|	|	|	|	0.12
137.417	0.00	0.04	0.142	O	|	|	|	|	0.12
137.500	0.00	0.04	0.142	O	|	|	|	|	0.12
137.583	0.00	0.04	0.141	O	|	|	|	|	0.11
137.667	0.00	0.04	0.141	O	|	|	|	|	0.11
137.750	0.00	0.04	0.141	O	|	|	|	|	0.11
137.833	0.00	0.04	0.141	O	|	|	|	|	0.11
137.917	0.00	0.04	0.140	O	|	|	|	|	0.11
138.000	0.00	0.04	0.140	O	|	|	|	|	0.11
138.083	0.00	0.04	0.140	O	|	|	|	|	0.11
138.167	0.00	0.04	0.140	O	|	|	|	|	0.11
138.250	0.00	0.04	0.139	O	|	|	|	|	0.11
138.333	0.00	0.04	0.139	O	|	|	|	|	0.11
138.417	0.00	0.04	0.139	O	|	|	|	|	0.11
138.500	0.00	0.04	0.139	O	|	|	|	|	0.11
138.583	0.00	0.04	0.138	O	|	|	|	|	0.11
138.667	0.00	0.04	0.138	O	|	|	|	|	0.11
138.750	0.00	0.04	0.138	O	|	|	|	|	0.11
138.833	0.00	0.04	0.137	O	|	|	|	|	0.11
138.917	0.00	0.04	0.137	O	|	|	|	|	0.11
139.000	0.00	0.04	0.137	O	|	|	|	|	0.11
139.083	0.00	0.04	0.137	O	|	|	|	|	0.11
139.167	0.00	0.04	0.136	O	|	|	|	|	0.11
139.250	0.00	0.04	0.136	O	|	|	|	|	0.11
139.333	0.00	0.04	0.136	O	|	|	|	|	0.11
139.417	0.00	0.04	0.136	O	|	|	|	|	0.11
139.500	0.00	0.04	0.135	O	|	|	|	|	0.11
139.583	0.00	0.04	0.135	O	|	|	|	|	0.11
139.667	0.00	0.04	0.135	O	|	|	|	|	0.11
139.750	0.00	0.04	0.135	O	|	|	|	|	0.11
139.833	0.00	0.04	0.134	O	|	|	|	|	0.11
139.917	0.00	0.04	0.134	O	|	|	|	|	0.11
140.000	0.00	0.04	0.134	O	|	|	|	|	0.11
140.083	0.00	0.04	0.134	O	|	|	|	|	0.11
140.167	0.00	0.04	0.133	O	|	|	|	|	0.11
140.250	0.00	0.04	0.133	O	|	|	|	|	0.11
140.333	0.00	0.04	0.133	O	|	|	|	|	0.11
140.417	0.00	0.04	0.133	O	|	|	|	|	0.11
140.500	0.00	0.04	0.132	O	|	|	|	|	0.11
140.583	0.00	0.04	0.132	O	|	|	|	|	0.11
140.667	0.00	0.04	0.132	O	|	|	|	|	0.11
140.750	0.00	0.04	0.131	O	|	|	|	|	0.11
140.833	0.00	0.04	0.131	O	|	|	|	|	0.11
140.917	0.00	0.04	0.131	O	|	|	|	|	0.11
141.000	0.00	0.04	0.131	O	|	|	|	|	0.11
141.083	0.00	0.04	0.130	O	|	|	|	|	0.11
141.167	0.00	0.04	0.130	O	|	|	|	|	0.11
141.250	0.00	0.04	0.130	O	|	|	|	|	0.11
141.333	0.00	0.04	0.130	O	|	|	|	|	0.11
141.417	0.00	0.04	0.129	O	|	|	|	|	0.11
141.500	0.00	0.04	0.129	O	|	|	|	|	0.10
141.583	0.00	0.04	0.129	O	|	|	|	|	0.10
141.667	0.00	0.04	0.129	O	|	|	|	|	0.10
141.750	0.00	0.04	0.128	O	|	|	|	|	0.10
141.833	0.00	0.04	0.128	O	|	|	|	|	0.10
141.917	0.00	0.04	0.128	O	|	|	|	|	0.10
142.000	0.00	0.04	0.128	O	|	|	|	|	0.10
142.083	0.00	0.04	0.128	O	|	|	|	|	0.10
142.167	0.00	0.04	0.127	O	|	|	|	|	0.10

142.250	0.00	0.04	0.127	O	|	|	|	|	0.10
142.333	0.00	0.04	0.127	O	|	|	|	|	0.10
142.417	0.00	0.04	0.127	O	|	|	|	|	0.10
142.500	0.00	0.04	0.126	O	|	|	|	|	0.10
142.583	0.00	0.04	0.126	O	|	|	|	|	0.10
142.667	0.00	0.04	0.126	O	|	|	|	|	0.10
142.750	0.00	0.04	0.126	O	|	|	|	|	0.10
142.833	0.00	0.03	0.125	O	|	|	|	|	0.10
142.917	0.00	0.03	0.125	O	|	|	|	|	0.10
143.000	0.00	0.03	0.125	O	|	|	|	|	0.10
143.083	0.00	0.03	0.125	O	|	|	|	|	0.10
143.167	0.00	0.03	0.124	O	|	|	|	|	0.10
143.250	0.00	0.03	0.124	O	|	|	|	|	0.10
143.333	0.00	0.03	0.124	O	|	|	|	|	0.10
143.417	0.00	0.03	0.124	O	|	|	|	|	0.10
143.500	0.00	0.03	0.123	O	|	|	|	|	0.10
143.583	0.00	0.03	0.123	O	|	|	|	|	0.10
143.667	0.00	0.03	0.123	O	|	|	|	|	0.10
143.750	0.00	0.03	0.123	O	|	|	|	|	0.10
143.833	0.00	0.03	0.122	O	|	|	|	|	0.10
143.917	0.00	0.03	0.122	O	|	|	|	|	0.10
144.000	0.00	0.03	0.122	O	|	|	|	|	0.10
144.083	0.00	0.03	0.122	O	|	|	|	|	0.10
144.167	0.00	0.03	0.122	O	|	|	|	|	0.10
144.250	0.00	0.03	0.121	O	|	|	|	|	0.10
144.333	0.00	0.03	0.121	O	|	|	|	|	0.10
144.417	0.00	0.03	0.121	O	|	|	|	|	0.10
144.500	0.00	0.03	0.121	O	|	|	|	|	0.10
144.583	0.00	0.03	0.120	O	|	|	|	|	0.10
144.667	0.00	0.03	0.120	O	|	|	|	|	0.10
144.750	0.00	0.03	0.120	O	|	|	|	|	0.10
144.833	0.00	0.03	0.120	O	|	|	|	|	0.10
144.917	0.00	0.03	0.119	O	|	|	|	|	0.10
145.000	0.00	0.03	0.119	O	|	|	|	|	0.10
145.083	0.00	0.03	0.119	O	|	|	|	|	0.10
145.167	0.00	0.03	0.119	O	|	|	|	|	0.10
145.250	0.00	0.03	0.119	O	|	|	|	|	0.10
145.333	0.00	0.03	0.118	O	|	|	|	|	0.10
145.417	0.00	0.03	0.118	O	|	|	|	|	0.10
145.500	0.00	0.03	0.118	O	|	|	|	|	0.10
145.583	0.00	0.03	0.118	O	|	|	|	|	0.10
145.667	0.00	0.03	0.117	O	|	|	|	|	0.10
145.750	0.00	0.03	0.117	O	|	|	|	|	0.10
145.833	0.00	0.03	0.117	O	|	|	|	|	0.09
145.917	0.00	0.03	0.117	O	|	|	|	|	0.09
146.000	0.00	0.03	0.116	O	|	|	|	|	0.09
146.083	0.00	0.03	0.116	O	|	|	|	|	0.09
146.167	0.00	0.03	0.116	O	|	|	|	|	0.09
146.250	0.00	0.03	0.116	O	|	|	|	|	0.09
146.333	0.00	0.03	0.116	O	|	|	|	|	0.09
146.417	0.00	0.03	0.115	O	|	|	|	|	0.09
146.500	0.00	0.03	0.115	O	|	|	|	|	0.09
146.583	0.00	0.03	0.115	O	|	|	|	|	0.09
146.667	0.00	0.03	0.115	O	|	|	|	|	0.09
146.750	0.00	0.03	0.114	O	|	|	|	|	0.09
146.833	0.00	0.03	0.114	O	|	|	|	|	0.09
146.917	0.00	0.03	0.114	O	|	|	|	|	0.09
147.000	0.00	0.03	0.114	O	|	|	|	|	0.09
147.083	0.00	0.03	0.114	O	|	|	|	|	0.09
147.167	0.00	0.03	0.113	O	|	|	|	|	0.09
147.250	0.00	0.03	0.113	O	|	|	|	|	0.09
147.333	0.00	0.03	0.113	O	|	|	|	|	0.09
147.417	0.00	0.03	0.113	O	|	|	|	|	0.09
147.500	0.00	0.03	0.113	O	|	|	|	|	0.09
147.583	0.00	0.03	0.112	O	|	|	|	|	0.09
147.667	0.00	0.03	0.112	O	|	|	|	|	0.09
147.750	0.00	0.03	0.112	O	|	|	|	|	0.09
147.833	0.00	0.03	0.112	O	|	|	|	|	0.09
147.917	0.00	0.03	0.111	O	|	|	|	|	0.09
148.000	0.00	0.03	0.111	O	|	|	|	|	0.09
148.083	0.00	0.03	0.111	O	|	|	|	|	0.09

148.167	0.00	0.03	0.111	O	|	|	|	|	0.09
148.250	0.00	0.03	0.111	O	|	|	|	|	0.09
148.333	0.00	0.03	0.110	O	|	|	|	|	0.09
148.417	0.00	0.03	0.110	O	|	|	|	|	0.09
148.500	0.00	0.03	0.110	O	|	|	|	|	0.09
148.583	0.00	0.03	0.110	O	|	|	|	|	0.09
148.667	0.00	0.03	0.110	O	|	|	|	|	0.09
148.750	0.00	0.03	0.109	O	|	|	|	|	0.09
148.833	0.00	0.03	0.109	O	|	|	|	|	0.09
148.917	0.00	0.03	0.109	O	|	|	|	|	0.09
149.000	0.00	0.03	0.109	O	|	|	|	|	0.09
149.083	0.00	0.03	0.108	O	|	|	|	|	0.09
149.167	0.00	0.03	0.108	O	|	|	|	|	0.09
149.250	0.00	0.03	0.108	O	|	|	|	|	0.09
149.333	0.00	0.03	0.108	O	|	|	|	|	0.09
149.417	0.00	0.03	0.108	O	|	|	|	|	0.09
149.500	0.00	0.03	0.107	O	|	|	|	|	0.09
149.583	0.00	0.03	0.107	O	|	|	|	|	0.09
149.667	0.00	0.03	0.107	O	|	|	|	|	0.09
149.750	0.00	0.03	0.107	O	|	|	|	|	0.09
149.833	0.00	0.03	0.107	O	|	|	|	|	0.09
149.917	0.00	0.03	0.106	O	|	|	|	|	0.09
150.000	0.00	0.03	0.106	O	|	|	|	|	0.09
150.083	0.00	0.03	0.106	O	|	|	|	|	0.09
150.167	0.00	0.03	0.106	O	|	|	|	|	0.09
150.250	0.00	0.03	0.106	O	|	|	|	|	0.09
150.333	0.00	0.03	0.105	O	|	|	|	|	0.09
150.417	0.00	0.03	0.105	O	|	|	|	|	0.09
150.500	0.00	0.03	0.105	O	|	|	|	|	0.09
150.583	0.00	0.03	0.105	O	|	|	|	|	0.09
150.667	0.00	0.03	0.105	O	|	|	|	|	0.08
150.750	0.00	0.03	0.104	O	|	|	|	|	0.08
150.833	0.00	0.03	0.104	O	|	|	|	|	0.08
150.917	0.00	0.03	0.104	O	|	|	|	|	0.08
151.000	0.00	0.03	0.104	O	|	|	|	|	0.08
151.083	0.00	0.03	0.104	O	|	|	|	|	0.08
151.167	0.00	0.03	0.103	O	|	|	|	|	0.08
151.250	0.00	0.03	0.103	O	|	|	|	|	0.08
151.333	0.00	0.03	0.103	O	|	|	|	|	0.08
151.417	0.00	0.03	0.103	O	|	|	|	|	0.08
151.500	0.00	0.03	0.103	O	|	|	|	|	0.08
151.583	0.00	0.03	0.102	O	|	|	|	|	0.08
151.667	0.00	0.03	0.102	O	|	|	|	|	0.08
151.750	0.00	0.03	0.102	O	|	|	|	|	0.08
151.833	0.00	0.03	0.102	O	|	|	|	|	0.08
151.917	0.00	0.03	0.102	O	|	|	|	|	0.08
152.000	0.00	0.03	0.101	O	|	|	|	|	0.08
152.083	0.00	0.03	0.101	O	|	|	|	|	0.08
152.167	0.00	0.03	0.101	O	|	|	|	|	0.08
152.250	0.00	0.03	0.101	O	|	|	|	|	0.08
152.333	0.00	0.03	0.101	O	|	|	|	|	0.08
152.417	0.00	0.03	0.100	O	|	|	|	|	0.08
152.500	0.00	0.03	0.100	O	|	|	|	|	0.08
152.583	0.00	0.03	0.100	O	|	|	|	|	0.08
152.667	0.00	0.03	0.100	O	|	|	|	|	0.08
152.750	0.00	0.03	0.100	O	|	|	|	|	0.08
152.833	0.00	0.03	0.100	O	|	|	|	|	0.08
152.917	0.00	0.03	0.099	O	|	|	|	|	0.08
153.000	0.00	0.03	0.099	O	|	|	|	|	0.08
153.083	0.00	0.03	0.099	O	|	|	|	|	0.08
153.167	0.00	0.03	0.099	O	|	|	|	|	0.08
153.250	0.00	0.03	0.099	O	|	|	|	|	0.08
153.333	0.00	0.03	0.098	O	|	|	|	|	0.08
153.417	0.00	0.03	0.098	O	|	|	|	|	0.08
153.500	0.00	0.03	0.098	O	|	|	|	|	0.08
153.583	0.00	0.03	0.098	O	|	|	|	|	0.08
153.667	0.00	0.03	0.098	O	|	|	|	|	0.08
153.750	0.00	0.03	0.097	O	|	|	|	|	0.08
153.833	0.00	0.03	0.097	O	|	|	|	|	0.08
153.917	0.00	0.03	0.097	O	|	|	|	|	0.08
154.000	0.00	0.03	0.097	O	|	|	|	|	0.08

154.083	0.00	0.03	0.097	O	|	|	|	|	0.08
154.167	0.00	0.03	0.096	O	|	|	|	|	0.08
154.250	0.00	0.03	0.096	O	|	|	|	|	0.08
154.333	0.00	0.03	0.096	O	|	|	|	|	0.08
154.417	0.00	0.03	0.096	O	|	|	|	|	0.08
154.500	0.00	0.03	0.096	O	|	|	|	|	0.08
154.583	0.00	0.03	0.096	O	|	|	|	|	0.08
154.667	0.00	0.03	0.095	O	|	|	|	|	0.08
154.750	0.00	0.03	0.095	O	|	|	|	|	0.08
154.833	0.00	0.03	0.095	O	|	|	|	|	0.08
154.917	0.00	0.03	0.095	O	|	|	|	|	0.08
155.000	0.00	0.03	0.095	O	|	|	|	|	0.08
155.083	0.00	0.03	0.094	O	|	|	|	|	0.08
155.167	0.00	0.03	0.094	O	|	|	|	|	0.08
155.250	0.00	0.03	0.094	O	|	|	|	|	0.08
155.333	0.00	0.03	0.094	O	|	|	|	|	0.08
155.417	0.00	0.03	0.094	O	|	|	|	|	0.08
155.500	0.00	0.03	0.094	O	|	|	|	|	0.08
155.583	0.00	0.03	0.093	O	|	|	|	|	0.08
155.667	0.00	0.03	0.093	O	|	|	|	|	0.08
155.750	0.00	0.03	0.093	O	|	|	|	|	0.08
155.833	0.00	0.03	0.093	O	|	|	|	|	0.08
155.917	0.00	0.03	0.093	O	|	|	|	|	0.08
156.000	0.00	0.03	0.092	O	|	|	|	|	0.08
156.083	0.00	0.03	0.092	O	|	|	|	|	0.07
156.167	0.00	0.03	0.092	O	|	|	|	|	0.07
156.250	0.00	0.03	0.092	O	|	|	|	|	0.07
156.333	0.00	0.03	0.092	O	|	|	|	|	0.07
156.417	0.00	0.03	0.092	O	|	|	|	|	0.07
156.500	0.00	0.03	0.091	O	|	|	|	|	0.07
156.583	0.00	0.03	0.091	O	|	|	|	|	0.07
156.667	0.00	0.03	0.091	O	|	|	|	|	0.07
156.750	0.00	0.03	0.091	O	|	|	|	|	0.07
156.833	0.00	0.03	0.091	O	|	|	|	|	0.07
156.917	0.00	0.03	0.091	O	|	|	|	|	0.07
157.000	0.00	0.03	0.090	O	|	|	|	|	0.07
157.083	0.00	0.03	0.090	O	|	|	|	|	0.07
157.167	0.00	0.03	0.090	O	|	|	|	|	0.07
157.250	0.00	0.03	0.090	O	|	|	|	|	0.07
157.333	0.00	0.03	0.090	O	|	|	|	|	0.07
157.417	0.00	0.02	0.090	O	|	|	|	|	0.07
157.500	0.00	0.02	0.089	O	|	|	|	|	0.07
157.583	0.00	0.02	0.089	O	|	|	|	|	0.07
157.667	0.00	0.02	0.089	O	|	|	|	|	0.07
157.750	0.00	0.02	0.089	O	|	|	|	|	0.07
157.833	0.00	0.02	0.089	O	|	|	|	|	0.07
157.917	0.00	0.02	0.088	O	|	|	|	|	0.07
158.000	0.00	0.02	0.088	O	|	|	|	|	0.07
158.083	0.00	0.02	0.088	O	|	|	|	|	0.07
158.167	0.00	0.02	0.088	O	|	|	|	|	0.07
158.250	0.00	0.02	0.088	O	|	|	|	|	0.07
158.333	0.00	0.02	0.088	O	|	|	|	|	0.07
158.417	0.00	0.02	0.087	O	|	|	|	|	0.07
158.500	0.00	0.02	0.087	O	|	|	|	|	0.07
158.583	0.00	0.02	0.087	O	|	|	|	|	0.07
158.667	0.00	0.02	0.087	O	|	|	|	|	0.07
158.750	0.00	0.02	0.087	O	|	|	|	|	0.07
158.833	0.00	0.02	0.087	O	|	|	|	|	0.07
158.917	0.00	0.02	0.086	O	|	|	|	|	0.07
159.000	0.00	0.02	0.086	O	|	|	|	|	0.07
159.083	0.00	0.02	0.086	O	|	|	|	|	0.07
159.167	0.00	0.02	0.086	O	|	|	|	|	0.07
159.250	0.00	0.02	0.086	O	|	|	|	|	0.07
159.333	0.00	0.02	0.086	O	|	|	|	|	0.07
159.417	0.00	0.02	0.085	O	|	|	|	|	0.07
159.500	0.00	0.02	0.085	O	|	|	|	|	0.07
159.583	0.00	0.02	0.085	O	|	|	|	|	0.07
159.667	0.00	0.02	0.085	O	|	|	|	|	0.07
159.750	0.00	0.02	0.085	O	|	|	|	|	0.07
159.833	0.00	0.02	0.085	O	|	|	|	|	0.07
159.917	0.00	0.02	0.084	O	|	|	|	|	0.07

160.000	0.00	0.02	0.084	O	|	|	|	|	0.07
160.083	0.00	0.02	0.084	O	|	|	|	|	0.07
160.167	0.00	0.02	0.084	O	|	|	|	|	0.07
160.250	0.00	0.02	0.084	O	|	|	|	|	0.07
160.333	0.00	0.02	0.084	O	|	|	|	|	0.07
160.417	0.00	0.02	0.084	O	|	|	|	|	0.07
160.500	0.00	0.02	0.083	O	|	|	|	|	0.07
160.583	0.00	0.02	0.083	O	|	|	|	|	0.07
160.667	0.00	0.02	0.083	O	|	|	|	|	0.07
160.750	0.00	0.02	0.083	O	|	|	|	|	0.07
160.833	0.00	0.02	0.083	O	|	|	|	|	0.07
160.917	0.00	0.02	0.083	O	|	|	|	|	0.07
161.000	0.00	0.02	0.082	O	|	|	|	|	0.07
161.083	0.00	0.02	0.082	O	|	|	|	|	0.07
161.167	0.00	0.02	0.082	O	|	|	|	|	0.07
161.250	0.00	0.02	0.082	O	|	|	|	|	0.07
161.333	0.00	0.02	0.082	O	|	|	|	|	0.07
161.417	0.00	0.02	0.082	O	|	|	|	|	0.07
161.500	0.00	0.02	0.081	O	|	|	|	|	0.07
161.583	0.00	0.02	0.081	O	|	|	|	|	0.07
161.667	0.00	0.02	0.081	O	|	|	|	|	0.07
161.750	0.00	0.02	0.081	O	|	|	|	|	0.07
161.833	0.00	0.02	0.081	O	|	|	|	|	0.07
161.917	0.00	0.02	0.081	O	|	|	|	|	0.07
162.000	0.00	0.02	0.081	O	|	|	|	|	0.07
162.083	0.00	0.02	0.080	O	|	|	|	|	0.07
162.167	0.00	0.02	0.080	O	|	|	|	|	0.07
162.250	0.00	0.02	0.080	O	|	|	|	|	0.06
162.333	0.00	0.02	0.080	O	|	|	|	|	0.06
162.417	0.00	0.02	0.080	O	|	|	|	|	0.06
162.500	0.00	0.02	0.080	O	|	|	|	|	0.06
162.583	0.00	0.02	0.079	O	|	|	|	|	0.06
162.667	0.00	0.02	0.079	O	|	|	|	|	0.06
162.750	0.00	0.02	0.079	O	|	|	|	|	0.06
162.833	0.00	0.02	0.079	O	|	|	|	|	0.06
162.917	0.00	0.02	0.079	O	|	|	|	|	0.06
163.000	0.00	0.02	0.079	O	|	|	|	|	0.06
163.083	0.00	0.02	0.079	O	|	|	|	|	0.06
163.167	0.00	0.02	0.078	O	|	|	|	|	0.06
163.250	0.00	0.02	0.078	O	|	|	|	|	0.06
163.333	0.00	0.02	0.078	O	|	|	|	|	0.06
163.417	0.00	0.02	0.078	O	|	|	|	|	0.06
163.500	0.00	0.02	0.078	O	|	|	|	|	0.06
163.583	0.00	0.02	0.078	O	|	|	|	|	0.06
163.667	0.00	0.02	0.077	O	|	|	|	|	0.06
163.750	0.00	0.02	0.077	O	|	|	|	|	0.06
163.833	0.00	0.02	0.077	O	|	|	|	|	0.06
163.917	0.00	0.02	0.077	O	|	|	|	|	0.06
164.000	0.00	0.02	0.077	O	|	|	|	|	0.06
164.083	0.00	0.02	0.077	O	|	|	|	|	0.06
164.167	0.00	0.02	0.077	O	|	|	|	|	0.06
164.250	0.00	0.02	0.076	O	|	|	|	|	0.06
164.333	0.00	0.02	0.076	O	|	|	|	|	0.06
164.417	0.00	0.02	0.076	O	|	|	|	|	0.06
164.500	0.00	0.02	0.076	O	|	|	|	|	0.06
164.583	0.00	0.02	0.076	O	|	|	|	|	0.06
164.667	0.00	0.02	0.076	O	|	|	|	|	0.06
164.750	0.00	0.02	0.076	O	|	|	|	|	0.06
164.833	0.00	0.02	0.075	O	|	|	|	|	0.06
164.917	0.00	0.02	0.075	O	|	|	|	|	0.06
165.000	0.00	0.02	0.075	O	|	|	|	|	0.06
165.083	0.00	0.02	0.075	O	|	|	|	|	0.06
165.167	0.00	0.02	0.075	O	|	|	|	|	0.06
165.250	0.00	0.02	0.075	O	|	|	|	|	0.06
165.333	0.00	0.02	0.075	O	|	|	|	|	0.06
165.417	0.00	0.02	0.074	O	|	|	|	|	0.06
165.500	0.00	0.02	0.074	O	|	|	|	|	0.06
165.583	0.00	0.02	0.074	O	|	|	|	|	0.06
165.667	0.00	0.02	0.074	O	|	|	|	|	0.06
165.750	0.00	0.02	0.074	O	|	|	|	|	0.06
165.833	0.00	0.02	0.074	O	|	|	|	|	0.06

165.917	0.00	0.02	0.074	O	|	|	|	|	0.06
166.000	0.00	0.02	0.073	O	|	|	|	|	0.06
166.083	0.00	0.02	0.073	O	|	|	|	|	0.06
166.167	0.00	0.02	0.073	O	|	|	|	|	0.06
166.250	0.00	0.02	0.073	O	|	|	|	|	0.06
166.333	0.00	0.02	0.073	O	|	|	|	|	0.06
166.417	0.00	0.02	0.073	O	|	|	|	|	0.06
166.500	0.00	0.02	0.073	O	|	|	|	|	0.06
166.583	0.00	0.02	0.072	O	|	|	|	|	0.06
166.667	0.00	0.02	0.072	O	|	|	|	|	0.06
166.750	0.00	0.02	0.072	O	|	|	|	|	0.06
166.833	0.00	0.02	0.072	O	|	|	|	|	0.06
166.917	0.00	0.02	0.072	O	|	|	|	|	0.06
167.000	0.00	0.02	0.072	O	|	|	|	|	0.06
167.083	0.00	0.02	0.072	O	|	|	|	|	0.06
167.167	0.00	0.02	0.071	O	|	|	|	|	0.06
167.250	0.00	0.02	0.071	O	|	|	|	|	0.06
167.333	0.00	0.02	0.071	O	|	|	|	|	0.06
167.417	0.00	0.02	0.071	O	|	|	|	|	0.06
167.500	0.00	0.02	0.071	O	|	|	|	|	0.06
167.583	0.00	0.02	0.071	O	|	|	|	|	0.06
167.667	0.00	0.02	0.071	O	|	|	|	|	0.06
167.750	0.00	0.02	0.071	O	|	|	|	|	0.06
167.833	0.00	0.02	0.070	O	|	|	|	|	0.06
167.917	0.00	0.02	0.070	O	|	|	|	|	0.06
168.000	0.00	0.02	0.070	O	|	|	|	|	0.06
168.083	0.00	0.02	0.070	O	|	|	|	|	0.06
168.167	0.00	0.02	0.070	O	|	|	|	|	0.06
168.250	0.00	0.02	0.070	O	|	|	|	|	0.06
168.333	0.00	0.02	0.070	O	|	|	|	|	0.06
168.417	0.00	0.02	0.069	O	|	|	|	|	0.06
168.500	0.00	0.02	0.069	O	|	|	|	|	0.06
168.583	0.00	0.02	0.069	O	|	|	|	|	0.06
168.667	0.00	0.02	0.069	O	|	|	|	|	0.06
168.750	0.00	0.02	0.069	O	|	|	|	|	0.06
168.833	0.00	0.02	0.069	O	|	|	|	|	0.06
168.917	0.00	0.02	0.069	O	|	|	|	|	0.06
169.000	0.00	0.02	0.069	O	|	|	|	|	0.06
169.083	0.00	0.02	0.068	O	|	|	|	|	0.06
169.167	0.00	0.02	0.068	O	|	|	|	|	0.06
169.250	0.00	0.02	0.068	O	|	|	|	|	0.06
169.333	0.00	0.02	0.068	O	|	|	|	|	0.06
169.417	0.00	0.02	0.068	O	|	|	|	|	0.06
169.500	0.00	0.02	0.068	O	|	|	|	|	0.05
169.583	0.00	0.02	0.068	O	|	|	|	|	0.05
169.667	0.00	0.02	0.067	O	|	|	|	|	0.05
169.750	0.00	0.02	0.067	O	|	|	|	|	0.05
169.833	0.00	0.02	0.067	O	|	|	|	|	0.05
169.917	0.00	0.02	0.067	O	|	|	|	|	0.05
170.000	0.00	0.02	0.067	O	|	|	|	|	0.05
170.083	0.00	0.02	0.067	O	|	|	|	|	0.05
170.167	0.00	0.02	0.067	O	|	|	|	|	0.05
170.250	0.00	0.02	0.067	O	|	|	|	|	0.05
170.333	0.00	0.02	0.066	O	|	|	|	|	0.05
170.417	0.00	0.02	0.066	O	|	|	|	|	0.05
170.500	0.00	0.02	0.066	O	|	|	|	|	0.05
170.583	0.00	0.02	0.066	O	|	|	|	|	0.05
170.667	0.00	0.02	0.066	O	|	|	|	|	0.05
170.750	0.00	0.02	0.066	O	|	|	|	|	0.05
170.833	0.00	0.02	0.066	O	|	|	|	|	0.05
170.917	0.00	0.02	0.066	O	|	|	|	|	0.05
171.000	0.00	0.02	0.065	O	|	|	|	|	0.05
171.083	0.00	0.02	0.065	O	|	|	|	|	0.05
171.167	0.00	0.02	0.065	O	|	|	|	|	0.05
171.250	0.00	0.02	0.065	O	|	|	|	|	0.05
171.333	0.00	0.02	0.065	O	|	|	|	|	0.05
171.417	0.00	0.02	0.065	O	|	|	|	|	0.05
171.500	0.00	0.02	0.065	O	|	|	|	|	0.05
171.583	0.00	0.02	0.065	O	|	|	|	|	0.05
171.667	0.00	0.02	0.064	O	|	|	|	|	0.05
171.750	0.00	0.02	0.064	O	|	|	|	|	0.05

171.833	0.00	0.02	0.064	O	|	|	|	|	0.05
171.917	0.00	0.02	0.064	O	|	|	|	|	0.05
172.000	0.00	0.02	0.064	O	|	|	|	|	0.05
172.083	0.00	0.02	0.064	O	|	|	|	|	0.05
172.167	0.00	0.02	0.064	O	|	|	|	|	0.05
172.250	0.00	0.02	0.064	O	|	|	|	|	0.05
172.333	0.00	0.02	0.063	O	|	|	|	|	0.05
172.417	0.00	0.02	0.063	O	|	|	|	|	0.05
172.500	0.00	0.02	0.063	O	|	|	|	|	0.05
172.583	0.00	0.02	0.063	O	|	|	|	|	0.05
172.667	0.00	0.02	0.063	O	|	|	|	|	0.05
172.750	0.00	0.02	0.063	O	|	|	|	|	0.05
172.833	0.00	0.02	0.063	O	|	|	|	|	0.05
172.917	0.00	0.02	0.063	O	|	|	|	|	0.05
173.000	0.00	0.02	0.062	O	|	|	|	|	0.05
173.083	0.00	0.02	0.062	O	|	|	|	|	0.05
173.167	0.00	0.02	0.062	O	|	|	|	|	0.05
173.250	0.00	0.02	0.062	O	|	|	|	|	0.05
173.333	0.00	0.02	0.062	O	|	|	|	|	0.05
173.417	0.00	0.02	0.062	O	|	|	|	|	0.05
173.500	0.00	0.02	0.062	O	|	|	|	|	0.05
173.583	0.00	0.02	0.062	O	|	|	|	|	0.05
173.667	0.00	0.02	0.062	O	|	|	|	|	0.05
173.750	0.00	0.02	0.061	O	|	|	|	|	0.05
173.833	0.00	0.02	0.061	O	|	|	|	|	0.05
173.917	0.00	0.02	0.061	O	|	|	|	|	0.05
174.000	0.00	0.02	0.061	O	|	|	|	|	0.05
174.083	0.00	0.02	0.061	O	|	|	|	|	0.05
174.167	0.00	0.02	0.061	O	|	|	|	|	0.05
174.250	0.00	0.02	0.061	O	|	|	|	|	0.05
174.333	0.00	0.02	0.061	O	|	|	|	|	0.05
174.417	0.00	0.02	0.060	O	|	|	|	|	0.05
174.500	0.00	0.02	0.060	O	|	|	|	|	0.05
174.583	0.00	0.02	0.060	O	|	|	|	|	0.05
174.667	0.00	0.02	0.060	O	|	|	|	|	0.05
174.750	0.00	0.02	0.060	O	|	|	|	|	0.05
174.833	0.00	0.02	0.060	O	|	|	|	|	0.05
174.917	0.00	0.02	0.060	O	|	|	|	|	0.05
175.000	0.00	0.02	0.060	O	|	|	|	|	0.05
175.083	0.00	0.02	0.060	O	|	|	|	|	0.05
175.167	0.00	0.02	0.059	O	|	|	|	|	0.05
175.250	0.00	0.02	0.059	O	|	|	|	|	0.05
175.333	0.00	0.02	0.059	O	|	|	|	|	0.05
175.417	0.00	0.02	0.059	O	|	|	|	|	0.05
175.500	0.00	0.02	0.059	O	|	|	|	|	0.05
175.583	0.00	0.02	0.059	O	|	|	|	|	0.05
175.667	0.00	0.02	0.059	O	|	|	|	|	0.05
175.750	0.00	0.02	0.059	O	|	|	|	|	0.05
175.833	0.00	0.02	0.059	O	|	|	|	|	0.05
175.917	0.00	0.02	0.058	O	|	|	|	|	0.05
176.000	0.00	0.02	0.058	O	|	|	|	|	0.05
176.083	0.00	0.02	0.058	O	|	|	|	|	0.05
176.167	0.00	0.02	0.058	O	|	|	|	|	0.05
176.250	0.00	0.02	0.058	O	|	|	|	|	0.05
176.333	0.00	0.02	0.058	O	|	|	|	|	0.05
176.417	0.00	0.02	0.058	O	|	|	|	|	0.05
176.500	0.00	0.02	0.058	O	|	|	|	|	0.05
176.583	0.00	0.02	0.058	O	|	|	|	|	0.05
176.667	0.00	0.02	0.057	O	|	|	|	|	0.05
176.750	0.00	0.02	0.057	O	|	|	|	|	0.05
176.833	0.00	0.02	0.057	O	|	|	|	|	0.05
176.917	0.00	0.02	0.057	O	|	|	|	|	0.05
177.000	0.00	0.02	0.057	O	|	|	|	|	0.05
177.083	0.00	0.02	0.057	O	|	|	|	|	0.05
177.167	0.00	0.02	0.057	O	|	|	|	|	0.05
177.250	0.00	0.02	0.057	O	|	|	|	|	0.05
177.333	0.00	0.02	0.057	O	|	|	|	|	0.05
177.417	0.00	0.02	0.056	O	|	|	|	|	0.05
177.500	0.00	0.02	0.056	O	|	|	|	|	0.05
177.583	0.00	0.02	0.056	O	|	|	|	|	0.05
177.667	0.00	0.02	0.056	O	|	|	|	|	0.05

177.750	0.00	0.02	0.056	O	|	|	|	|	0.05
177.833	0.00	0.02	0.056	O	|	|	|	|	0.05
177.917	0.00	0.02	0.056	O	|	|	|	|	0.05
178.000	0.00	0.02	0.056	O	|	|	|	|	0.05
178.083	0.00	0.02	0.056	O	|	|	|	|	0.05
178.167	0.00	0.02	0.055	O	|	|	|	|	0.05
178.250	0.00	0.02	0.055	O	|	|	|	|	0.04
178.333	0.00	0.02	0.055	O	|	|	|	|	0.04
178.417	0.00	0.02	0.055	O	|	|	|	|	0.04
178.500	0.00	0.02	0.055	O	|	|	|	|	0.04
178.583	0.00	0.02	0.055	O	|	|	|	|	0.04
178.667	0.00	0.02	0.055	O	|	|	|	|	0.04
178.750	0.00	0.02	0.055	O	|	|	|	|	0.04
178.833	0.00	0.02	0.055	O	|	|	|	|	0.04
178.917	0.00	0.02	0.055	O	|	|	|	|	0.04
179.000	0.00	0.02	0.054	O	|	|	|	|	0.04
179.083	0.00	0.02	0.054	O	|	|	|	|	0.04
179.167	0.00	0.02	0.054	O	|	|	|	|	0.04
179.250	0.00	0.02	0.054	O	|	|	|	|	0.04
179.333	0.00	0.02	0.054	O	|	|	|	|	0.04
179.417	0.00	0.02	0.054	O	|	|	|	|	0.04
179.500	0.00	0.02	0.054	O	|	|	|	|	0.04
179.583	0.00	0.01	0.054	O	|	|	|	|	0.04
179.667	0.00	0.01	0.054	O	|	|	|	|	0.04
179.750	0.00	0.01	0.053	O	|	|	|	|	0.04
179.833	0.00	0.01	0.053	O	|	|	|	|	0.04
179.917	0.00	0.01	0.053	O	|	|	|	|	0.04
180.000	0.00	0.01	0.053	O	|	|	|	|	0.04
180.083	0.00	0.01	0.053	O	|	|	|	|	0.04
180.167	0.00	0.01	0.053	O	|	|	|	|	0.04
180.250	0.00	0.01	0.053	O	|	|	|	|	0.04
180.333	0.00	0.01	0.053	O	|	|	|	|	0.04
180.417	0.00	0.01	0.053	O	|	|	|	|	0.04
180.500	0.00	0.01	0.053	O	|	|	|	|	0.04
180.583	0.00	0.01	0.052	O	|	|	|	|	0.04
180.667	0.00	0.01	0.052	O	|	|	|	|	0.04
180.750	0.00	0.01	0.052	O	|	|	|	|	0.04
180.833	0.00	0.01	0.052	O	|	|	|	|	0.04
180.917	0.00	0.01	0.052	O	|	|	|	|	0.04
181.000	0.00	0.01	0.052	O	|	|	|	|	0.04
181.083	0.00	0.01	0.052	O	|	|	|	|	0.04
181.167	0.00	0.01	0.052	O	|	|	|	|	0.04
181.250	0.00	0.01	0.052	O	|	|	|	|	0.04
181.333	0.00	0.01	0.052	O	|	|	|	|	0.04
181.417	0.00	0.01	0.051	O	|	|	|	|	0.04
181.500	0.00	0.01	0.051	O	|	|	|	|	0.04
181.583	0.00	0.01	0.051	O	|	|	|	|	0.04
181.667	0.00	0.01	0.051	O	|	|	|	|	0.04
181.750	0.00	0.01	0.051	O	|	|	|	|	0.04
181.833	0.00	0.01	0.051	O	|	|	|	|	0.04
181.917	0.00	0.01	0.051	O	|	|	|	|	0.04
182.000	0.00	0.01	0.051	O	|	|	|	|	0.04
182.083	0.00	0.01	0.051	O	|	|	|	|	0.04
182.167	0.00	0.01	0.051	O	|	|	|	|	0.04
182.250	0.00	0.01	0.050	O	|	|	|	|	0.04
182.333	0.00	0.01	0.050	O	|	|	|	|	0.04
182.417	0.00	0.01	0.050	O	|	|	|	|	0.04
182.500	0.00	0.01	0.050	O	|	|	|	|	0.04
182.583	0.00	0.01	0.050	O	|	|	|	|	0.04
182.667	0.00	0.01	0.050	O	|	|	|	|	0.04
182.750	0.00	0.01	0.050	O	|	|	|	|	0.04
182.833	0.00	0.01	0.050	O	|	|	|	|	0.04
182.917	0.00	0.01	0.050	O	|	|	|	|	0.04
183.000	0.00	0.01	0.050	O	|	|	|	|	0.04
183.083	0.00	0.01	0.050	O	|	|	|	|	0.04
183.167	0.00	0.01	0.049	O	|	|	|	|	0.04
183.250	0.00	0.01	0.049	O	|	|	|	|	0.04
183.333	0.00	0.01	0.049	O	|	|	|	|	0.04
183.417	0.00	0.01	0.049	O	|	|	|	|	0.04
183.500	0.00	0.01	0.049	O	|	|	|	|	0.04
183.583	0.00	0.01	0.049	O	|	|	|	|	0.04

183.667	0.00	0.01	0.049	O	|	|	|	|	0.04
183.750	0.00	0.01	0.049	O	|	|	|	|	0.04
183.833	0.00	0.01	0.049	O	|	|	|	|	0.04
183.917	0.00	0.01	0.049	O	|	|	|	|	0.04
184.000	0.00	0.01	0.048	O	|	|	|	|	0.04
184.083	0.00	0.01	0.048	O	|	|	|	|	0.04
184.167	0.00	0.01	0.048	O	|	|	|	|	0.04
184.250	0.00	0.01	0.048	O	|	|	|	|	0.04
184.333	0.00	0.01	0.048	O	|	|	|	|	0.04
184.417	0.00	0.01	0.048	O	|	|	|	|	0.04
184.500	0.00	0.01	0.048	O	|	|	|	|	0.04
184.583	0.00	0.01	0.048	O	|	|	|	|	0.04
184.667	0.00	0.01	0.048	O	|	|	|	|	0.04
184.750	0.00	0.01	0.048	O	|	|	|	|	0.04
184.833	0.00	0.01	0.048	O	|	|	|	|	0.04
184.917	0.00	0.01	0.047	O	|	|	|	|	0.04
185.000	0.00	0.01	0.047	O	|	|	|	|	0.04
185.083	0.00	0.01	0.047	O	|	|	|	|	0.04
185.167	0.00	0.01	0.047	O	|	|	|	|	0.04
185.250	0.00	0.01	0.047	O	|	|	|	|	0.04
185.333	0.00	0.01	0.047	O	|	|	|	|	0.04
185.417	0.00	0.01	0.047	O	|	|	|	|	0.04
185.500	0.00	0.01	0.047	O	|	|	|	|	0.04
185.583	0.00	0.01	0.047	O	|	|	|	|	0.04
185.667	0.00	0.01	0.047	O	|	|	|	|	0.04
185.750	0.00	0.01	0.047	O	|	|	|	|	0.04
185.833	0.00	0.01	0.046	O	|	|	|	|	0.04
185.917	0.00	0.01	0.046	O	|	|	|	|	0.04
186.000	0.00	0.01	0.046	O	|	|	|	|	0.04
186.083	0.00	0.01	0.046	O	|	|	|	|	0.04
186.167	0.00	0.01	0.046	O	|	|	|	|	0.04
186.250	0.00	0.01	0.046	O	|	|	|	|	0.04
186.333	0.00	0.01	0.046	O	|	|	|	|	0.04
186.417	0.00	0.01	0.046	O	|	|	|	|	0.04
186.500	0.00	0.01	0.046	O	|	|	|	|	0.04
186.583	0.00	0.01	0.046	O	|	|	|	|	0.04
186.667	0.00	0.01	0.046	O	|	|	|	|	0.04
186.750	0.00	0.01	0.045	O	|	|	|	|	0.04
186.833	0.00	0.01	0.045	O	|	|	|	|	0.04
186.917	0.00	0.01	0.045	O	|	|	|	|	0.04
187.000	0.00	0.01	0.045	O	|	|	|	|	0.04
187.083	0.00	0.01	0.045	O	|	|	|	|	0.04
187.167	0.00	0.01	0.045	O	|	|	|	|	0.04
187.250	0.00	0.01	0.045	O	|	|	|	|	0.04
187.333	0.00	0.01	0.045	O	|	|	|	|	0.04
187.417	0.00	0.01	0.045	O	|	|	|	|	0.04
187.500	0.00	0.01	0.045	O	|	|	|	|	0.04
187.583	0.00	0.01	0.045	O	|	|	|	|	0.04
187.667	0.00	0.01	0.045	O	|	|	|	|	0.04
187.750	0.00	0.01	0.044	O	|	|	|	|	0.04
187.833	0.00	0.01	0.044	O	|	|	|	|	0.04
187.917	0.00	0.01	0.044	O	|	|	|	|	0.04
188.000	0.00	0.01	0.044	O	|	|	|	|	0.04
188.083	0.00	0.01	0.044	O	|	|	|	|	0.04
188.167	0.00	0.01	0.044	O	|	|	|	|	0.04
188.250	0.00	0.01	0.044	O	|	|	|	|	0.04
188.333	0.00	0.01	0.044	O	|	|	|	|	0.04
188.417	0.00	0.01	0.044	O	|	|	|	|	0.04
188.500	0.00	0.01	0.044	O	|	|	|	|	0.04
188.583	0.00	0.01	0.044	O	|	|	|	|	0.04
188.667	0.00	0.01	0.044	O	|	|	|	|	0.04
188.750	0.00	0.01	0.043	O	|	|	|	|	0.04
188.833	0.00	0.01	0.043	O	|	|	|	|	0.04
188.917	0.00	0.01	0.043	O	|	|	|	|	0.04
189.000	0.00	0.01	0.043	O	|	|	|	|	0.04
189.083	0.00	0.01	0.043	O	|	|	|	|	0.03
189.167	0.00	0.01	0.043	O	|	|	|	|	0.03
189.250	0.00	0.01	0.043	O	|	|	|	|	0.03
189.333	0.00	0.01	0.043	O	|	|	|	|	0.03
189.417	0.00	0.01	0.043	O	|	|	|	|	0.03
189.500	0.00	0.01	0.043	O	|	|	|	|	0.03

189.583	0.00	0.01	0.043	O	|	|	|	|	0.03
189.667	0.00	0.01	0.043	O	|	|	|	|	0.03
189.750	0.00	0.01	0.042	O	|	|	|	|	0.03
189.833	0.00	0.01	0.042	O	|	|	|	|	0.03
189.917	0.00	0.01	0.042	O	|	|	|	|	0.03
190.000	0.00	0.01	0.042	O	|	|	|	|	0.03
190.083	0.00	0.01	0.042	O	|	|	|	|	0.03
190.167	0.00	0.01	0.042	O	|	|	|	|	0.03
190.250	0.00	0.01	0.042	O	|	|	|	|	0.03
190.333	0.00	0.01	0.042	O	|	|	|	|	0.03
190.417	0.00	0.01	0.042	O	|	|	|	|	0.03
190.500	0.00	0.01	0.042	O	|	|	|	|	0.03
190.583	0.00	0.01	0.042	O	|	|	|	|	0.03
190.667	0.00	0.01	0.042	O	|	|	|	|	0.03
190.750	0.00	0.01	0.041	O	|	|	|	|	0.03
190.833	0.00	0.01	0.041	O	|	|	|	|	0.03
190.917	0.00	0.01	0.041	O	|	|	|	|	0.03
191.000	0.00	0.01	0.041	O	|	|	|	|	0.03
191.083	0.00	0.01	0.041	O	|	|	|	|	0.03
191.167	0.00	0.01	0.041	O	|	|	|	|	0.03
191.250	0.00	0.01	0.041	O	|	|	|	|	0.03
191.333	0.00	0.01	0.041	O	|	|	|	|	0.03
191.417	0.00	0.01	0.041	O	|	|	|	|	0.03
191.500	0.00	0.01	0.041	O	|	|	|	|	0.03
191.583	0.00	0.01	0.041	O	|	|	|	|	0.03
191.667	0.00	0.01	0.041	O	|	|	|	|	0.03
191.750	0.00	0.01	0.041	O	|	|	|	|	0.03
191.833	0.00	0.01	0.040	O	|	|	|	|	0.03
191.917	0.00	0.01	0.040	O	|	|	|	|	0.03
192.000	0.00	0.01	0.040	O	|	|	|	|	0.03
192.083	0.00	0.01	0.040	O	|	|	|	|	0.03
192.167	0.00	0.01	0.040	O	|	|	|	|	0.03
192.250	0.00	0.01	0.040	O	|	|	|	|	0.03
192.333	0.00	0.01	0.040	O	|	|	|	|	0.03
192.417	0.00	0.01	0.040	O	|	|	|	|	0.03
192.500	0.00	0.01	0.040	O	|	|	|	|	0.03
192.583	0.00	0.01	0.040	O	|	|	|	|	0.03
192.667	0.00	0.01	0.040	O	|	|	|	|	0.03
192.750	0.00	0.01	0.040	O	|	|	|	|	0.03
192.833	0.00	0.01	0.040	O	|	|	|	|	0.03
192.917	0.00	0.01	0.039	O	|	|	|	|	0.03
193.000	0.00	0.01	0.039	O	|	|	|	|	0.03
193.083	0.00	0.01	0.039	O	|	|	|	|	0.03
193.167	0.00	0.01	0.039	O	|	|	|	|	0.03
193.250	0.00	0.01	0.039	O	|	|	|	|	0.03
193.333	0.00	0.01	0.039	O	|	|	|	|	0.03
193.417	0.00	0.01	0.039	O	|	|	|	|	0.03
193.500	0.00	0.01	0.039	O	|	|	|	|	0.03
193.583	0.00	0.01	0.039	O	|	|	|	|	0.03
193.667	0.00	0.01	0.039	O	|	|	|	|	0.03
193.750	0.00	0.01	0.039	O	|	|	|	|	0.03
193.833	0.00	0.01	0.039	O	|	|	|	|	0.03
193.917	0.00	0.01	0.039	O	|	|	|	|	0.03
194.000	0.00	0.01	0.038	O	|	|	|	|	0.03
194.083	0.00	0.01	0.038	O	|	|	|	|	0.03
194.167	0.00	0.01	0.038	O	|	|	|	|	0.03
194.250	0.00	0.01	0.038	O	|	|	|	|	0.03
194.333	0.00	0.01	0.038	O	|	|	|	|	0.03
194.417	0.00	0.01	0.038	O	|	|	|	|	0.03
194.500	0.00	0.01	0.038	O	|	|	|	|	0.03
194.583	0.00	0.01	0.038	O	|	|	|	|	0.03
194.667	0.00	0.01	0.038	O	|	|	|	|	0.03
194.750	0.00	0.01	0.038	O	|	|	|	|	0.03
194.833	0.00	0.01	0.038	O	|	|	|	|	0.03
194.917	0.00	0.01	0.038	O	|	|	|	|	0.03
195.000	0.00	0.01	0.038	O	|	|	|	|	0.03
195.083	0.00	0.01	0.038	O	|	|	|	|	0.03
195.167	0.00	0.01	0.037	O	|	|	|	|	0.03
195.250	0.00	0.01	0.037	O	|	|	|	|	0.03
195.333	0.00	0.01	0.037	O	|	|	|	|	0.03
195.417	0.00	0.01	0.037	O	|	|	|	|	0.03

195.500	0.00	0.01	0.037	O	|	|	|	|	0.03
195.583	0.00	0.01	0.037	O	|	|	|	|	0.03
195.667	0.00	0.01	0.037	O	|	|	|	|	0.03
195.750	0.00	0.01	0.037	O	|	|	|	|	0.03
195.833	0.00	0.01	0.037	O	|	|	|	|	0.03
195.917	0.00	0.01	0.037	O	|	|	|	|	0.03
196.000	0.00	0.01	0.037	O	|	|	|	|	0.03
196.083	0.00	0.01	0.037	O	|	|	|	|	0.03
196.167	0.00	0.01	0.037	O	|	|	|	|	0.03
196.250	0.00	0.01	0.037	O	|	|	|	|	0.03
196.333	0.00	0.01	0.036	O	|	|	|	|	0.03
196.417	0.00	0.01	0.036	O	|	|	|	|	0.03
196.500	0.00	0.01	0.036	O	|	|	|	|	0.03
196.583	0.00	0.01	0.036	O	|	|	|	|	0.03
196.667	0.00	0.01	0.036	O	|	|	|	|	0.03
196.750	0.00	0.01	0.036	O	|	|	|	|	0.03
196.833	0.00	0.01	0.036	O	|	|	|	|	0.03
196.917	0.00	0.01	0.036	O	|	|	|	|	0.03
197.000	0.00	0.01	0.036	O	|	|	|	|	0.03
197.083	0.00	0.01	0.036	O	|	|	|	|	0.03
197.167	0.00	0.01	0.036	O	|	|	|	|	0.03
197.250	0.00	0.01	0.036	O	|	|	|	|	0.03
197.333	0.00	0.01	0.036	O	|	|	|	|	0.03
197.417	0.00	0.01	0.036	O	|	|	|	|	0.03
197.500	0.00	0.01	0.035	O	|	|	|	|	0.03
197.583	0.00	0.01	0.035	O	|	|	|	|	0.03
197.667	0.00	0.01	0.035	O	|	|	|	|	0.03
197.750	0.00	0.01	0.035	O	|	|	|	|	0.03
197.833	0.00	0.01	0.035	O	|	|	|	|	0.03
197.917	0.00	0.01	0.035	O	|	|	|	|	0.03
198.000	0.00	0.01	0.035	O	|	|	|	|	0.03
198.083	0.00	0.01	0.035	O	|	|	|	|	0.03
198.167	0.00	0.01	0.035	O	|	|	|	|	0.03
198.250	0.00	0.01	0.035	O	|	|	|	|	0.03
198.333	0.00	0.01	0.035	O	|	|	|	|	0.03
198.417	0.00	0.01	0.035	O	|	|	|	|	0.03
198.500	0.00	0.01	0.035	O	|	|	|	|	0.03
198.583	0.00	0.01	0.035	O	|	|	|	|	0.03
198.667	0.00	0.01	0.035	O	|	|	|	|	0.03
198.750	0.00	0.01	0.034	O	|	|	|	|	0.03
198.833	0.00	0.01	0.034	O	|	|	|	|	0.03
198.917	0.00	0.01	0.034	O	|	|	|	|	0.03
199.000	0.00	0.01	0.034	O	|	|	|	|	0.03
199.083	0.00	0.01	0.034	O	|	|	|	|	0.03
199.167	0.00	0.01	0.034	O	|	|	|	|	0.03
199.250	0.00	0.01	0.034	O	|	|	|	|	0.03
199.333	0.00	0.01	0.034	O	|	|	|	|	0.03
199.417	0.00	0.01	0.034	O	|	|	|	|	0.03
199.500	0.00	0.01	0.034	O	|	|	|	|	0.03
199.583	0.00	0.01	0.034	O	|	|	|	|	0.03
199.667	0.00	0.01	0.034	O	|	|	|	|	0.03
199.750	0.00	0.01	0.034	O	|	|	|	|	0.03
199.833	0.00	0.01	0.034	O	|	|	|	|	0.03
199.917	0.00	0.01	0.034	O	|	|	|	|	0.03
200.000	0.00	0.01	0.034	O	|	|	|	|	0.03
200.083	0.00	0.01	0.033	O	|	|	|	|	0.03
200.167	0.00	0.01	0.033	O	|	|	|	|	0.03
200.250	0.00	0.01	0.033	O	|	|	|	|	0.03
200.333	0.00	0.01	0.033	O	|	|	|	|	0.03
200.417	0.00	0.01	0.033	O	|	|	|	|	0.03
200.500	0.00	0.01	0.033	O	|	|	|	|	0.03
200.583	0.00	0.01	0.033	O	|	|	|	|	0.03
200.667	0.00	0.01	0.033	O	|	|	|	|	0.03
200.750	0.00	0.01	0.033	O	|	|	|	|	0.03
200.833	0.00	0.01	0.033	O	|	|	|	|	0.03
200.917	0.00	0.01	0.033	O	|	|	|	|	0.03
201.000	0.00	0.01	0.033	O	|	|	|	|	0.03
201.083	0.00	0.01	0.033	O	|	|	|	|	0.03
201.167	0.00	0.01	0.033	O	|	|	|	|	0.03
201.250	0.00	0.01	0.033	O	|	|	|	|	0.03
201.333	0.00	0.01	0.032	O	|	|	|	|	0.03

201.417	0.00	0.01	0.032	O	|	|	|	|	0.03
201.500	0.00	0.01	0.032	O	|	|	|	|	0.03
201.583	0.00	0.01	0.032	O	|	|	|	|	0.03
201.667	0.00	0.01	0.032	O	|	|	|	|	0.03
201.750	0.00	0.01	0.032	O	|	|	|	|	0.03
201.833	0.00	0.01	0.032	O	|	|	|	|	0.03
201.917	0.00	0.01	0.032	O	|	|	|	|	0.03
202.000	0.00	0.01	0.032	O	|	|	|	|	0.03
202.083	0.00	0.01	0.032	O	|	|	|	|	0.03
202.167	0.00	0.01	0.032	O	|	|	|	|	0.03
202.250	0.00	0.01	0.032	O	|	|	|	|	0.03
202.333	0.00	0.01	0.032	O	|	|	|	|	0.03
202.417	0.00	0.01	0.032	O	|	|	|	|	0.03
202.500	0.00	0.01	0.032	O	|	|	|	|	0.03
202.583	0.00	0.01	0.032	O	|	|	|	|	0.03
202.667	0.00	0.01	0.032	O	|	|	|	|	0.03
202.750	0.00	0.01	0.031	O	|	|	|	|	0.03
202.833	0.00	0.01	0.031	O	|	|	|	|	0.03
202.917	0.00	0.01	0.031	O	|	|	|	|	0.03
203.000	0.00	0.01	0.031	O	|	|	|	|	0.03
203.083	0.00	0.01	0.031	O	|	|	|	|	0.03
203.167	0.00	0.01	0.031	O	|	|	|	|	0.03
203.250	0.00	0.01	0.031	O	|	|	|	|	0.03
203.333	0.00	0.01	0.031	O	|	|	|	|	0.03
203.417	0.00	0.01	0.031	O	|	|	|	|	0.03
203.500	0.00	0.01	0.031	O	|	|	|	|	0.03
203.583	0.00	0.01	0.031	O	|	|	|	|	0.03
203.667	0.00	0.01	0.031	O	|	|	|	|	0.02
203.750	0.00	0.01	0.031	O	|	|	|	|	0.02
203.833	0.00	0.01	0.031	O	|	|	|	|	0.02
203.917	0.00	0.01	0.031	O	|	|	|	|	0.02
204.000	0.00	0.01	0.031	O	|	|	|	|	0.02
204.083	0.00	0.01	0.030	O	|	|	|	|	0.02
204.167	0.00	0.01	0.030	O	|	|	|	|	0.02
204.250	0.00	0.01	0.030	O	|	|	|	|	0.02
204.333	0.00	0.01	0.030	O	|	|	|	|	0.02
204.417	0.00	0.01	0.030	O	|	|	|	|	0.02
204.500	0.00	0.01	0.030	O	|	|	|	|	0.02
204.583	0.00	0.01	0.030	O	|	|	|	|	0.02
204.667	0.00	0.01	0.030	O	|	|	|	|	0.02
204.750	0.00	0.01	0.030	O	|	|	|	|	0.02
204.833	0.00	0.01	0.030	O	|	|	|	|	0.02
204.917	0.00	0.01	0.030	O	|	|	|	|	0.02
205.000	0.00	0.01	0.030	O	|	|	|	|	0.02
205.083	0.00	0.01	0.030	O	|	|	|	|	0.02
205.167	0.00	0.01	0.030	O	|	|	|	|	0.02
205.250	0.00	0.01	0.030	O	|	|	|	|	0.02
205.333	0.00	0.01	0.030	O	|	|	|	|	0.02
205.417	0.00	0.01	0.030	O	|	|	|	|	0.02
205.500	0.00	0.01	0.030	O	|	|	|	|	0.02
205.583	0.00	0.01	0.029	O	|	|	|	|	0.02
205.667	0.00	0.01	0.029	O	|	|	|	|	0.02
205.750	0.00	0.01	0.029	O	|	|	|	|	0.02
205.833	0.00	0.01	0.029	O	|	|	|	|	0.02
205.917	0.00	0.01	0.029	O	|	|	|	|	0.02
206.000	0.00	0.01	0.029	O	|	|	|	|	0.02
206.083	0.00	0.01	0.029	O	|	|	|	|	0.02
206.167	0.00	0.01	0.029	O	|	|	|	|	0.02
206.250	0.00	0.01	0.029	O	|	|	|	|	0.02
206.333	0.00	0.01	0.029	O	|	|	|	|	0.02
206.417	0.00	0.01	0.029	O	|	|	|	|	0.02
206.500	0.00	0.01	0.029	O	|	|	|	|	0.02
206.583	0.00	0.01	0.029	O	|	|	|	|	0.02
206.667	0.00	0.01	0.029	O	|	|	|	|	0.02
206.750	0.00	0.01	0.029	O	|	|	|	|	0.02
206.833	0.00	0.01	0.029	O	|	|	|	|	0.02
206.917	0.00	0.01	0.029	O	|	|	|	|	0.02
207.000	0.00	0.01	0.029	O	|	|	|	|	0.02
207.083	0.00	0.01	0.028	O	|	|	|	|	0.02
207.167	0.00	0.01	0.028	O	|	|	|	|	0.02
207.250	0.00	0.01	0.028	O	|	|	|	|	0.02

207.333	0.00	0.01	0.028	O	|	|	|	|	0.02
207.417	0.00	0.01	0.028	O	|	|	|	|	0.02
207.500	0.00	0.01	0.028	O	|	|	|	|	0.02
207.583	0.00	0.01	0.028	O	|	|	|	|	0.02
207.667	0.00	0.01	0.028	O	|	|	|	|	0.02
207.750	0.00	0.01	0.028	O	|	|	|	|	0.02
207.833	0.00	0.01	0.028	O	|	|	|	|	0.02
207.917	0.00	0.01	0.028	O	|	|	|	|	0.02
208.000	0.00	0.01	0.028	O	|	|	|	|	0.02
208.083	0.00	0.01	0.028	O	|	|	|	|	0.02
208.167	0.00	0.01	0.028	O	|	|	|	|	0.02
208.250	0.00	0.01	0.028	O	|	|	|	|	0.02
208.333	0.00	0.01	0.028	O	|	|	|	|	0.02
208.417	0.00	0.01	0.028	O	|	|	|	|	0.02
208.500	0.00	0.01	0.028	O	|	|	|	|	0.02
208.583	0.00	0.01	0.027	O	|	|	|	|	0.02
208.667	0.00	0.01	0.027	O	|	|	|	|	0.02
208.750	0.00	0.01	0.027	O	|	|	|	|	0.02
208.833	0.00	0.01	0.027	O	|	|	|	|	0.02
208.917	0.00	0.01	0.027	O	|	|	|	|	0.02
209.000	0.00	0.01	0.027	O	|	|	|	|	0.02
209.083	0.00	0.01	0.027	O	|	|	|	|	0.02
209.167	0.00	0.01	0.027	O	|	|	|	|	0.02
209.250	0.00	0.01	0.027	O	|	|	|	|	0.02
209.333	0.00	0.01	0.027	O	|	|	|	|	0.02
209.417	0.00	0.01	0.027	O	|	|	|	|	0.02
209.500	0.00	0.01	0.027	O	|	|	|	|	0.02
209.583	0.00	0.01	0.027	O	|	|	|	|	0.02
209.667	0.00	0.01	0.027	O	|	|	|	|	0.02
209.750	0.00	0.01	0.027	O	|	|	|	|	0.02
209.833	0.00	0.01	0.027	O	|	|	|	|	0.02
209.917	0.00	0.01	0.027	O	|	|	|	|	0.02
210.000	0.00	0.01	0.027	O	|	|	|	|	0.02
210.083	0.00	0.01	0.027	O	|	|	|	|	0.02
210.167	0.00	0.01	0.026	O	|	|	|	|	0.02
210.250	0.00	0.01	0.026	O	|	|	|	|	0.02
210.333	0.00	0.01	0.026	O	|	|	|	|	0.02
210.417	0.00	0.01	0.026	O	|	|	|	|	0.02
210.500	0.00	0.01	0.026	O	|	|	|	|	0.02
210.583	0.00	0.01	0.026	O	|	|	|	|	0.02
210.667	0.00	0.01	0.026	O	|	|	|	|	0.02
210.750	0.00	0.01	0.026	O	|	|	|	|	0.02
210.833	0.00	0.01	0.026	O	|	|	|	|	0.02
210.917	0.00	0.01	0.026	O	|	|	|	|	0.02
211.000	0.00	0.01	0.026	O	|	|	|	|	0.02
211.083	0.00	0.01	0.026	O	|	|	|	|	0.02
211.167	0.00	0.01	0.026	O	|	|	|	|	0.02
211.250	0.00	0.01	0.026	O	|	|	|	|	0.02
211.333	0.00	0.01	0.026	O	|	|	|	|	0.02
211.417	0.00	0.01	0.026	O	|	|	|	|	0.02
211.500	0.00	0.01	0.026	O	|	|	|	|	0.02
211.583	0.00	0.01	0.026	O	|	|	|	|	0.02
211.667	0.00	0.01	0.026	O	|	|	|	|	0.02
211.750	0.00	0.01	0.026	O	|	|	|	|	0.02
211.833	0.00	0.01	0.025	O	|	|	|	|	0.02
211.917	0.00	0.01	0.025	O	|	|	|	|	0.02
212.000	0.00	0.01	0.025	O	|	|	|	|	0.02
212.083	0.00	0.01	0.025	O	|	|	|	|	0.02
212.167	0.00	0.01	0.025	O	|	|	|	|	0.02
212.250	0.00	0.01	0.025	O	|	|	|	|	0.02
212.333	0.00	0.01	0.025	O	|	|	|	|	0.02
212.417	0.00	0.01	0.025	O	|	|	|	|	0.02
212.500	0.00	0.01	0.025	O	|	|	|	|	0.02
212.583	0.00	0.01	0.025	O	|	|	|	|	0.02
212.667	0.00	0.01	0.025	O	|	|	|	|	0.02
212.750	0.00	0.01	0.025	O	|	|	|	|	0.02
212.833	0.00	0.01	0.025	O	|	|	|	|	0.02
212.917	0.00	0.01	0.025	O	|	|	|	|	0.02
213.000	0.00	0.01	0.025	O	|	|	|	|	0.02
213.083	0.00	0.01	0.025	O	|	|	|	|	0.02
213.167	0.00	0.01	0.025	O	|	|	|	|	0.02

213.250	0.00	0.01	0.025	O	|	|	|	|	0.02
213.333	0.00	0.01	0.025	O	|	|	|	|	0.02
213.417	0.00	0.01	0.025	O	|	|	|	|	0.02
213.500	0.00	0.01	0.025	O	|	|	|	|	0.02
213.583	0.00	0.01	0.024	O	|	|	|	|	0.02
213.667	0.00	0.01	0.024	O	|	|	|	|	0.02
213.750	0.00	0.01	0.024	O	|	|	|	|	0.02
213.833	0.00	0.01	0.024	O	|	|	|	|	0.02
213.917	0.00	0.01	0.024	O	|	|	|	|	0.02
214.000	0.00	0.01	0.024	O	|	|	|	|	0.02
214.083	0.00	0.01	0.024	O	|	|	|	|	0.02
214.167	0.00	0.01	0.024	O	|	|	|	|	0.02
214.250	0.00	0.01	0.024	O	|	|	|	|	0.02
214.333	0.00	0.01	0.024	O	|	|	|	|	0.02
214.417	0.00	0.01	0.024	O	|	|	|	|	0.02
214.500	0.00	0.01	0.024	O	|	|	|	|	0.02
214.583	0.00	0.01	0.024	O	|	|	|	|	0.02
214.667	0.00	0.01	0.024	O	|	|	|	|	0.02
214.750	0.00	0.01	0.024	O	|	|	|	|	0.02
214.833	0.00	0.01	0.024	O	|	|	|	|	0.02
214.917	0.00	0.01	0.024	O	|	|	|	|	0.02
215.000	0.00	0.01	0.024	O	|	|	|	|	0.02
215.083	0.00	0.01	0.024	O	|	|	|	|	0.02
215.167	0.00	0.01	0.024	O	|	|	|	|	0.02
215.250	0.00	0.01	0.024	O	|	|	|	|	0.02
215.333	0.00	0.01	0.024	O	|	|	|	|	0.02
215.417	0.00	0.01	0.023	O	|	|	|	|	0.02
215.500	0.00	0.01	0.023	O	|	|	|	|	0.02
215.583	0.00	0.01	0.023	O	|	|	|	|	0.02
215.667	0.00	0.01	0.023	O	|	|	|	|	0.02
215.750	0.00	0.01	0.023	O	|	|	|	|	0.02
215.833	0.00	0.01	0.023	O	|	|	|	|	0.02
215.917	0.00	0.01	0.023	O	|	|	|	|	0.02
216.000	0.00	0.01	0.023	O	|	|	|	|	0.02
216.083	0.00	0.01	0.023	O	|	|	|	|	0.02
216.167	0.00	0.01	0.023	O	|	|	|	|	0.02
216.250	0.00	0.01	0.023	O	|	|	|	|	0.02
216.333	0.00	0.01	0.023	O	|	|	|	|	0.02
216.417	0.00	0.01	0.023	O	|	|	|	|	0.02
216.500	0.00	0.01	0.023	O	|	|	|	|	0.02
216.583	0.00	0.01	0.023	O	|	|	|	|	0.02
216.667	0.00	0.01	0.023	O	|	|	|	|	0.02
216.750	0.00	0.01	0.023	O	|	|	|	|	0.02
216.833	0.00	0.01	0.023	O	|	|	|	|	0.02
216.917	0.00	0.01	0.023	O	|	|	|	|	0.02
217.000	0.00	0.01	0.023	O	|	|	|	|	0.02
217.083	0.00	0.01	0.023	O	|	|	|	|	0.02
217.167	0.00	0.01	0.023	O	|	|	|	|	0.02
217.250	0.00	0.01	0.023	O	|	|	|	|	0.02
217.333	0.00	0.01	0.022	O	|	|	|	|	0.02
217.417	0.00	0.01	0.022	O	|	|	|	|	0.02
217.500	0.00	0.01	0.022	O	|	|	|	|	0.02
217.583	0.00	0.01	0.022	O	|	|	|	|	0.02
217.667	0.00	0.01	0.022	O	|	|	|	|	0.02
217.750	0.00	0.01	0.022	O	|	|	|	|	0.02
217.833	0.00	0.01	0.022	O	|	|	|	|	0.02
217.917	0.00	0.01	0.022	O	|	|	|	|	0.02
218.000	0.00	0.01	0.022	O	|	|	|	|	0.02
218.083	0.00	0.01	0.022	O	|	|	|	|	0.02
218.167	0.00	0.01	0.022	O	|	|	|	|	0.02
218.250	0.00	0.01	0.022	O	|	|	|	|	0.02
218.333	0.00	0.01	0.022	O	|	|	|	|	0.02
218.417	0.00	0.01	0.022	O	|	|	|	|	0.02
218.500	0.00	0.01	0.022	O	|	|	|	|	0.02
218.583	0.00	0.01	0.022	O	|	|	|	|	0.02
218.667	0.00	0.01	0.022	O	|	|	|	|	0.02
218.750	0.00	0.01	0.022	O	|	|	|	|	0.02
218.833	0.00	0.01	0.022	O	|	|	|	|	0.02
218.917	0.00	0.01	0.022	O	|	|	|	|	0.02
219.000	0.00	0.01	0.022	O	|	|	|	|	0.02
219.083	0.00	0.01	0.022	O	|	|	|	|	0.02

219.167	0.00	0.01	0.022	O	|	|	|	|	0.02
219.250	0.00	0.01	0.021	O	|	|	|	|	0.02
219.333	0.00	0.01	0.021	O	|	|	|	|	0.02
219.417	0.00	0.01	0.021	O	|	|	|	|	0.02
219.500	0.00	0.01	0.021	O	|	|	|	|	0.02
219.583	0.00	0.01	0.021	O	|	|	|	|	0.02
219.667	0.00	0.01	0.021	O	|	|	|	|	0.02
219.750	0.00	0.01	0.021	O	|	|	|	|	0.02
219.833	0.00	0.01	0.021	O	|	|	|	|	0.02
219.917	0.00	0.01	0.021	O	|	|	|	|	0.02
220.000	0.00	0.01	0.021	O	|	|	|	|	0.02
220.083	0.00	0.01	0.021	O	|	|	|	|	0.02
220.167	0.00	0.01	0.021	O	|	|	|	|	0.02
220.250	0.00	0.01	0.021	O	|	|	|	|	0.02
220.333	0.00	0.01	0.021	O	|	|	|	|	0.02
220.417	0.00	0.01	0.021	O	|	|	|	|	0.02
220.500	0.00	0.01	0.021	O	|	|	|	|	0.02
220.583	0.00	0.01	0.021	O	|	|	|	|	0.02
220.667	0.00	0.01	0.021	O	|	|	|	|	0.02
220.750	0.00	0.01	0.021	O	|	|	|	|	0.02
220.833	0.00	0.01	0.021	O	|	|	|	|	0.02
220.917	0.00	0.01	0.021	O	|	|	|	|	0.02
221.000	0.00	0.01	0.021	O	|	|	|	|	0.02
221.083	0.00	0.01	0.021	O	|	|	|	|	0.02
221.167	0.00	0.01	0.021	O	|	|	|	|	0.02
221.250	0.00	0.01	0.021	O	|	|	|	|	0.02
221.333	0.00	0.01	0.020	O	|	|	|	|	0.02
221.417	0.00	0.01	0.020	O	|	|	|	|	0.02
221.500	0.00	0.01	0.020	O	|	|	|	|	0.02
221.583	0.00	0.01	0.020	O	|	|	|	|	0.02
221.667	0.00	0.01	0.020	O	|	|	|	|	0.02
221.750	0.00	0.01	0.020	O	|	|	|	|	0.02
221.833	0.00	0.01	0.020	O	|	|	|	|	0.02
221.917	0.00	0.01	0.020	O	|	|	|	|	0.02
222.000	0.00	0.01	0.020	O	|	|	|	|	0.02
222.083	0.00	0.01	0.020	O	|	|	|	|	0.02
222.167	0.00	0.01	0.020	O	|	|	|	|	0.02
222.250	0.00	0.01	0.020	O	|	|	|	|	0.02
222.333	0.00	0.01	0.020	O	|	|	|	|	0.02
222.417	0.00	0.01	0.020	O	|	|	|	|	0.02
222.500	0.00	0.01	0.020	O	|	|	|	|	0.02
222.583	0.00	0.01	0.020	O	|	|	|	|	0.02
222.667	0.00	0.01	0.020	O	|	|	|	|	0.02
222.750	0.00	0.01	0.020	O	|	|	|	|	0.02
222.833	0.00	0.01	0.020	O	|	|	|	|	0.02
222.917	0.00	0.01	0.020	O	|	|	|	|	0.02
223.000	0.00	0.01	0.020	O	|	|	|	|	0.02
223.083	0.00	0.01	0.020	O	|	|	|	|	0.02
223.167	0.00	0.01	0.020	O	|	|	|	|	0.02
223.250	0.00	0.01	0.020	O	|	|	|	|	0.02
223.333	0.00	0.01	0.020	O	|	|	|	|	0.02
223.417	0.00	0.01	0.020	O	|	|	|	|	0.02
223.500	0.00	0.01	0.019	O	|	|	|	|	0.02
223.583	0.00	0.01	0.019	O	|	|	|	|	0.02
223.667	0.00	0.01	0.019	O	|	|	|	|	0.02
223.750	0.00	0.01	0.019	O	|	|	|	|	0.02
223.833	0.00	0.01	0.019	O	|	|	|	|	0.02
223.917	0.00	0.01	0.019	O	|	|	|	|	0.02
224.000	0.00	0.01	0.019	O	|	|	|	|	0.02
224.083	0.00	0.01	0.019	O	|	|	|	|	0.02
224.167	0.00	0.01	0.019	O	|	|	|	|	0.02
224.250	0.00	0.01	0.019	O	|	|	|	|	0.02
224.333	0.00	0.01	0.019	O	|	|	|	|	0.02
224.417	0.00	0.01	0.019	O	|	|	|	|	0.02
224.500	0.00	0.01	0.019	O	|	|	|	|	0.02
224.583	0.00	0.01	0.019	O	|	|	|	|	0.02
224.667	0.00	0.01	0.019	O	|	|	|	|	0.02
224.750	0.00	0.01	0.019	O	|	|	|	|	0.02
224.833	0.00	0.01	0.019	O	|	|	|	|	0.02
224.917	0.00	0.01	0.019	O	|	|	|	|	0.02
225.000	0.00	0.01	0.019	O	|	|	|	|	0.02

225.083	0.00	0.01	0.019	O	|	|	|	|	0.02
225.167	0.00	0.01	0.019	O	|	|	|	|	0.02
225.250	0.00	0.01	0.019	O	|	|	|	|	0.02
225.333	0.00	0.01	0.019	O	|	|	|	|	0.02
225.417	0.00	0.01	0.019	O	|	|	|	|	0.02
225.500	0.00	0.01	0.019	O	|	|	|	|	0.02
225.583	0.00	0.01	0.019	O	|	|	|	|	0.02
225.667	0.00	0.01	0.019	O	|	|	|	|	0.02
225.750	0.00	0.01	0.018	O	|	|	|	|	0.02
225.833	0.00	0.01	0.018	O	|	|	|	|	0.01
225.917	0.00	0.01	0.018	O	|	|	|	|	0.01
226.000	0.00	0.01	0.018	O	|	|	|	|	0.01
226.083	0.00	0.01	0.018	O	|	|	|	|	0.01
226.167	0.00	0.01	0.018	O	|	|	|	|	0.01
226.250	0.00	0.01	0.018	O	|	|	|	|	0.01
226.333	0.00	0.01	0.018	O	|	|	|	|	0.01
226.417	0.00	0.01	0.018	O	|	|	|	|	0.01
226.500	0.00	0.01	0.018	O	|	|	|	|	0.01
226.583	0.00	0.01	0.018	O	|	|	|	|	0.01
226.667	0.00	0.01	0.018	O	|	|	|	|	0.01
226.750	0.00	0.01	0.018	O	|	|	|	|	0.01
226.833	0.00	0.01	0.018	O	|	|	|	|	0.01
226.917	0.00	0.01	0.018	O	|	|	|	|	0.01
227.000	0.00	0.01	0.018	O	|	|	|	|	0.01
227.083	0.00	0.01	0.018	O	|	|	|	|	0.01
227.167	0.00	0.00	0.018	O	|	|	|	|	0.01
227.250	0.00	0.00	0.018	O	|	|	|	|	0.01
227.333	0.00	0.00	0.018	O	|	|	|	|	0.01
227.417	0.00	0.00	0.018	O	|	|	|	|	0.01
227.500	0.00	0.00	0.018	O	|	|	|	|	0.01
227.583	0.00	0.00	0.018	O	|	|	|	|	0.01
227.667	0.00	0.00	0.018	O	|	|	|	|	0.01
227.750	0.00	0.00	0.018	O	|	|	|	|	0.01
227.833	0.00	0.00	0.018	O	|	|	|	|	0.01
227.917	0.00	0.00	0.018	O	|	|	|	|	0.01
228.000	0.00	0.00	0.018	O	|	|	|	|	0.01
228.083	0.00	0.00	0.018	O	|	|	|	|	0.01
228.167	0.00	0.00	0.017	O	|	|	|	|	0.01
228.250	0.00	0.00	0.017	O	|	|	|	|	0.01
228.333	0.00	0.00	0.017	O	|	|	|	|	0.01
228.417	0.00	0.00	0.017	O	|	|	|	|	0.01
228.500	0.00	0.00	0.017	O	|	|	|	|	0.01
228.583	0.00	0.00	0.017	O	|	|	|	|	0.01
228.667	0.00	0.00	0.017	O	|	|	|	|	0.01
228.750	0.00	0.00	0.017	O	|	|	|	|	0.01
228.833	0.00	0.00	0.017	O	|	|	|	|	0.01
228.917	0.00	0.00	0.017	O	|	|	|	|	0.01
229.000	0.00	0.00	0.017	O	|	|	|	|	0.01
229.083	0.00	0.00	0.017	O	|	|	|	|	0.01
229.167	0.00	0.00	0.017	O	|	|	|	|	0.01
229.250	0.00	0.00	0.017	O	|	|	|	|	0.01
229.333	0.00	0.00	0.017	O	|	|	|	|	0.01
229.417	0.00	0.00	0.017	O	|	|	|	|	0.01
229.500	0.00	0.00	0.017	O	|	|	|	|	0.01
229.583	0.00	0.00	0.017	O	|	|	|	|	0.01
229.667	0.00	0.00	0.017	O	|	|	|	|	0.01
229.750	0.00	0.00	0.017	O	|	|	|	|	0.01
229.833	0.00	0.00	0.017	O	|	|	|	|	0.01
229.917	0.00	0.00	0.017	O	|	|	|	|	0.01
230.000	0.00	0.00	0.017	O	|	|	|	|	0.01
230.083	0.00	0.00	0.017	O	|	|	|	|	0.01
230.167	0.00	0.00	0.017	O	|	|	|	|	0.01
230.250	0.00	0.00	0.017	O	|	|	|	|	0.01
230.333	0.00	0.00	0.017	O	|	|	|	|	0.01
230.417	0.00	0.00	0.017	O	|	|	|	|	0.01
230.500	0.00	0.00	0.017	O	|	|	|	|	0.01
230.583	0.00	0.00	0.017	O	|	|	|	|	0.01
230.667	0.00	0.00	0.017	O	|	|	|	|	0.01
230.750	0.00	0.00	0.016	O	|	|	|	|	0.01
230.833	0.00	0.00	0.016	O	|	|	|	|	0.01
230.917	0.00	0.00	0.016	O	|	|	|	|	0.01

231.000	0.00	0.00	0.016	O	|	|	|	|	0.01
231.083	0.00	0.00	0.016	O	|	|	|	|	0.01
231.167	0.00	0.00	0.016	O	|	|	|	|	0.01
231.250	0.00	0.00	0.016	O	|	|	|	|	0.01
231.333	0.00	0.00	0.016	O	|	|	|	|	0.01
231.417	0.00	0.00	0.016	O	|	|	|	|	0.01
231.500	0.00	0.00	0.016	O	|	|	|	|	0.01
231.583	0.00	0.00	0.016	O	|	|	|	|	0.01
231.667	0.00	0.00	0.016	O	|	|	|	|	0.01
231.750	0.00	0.00	0.016	O	|	|	|	|	0.01
231.833	0.00	0.00	0.016	O	|	|	|	|	0.01
231.917	0.00	0.00	0.016	O	|	|	|	|	0.01
232.000	0.00	0.00	0.016	O	|	|	|	|	0.01
232.083	0.00	0.00	0.016	O	|	|	|	|	0.01
232.167	0.00	0.00	0.016	O	|	|	|	|	0.01
232.250	0.00	0.00	0.016	O	|	|	|	|	0.01
232.333	0.00	0.00	0.016	O	|	|	|	|	0.01
232.417	0.00	0.00	0.016	O	|	|	|	|	0.01
232.500	0.00	0.00	0.016	O	|	|	|	|	0.01
232.583	0.00	0.00	0.016	O	|	|	|	|	0.01
232.667	0.00	0.00	0.016	O	|	|	|	|	0.01
232.750	0.00	0.00	0.016	O	|	|	|	|	0.01
232.833	0.00	0.00	0.016	O	|	|	|	|	0.01
232.917	0.00	0.00	0.016	O	|	|	|	|	0.01
233.000	0.00	0.00	0.016	O	|	|	|	|	0.01
233.083	0.00	0.00	0.016	O	|	|	|	|	0.01
233.167	0.00	0.00	0.016	O	|	|	|	|	0.01
233.250	0.00	0.00	0.016	O	|	|	|	|	0.01
233.333	0.00	0.00	0.016	O	|	|	|	|	0.01
233.417	0.00	0.00	0.015	O	|	|	|	|	0.01
233.500	0.00	0.00	0.015	O	|	|	|	|	0.01
233.583	0.00	0.00	0.015	O	|	|	|	|	0.01
233.667	0.00	0.00	0.015	O	|	|	|	|	0.01
233.750	0.00	0.00	0.015	O	|	|	|	|	0.01
233.833	0.00	0.00	0.015	O	|	|	|	|	0.01
233.917	0.00	0.00	0.015	O	|	|	|	|	0.01
234.000	0.00	0.00	0.015	O	|	|	|	|	0.01
234.083	0.00	0.00	0.015	O	|	|	|	|	0.01
234.167	0.00	0.00	0.015	O	|	|	|	|	0.01
234.250	0.00	0.00	0.015	O	|	|	|	|	0.01
234.333	0.00	0.00	0.015	O	|	|	|	|	0.01
234.417	0.00	0.00	0.015	O	|	|	|	|	0.01
234.500	0.00	0.00	0.015	O	|	|	|	|	0.01
234.583	0.00	0.00	0.015	O	|	|	|	|	0.01
234.667	0.00	0.00	0.015	O	|	|	|	|	0.01
234.750	0.00	0.00	0.015	O	|	|	|	|	0.01
234.833	0.00	0.00	0.015	O	|	|	|	|	0.01
234.917	0.00	0.00	0.015	O	|	|	|	|	0.01
235.000	0.00	0.00	0.015	O	|	|	|	|	0.01
235.083	0.00	0.00	0.015	O	|	|	|	|	0.01
235.167	0.00	0.00	0.015	O	|	|	|	|	0.01
235.250	0.00	0.00	0.015	O	|	|	|	|	0.01
235.333	0.00	0.00	0.015	O	|	|	|	|	0.01
235.417	0.00	0.00	0.015	O	|	|	|	|	0.01
235.500	0.00	0.00	0.015	O	|	|	|	|	0.01
235.583	0.00	0.00	0.015	O	|	|	|	|	0.01
235.667	0.00	0.00	0.015	O	|	|	|	|	0.01
235.750	0.00	0.00	0.015	O	|	|	|	|	0.01
235.833	0.00	0.00	0.015	O	|	|	|	|	0.01
235.917	0.00	0.00	0.015	O	|	|	|	|	0.01
236.000	0.00	0.00	0.015	O	|	|	|	|	0.01
236.083	0.00	0.00	0.015	O	|	|	|	|	0.01
236.167	0.00	0.00	0.015	O	|	|	|	|	0.01
236.250	0.00	0.00	0.015	O	|	|	|	|	0.01
236.333	0.00	0.00	0.014	O	|	|	|	|	0.01
236.417	0.00	0.00	0.014	O	|	|	|	|	0.01
236.500	0.00	0.00	0.014	O	|	|	|	|	0.01
236.583	0.00	0.00	0.014	O	|	|	|	|	0.01
236.667	0.00	0.00	0.014	O	|	|	|	|	0.01
236.750	0.00	0.00	0.014	O	|	|	|	|	0.01
236.833	0.00	0.00	0.014	O	|	|	|	|	0.01

236.917	0.00	0.00	0.014	O	|	|	|	|	0.01
237.000	0.00	0.00	0.014	O	|	|	|	|	0.01
237.083	0.00	0.00	0.014	O	|	|	|	|	0.01
237.167	0.00	0.00	0.014	O	|	|	|	|	0.01
237.250	0.00	0.00	0.014	O	|	|	|	|	0.01
237.333	0.00	0.00	0.014	O	|	|	|	|	0.01
237.417	0.00	0.00	0.014	O	|	|	|	|	0.01
237.500	0.00	0.00	0.014	O	|	|	|	|	0.01
237.583	0.00	0.00	0.014	O	|	|	|	|	0.01
237.667	0.00	0.00	0.014	O	|	|	|	|	0.01
237.750	0.00	0.00	0.014	O	|	|	|	|	0.01
237.833	0.00	0.00	0.014	O	|	|	|	|	0.01
237.917	0.00	0.00	0.014	O	|	|	|	|	0.01
238.000	0.00	0.00	0.014	O	|	|	|	|	0.01
238.083	0.00	0.00	0.014	O	|	|	|	|	0.01
238.167	0.00	0.00	0.014	O	|	|	|	|	0.01
238.250	0.00	0.00	0.014	O	|	|	|	|	0.01
238.333	0.00	0.00	0.014	O	|	|	|	|	0.01
238.417	0.00	0.00	0.014	O	|	|	|	|	0.01
238.500	0.00	0.00	0.014	O	|	|	|	|	0.01
238.583	0.00	0.00	0.014	O	|	|	|	|	0.01
238.667	0.00	0.00	0.014	O	|	|	|	|	0.01
238.750	0.00	0.00	0.014	O	|	|	|	|	0.01
238.833	0.00	0.00	0.014	O	|	|	|	|	0.01
238.917	0.00	0.00	0.014	O	|	|	|	|	0.01
239.000	0.00	0.00	0.014	O	|	|	|	|	0.01
239.083	0.00	0.00	0.014	O	|	|	|	|	0.01
239.167	0.00	0.00	0.014	O	|	|	|	|	0.01
239.250	0.00	0.00	0.014	O	|	|	|	|	0.01
239.333	0.00	0.00	0.014	O	|	|	|	|	0.01
239.417	0.00	0.00	0.013	O	|	|	|	|	0.01
239.500	0.00	0.00	0.013	O	|	|	|	|	0.01
239.583	0.00	0.00	0.013	O	|	|	|	|	0.01
239.667	0.00	0.00	0.013	O	|	|	|	|	0.01
239.750	0.00	0.00	0.013	O	|	|	|	|	0.01
239.833	0.00	0.00	0.013	O	|	|	|	|	0.01
239.917	0.00	0.00	0.013	O	|	|	|	|	0.01
240.000	0.00	0.00	0.013	O	|	|	|	|	0.01
240.083	0.00	0.00	0.013	O	|	|	|	|	0.01
240.167	0.00	0.00	0.013	O	|	|	|	|	0.01
240.250	0.00	0.00	0.013	O	|	|	|	|	0.01
240.333	0.00	0.00	0.013	O	|	|	|	|	0.01
240.417	0.00	0.00	0.013	O	|	|	|	|	0.01
240.500	0.00	0.00	0.013	O	|	|	|	|	0.01
240.583	0.00	0.00	0.013	O	|	|	|	|	0.01
240.667	0.00	0.00	0.013	O	|	|	|	|	0.01
240.750	0.00	0.00	0.013	O	|	|	|	|	0.01
240.833	0.00	0.00	0.013	O	|	|	|	|	0.01
240.917	0.00	0.00	0.013	O	|	|	|	|	0.01
241.000	0.00	0.00	0.013	O	|	|	|	|	0.01
241.083	0.00	0.00	0.013	O	|	|	|	|	0.01
241.167	0.00	0.00	0.013	O	|	|	|	|	0.01
241.250	0.00	0.00	0.013	O	|	|	|	|	0.01
241.333	0.00	0.00	0.013	O	|	|	|	|	0.01
241.417	0.00	0.00	0.013	O	|	|	|	|	0.01
241.500	0.00	0.00	0.013	O	|	|	|	|	0.01
241.583	0.00	0.00	0.013	O	|	|	|	|	0.01
241.667	0.00	0.00	0.013	O	|	|	|	|	0.01
241.750	0.00	0.00	0.013	O	|	|	|	|	0.01
241.833	0.00	0.00	0.013	O	|	|	|	|	0.01
241.917	0.00	0.00	0.013	O	|	|	|	|	0.01
242.000	0.00	0.00	0.013	O	|	|	|	|	0.01
242.083	0.00	0.00	0.013	O	|	|	|	|	0.01
242.167	0.00	0.00	0.013	O	|	|	|	|	0.01
242.250	0.00	0.00	0.013	O	|	|	|	|	0.01
242.333	0.00	0.00	0.013	O	|	|	|	|	0.01
242.417	0.00	0.00	0.013	O	|	|	|	|	0.01
242.500	0.00	0.00	0.013	O	|	|	|	|	0.01
242.583	0.00	0.00	0.013	O	|	|	|	|	0.01
242.667	0.00	0.00	0.013	O	|	|	|	|	0.01
242.750	0.00	0.00	0.012	O	|	|	|	|	0.01

242.833	0.00	0.00	0.012	O	|	|	|	|	0.01
242.917	0.00	0.00	0.012	O	|	|	|	|	0.01
243.000	0.00	0.00	0.012	O	|	|	|	|	0.01
243.083	0.00	0.00	0.012	O	|	|	|	|	0.01
243.167	0.00	0.00	0.012	O	|	|	|	|	0.01
243.250	0.00	0.00	0.012	O	|	|	|	|	0.01
243.333	0.00	0.00	0.012	O	|	|	|	|	0.01
243.417	0.00	0.00	0.012	O	|	|	|	|	0.01
243.500	0.00	0.00	0.012	O	|	|	|	|	0.01
243.583	0.00	0.00	0.012	O	|	|	|	|	0.01
243.667	0.00	0.00	0.012	O	|	|	|	|	0.01
243.750	0.00	0.00	0.012	O	|	|	|	|	0.01
243.833	0.00	0.00	0.012	O	|	|	|	|	0.01
243.917	0.00	0.00	0.012	O	|	|	|	|	0.01
244.000	0.00	0.00	0.012	O	|	|	|	|	0.01
244.083	0.00	0.00	0.012	O	|	|	|	|	0.01
244.167	0.00	0.00	0.012	O	|	|	|	|	0.01
244.250	0.00	0.00	0.012	O	|	|	|	|	0.01
244.333	0.00	0.00	0.012	O	|	|	|	|	0.01
244.417	0.00	0.00	0.012	O	|	|	|	|	0.01
244.500	0.00	0.00	0.012	O	|	|	|	|	0.01
244.583	0.00	0.00	0.012	O	|	|	|	|	0.01
244.667	0.00	0.00	0.012	O	|	|	|	|	0.01
244.750	0.00	0.00	0.012	O	|	|	|	|	0.01
244.833	0.00	0.00	0.012	O	|	|	|	|	0.01
244.917	0.00	0.00	0.012	O	|	|	|	|	0.01
245.000	0.00	0.00	0.012	O	|	|	|	|	0.01
245.083	0.00	0.00	0.012	O	|	|	|	|	0.01
245.167	0.00	0.00	0.012	O	|	|	|	|	0.01
245.250	0.00	0.00	0.012	O	|	|	|	|	0.01
245.333	0.00	0.00	0.012	O	|	|	|	|	0.01
245.417	0.00	0.00	0.012	O	|	|	|	|	0.01
245.500	0.00	0.00	0.012	O	|	|	|	|	0.01
245.583	0.00	0.00	0.012	O	|	|	|	|	0.01
245.667	0.00	0.00	0.012	O	|	|	|	|	0.01
245.750	0.00	0.00	0.012	O	|	|	|	|	0.01
245.833	0.00	0.00	0.012	O	|	|	|	|	0.01
245.917	0.00	0.00	0.012	O	|	|	|	|	0.01
246.000	0.00	0.00	0.012	O	|	|	|	|	0.01
246.083	0.00	0.00	0.012	O	|	|	|	|	0.01
246.167	0.00	0.00	0.012	O	|	|	|	|	0.01
246.250	0.00	0.00	0.012	O	|	|	|	|	0.01
246.333	0.00	0.00	0.012	O	|	|	|	|	0.01
246.417	0.00	0.00	0.011	O	|	|	|	|	0.01
246.500	0.00	0.00	0.011	O	|	|	|	|	0.01
246.583	0.00	0.00	0.011	O	|	|	|	|	0.01
246.667	0.00	0.00	0.011	O	|	|	|	|	0.01
246.750	0.00	0.00	0.011	O	|	|	|	|	0.01
246.833	0.00	0.00	0.011	O	|	|	|	|	0.01
246.917	0.00	0.00	0.011	O	|	|	|	|	0.01
247.000	0.00	0.00	0.011	O	|	|	|	|	0.01
247.083	0.00	0.00	0.011	O	|	|	|	|	0.01
247.167	0.00	0.00	0.011	O	|	|	|	|	0.01
247.250	0.00	0.00	0.011	O	|	|	|	|	0.01
247.333	0.00	0.00	0.011	O	|	|	|	|	0.01
247.417	0.00	0.00	0.011	O	|	|	|	|	0.01
247.500	0.00	0.00	0.011	O	|	|	|	|	0.01
247.583	0.00	0.00	0.011	O	|	|	|	|	0.01
247.667	0.00	0.00	0.011	O	|	|	|	|	0.01
247.750	0.00	0.00	0.011	O	|	|	|	|	0.01
247.833	0.00	0.00	0.011	O	|	|	|	|	0.01
247.917	0.00	0.00	0.011	O	|	|	|	|	0.01
248.000	0.00	0.00	0.011	O	|	|	|	|	0.01
248.083	0.00	0.00	0.011	O	|	|	|	|	0.01
248.167	0.00	0.00	0.011	O	|	|	|	|	0.01
248.250	0.00	0.00	0.011	O	|	|	|	|	0.01
248.333	0.00	0.00	0.011	O	|	|	|	|	0.01
248.417	0.00	0.00	0.011	O	|	|	|	|	0.01
248.500	0.00	0.00	0.011	O	|	|	|	|	0.01
248.583	0.00	0.00	0.011	O	|	|	|	|	0.01
248.667	0.00	0.00	0.011	O	|	|	|	|	0.01

248.750	0.00	0.00	0.011	O	|	|	|	|	0.01
248.833	0.00	0.00	0.011	O	|	|	|	|	0.01
248.917	0.00	0.00	0.011	O	|	|	|	|	0.01
249.000	0.00	0.00	0.011	O	|	|	|	|	0.01
249.083	0.00	0.00	0.011	O	|	|	|	|	0.01
249.167	0.00	0.00	0.011	O	|	|	|	|	0.01
249.250	0.00	0.00	0.011	O	|	|	|	|	0.01
249.333	0.00	0.00	0.011	O	|	|	|	|	0.01
249.417	0.00	0.00	0.011	O	|	|	|	|	0.01
249.500	0.00	0.00	0.011	O	|	|	|	|	0.01
249.583	0.00	0.00	0.011	O	|	|	|	|	0.01
249.667	0.00	0.00	0.011	O	|	|	|	|	0.01
249.750	0.00	0.00	0.011	O	|	|	|	|	0.01
249.833	0.00	0.00	0.011	O	|	|	|	|	0.01
249.917	0.00	0.00	0.011	O	|	|	|	|	0.01
250.000	0.00	0.00	0.011	O	|	|	|	|	0.01
250.083	0.00	0.00	0.011	O	|	|	|	|	0.01
250.167	0.00	0.00	0.011	O	|	|	|	|	0.01
250.250	0.00	0.00	0.011	O	|	|	|	|	0.01
250.333	0.00	0.00	0.010	O	|	|	|	|	0.01
250.417	0.00	0.00	0.010	O	|	|	|	|	0.01
250.500	0.00	0.00	0.010	O	|	|	|	|	0.01
250.583	0.00	0.00	0.010	O	|	|	|	|	0.01
250.667	0.00	0.00	0.010	O	|	|	|	|	0.01
250.750	0.00	0.00	0.010	O	|	|	|	|	0.01
250.833	0.00	0.00	0.010	O	|	|	|	|	0.01
250.917	0.00	0.00	0.010	O	|	|	|	|	0.01
251.000	0.00	0.00	0.010	O	|	|	|	|	0.01
251.083	0.00	0.00	0.010	O	|	|	|	|	0.01
251.167	0.00	0.00	0.010	O	|	|	|	|	0.01
251.250	0.00	0.00	0.010	O	|	|	|	|	0.01
251.333	0.00	0.00	0.010	O	|	|	|	|	0.01
251.417	0.00	0.00	0.010	O	|	|	|	|	0.01
251.500	0.00	0.00	0.010	O	|	|	|	|	0.01
251.583	0.00	0.00	0.010	O	|	|	|	|	0.01
251.667	0.00	0.00	0.010	O	|	|	|	|	0.01
251.750	0.00	0.00	0.010	O	|	|	|	|	0.01
251.833	0.00	0.00	0.010	O	|	|	|	|	0.01
251.917	0.00	0.00	0.010	O	|	|	|	|	0.01
252.000	0.00	0.00	0.010	O	|	|	|	|	0.01
252.083	0.00	0.00	0.010	O	|	|	|	|	0.01
252.167	0.00	0.00	0.010	O	|	|	|	|	0.01
252.250	0.00	0.00	0.010	O	|	|	|	|	0.01
252.333	0.00	0.00	0.010	O	|	|	|	|	0.01
252.417	0.00	0.00	0.010	O	|	|	|	|	0.01
252.500	0.00	0.00	0.010	O	|	|	|	|	0.01
252.583	0.00	0.00	0.010	O	|	|	|	|	0.01
252.667	0.00	0.00	0.010	O	|	|	|	|	0.01
252.750	0.00	0.00	0.010	O	|	|	|	|	0.01
252.833	0.00	0.00	0.010	O	|	|	|	|	0.01
252.917	0.00	0.00	0.010	O	|	|	|	|	0.01
253.000	0.00	0.00	0.010	O	|	|	|	|	0.01
253.083	0.00	0.00	0.010	O	|	|	|	|	0.01
253.167	0.00	0.00	0.010	O	|	|	|	|	0.01
253.250	0.00	0.00	0.010	O	|	|	|	|	0.01
253.333	0.00	0.00	0.010	O	|	|	|	|	0.01
253.417	0.00	0.00	0.010	O	|	|	|	|	0.01
253.500	0.00	0.00	0.010	O	|	|	|	|	0.01
253.583	0.00	0.00	0.010	O	|	|	|	|	0.01
253.667	0.00	0.00	0.010	O	|	|	|	|	0.01
253.750	0.00	0.00	0.010	O	|	|	|	|	0.01
253.833	0.00	0.00	0.010	O	|	|	|	|	0.01
253.917	0.00	0.00	0.010	O	|	|	|	|	0.01
254.000	0.00	0.00	0.010	O	|	|	|	|	0.01
254.083	0.00	0.00	0.010	O	|	|	|	|	0.01
254.167	0.00	0.00	0.010	O	|	|	|	|	0.01
254.250	0.00	0.00	0.010	O	|	|	|	|	0.01
254.333	0.00	0.00	0.010	O	|	|	|	|	0.01
254.417	0.00	0.00	0.010	O	|	|	|	|	0.01
254.500	0.00	0.00	0.010	O	|	|	|	|	0.01
254.583	0.00	0.00	0.010	O	|	|	|	|	0.01

254.667	0.00	0.00	0.009	O	|	|	|	|	0.01
254.750	0.00	0.00	0.009	O	|	|	|	|	0.01
254.833	0.00	0.00	0.009	O	|	|	|	|	0.01
254.917	0.00	0.00	0.009	O	|	|	|	|	0.01
255.000	0.00	0.00	0.009	O	|	|	|	|	0.01
255.083	0.00	0.00	0.009	O	|	|	|	|	0.01
255.167	0.00	0.00	0.009	O	|	|	|	|	0.01
255.250	0.00	0.00	0.009	O	|	|	|	|	0.01
255.333	0.00	0.00	0.009	O	|	|	|	|	0.01
255.417	0.00	0.00	0.009	O	|	|	|	|	0.01
255.500	0.00	0.00	0.009	O	|	|	|	|	0.01
255.583	0.00	0.00	0.009	O	|	|	|	|	0.01
255.667	0.00	0.00	0.009	O	|	|	|	|	0.01
255.750	0.00	0.00	0.009	O	|	|	|	|	0.01
255.833	0.00	0.00	0.009	O	|	|	|	|	0.01
255.917	0.00	0.00	0.009	O	|	|	|	|	0.01
256.000	0.00	0.00	0.009	O	|	|	|	|	0.01
256.083	0.00	0.00	0.009	O	|	|	|	|	0.01
256.167	0.00	0.00	0.009	O	|	|	|	|	0.01
256.250	0.00	0.00	0.009	O	|	|	|	|	0.01
256.333	0.00	0.00	0.009	O	|	|	|	|	0.01
256.417	0.00	0.00	0.009	O	|	|	|	|	0.01
256.500	0.00	0.00	0.009	O	|	|	|	|	0.01
256.583	0.00	0.00	0.009	O	|	|	|	|	0.01
256.667	0.00	0.00	0.009	O	|	|	|	|	0.01
256.750	0.00	0.00	0.009	O	|	|	|	|	0.01
256.833	0.00	0.00	0.009	O	|	|	|	|	0.01
256.917	0.00	0.00	0.009	O	|	|	|	|	0.01
257.000	0.00	0.00	0.009	O	|	|	|	|	0.01
257.083	0.00	0.00	0.009	O	|	|	|	|	0.01
257.167	0.00	0.00	0.009	O	|	|	|	|	0.01
257.250	0.00	0.00	0.009	O	|	|	|	|	0.01
257.333	0.00	0.00	0.009	O	|	|	|	|	0.01
257.417	0.00	0.00	0.009	O	|	|	|	|	0.01
257.500	0.00	0.00	0.009	O	|	|	|	|	0.01
257.583	0.00	0.00	0.009	O	|	|	|	|	0.01
257.667	0.00	0.00	0.009	O	|	|	|	|	0.01
257.750	0.00	0.00	0.009	O	|	|	|	|	0.01
257.833	0.00	0.00	0.009	O	|	|	|	|	0.01
257.917	0.00	0.00	0.009	O	|	|	|	|	0.01
258.000	0.00	0.00	0.009	O	|	|	|	|	0.01
258.083	0.00	0.00	0.009	O	|	|	|	|	0.01
258.167	0.00	0.00	0.009	O	|	|	|	|	0.01
258.250	0.00	0.00	0.009	O	|	|	|	|	0.01
258.333	0.00	0.00	0.009	O	|	|	|	|	0.01
258.417	0.00	0.00	0.009	O	|	|	|	|	0.01
258.500	0.00	0.00	0.009	O	|	|	|	|	0.01
258.583	0.00	0.00	0.009	O	|	|	|	|	0.01
258.667	0.00	0.00	0.009	O	|	|	|	|	0.01
258.750	0.00	0.00	0.009	O	|	|	|	|	0.01
258.833	0.00	0.00	0.009	O	|	|	|	|	0.01
258.917	0.00	0.00	0.009	O	|	|	|	|	0.01
259.000	0.00	0.00	0.009	O	|	|	|	|	0.01
259.083	0.00	0.00	0.009	O	|	|	|	|	0.01
259.167	0.00	0.00	0.009	O	|	|	|	|	0.01
259.250	0.00	0.00	0.009	O	|	|	|	|	0.01
259.333	0.00	0.00	0.009	O	|	|	|	|	0.01
259.417	0.00	0.00	0.009	O	|	|	|	|	0.01
259.500	0.00	0.00	0.008	O	|	|	|	|	0.01
259.583	0.00	0.00	0.008	O	|	|	|	|	0.01
259.667	0.00	0.00	0.008	O	|	|	|	|	0.01
259.750	0.00	0.00	0.008	O	|	|	|	|	0.01
259.833	0.00	0.00	0.008	O	|	|	|	|	0.01
259.917	0.00	0.00	0.008	O	|	|	|	|	0.01
260.000	0.00	0.00	0.008	O	|	|	|	|	0.01
260.083	0.00	0.00	0.008	O	|	|	|	|	0.01
260.167	0.00	0.00	0.008	O	|	|	|	|	0.01
260.250	0.00	0.00	0.008	O	|	|	|	|	0.01
260.333	0.00	0.00	0.008	O	|	|	|	|	0.01
260.417	0.00	0.00	0.008	O	|	|	|	|	0.01
260.500	0.00	0.00	0.008	O	|	|	|	|	0.01

260.583	0.00	0.00	0.008	O	|	|	|	|	0.01
260.667	0.00	0.00	0.008	O	|	|	|	|	0.01
260.750	0.00	0.00	0.008	O	|	|	|	|	0.01
260.833	0.00	0.00	0.008	O	|	|	|	|	0.01
260.917	0.00	0.00	0.008	O	|	|	|	|	0.01
261.000	0.00	0.00	0.008	O	|	|	|	|	0.01
261.083	0.00	0.00	0.008	O	|	|	|	|	0.01
261.167	0.00	0.00	0.008	O	|	|	|	|	0.01
261.250	0.00	0.00	0.008	O	|	|	|	|	0.01
261.333	0.00	0.00	0.008	O	|	|	|	|	0.01
261.417	0.00	0.00	0.008	O	|	|	|	|	0.01
261.500	0.00	0.00	0.008	O	|	|	|	|	0.01
261.583	0.00	0.00	0.008	O	|	|	|	|	0.01
261.667	0.00	0.00	0.008	O	|	|	|	|	0.01
261.750	0.00	0.00	0.008	O	|	|	|	|	0.01
261.833	0.00	0.00	0.008	O	|	|	|	|	0.01
261.917	0.00	0.00	0.008	O	|	|	|	|	0.01
262.000	0.00	0.00	0.008	O	|	|	|	|	0.01
262.083	0.00	0.00	0.008	O	|	|	|	|	0.01
262.167	0.00	0.00	0.008	O	|	|	|	|	0.01
262.250	0.00	0.00	0.008	O	|	|	|	|	0.01
262.333	0.00	0.00	0.008	O	|	|	|	|	0.01
262.417	0.00	0.00	0.008	O	|	|	|	|	0.01
262.500	0.00	0.00	0.008	O	|	|	|	|	0.01
262.583	0.00	0.00	0.008	O	|	|	|	|	0.01
262.667	0.00	0.00	0.008	O	|	|	|	|	0.01
262.750	0.00	0.00	0.008	O	|	|	|	|	0.01
262.833	0.00	0.00	0.008	O	|	|	|	|	0.01
262.917	0.00	0.00	0.008	O	|	|	|	|	0.01
263.000	0.00	0.00	0.008	O	|	|	|	|	0.01
263.083	0.00	0.00	0.008	O	|	|	|	|	0.01
263.167	0.00	0.00	0.008	O	|	|	|	|	0.01
263.250	0.00	0.00	0.008	O	|	|	|	|	0.01
263.333	0.00	0.00	0.008	O	|	|	|	|	0.01
263.417	0.00	0.00	0.008	O	|	|	|	|	0.01
263.500	0.00	0.00	0.008	O	|	|	|	|	0.01
263.583	0.00	0.00	0.008	O	|	|	|	|	0.01
263.667	0.00	0.00	0.008	O	|	|	|	|	0.01
263.750	0.00	0.00	0.008	O	|	|	|	|	0.01
263.833	0.00	0.00	0.008	O	|	|	|	|	0.01
263.917	0.00	0.00	0.008	O	|	|	|	|	0.01
264.000	0.00	0.00	0.008	O	|	|	|	|	0.01
264.083	0.00	0.00	0.008	O	|	|	|	|	0.01
264.167	0.00	0.00	0.008	O	|	|	|	|	0.01
264.250	0.00	0.00	0.008	O	|	|	|	|	0.01
264.333	0.00	0.00	0.008	O	|	|	|	|	0.01
264.417	0.00	0.00	0.008	O	|	|	|	|	0.01
264.500	0.00	0.00	0.008	O	|	|	|	|	0.01
264.583	0.00	0.00	0.008	O	|	|	|	|	0.01
264.667	0.00	0.00	0.008	O	|	|	|	|	0.01
264.750	0.00	0.00	0.008	O	|	|	|	|	0.01
264.833	0.00	0.00	0.008	O	|	|	|	|	0.01
264.917	0.00	0.00	0.007	O	|	|	|	|	0.01
265.000	0.00	0.00	0.007	O	|	|	|	|	0.01
265.083	0.00	0.00	0.007	O	|	|	|	|	0.01
265.167	0.00	0.00	0.007	O	|	|	|	|	0.01
265.250	0.00	0.00	0.007	O	|	|	|	|	0.01
265.333	0.00	0.00	0.007	O	|	|	|	|	0.01
265.417	0.00	0.00	0.007	O	|	|	|	|	0.01
265.500	0.00	0.00	0.007	O	|	|	|	|	0.01
265.583	0.00	0.00	0.007	O	|	|	|	|	0.01
265.667	0.00	0.00	0.007	O	|	|	|	|	0.01
265.750	0.00	0.00	0.007	O	|	|	|	|	0.01
265.833	0.00	0.00	0.007	O	|	|	|	|	0.01
265.917	0.00	0.00	0.007	O	|	|	|	|	0.01
266.000	0.00	0.00	0.007	O	|	|	|	|	0.01
266.083	0.00	0.00	0.007	O	|	|	|	|	0.01
266.167	0.00	0.00	0.007	O	|	|	|	|	0.01
266.250	0.00	0.00	0.007	O	|	|	|	|	0.01
266.333	0.00	0.00	0.007	O	|	|	|	|	0.01
266.417	0.00	0.00	0.007	O	|	|	|	|	0.01

266.500	0.00	0.00	0.007	O	|	|	|	|	0.01
266.583	0.00	0.00	0.007	O	|	|	|	|	0.01
266.667	0.00	0.00	0.007	O	|	|	|	|	0.01
266.750	0.00	0.00	0.007	O	|	|	|	|	0.01
266.833	0.00	0.00	0.007	O	|	|	|	|	0.01
266.917	0.00	0.00	0.007	O	|	|	|	|	0.01
267.000	0.00	0.00	0.007	O	|	|	|	|	0.01
267.083	0.00	0.00	0.007	O	|	|	|	|	0.01
267.167	0.00	0.00	0.007	O	|	|	|	|	0.01
267.250	0.00	0.00	0.007	O	|	|	|	|	0.01
267.333	0.00	0.00	0.007	O	|	|	|	|	0.01
267.417	0.00	0.00	0.007	O	|	|	|	|	0.01
267.500	0.00	0.00	0.007	O	|	|	|	|	0.01
267.583	0.00	0.00	0.007	O	|	|	|	|	0.01
267.667	0.00	0.00	0.007	O	|	|	|	|	0.01
267.750	0.00	0.00	0.007	O	|	|	|	|	0.01
267.833	0.00	0.00	0.007	O	|	|	|	|	0.01
267.917	0.00	0.00	0.007	O	|	|	|	|	0.01
268.000	0.00	0.00	0.007	O	|	|	|	|	0.01
268.083	0.00	0.00	0.007	O	|	|	|	|	0.01
268.167	0.00	0.00	0.007	O	|	|	|	|	0.01
268.250	0.00	0.00	0.007	O	|	|	|	|	0.01
268.333	0.00	0.00	0.007	O	|	|	|	|	0.01
268.417	0.00	0.00	0.007	O	|	|	|	|	0.01
268.500	0.00	0.00	0.007	O	|	|	|	|	0.01
268.583	0.00	0.00	0.007	O	|	|	|	|	0.01
268.667	0.00	0.00	0.007	O	|	|	|	|	0.01
268.750	0.00	0.00	0.007	O	|	|	|	|	0.01
268.833	0.00	0.00	0.007	O	|	|	|	|	0.01
268.917	0.00	0.00	0.007	O	|	|	|	|	0.01
269.000	0.00	0.00	0.007	O	|	|	|	|	0.01
269.083	0.00	0.00	0.007	O	|	|	|	|	0.01
269.167	0.00	0.00	0.007	O	|	|	|	|	0.01
269.250	0.00	0.00	0.007	O	|	|	|	|	0.01
269.333	0.00	0.00	0.007	O	|	|	|	|	0.01
269.417	0.00	0.00	0.007	O	|	|	|	|	0.01
269.500	0.00	0.00	0.007	O	|	|	|	|	0.01
269.583	0.00	0.00	0.007	O	|	|	|	|	0.01
269.667	0.00	0.00	0.007	O	|	|	|	|	0.01
269.750	0.00	0.00	0.007	O	|	|	|	|	0.01
269.833	0.00	0.00	0.007	O	|	|	|	|	0.01
269.917	0.00	0.00	0.007	O	|	|	|	|	0.01
270.000	0.00	0.00	0.007	O	|	|	|	|	0.01
270.083	0.00	0.00	0.007	O	|	|	|	|	0.01
270.167	0.00	0.00	0.007	O	|	|	|	|	0.01
270.250	0.00	0.00	0.007	O	|	|	|	|	0.01
270.333	0.00	0.00	0.007	O	|	|	|	|	0.01
270.417	0.00	0.00	0.007	O	|	|	|	|	0.01
270.500	0.00	0.00	0.007	O	|	|	|	|	0.01
270.583	0.00	0.00	0.007	O	|	|	|	|	0.01
270.667	0.00	0.00	0.007	O	|	|	|	|	0.01
270.750	0.00	0.00	0.007	O	|	|	|	|	0.01
270.833	0.00	0.00	0.007	O	|	|	|	|	0.01
270.917	0.00	0.00	0.007	O	|	|	|	|	0.01
271.000	0.00	0.00	0.007	O	|	|	|	|	0.01
271.083	0.00	0.00	0.006	O	|	|	|	|	0.01
271.167	0.00	0.00	0.006	O	|	|	|	|	0.01
271.250	0.00	0.00	0.006	O	|	|	|	|	0.01
271.333	0.00	0.00	0.006	O	|	|	|	|	0.01
271.417	0.00	0.00	0.006	O	|	|	|	|	0.01
271.500	0.00	0.00	0.006	O	|	|	|	|	0.01
271.583	0.00	0.00	0.006	O	|	|	|	|	0.01
271.667	0.00	0.00	0.006	O	|	|	|	|	0.01
271.750	0.00	0.00	0.006	O	|	|	|	|	0.01
271.833	0.00	0.00	0.006	O	|	|	|	|	0.01
271.917	0.00	0.00	0.006	O	|	|	|	|	0.01
272.000	0.00	0.00	0.006	O	|	|	|	|	0.01
272.083	0.00	0.00	0.006	O	|	|	|	|	0.01
272.167	0.00	0.00	0.006	O	|	|	|	|	0.01
272.250	0.00	0.00	0.006	O	|	|	|	|	0.01
272.333	0.00	0.00	0.006	O	|	|	|	|	0.01

272.417	0.00	0.00	0.006	O	|	|	|	|	0.01
272.500	0.00	0.00	0.006	O	|	|	|	|	0.01
272.583	0.00	0.00	0.006	O	|	|	|	|	0.01
272.667	0.00	0.00	0.006	O	|	|	|	|	0.01
272.750	0.00	0.00	0.006	O	|	|	|	|	0.01
272.833	0.00	0.00	0.006	O	|	|	|	|	0.01
272.917	0.00	0.00	0.006	O	|	|	|	|	0.01
273.000	0.00	0.00	0.006	O	|	|	|	|	0.01
273.083	0.00	0.00	0.006	O	|	|	|	|	0.01
273.167	0.00	0.00	0.006	O	|	|	|	|	0.01
273.250	0.00	0.00	0.006	O	|	|	|	|	0.01
273.333	0.00	0.00	0.006	O	|	|	|	|	0.01
273.417	0.00	0.00	0.006	O	|	|	|	|	0.00
273.500	0.00	0.00	0.006	O	|	|	|	|	0.00
273.583	0.00	0.00	0.006	O	|	|	|	|	0.00
273.667	0.00	0.00	0.006	O	|	|	|	|	0.00
273.750	0.00	0.00	0.006	O	|	|	|	|	0.00
273.833	0.00	0.00	0.006	O	|	|	|	|	0.00
273.917	0.00	0.00	0.006	O	|	|	|	|	0.00
274.000	0.00	0.00	0.006	O	|	|	|	|	0.00
274.083	0.00	0.00	0.006	O	|	|	|	|	0.00
274.167	0.00	0.00	0.006	O	|	|	|	|	0.00
274.250	0.00	0.00	0.006	O	|	|	|	|	0.00
274.333	0.00	0.00	0.006	O	|	|	|	|	0.00
274.417	0.00	0.00	0.006	O	|	|	|	|	0.00
274.500	0.00	0.00	0.006	O	|	|	|	|	0.00
274.583	0.00	0.00	0.006	O	|	|	|	|	0.00
274.667	0.00	0.00	0.006	O	|	|	|	|	0.00
274.750	0.00	0.00	0.006	O	|	|	|	|	0.00
274.833	0.00	0.00	0.006	O	|	|	|	|	0.00
274.917	0.00	0.00	0.006	O	|	|	|	|	0.00
275.000	0.00	0.00	0.006	O	|	|	|	|	0.00
275.083	0.00	0.00	0.006	O	|	|	|	|	0.00
275.167	0.00	0.00	0.006	O	|	|	|	|	0.00
275.250	0.00	0.00	0.006	O	|	|	|	|	0.00
275.333	0.00	0.00	0.006	O	|	|	|	|	0.00
275.417	0.00	0.00	0.006	O	|	|	|	|	0.00
275.500	0.00	0.00	0.006	O	|	|	|	|	0.00
275.583	0.00	0.00	0.006	O	|	|	|	|	0.00
275.667	0.00	0.00	0.006	O	|	|	|	|	0.00
275.750	0.00	0.00	0.006	O	|	|	|	|	0.00
275.833	0.00	0.00	0.006	O	|	|	|	|	0.00
275.917	0.00	0.00	0.006	O	|	|	|	|	0.00
276.000	0.00	0.00	0.006	O	|	|	|	|	0.00
276.083	0.00	0.00	0.006	O	|	|	|	|	0.00
276.167	0.00	0.00	0.006	O	|	|	|	|	0.00
276.250	0.00	0.00	0.006	O	|	|	|	|	0.00
276.333	0.00	0.00	0.006	O	|	|	|	|	0.00
276.417	0.00	0.00	0.006	O	|	|	|	|	0.00
276.500	0.00	0.00	0.006	O	|	|	|	|	0.00
276.583	0.00	0.00	0.006	O	|	|	|	|	0.00
276.667	0.00	0.00	0.006	O	|	|	|	|	0.00
276.750	0.00	0.00	0.006	O	|	|	|	|	0.00
276.833	0.00	0.00	0.006	O	|	|	|	|	0.00
276.917	0.00	0.00	0.006	O	|	|	|	|	0.00
277.000	0.00	0.00	0.006	O	|	|	|	|	0.00
277.083	0.00	0.00	0.006	O	|	|	|	|	0.00
277.167	0.00	0.00	0.006	O	|	|	|	|	0.00
277.250	0.00	0.00	0.006	O	|	|	|	|	0.00
277.333	0.00	0.00	0.006	O	|	|	|	|	0.00
277.417	0.00	0.00	0.006	O	|	|	|	|	0.00
277.500	0.00	0.00	0.006	O	|	|	|	|	0.00
277.583	0.00	0.00	0.006	O	|	|	|	|	0.00
277.667	0.00	0.00	0.006	O	|	|	|	|	0.00
277.750	0.00	0.00	0.006	O	|	|	|	|	0.00
277.833	0.00	0.00	0.006	O	|	|	|	|	0.00
277.917	0.00	0.00	0.006	O	|	|	|	|	0.00
278.000	0.00	0.00	0.006	O	|	|	|	|	0.00
278.083	0.00	0.00	0.006	O	|	|	|	|	0.00
278.167	0.00	0.00	0.006	O	|	|	|	|	0.00
278.250	0.00	0.00	0.006	O	|	|	|	|	0.00

278.333	0.00	0.00	0.005	O	|	|	|	|	0.00
278.417	0.00	0.00	0.005	O	|	|	|	|	0.00
278.500	0.00	0.00	0.005	O	|	|	|	|	0.00
278.583	0.00	0.00	0.005	O	|	|	|	|	0.00
278.667	0.00	0.00	0.005	O	|	|	|	|	0.00
278.750	0.00	0.00	0.005	O	|	|	|	|	0.00
278.833	0.00	0.00	0.005	O	|	|	|	|	0.00
278.917	0.00	0.00	0.005	O	|	|	|	|	0.00
279.000	0.00	0.00	0.005	O	|	|	|	|	0.00
279.083	0.00	0.00	0.005	O	|	|	|	|	0.00
279.167	0.00	0.00	0.005	O	|	|	|	|	0.00
279.250	0.00	0.00	0.005	O	|	|	|	|	0.00
279.333	0.00	0.00	0.005	O	|	|	|	|	0.00
279.417	0.00	0.00	0.005	O	|	|	|	|	0.00
279.500	0.00	0.00	0.005	O	|	|	|	|	0.00
279.583	0.00	0.00	0.005	O	|	|	|	|	0.00
279.667	0.00	0.00	0.005	O	|	|	|	|	0.00
279.750	0.00	0.00	0.005	O	|	|	|	|	0.00
279.833	0.00	0.00	0.005	O	|	|	|	|	0.00
279.917	0.00	0.00	0.005	O	|	|	|	|	0.00
280.000	0.00	0.00	0.005	O	|	|	|	|	0.00
280.083	0.00	0.00	0.005	O	|	|	|	|	0.00
280.167	0.00	0.00	0.005	O	|	|	|	|	0.00
280.250	0.00	0.00	0.005	O	|	|	|	|	0.00
280.333	0.00	0.00	0.005	O	|	|	|	|	0.00
280.417	0.00	0.00	0.005	O	|	|	|	|	0.00
280.500	0.00	0.00	0.005	O	|	|	|	|	0.00
280.583	0.00	0.00	0.005	O	|	|	|	|	0.00
280.667	0.00	0.00	0.005	O	|	|	|	|	0.00
280.750	0.00	0.00	0.005	O	|	|	|	|	0.00
280.833	0.00	0.00	0.005	O	|	|	|	|	0.00
280.917	0.00	0.00	0.005	O	|	|	|	|	0.00
281.000	0.00	0.00	0.005	O	|	|	|	|	0.00
281.083	0.00	0.00	0.005	O	|	|	|	|	0.00
281.167	0.00	0.00	0.005	O	|	|	|	|	0.00
281.250	0.00	0.00	0.005	O	|	|	|	|	0.00
281.333	0.00	0.00	0.005	O	|	|	|	|	0.00
281.417	0.00	0.00	0.005	O	|	|	|	|	0.00
281.500	0.00	0.00	0.005	O	|	|	|	|	0.00
281.583	0.00	0.00	0.005	O	|	|	|	|	0.00
281.667	0.00	0.00	0.005	O	|	|	|	|	0.00
281.750	0.00	0.00	0.005	O	|	|	|	|	0.00
281.833	0.00	0.00	0.005	O	|	|	|	|	0.00
281.917	0.00	0.00	0.005	O	|	|	|	|	0.00
282.000	0.00	0.00	0.005	O	|	|	|	|	0.00
282.083	0.00	0.00	0.005	O	|	|	|	|	0.00
282.167	0.00	0.00	0.005	O	|	|	|	|	0.00
282.250	0.00	0.00	0.005	O	|	|	|	|	0.00
282.333	0.00	0.00	0.005	O	|	|	|	|	0.00
282.417	0.00	0.00	0.005	O	|	|	|	|	0.00
282.500	0.00	0.00	0.005	O	|	|	|	|	0.00
282.583	0.00	0.00	0.005	O	|	|	|	|	0.00
282.667	0.00	0.00	0.005	O	|	|	|	|	0.00
282.750	0.00	0.00	0.005	O	|	|	|	|	0.00
282.833	0.00	0.00	0.005	O	|	|	|	|	0.00
282.917	0.00	0.00	0.005	O	|	|	|	|	0.00
283.000	0.00	0.00	0.005	O	|	|	|	|	0.00
283.083	0.00	0.00	0.005	O	|	|	|	|	0.00
283.167	0.00	0.00	0.005	O	|	|	|	|	0.00
283.250	0.00	0.00	0.005	O	|	|	|	|	0.00
283.333	0.00	0.00	0.005	O	|	|	|	|	0.00
283.417	0.00	0.00	0.005	O	|	|	|	|	0.00
283.500	0.00	0.00	0.005	O	|	|	|	|	0.00
283.583	0.00	0.00	0.005	O	|	|	|	|	0.00
283.667	0.00	0.00	0.005	O	|	|	|	|	0.00
283.750	0.00	0.00	0.005	O	|	|	|	|	0.00
283.833	0.00	0.00	0.005	O	|	|	|	|	0.00
283.917	0.00	0.00	0.005	O	|	|	|	|	0.00
284.000	0.00	0.00	0.005	O	|	|	|	|	0.00
284.083	0.00	0.00	0.005	O	|	|	|	|	0.00
284.167	0.00	0.00	0.005	O	|	|	|	|	0.00

284.250	0.00	0.00	0.005	O	|	|	|	|	0.00
284.333	0.00	0.00	0.005	O	|	|	|	|	0.00
284.417	0.00	0.00	0.005	O	|	|	|	|	0.00
284.500	0.00	0.00	0.005	O	|	|	|	|	0.00
284.583	0.00	0.00	0.005	O	|	|	|	|	0.00
284.667	0.00	0.00	0.005	O	|	|	|	|	0.00
284.750	0.00	0.00	0.005	O	|	|	|	|	0.00
284.833	0.00	0.00	0.005	O	|	|	|	|	0.00
284.917	0.00	0.00	0.005	O	|	|	|	|	0.00
285.000	0.00	0.00	0.005	O	|	|	|	|	0.00
285.083	0.00	0.00	0.005	O	|	|	|	|	0.00
285.167	0.00	0.00	0.005	O	|	|	|	|	0.00
285.250	0.00	0.00	0.005	O	|	|	|	|	0.00
285.333	0.00	0.00	0.005	O	|	|	|	|	0.00
285.417	0.00	0.00	0.005	O	|	|	|	|	0.00
285.500	0.00	0.00	0.005	O	|	|	|	|	0.00
285.583	0.00	0.00	0.005	O	|	|	|	|	0.00
285.667	0.00	0.00	0.005	O	|	|	|	|	0.00
285.750	0.00	0.00	0.005	O	|	|	|	|	0.00
285.833	0.00	0.00	0.005	O	|	|	|	|	0.00
285.917	0.00	0.00	0.005	O	|	|	|	|	0.00
286.000	0.00	0.00	0.005	O	|	|	|	|	0.00
286.083	0.00	0.00	0.005	O	|	|	|	|	0.00
286.167	0.00	0.00	0.005	O	|	|	|	|	0.00
286.250	0.00	0.00	0.005	O	|	|	|	|	0.00
286.333	0.00	0.00	0.005	O	|	|	|	|	0.00
286.417	0.00	0.00	0.005	O	|	|	|	|	0.00
286.500	0.00	0.00	0.005	O	|	|	|	|	0.00
286.583	0.00	0.00	0.005	O	|	|	|	|	0.00
286.667	0.00	0.00	0.005	O	|	|	|	|	0.00
286.750	0.00	0.00	0.005	O	|	|	|	|	0.00
286.833	0.00	0.00	0.005	O	|	|	|	|	0.00
286.917	0.00	0.00	0.005	O	|	|	|	|	0.00
287.000	0.00	0.00	0.005	O	|	|	|	|	0.00
287.083	0.00	0.00	0.004	O	|	|	|	|	0.00
287.167	0.00	0.00	0.004	O	|	|	|	|	0.00
287.250	0.00	0.00	0.004	O	|	|	|	|	0.00
287.333	0.00	0.00	0.004	O	|	|	|	|	0.00
287.417	0.00	0.00	0.004	O	|	|	|	|	0.00
287.500	0.00	0.00	0.004	O	|	|	|	|	0.00
287.583	0.00	0.00	0.004	O	|	|	|	|	0.00
287.667	0.00	0.00	0.004	O	|	|	|	|	0.00
287.750	0.00	0.00	0.004	O	|	|	|	|	0.00
287.833	0.00	0.00	0.004	O	|	|	|	|	0.00
287.917	0.00	0.00	0.004	O	|	|	|	|	0.00
288.000	0.00	0.00	0.004	O	|	|	|	|	0.00
288.083	0.00	0.00	0.004	O	|	|	|	|	0.00
288.167	0.00	0.00	0.004	O	|	|	|	|	0.00
288.250	0.00	0.00	0.004	O	|	|	|	|	0.00
288.333	0.00	0.00	0.004	O	|	|	|	|	0.00
288.417	0.00	0.00	0.004	O	|	|	|	|	0.00
288.500	0.00	0.00	0.004	O	|	|	|	|	0.00
288.583	0.00	0.00	0.004	O	|	|	|	|	0.00
288.667	0.00	0.00	0.004	O	|	|	|	|	0.00
288.750	0.00	0.00	0.004	O	|	|	|	|	0.00
288.833	0.00	0.00	0.004	O	|	|	|	|	0.00
288.917	0.00	0.00	0.004	O	|	|	|	|	0.00
289.000	0.00	0.00	0.004	O	|	|	|	|	0.00
289.083	0.00	0.00	0.004	O	|	|	|	|	0.00
289.167	0.00	0.00	0.004	O	|	|	|	|	0.00
289.250	0.00	0.00	0.004	O	|	|	|	|	0.00
289.333	0.00	0.00	0.004	O	|	|	|	|	0.00
289.417	0.00	0.00	0.004	O	|	|	|	|	0.00
289.500	0.00	0.00	0.004	O	|	|	|	|	0.00
289.583	0.00	0.00	0.004	O	|	|	|	|	0.00
289.667	0.00	0.00	0.004	O	|	|	|	|	0.00
289.750	0.00	0.00	0.004	O	|	|	|	|	0.00
289.833	0.00	0.00	0.004	O	|	|	|	|	0.00
289.917	0.00	0.00	0.004	O	|	|	|	|	0.00
290.000	0.00	0.00	0.004	O	|	|	|	|	0.00
290.083	0.00	0.00	0.004	O	|	|	|	|	0.00

290.167	0.00	0.00	0.004	O	|	|	|	|	0.00
290.250	0.00	0.00	0.004	O	|	|	|	|	0.00
290.333	0.00	0.00	0.004	O	|	|	|	|	0.00
290.417	0.00	0.00	0.004	O	|	|	|	|	0.00
290.500	0.00	0.00	0.004	O	|	|	|	|	0.00
290.583	0.00	0.00	0.004	O	|	|	|	|	0.00
290.667	0.00	0.00	0.004	O	|	|	|	|	0.00
290.750	0.00	0.00	0.004	O	|	|	|	|	0.00
290.833	0.00	0.00	0.004	O	|	|	|	|	0.00
290.917	0.00	0.00	0.004	O	|	|	|	|	0.00
291.000	0.00	0.00	0.004	O	|	|	|	|	0.00
291.083	0.00	0.00	0.004	O	|	|	|	|	0.00
291.167	0.00	0.00	0.004	O	|	|	|	|	0.00
291.250	0.00	0.00	0.004	O	|	|	|	|	0.00
291.333	0.00	0.00	0.004	O	|	|	|	|	0.00
291.417	0.00	0.00	0.004	O	|	|	|	|	0.00
291.500	0.00	0.00	0.004	O	|	|	|	|	0.00
291.583	0.00	0.00	0.004	O	|	|	|	|	0.00
291.667	0.00	0.00	0.004	O	|	|	|	|	0.00
291.750	0.00	0.00	0.004	O	|	|	|	|	0.00
291.833	0.00	0.00	0.004	O	|	|	|	|	0.00
291.917	0.00	0.00	0.004	O	|	|	|	|	0.00
292.000	0.00	0.00	0.004	O	|	|	|	|	0.00
292.083	0.00	0.00	0.004	O	|	|	|	|	0.00
292.167	0.00	0.00	0.004	O	|	|	|	|	0.00
292.250	0.00	0.00	0.004	O	|	|	|	|	0.00
292.333	0.00	0.00	0.004	O	|	|	|	|	0.00
292.417	0.00	0.00	0.004	O	|	|	|	|	0.00
292.500	0.00	0.00	0.004	O	|	|	|	|	0.00
292.583	0.00	0.00	0.004	O	|	|	|	|	0.00
292.667	0.00	0.00	0.004	O	|	|	|	|	0.00
292.750	0.00	0.00	0.004	O	|	|	|	|	0.00
292.833	0.00	0.00	0.004	O	|	|	|	|	0.00
292.917	0.00	0.00	0.004	O	|	|	|	|	0.00
293.000	0.00	0.00	0.004	O	|	|	|	|	0.00
293.083	0.00	0.00	0.004	O	|	|	|	|	0.00
293.167	0.00	0.00	0.004	O	|	|	|	|	0.00
293.250	0.00	0.00	0.004	O	|	|	|	|	0.00
293.333	0.00	0.00	0.004	O	|	|	|	|	0.00
293.417	0.00	0.00	0.004	O	|	|	|	|	0.00
293.500	0.00	0.00	0.004	O	|	|	|	|	0.00
293.583	0.00	0.00	0.004	O	|	|	|	|	0.00
293.667	0.00	0.00	0.004	O	|	|	|	|	0.00
293.750	0.00	0.00	0.004	O	|	|	|	|	0.00
293.833	0.00	0.00	0.004	O	|	|	|	|	0.00
293.917	0.00	0.00	0.004	O	|	|	|	|	0.00
294.000	0.00	0.00	0.004	O	|	|	|	|	0.00
294.083	0.00	0.00	0.004	O	|	|	|	|	0.00
294.167	0.00	0.00	0.004	O	|	|	|	|	0.00
294.250	0.00	0.00	0.004	O	|	|	|	|	0.00
294.333	0.00	0.00	0.004	O	|	|	|	|	0.00
294.417	0.00	0.00	0.004	O	|	|	|	|	0.00
294.500	0.00	0.00	0.004	O	|	|	|	|	0.00
294.583	0.00	0.00	0.004	O	|	|	|	|	0.00
294.667	0.00	0.00	0.004	O	|	|	|	|	0.00
294.750	0.00	0.00	0.004	O	|	|	|	|	0.00
294.833	0.00	0.00	0.004	O	|	|	|	|	0.00
294.917	0.00	0.00	0.004	O	|	|	|	|	0.00
295.000	0.00	0.00	0.004	O	|	|	|	|	0.00
295.083	0.00	0.00	0.004	O	|	|	|	|	0.00
295.167	0.00	0.00	0.004	O	|	|	|	|	0.00
295.250	0.00	0.00	0.004	O	|	|	|	|	0.00
295.333	0.00	0.00	0.004	O	|	|	|	|	0.00
295.417	0.00	0.00	0.004	O	|	|	|	|	0.00
295.500	0.00	0.00	0.004	O	|	|	|	|	0.00
295.583	0.00	0.00	0.004	O	|	|	|	|	0.00
295.667	0.00	0.00	0.004	O	|	|	|	|	0.00
295.750	0.00	0.00	0.004	O	|	|	|	|	0.00
295.833	0.00	0.00	0.004	O	|	|	|	|	0.00
295.917	0.00	0.00	0.004	O	|	|	|	|	0.00
296.000	0.00	0.00	0.004	O	|	|	|	|	0.00

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296.083    0.00    0.00      0.004  O       |       |       |       |     0.00
296.167    0.00    0.00      0.004  O       |       |       |       |     0.00
296.250    0.00    0.00      0.004  O       |       |       |       |     0.00
296.333    0.00    0.00      0.004  O       |       |       |       |     0.00
296.417    0.00    0.00      0.004  O       |       |       |       |     0.00
296.500    0.00    0.00      0.004  O       |       |       |       |     0.00
296.583    0.00    0.00      0.004  O       |       |       |       |     0.00
296.667    0.00    0.00      0.004  O       |       |       |       |     0.00
296.750    0.00    0.00      0.004  O       |       |       |       |     0.00
296.833    0.00    0.00      0.004  O       |       |       |       |     0.00
296.917    0.00    0.00      0.004  O       |       |       |       |     0.00

        Remaining water in basin =    0.00 (Ac.Ft)


        ****************************HYDROGRAPH DATA****************************
                      Number of intervals =  3563
                      Time interval =    5.0 (Min.)
                      Maximum/Peak flow rate =        0.266 (CFS)
                      Total volume =       1.821 (Ac.Ft)
               Status of hydrographs being held in storage
                           Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
               Peak (CFS)      0.000     0.000     0.000     0.000     0.000
               Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
        ***********************************************************************

        -----------------------------------------------------------------
```

APPENDIX G.4: ONSITE BASIN ROUTING CALCULATIONS – 10-YEAR, 24-HOUR STORM DURATION

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014
Study date: 10/28/21

HEMET 30 ONSITE BASIN A ROUTING
10-YEAR, 24-HOUR ROUTING ANALYSIS
FILENAME: BASINA2410

Program License Serial Number 6279

********** HYDROGRAPH INFORMATION **********

From study/file name: ARA1POST2410.rte
**********HYDROGRAPH DATA**********
Number of intervals = 291
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 4.474 (CFS)
Total volume = 2.211 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****
_____

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 291
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.500	0.616	0.172	0.615	0.617
1.500	1.965	0.312	1.964	1.966
2.500	3.433	15.406	3.380	3.486
3.500	5.020	37.934	4.889	5.151

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 1.1 2.24 3.36 4.47	Depth (Ft.)
0.083	0.14	0.00	0.000	O | | | |	0.00
0.167	0.25	0.00	0.002	OI | | | |	0.00

0.250	0.28	0.00	0.004	OI	|	|	|	0.00
0.333	0.35	0.00	0.006	O I	|	|	|	0.00
0.417	0.41	0.00	0.008	O I	|	|	|	0.01
0.500	0.42	0.00	0.011	O I	|	|	|	0.01
0.583	0.43	0.00	0.014	O I	|	|	|	0.01
0.667	0.43	0.00	0.017	O I	|	|	|	0.01
0.750	0.43	0.01	0.020	O I	|	|	|	0.02
0.833	0.50	0.01	0.023	O I	|	|	|	0.02
0.917	0.56	0.01	0.027	O I	|	|	|	0.02
1.000	0.57	0.01	0.031	O I	|	|	|	0.02
1.083	0.50	0.01	0.034	O I	|	|	|	0.03
1.167	0.44	0.01	0.037	O I	|	|	|	0.03
1.250	0.43	0.01	0.040	O I	|	|	|	0.03
1.333	0.43	0.01	0.043	O I	|	|	|	0.04
1.417	0.43	0.01	0.046	O I	|	|	|	0.04
1.500	0.43	0.01	0.049	O I	|	|	|	0.04
1.583	0.43	0.01	0.052	O I	|	|	|	0.04
1.667	0.43	0.02	0.055	O I	|	|	|	0.04
1.750	0.43	0.02	0.057	O I	|	|	|	0.05
1.833	0.50	0.02	0.061	O I	|	|	|	0.05
1.917	0.56	0.02	0.064	O I	|	|	|	0.05
2.000	0.57	0.02	0.068	O I	|	|	|	0.06
2.083	0.57	0.02	0.072	O I	|	|	|	0.06
2.167	0.57	0.02	0.075	O I	|	|	|	0.06
2.250	0.57	0.02	0.079	O I	|	|	|	0.06
2.333	0.57	0.02	0.083	O I	|	|	|	0.07
2.417	0.57	0.02	0.087	O I	|	|	|	0.07
2.500	0.57	0.03	0.090	O I	|	|	|	0.07
2.583	0.64	0.03	0.094	O I	|	|	|	0.08
2.667	0.70	0.03	0.099	O I	|	|	|	0.08
2.750	0.71	0.03	0.104	O I	|	|	|	0.08
2.833	0.71	0.03	0.108	O I	|	|	|	0.09
2.917	0.71	0.03	0.113	O I	|	|	|	0.09
3.000	0.71	0.03	0.118	O I	|	|	|	0.10
3.083	0.71	0.03	0.122	O I	|	|	|	0.10
3.167	0.71	0.04	0.127	O I	|	|	|	0.10
3.250	0.71	0.04	0.132	O I	|	|	|	0.11
3.333	0.71	0.04	0.136	O I	|	|	|	0.11
3.417	0.71	0.04	0.141	O I	|	|	|	0.11
3.500	0.71	0.04	0.146	O I	|	|	|	0.12
3.583	0.71	0.04	0.150	O I	|	|	|	0.12
3.667	0.71	0.04	0.155	O I	|	|	|	0.13
3.750	0.71	0.04	0.159	O I	|	|	|	0.13
3.833	0.78	0.05	0.164	O I	|	|	|	0.13
3.917	0.84	0.05	0.170	O I	|	|	|	0.14
4.000	0.85	0.05	0.175	O I	|	|	|	0.14
4.083	0.86	0.05	0.181	O I	|	|	|	0.15
4.167	0.86	0.05	0.186	O I	|	|	|	0.15
4.250	0.86	0.05	0.192	O I	|	|	|	0.16
4.333	0.92	0.06	0.197	O I	|	|	|	0.16
4.417	0.98	0.06	0.204	O I	|	|	|	0.17
4.500	1.00	0.06	0.210	O I	|	|	|	0.17
4.583	1.00	0.06	0.217	O I	|	|	|	0.18
4.667	1.00	0.06	0.223	O I	|	|	|	0.18
4.750	1.00	0.06	0.229	O I	|	|	|	0.19
4.833	1.07	0.07	0.236	O I	|	|	|	0.19
4.917	1.13	0.07	0.243	O I	|	|	|	0.20
5.000	1.14	0.07	0.251	O I	|	|	|	0.20
5.083	1.01	0.07	0.257	O I	|	|	|	0.21
5.167	0.89	0.07	0.263	O I	|	|	|	0.21
5.250	0.87	0.08	0.269	O I	|	|	|	0.22
5.333	0.92	0.08	0.275	O I	|	|	|	0.22
5.417	0.98	0.08	0.281	O I	|	|	|	0.23
5.500	1.00	0.08	0.287	O I	|	|	|	0.23
5.583	1.07	0.08	0.294	O I	|	|	|	0.24
5.667	1.13	0.08	0.301	O I	|	|	|	0.24
5.750	1.14	0.09	0.308	O I	|	|	|	0.25
5.833	1.14	0.09	0.315	O I	|	|	|	0.26
5.917	1.14	0.09	0.322	O I	|	|	|	0.26
6.000	1.14	0.09	0.329	O I	|	|	|	0.27
6.083	1.21	0.09	0.337	O I	|	|	|	0.27

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 6.167    1.27    0.10      0.345  O       |I      |       |       |      0.28
 6.250    1.28    0.10      0.353  O       |I      |       |       |      0.29
 6.333    1.29    0.10      0.361  O       |I      |       |       |      0.29
 6.417    1.29    0.10      0.369  O       |I      |       |       |      0.30
 6.500    1.29    0.11      0.377  O       |I      |       |       |      0.31
 6.583    1.35    0.11      0.386  O       |I      |       |       |      0.31
 6.667    1.41    0.11      0.394  O       | I     |       |       |      0.32
 6.750    1.42    0.11      0.403  O       | I     |       |       |      0.33
 6.833    1.43    0.12      0.413  O       | I     |       |       |      0.33
 6.917    1.43    0.12      0.422  O       | I     |       |       |      0.34
 7.000    1.43    0.12      0.431  O       | I     |       |       |      0.35
 7.083    1.43    0.12      0.440  O       | I     |       |       |      0.36
 7.167    1.43    0.13      0.449  O       | I     |       |       |      0.36
 7.250    1.43    0.13      0.458  O       | I     |       |       |      0.37
 7.333    1.50    0.13      0.467  O       | I     |       |       |      0.38
 7.417    1.56    0.13      0.476  O       |  I    |       |       |      0.39
 7.500    1.57    0.14      0.486  O       |  I    |       |       |      0.39
 7.583    1.64    0.14      0.496  O       |  I    |       |       |      0.40
 7.667    1.70    0.14      0.507  |O      |   I   |       |       |      0.41
 7.750    1.71    0.14      0.518  |O      |   I   |       |       |      0.42
 7.833    1.78    0.15      0.529  |O      |   I   |       |       |      0.43
 7.917    1.84    0.15      0.540  |O      |    I  |       |       |      0.44
 8.000    1.85    0.15      0.552  |O      |    I  |       |       |      0.45
 8.083    1.99    0.16      0.564  |O      |     I |       |       |      0.46
 8.167    2.11    0.16      0.577  |O      |      I|       |       |      0.47
 8.250    2.13    0.16      0.590  |O      |      I|       |       |      0.48
 8.333    2.14    0.17      0.604  |O      |      I|       |       |      0.49
 8.417    2.14    0.17      0.617  |O      |      I|       |       |      0.50
 8.500    2.14    0.17      0.631  |O      |      I|       |       |      0.51
 8.583    2.21    0.17      0.645  |O      |      I|       |       |      0.52
 8.667    2.27    0.18      0.659  |O      |       I       |       |      0.53
 8.750    2.28    0.18      0.674  |O      |       I       |       |      0.54
 8.833    2.35    0.18      0.688  |O      |       I       |       |      0.55
 8.917    2.41    0.18      0.703  |O      |       |I      |       |      0.56
 9.000    2.42    0.18      0.719  |O      |       |I      |       |      0.58
 9.083    2.56    0.18      0.735  |O      |       | I     |       |      0.59
 9.167    2.68    0.19      0.752  |O      |       |  I    |       |      0.60
 9.250    2.70    0.19      0.769  |O      |       |  I    |       |      0.61
 9.333    2.78    0.19      0.786  |O      |       |  I    |       |      0.63
 9.417    2.84    0.19      0.804  |O      |       |   I   |       |      0.64
 9.500    2.85    0.19      0.823  |O      |       |   I   |       |      0.65
 9.583    1.54    0.19      0.836  |O      |  I    |       |       |      0.66
 9.667    0.40    0.20      0.842  |OI     |       |       |       |      0.67
 9.750    0.20    0.20      0.843  |O      |       |       |       |      0.67
 9.833    0.26    0.20      0.843  |O      |       |       |       |      0.67
 9.917    0.39    0.20      0.844  |OI     |       |       |       |      0.67
10.000    0.44    0.20      0.845  |O I    |       |       |       |      0.67
10.083    1.25    0.20      0.850  |O     I|       |       |       |      0.67
10.167    1.96    0.20      0.859  |O      |     I |       |       |      0.68
10.250    2.09    0.20      0.872  |O      |     I |       |       |      0.69
10.333    2.14    0.20      0.885  |O      |      I|       |       |      0.70
10.417    2.14    0.20      0.898  |O      |      I|       |       |      0.71
10.500    2.14    0.20      0.912  |O      |      I|       |       |      0.72
10.583    1.19    0.20      0.922  |O     I|       |       |       |      0.73
10.667    0.36    0.20      0.926  |OI     |       |       |       |      0.73
10.750    0.22    0.20      0.926  |O      |       |       |       |      0.73
10.833    0.18    0.20      0.926  |O      |       |       |       |      0.73
10.917    0.20    0.20      0.926  |O      |       |       |       |      0.73
11.000    0.23    0.20      0.926  |O      |       |       |       |      0.73
11.083    0.13    0.20      0.926  IO      |       |       |       |      0.73
11.167    0.05    0.20      0.925  IO      |       |       |       |      0.73
11.250    0.05    0.20      0.924  IO      |       |       |       |      0.73
11.333    0.07    0.20      0.923  IO      |       |       |       |      0.73
11.417    0.09    0.20      0.923  IO      |       |       |       |      0.73
11.500    0.12    0.20      0.922  IO      |       |       |       |      0.73
11.583    1.22    0.20      0.925  |O     I|       |       |       |      0.73
11.667    2.18    0.21      0.935  |O      |      I|       |       |      0.74
11.750    2.36    0.21      0.950  |O      |       I       |       |      0.75
11.833    2.50    0.21      0.965  |O      |       |I      |       |      0.76
11.917    2.56    0.21      0.981  |O      |       | I     |       |      0.77
12.000    1.36    0.21      0.993  |O      |I      |       |       |      0.78
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12.083    1.15    0.21      1.000  |O      I       |        |        |      0.78
12.167    1.71    0.21      1.008  |O      |   I   |        |        |      0.79
12.250    1.80    0.21      1.019  |O      |   I   |        |        |      0.80
12.333    2.00    0.22      1.031  |O      |     I |        |        |      0.81
12.417    2.12    0.22      1.043  |O      |      I|        |        |      0.82
12.500    2.17    0.22      1.057  |O      |      I|        |        |      0.83
12.583    2.44    0.22      1.071  |O      |       |I       |        |      0.84
12.667    2.67    0.22      1.087  |O      |       |  I     |        |      0.85
12.750    2.73    0.22      1.104  |O      |       |  I     |        |      0.86
12.833    2.89    0.22      1.122  |O      |       |   I    |        |      0.88
12.917    3.02    0.23      1.141  |O      |       |    I   |        |      0.89
13.000    3.06    0.23      1.160  |O      |       |    I   |        |      0.90
13.083    3.70    0.23      1.182  |O      |       |        | I      |      0.92
13.167    4.25    0.23      1.208  |O      |       |        |     I  |      0.94
13.250    4.37    0.24      1.236  |O      |       |        |      I |      0.96
13.333    4.43    0.24      1.264  |O      |       |        |      I |      0.98
13.417    4.45    0.24      1.293  |O      |       |        |      I |      1.00
13.500    4.47    0.25      1.322  |O      |       |        |       I|      1.02
13.583    3.17    0.25      1.347  |O      |       |    I   |        |      1.04
13.667    2.02    0.25      1.363  |O      |     I |        |        |      1.05
13.750    1.82    0.25      1.375  |O      |    I  |        |        |      1.06
13.833    1.76    0.25      1.385  |O      |   I   |        |        |      1.07
13.917    1.78    0.25      1.396  |O      |   I   |        |        |      1.08
14.000    1.80    0.25      1.406  |O      |   I   |        |        |      1.09
14.083    2.30    0.26      1.419  |O      |       I        |        |      1.09
14.167    2.75    0.26      1.434  |O      |       |  I     |        |      1.11
14.250    2.85    0.26      1.452  |O      |       |   I    |        |      1.12
14.333    2.78    0.26      1.469  |O      |       |  I     |        |      1.13
14.417    2.69    0.26      1.486  |O      |       |  I     |        |      1.15
14.500    2.69    0.26      1.503  |O      |       |  I     |        |      1.16
14.583    2.71    0.27      1.520  |O      |       |  I     |        |      1.17
14.667    2.73    0.27      1.537  |O      |       |  I     |        |      1.18
14.750    2.75    0.27      1.554  |O      |       |  I     |        |      1.20
14.833    2.65    0.27      1.570  |O      |       | I      |        |      1.21
14.917    2.56    0.27      1.586  |O      |       | I      |        |      1.22
15.000    2.56    0.27      1.602  |O      |       | I      |        |      1.23
15.083    2.45    0.28      1.618  |O      |       |I       |        |      1.24
15.167    2.36    0.28      1.632  |O      |       I        |        |      1.25
15.250    2.36    0.28      1.647  |O      |       I        |        |      1.26
15.333    2.25    0.28      1.661  | O     |       I        |        |      1.27
15.417    2.17    0.28      1.674  | O     |      I|        |        |      1.28
15.500    2.17    0.28      1.687  | O     |      I|        |        |      1.29
15.583    1.69    0.28      1.698  | O     |   I   |        |        |      1.30
15.667    1.29    0.29      1.706  | O     |I      |        |        |      1.31
15.750    1.23    0.29      1.713  | O     I       |        |        |      1.31
15.833    1.21    0.29      1.720  | O     I       |        |        |      1.32
15.917    1.23    0.29      1.726  | O     I       |        |        |      1.32
16.000    1.25    0.29      1.733  | O     I       |        |        |      1.33
16.083    0.93    0.29      1.738  | O   I |       |        |        |      1.33
16.167    0.65    0.29      1.742  | O I   |       |        |        |      1.33
16.250    0.59    0.29      1.744  | O I   |       |        |        |      1.34
16.333    0.57    0.29      1.746  | O I   |       |        |        |      1.34
16.417    0.57    0.29      1.748  | O I   |       |        |        |      1.34
16.500    0.57    0.29      1.750  | O I   |       |        |        |      1.34
16.583    0.50    0.29      1.751  | OI    |       |        |        |      1.34
16.667    0.44    0.29      1.753  | OI    |       |        |        |      1.34
16.750    0.43    0.29      1.754  | OI    |       |        |        |      1.34
16.833    0.43    0.29      1.755  | OI    |       |        |        |      1.34
16.917    0.43    0.29      1.756  | OI    |       |        |        |      1.34
17.000    0.43    0.29      1.757  | OI    |       |        |        |      1.35
17.083    0.56    0.29      1.758  | O I   |       |        |        |      1.35
17.167    0.68    0.29      1.760  | O I   |       |        |        |      1.35
17.250    0.71    0.29      1.763  | O  I  |       |        |        |      1.35
17.333    0.71    0.29      1.766  | O  I  |       |        |        |      1.35
17.417    0.71    0.29      1.769  | O  I  |       |        |        |      1.35
17.500    0.71    0.29      1.772  | O  I  |       |        |        |      1.36
17.583    0.71    0.29      1.775  | O  I  |       |        |        |      1.36
17.667    0.71    0.29      1.778  | O  I  |       |        |        |      1.36
17.750    0.71    0.29      1.781  | O  I  |       |        |        |      1.36
17.833    0.65    0.29      1.783  | O I   |       |        |        |      1.37
17.917    0.59    0.29      1.785  | O I   |       |        |        |      1.37
```

18.000	0.58	0.29	1.787	O I				1.37
18.083	0.57	0.29	1.789	O I				1.37
18.167	0.57	0.29	1.791	O I				1.37
18.250	0.57	0.29	1.793	O I				1.37
18.333	0.57	0.29	1.795	O I				1.37
18.417	0.57	0.29	1.797	O I				1.38
18.500	0.57	0.29	1.799	O I				1.38
18.583	0.50	0.29	1.801	OI				1.38
18.667	0.44	0.30	1.802	OI				1.38
18.750	0.43	0.30	1.803	OI				1.38
18.833	0.36	0.30	1.803	O				1.38
18.917	0.30	0.30	1.804	O				1.38
19.000	0.29	0.30	1.804	O				1.38
19.083	0.35	0.30	1.804	O				1.38
19.167	0.41	0.30	1.804	O				1.38
19.250	0.42	0.30	1.805	OI				1.38
19.333	0.50	0.30	1.806	OI				1.38
19.417	0.56	0.30	1.808	OI				1.38
19.500	0.57	0.30	1.810	O I				1.39
19.583	0.50	0.30	1.812	OI				1.39
19.667	0.44	0.30	1.813	OI				1.39
19.750	0.43	0.30	1.814	OI				1.39
19.833	0.36	0.30	1.814	O				1.39
19.917	0.30	0.30	1.815	O				1.39
20.000	0.29	0.30	1.815	O				1.39
20.083	0.35	0.30	1.815	O				1.39
20.167	0.41	0.30	1.815	O				1.39
20.250	0.42	0.30	1.816	OI				1.39
20.333	0.43	0.30	1.817	OI				1.39
20.417	0.43	0.30	1.818	OI				1.39
20.500	0.43	0.30	1.819	OI				1.39
20.583	0.43	0.30	1.820	OI				1.39
20.667	0.43	0.30	1.821	OI				1.39
20.750	0.43	0.30	1.822	OI				1.39
20.833	0.36	0.30	1.822	O				1.39
20.917	0.30	0.30	1.823	O				1.39
21.000	0.29	0.30	1.823	O				1.39
21.083	0.35	0.30	1.823	O				1.39
21.167	0.41	0.30	1.823	O				1.39
21.250	0.42	0.30	1.824	OI				1.40
21.333	0.36	0.30	1.825	O				1.40
21.417	0.30	0.30	1.825	O				1.40
21.500	0.29	0.30	1.825	O				1.40
21.583	0.35	0.30	1.825	O				1.40
21.667	0.41	0.30	1.826	O				1.40
21.750	0.42	0.30	1.827	OI				1.40
21.833	0.36	0.30	1.827	O				1.40
21.917	0.30	0.30	1.828	O				1.40
22.000	0.29	0.30	1.828	O				1.40
22.083	0.35	0.30	1.828	O				1.40
22.167	0.41	0.30	1.828	O				1.40
22.250	0.42	0.30	1.829	OI				1.40
22.333	0.36	0.30	1.830	O				1.40
22.417	0.30	0.30	1.830	O				1.40
22.500	0.29	0.30	1.830	O				1.40
22.583	0.29	0.30	1.830	O				1.40
22.667	0.29	0.30	1.830	O				1.40
22.750	0.29	0.30	1.830	O				1.40
22.833	0.29	0.30	1.830	O				1.40
22.917	0.29	0.30	1.830	O				1.40
23.000	0.29	0.30	1.829	O				1.40
23.083	0.29	0.30	1.829	O				1.40
23.167	0.29	0.30	1.829	O				1.40
23.250	0.29	0.30	1.829	O				1.40
23.333	0.29	0.30	1.829	O				1.40
23.417	0.29	0.30	1.829	O				1.40
23.500	0.29	0.30	1.829	O				1.40
23.583	0.29	0.30	1.829	O				1.40
23.667	0.29	0.30	1.829	O				1.40
23.750	0.29	0.30	1.829	O				1.40
23.833	0.29	0.30	1.829	O				1.40

23.917	0.29	0.30	1.829	| O	|	|	|	|	1.40
24.000	0.29	0.30	1.828	| O	|	|	|	|	1.40
24.083	0.15	0.30	1.828	|IO	|	|	|	|	1.40
24.167	0.03	0.30	1.826	I O	|	|	|	|	1.40
24.250	0.01	0.30	1.825	I O	|	|	|	|	1.40
24.333	0.00	0.30	1.823	I O	|	|	|	|	1.39
24.417	0.00	0.30	1.821	I O	|	|	|	|	1.39
24.500	0.00	0.30	1.818	I O	|	|	|	|	1.39
24.583	0.00	0.30	1.816	I O	|	|	|	|	1.39
24.667	0.00	0.30	1.814	I O	|	|	|	|	1.39
24.750	0.00	0.30	1.812	I O	|	|	|	|	1.39
24.833	0.00	0.30	1.810	I O	|	|	|	|	1.39
24.917	0.00	0.30	1.808	I O	|	|	|	|	1.38
25.000	0.00	0.30	1.806	I O	|	|	|	|	1.38
25.083	0.00	0.30	1.804	I O	|	|	|	|	1.38
25.167	0.00	0.30	1.802	I O	|	|	|	|	1.38
25.250	0.00	0.29	1.800	I O	|	|	|	|	1.38
25.333	0.00	0.29	1.798	I O	|	|	|	|	1.38
25.417	0.00	0.29	1.796	I O	|	|	|	|	1.37
25.500	0.00	0.29	1.794	I O	|	|	|	|	1.37
25.583	0.00	0.29	1.792	I O	|	|	|	|	1.37
25.667	0.00	0.29	1.790	I O	|	|	|	|	1.37
25.750	0.00	0.29	1.788	I O	|	|	|	|	1.37
25.833	0.00	0.29	1.786	I O	|	|	|	|	1.37
25.917	0.00	0.29	1.784	I O	|	|	|	|	1.37
26.000	0.00	0.29	1.782	I O	|	|	|	|	1.36
26.083	0.00	0.29	1.780	I O	|	|	|	|	1.36
26.167	0.00	0.29	1.778	I O	|	|	|	|	1.36
26.250	0.00	0.29	1.776	I O	|	|	|	|	1.36
26.333	0.00	0.29	1.774	I O	|	|	|	|	1.36
26.417	0.00	0.29	1.772	I O	|	|	|	|	1.36
26.500	0.00	0.29	1.770	I O	|	|	|	|	1.36
26.583	0.00	0.29	1.768	I O	|	|	|	|	1.35
26.667	0.00	0.29	1.766	I O	|	|	|	|	1.35
26.750	0.00	0.29	1.764	I O	|	|	|	|	1.35
26.833	0.00	0.29	1.762	I O	|	|	|	|	1.35
26.917	0.00	0.29	1.760	I O	|	|	|	|	1.35
27.000	0.00	0.29	1.758	I O	|	|	|	|	1.35
27.083	0.00	0.29	1.756	I O	|	|	|	|	1.34
27.167	0.00	0.29	1.754	I O	|	|	|	|	1.34
27.250	0.00	0.29	1.752	I O	|	|	|	|	1.34
27.333	0.00	0.29	1.750	I O	|	|	|	|	1.34
27.417	0.00	0.29	1.748	I O	|	|	|	|	1.34
27.500	0.00	0.29	1.746	I O	|	|	|	|	1.34
27.583	0.00	0.29	1.744	I O	|	|	|	|	1.34
27.667	0.00	0.29	1.742	I O	|	|	|	|	1.33
27.750	0.00	0.29	1.740	I O	|	|	|	|	1.33
27.833	0.00	0.29	1.738	I O	|	|	|	|	1.33
27.917	0.00	0.29	1.736	I O	|	|	|	|	1.33
28.000	0.00	0.29	1.734	I O	|	|	|	|	1.33
28.083	0.00	0.29	1.732	I O	|	|	|	|	1.33
28.167	0.00	0.29	1.730	I O	|	|	|	|	1.33
28.250	0.00	0.29	1.728	I O	|	|	|	|	1.32
28.333	0.00	0.29	1.726	I O	|	|	|	|	1.32
28.417	0.00	0.29	1.724	I O	|	|	|	|	1.32
28.500	0.00	0.29	1.722	I O	|	|	|	|	1.32
28.583	0.00	0.29	1.720	I O	|	|	|	|	1.32
28.667	0.00	0.29	1.718	I O	|	|	|	|	1.32
28.750	0.00	0.29	1.716	I O	|	|	|	|	1.32
28.833	0.00	0.29	1.714	I O	|	|	|	|	1.31
28.917	0.00	0.29	1.712	I O	|	|	|	|	1.31
29.000	0.00	0.29	1.710	I O	|	|	|	|	1.31
29.083	0.00	0.29	1.708	I O	|	|	|	|	1.31
29.167	0.00	0.29	1.706	I O	|	|	|	|	1.31
29.250	0.00	0.28	1.704	I O	|	|	|	|	1.31
29.333	0.00	0.28	1.702	I O	|	|	|	|	1.31
29.417	0.00	0.28	1.700	I O	|	|	|	|	1.30
29.500	0.00	0.28	1.698	I O	|	|	|	|	1.30
29.583	0.00	0.28	1.696	I O	|	|	|	|	1.30
29.667	0.00	0.28	1.695	I O	|	|	|	|	1.30
29.750	0.00	0.28	1.693	I O	|	|	|	|	1.30

29.833	0.00	0.28	1.691	I O				1.30
29.917	0.00	0.28	1.689	I O				1.30
30.000	0.00	0.28	1.687	I O				1.29
30.083	0.00	0.28	1.685	I O				1.29
30.167	0.00	0.28	1.683	I O				1.29
30.250	0.00	0.28	1.681	I O				1.29
30.333	0.00	0.28	1.679	I O				1.29
30.417	0.00	0.28	1.677	I O				1.29
30.500	0.00	0.28	1.675	I O				1.29
30.583	0.00	0.28	1.673	I O				1.28
30.667	0.00	0.28	1.671	I O				1.28
30.750	0.00	0.28	1.669	I O				1.28
30.833	0.00	0.28	1.667	I O				1.28
30.917	0.00	0.28	1.665	I O				1.28
31.000	0.00	0.28	1.663	I O				1.28
31.083	0.00	0.28	1.661	I O				1.27
31.167	0.00	0.28	1.660	I O				1.27
31.250	0.00	0.28	1.658	I O				1.27
31.333	0.00	0.28	1.656	I O				1.27
31.417	0.00	0.28	1.654	I O				1.27
31.500	0.00	0.28	1.652	IO				1.27
31.583	0.00	0.28	1.650	IO				1.27
31.667	0.00	0.28	1.648	IO				1.26
31.750	0.00	0.28	1.646	IO				1.26
31.833	0.00	0.28	1.644	IO				1.26
31.917	0.00	0.28	1.642	IO				1.26
32.000	0.00	0.28	1.640	IO				1.26
32.083	0.00	0.28	1.638	IO				1.26
32.167	0.00	0.28	1.636	IO				1.26
32.250	0.00	0.28	1.635	IO				1.26
32.333	0.00	0.28	1.633	IO				1.25
32.417	0.00	0.28	1.631	IO				1.25
32.500	0.00	0.28	1.629	IO				1.25
32.583	0.00	0.28	1.627	IO				1.25
32.667	0.00	0.28	1.625	IO				1.25
32.750	0.00	0.28	1.623	IO				1.25
32.833	0.00	0.28	1.621	IO				1.25
32.917	0.00	0.28	1.619	IO				1.24
33.000	0.00	0.28	1.617	IO				1.24
33.083	0.00	0.28	1.615	IO				1.24
33.167	0.00	0.28	1.614	IO				1.24
33.250	0.00	0.28	1.612	IO				1.24
33.333	0.00	0.28	1.610	IO				1.24
33.417	0.00	0.27	1.608	IO				1.24
33.500	0.00	0.27	1.606	IO				1.23
33.583	0.00	0.27	1.604	IO				1.23
33.667	0.00	0.27	1.602	IO				1.23
33.750	0.00	0.27	1.600	IO				1.23
33.833	0.00	0.27	1.598	IO				1.23
33.917	0.00	0.27	1.597	IO				1.23
34.000	0.00	0.27	1.595	IO				1.23
34.083	0.00	0.27	1.593	IO				1.22
34.167	0.00	0.27	1.591	IO				1.22
34.250	0.00	0.27	1.589	IO				1.22
34.333	0.00	0.27	1.587	IO				1.22
34.417	0.00	0.27	1.585	IO				1.22
34.500	0.00	0.27	1.583	IO				1.22
34.583	0.00	0.27	1.582	IO				1.22
34.667	0.00	0.27	1.580	IO				1.21
34.750	0.00	0.27	1.578	IO				1.21
34.833	0.00	0.27	1.576	IO				1.21
34.917	0.00	0.27	1.574	IO				1.21
35.000	0.00	0.27	1.572	IO				1.21
35.083	0.00	0.27	1.570	IO				1.21
35.167	0.00	0.27	1.568	IO				1.21
35.250	0.00	0.27	1.567	IO				1.20
35.333	0.00	0.27	1.565	IO				1.20
35.417	0.00	0.27	1.563	IO				1.20
35.500	0.00	0.27	1.561	IO				1.20
35.583	0.00	0.27	1.559	IO				1.20
35.667	0.00	0.27	1.557	IO				1.20

35.750	0.00	0.27	1.555	IO				1.20
35.833	0.00	0.27	1.554	IO				1.20
35.917	0.00	0.27	1.552	IO				1.19
36.000	0.00	0.27	1.550	IO				1.19
36.083	0.00	0.27	1.548	IO				1.19
36.167	0.00	0.27	1.546	IO				1.19
36.250	0.00	0.27	1.544	IO				1.19
36.333	0.00	0.27	1.542	IO				1.19
36.417	0.00	0.27	1.541	IO				1.19
36.500	0.00	0.27	1.539	IO				1.18
36.583	0.00	0.27	1.537	IO				1.18
36.667	0.00	0.27	1.535	IO				1.18
36.750	0.00	0.27	1.533	IO				1.18
36.833	0.00	0.27	1.531	IO				1.18
36.917	0.00	0.27	1.530	IO				1.18
37.000	0.00	0.27	1.528	IO				1.18
37.083	0.00	0.27	1.526	IO				1.17
37.167	0.00	0.27	1.524	IO				1.17
37.250	0.00	0.27	1.522	IO				1.17
37.333	0.00	0.27	1.520	IO				1.17
37.417	0.00	0.27	1.519	IO				1.17
37.500	0.00	0.27	1.517	IO				1.17
37.583	0.00	0.27	1.515	IO				1.17
37.667	0.00	0.27	1.513	IO				1.16
37.750	0.00	0.26	1.511	IO				1.16
37.833	0.00	0.26	1.509	IO				1.16
37.917	0.00	0.26	1.508	IO				1.16
38.000	0.00	0.26	1.506	IO				1.16
38.083	0.00	0.26	1.504	IO				1.16
38.167	0.00	0.26	1.502	IO				1.16
38.250	0.00	0.26	1.500	IO				1.16
38.333	0.00	0.26	1.499	IO				1.15
38.417	0.00	0.26	1.497	IO				1.15
38.500	0.00	0.26	1.495	IO				1.15
38.583	0.00	0.26	1.493	IO				1.15
38.667	0.00	0.26	1.491	IO				1.15
38.750	0.00	0.26	1.489	IO				1.15
38.833	0.00	0.26	1.488	IO				1.15
38.917	0.00	0.26	1.486	IO				1.14
39.000	0.00	0.26	1.484	IO				1.14
39.083	0.00	0.26	1.482	IO				1.14
39.167	0.00	0.26	1.480	IO				1.14
39.250	0.00	0.26	1.479	IO				1.14
39.333	0.00	0.26	1.477	IO				1.14
39.417	0.00	0.26	1.475	IO				1.14
39.500	0.00	0.26	1.473	IO				1.14
39.583	0.00	0.26	1.471	IO				1.13
39.667	0.00	0.26	1.470	IO				1.13
39.750	0.00	0.26	1.468	IO				1.13
39.833	0.00	0.26	1.466	IO				1.13
39.917	0.00	0.26	1.464	IO				1.13
40.000	0.00	0.26	1.462	IO				1.13
40.083	0.00	0.26	1.461	IO				1.13
40.167	0.00	0.26	1.459	IO				1.12
40.250	0.00	0.26	1.457	IO				1.12
40.333	0.00	0.26	1.455	IO				1.12
40.417	0.00	0.26	1.454	IO				1.12
40.500	0.00	0.26	1.452	IO				1.12
40.583	0.00	0.26	1.450	IO				1.12
40.667	0.00	0.26	1.448	IO				1.12
40.750	0.00	0.26	1.446	IO				1.12
40.833	0.00	0.26	1.445	IO				1.11
40.917	0.00	0.26	1.443	IO				1.11
41.000	0.00	0.26	1.441	IO				1.11
41.083	0.00	0.26	1.439	IO				1.11
41.167	0.00	0.26	1.438	IO				1.11
41.250	0.00	0.26	1.436	IO				1.11
41.333	0.00	0.26	1.434	IO				1.11
41.417	0.00	0.26	1.432	IO				1.11
41.500	0.00	0.26	1.430	IO				1.10
41.583	0.00	0.26	1.429	IO				1.10

41.667	0.00	0.26	1.427	IO				1.10
41.750	0.00	0.26	1.425	IO				1.10
41.833	0.00	0.26	1.423	IO				1.10
41.917	0.00	0.26	1.422	IO				1.10
42.000	0.00	0.26	1.420	IO				1.10
42.083	0.00	0.26	1.418	IO				1.09
42.167	0.00	0.26	1.416	IO				1.09
42.250	0.00	0.25	1.415	IO				1.09
42.333	0.00	0.25	1.413	IO				1.09
42.417	0.00	0.25	1.411	IO				1.09
42.500	0.00	0.25	1.409	IO				1.09
42.583	0.00	0.25	1.408	IO				1.09
42.667	0.00	0.25	1.406	IO				1.09
42.750	0.00	0.25	1.404	IO				1.08
42.833	0.00	0.25	1.402	IO				1.08
42.917	0.00	0.25	1.401	IO				1.08
43.000	0.00	0.25	1.399	IO				1.08
43.083	0.00	0.25	1.397	IO				1.08
43.167	0.00	0.25	1.395	IO				1.08
43.250	0.00	0.25	1.394	IO				1.08
43.333	0.00	0.25	1.392	IO				1.08
43.417	0.00	0.25	1.390	IO				1.07
43.500	0.00	0.25	1.388	IO				1.07
43.583	0.00	0.25	1.387	IO				1.07
43.667	0.00	0.25	1.385	IO				1.07
43.750	0.00	0.25	1.383	IO				1.07
43.833	0.00	0.25	1.381	IO				1.07
43.917	0.00	0.25	1.380	IO				1.07
44.000	0.00	0.25	1.378	IO				1.06
44.083	0.00	0.25	1.376	IO				1.06
44.167	0.00	0.25	1.375	IO				1.06
44.250	0.00	0.25	1.373	IO				1.06
44.333	0.00	0.25	1.371	IO				1.06
44.417	0.00	0.25	1.369	IO				1.06
44.500	0.00	0.25	1.368	IO				1.06
44.583	0.00	0.25	1.366	IO				1.06
44.667	0.00	0.25	1.364	IO				1.05
44.750	0.00	0.25	1.363	IO				1.05
44.833	0.00	0.25	1.361	IO				1.05
44.917	0.00	0.25	1.359	IO				1.05
45.000	0.00	0.25	1.357	IO				1.05
45.083	0.00	0.25	1.356	IO				1.05
45.167	0.00	0.25	1.354	IO				1.05
45.250	0.00	0.25	1.352	IO				1.05
45.333	0.00	0.25	1.351	IO				1.04
45.417	0.00	0.25	1.349	IO				1.04
45.500	0.00	0.25	1.347	IO				1.04
45.583	0.00	0.25	1.345	IO				1.04
45.667	0.00	0.25	1.344	IO				1.04
45.750	0.00	0.25	1.342	IO				1.04
45.833	0.00	0.25	1.340	IO				1.04
45.917	0.00	0.25	1.339	IO				1.04
46.000	0.00	0.25	1.337	IO				1.03
46.083	0.00	0.25	1.335	IO				1.03
46.167	0.00	0.25	1.333	IO				1.03
46.250	0.00	0.25	1.332	IO				1.03
46.333	0.00	0.25	1.330	IO				1.03
46.417	0.00	0.25	1.328	IO				1.03
46.500	0.00	0.25	1.327	IO				1.03
46.583	0.00	0.25	1.325	IO				1.03
46.667	0.00	0.25	1.323	IO				1.02
46.750	0.00	0.25	1.322	IO				1.02
46.833	0.00	0.25	1.320	IO				1.02
46.917	0.00	0.24	1.318	IO				1.02
47.000	0.00	0.24	1.317	IO				1.02
47.083	0.00	0.24	1.315	IO				1.02
47.167	0.00	0.24	1.313	IO				1.02
47.250	0.00	0.24	1.312	IO				1.02
47.333	0.00	0.24	1.310	IO				1.01
47.417	0.00	0.24	1.308	IO				1.01
47.500	0.00	0.24	1.306	IO				1.01

47.583	0.00	0.24	1.305	IO				1.01
47.667	0.00	0.24	1.303	IO				1.01
47.750	0.00	0.24	1.301	IO				1.01
47.833	0.00	0.24	1.300	IO				1.01
47.917	0.00	0.24	1.298	IO				1.01
48.000	0.00	0.24	1.296	IO				1.00
48.083	0.00	0.24	1.295	IO				1.00
48.167	0.00	0.24	1.293	IO				1.00
48.250	0.00	0.24	1.291	IO				1.00
48.333	0.00	0.24	1.290	IO				1.00
48.417	0.00	0.24	1.288	IO				1.00
48.500	0.00	0.24	1.286	IO				1.00
48.583	0.00	0.24	1.285	IO				1.00
48.667	0.00	0.24	1.283	IO				0.99
48.750	0.00	0.24	1.281	IO				0.99
48.833	0.00	0.24	1.280	IO				0.99
48.917	0.00	0.24	1.278	IO				0.99
49.000	0.00	0.24	1.276	IO				0.99
49.083	0.00	0.24	1.275	IO				0.99
49.167	0.00	0.24	1.273	IO				0.99
49.250	0.00	0.24	1.271	IO				0.99
49.333	0.00	0.24	1.270	IO				0.98
49.417	0.00	0.24	1.268	IO				0.98
49.500	0.00	0.24	1.267	IO				0.98
49.583	0.00	0.24	1.265	IO				0.98
49.667	0.00	0.24	1.263	IO				0.98
49.750	0.00	0.24	1.262	IO				0.98
49.833	0.00	0.24	1.260	IO				0.98
49.917	0.00	0.24	1.258	IO				0.98
50.000	0.00	0.24	1.257	IO				0.97
50.083	0.00	0.24	1.255	IO				0.97
50.167	0.00	0.24	1.253	IO				0.97
50.250	0.00	0.24	1.252	IO				0.97
50.333	0.00	0.24	1.250	IO				0.97
50.417	0.00	0.24	1.248	IO				0.97
50.500	0.00	0.24	1.247	IO				0.97
50.583	0.00	0.24	1.245	IO				0.97
50.667	0.00	0.24	1.244	IO				0.97
50.750	0.00	0.24	1.242	IO				0.96
50.833	0.00	0.24	1.240	IO				0.96
50.917	0.00	0.24	1.239	IO				0.96
51.000	0.00	0.24	1.237	IO				0.96
51.083	0.00	0.24	1.235	IO				0.96
51.167	0.00	0.24	1.234	IO				0.96
51.250	0.00	0.24	1.232	IO				0.96
51.333	0.00	0.24	1.231	IO				0.96
51.417	0.00	0.24	1.229	IO				0.95
51.500	0.00	0.24	1.227	IO				0.95
51.583	0.00	0.24	1.226	IO				0.95
51.667	0.00	0.24	1.224	IO				0.95
51.750	0.00	0.23	1.222	IO				0.95
51.833	0.00	0.23	1.221	IO				0.95
51.917	0.00	0.23	1.219	IO				0.95
52.000	0.00	0.23	1.218	IO				0.95
52.083	0.00	0.23	1.216	IO				0.94
52.167	0.00	0.23	1.214	IO				0.94
52.250	0.00	0.23	1.213	IO				0.94
52.333	0.00	0.23	1.211	IO				0.94
52.417	0.00	0.23	1.210	IO				0.94
52.500	0.00	0.23	1.208	IO				0.94
52.583	0.00	0.23	1.206	IO				0.94
52.667	0.00	0.23	1.205	IO				0.94
52.750	0.00	0.23	1.203	IO				0.94
52.833	0.00	0.23	1.201	IO				0.93
52.917	0.00	0.23	1.200	IO				0.93
53.000	0.00	0.23	1.198	IO				0.93
53.083	0.00	0.23	1.197	IO				0.93
53.167	0.00	0.23	1.195	IO				0.93
53.250	0.00	0.23	1.193	IO				0.93
53.333	0.00	0.23	1.192	IO				0.93
53.417	0.00	0.23	1.190	IO				0.93

53.500	0.00	0.23	1.189	IO				0.92
53.583	0.00	0.23	1.187	IO				0.92
53.667	0.00	0.23	1.186	IO				0.92
53.750	0.00	0.23	1.184	IO				0.92
53.833	0.00	0.23	1.182	IO				0.92
53.917	0.00	0.23	1.181	IO				0.92
54.000	0.00	0.23	1.179	IO				0.92
54.083	0.00	0.23	1.178	IO				0.92
54.167	0.00	0.23	1.176	IO				0.92
54.250	0.00	0.23	1.174	IO				0.91
54.333	0.00	0.23	1.173	IO				0.91
54.417	0.00	0.23	1.171	IO				0.91
54.500	0.00	0.23	1.170	IO				0.91
54.583	0.00	0.23	1.168	IO				0.91
54.667	0.00	0.23	1.167	IO				0.91
54.750	0.00	0.23	1.165	IO				0.91
54.833	0.00	0.23	1.163	IO				0.91
54.917	0.00	0.23	1.162	IO				0.90
55.000	0.00	0.23	1.160	IO				0.90
55.083	0.00	0.23	1.159	IO				0.90
55.167	0.00	0.23	1.157	IO				0.90
55.250	0.00	0.23	1.155	IO				0.90
55.333	0.00	0.23	1.154	IO				0.90
55.417	0.00	0.23	1.152	IO				0.90
55.500	0.00	0.23	1.151	IO				0.90
55.583	0.00	0.23	1.149	IO				0.90
55.667	0.00	0.23	1.148	IO				0.89
55.750	0.00	0.23	1.146	IO				0.89
55.833	0.00	0.23	1.145	IO				0.89
55.917	0.00	0.23	1.143	IO				0.89
56.000	0.00	0.23	1.141	IO				0.89
56.083	0.00	0.23	1.140	IO				0.89
56.167	0.00	0.23	1.138	IO				0.89
56.250	0.00	0.23	1.137	IO				0.89
56.333	0.00	0.23	1.135	IO				0.88
56.417	0.00	0.23	1.134	IO				0.88
56.500	0.00	0.23	1.132	IO				0.88
56.583	0.00	0.23	1.131	IO				0.88
56.667	0.00	0.23	1.129	IO				0.88
56.750	0.00	0.23	1.127	IO				0.88
56.833	0.00	0.22	1.126	IO				0.88
56.917	0.00	0.22	1.124	IO				0.88
57.000	0.00	0.22	1.123	IO				0.88
57.083	0.00	0.22	1.121	IO				0.87
57.167	0.00	0.22	1.120	IO				0.87
57.250	0.00	0.22	1.118	IO				0.87
57.333	0.00	0.22	1.117	IO				0.87
57.417	0.00	0.22	1.115	IO				0.87
57.500	0.00	0.22	1.113	IO				0.87
57.583	0.00	0.22	1.112	IO				0.87
57.667	0.00	0.22	1.110	IO				0.87
57.750	0.00	0.22	1.109	IO				0.87
57.833	0.00	0.22	1.107	IO				0.86
57.917	0.00	0.22	1.106	IO				0.86
58.000	0.00	0.22	1.104	IO				0.86
58.083	0.00	0.22	1.103	IO				0.86
58.167	0.00	0.22	1.101	IO				0.86
58.250	0.00	0.22	1.100	IO				0.86
58.333	0.00	0.22	1.098	IO				0.86
58.417	0.00	0.22	1.097	IO				0.86
58.500	0.00	0.22	1.095	IO				0.86
58.583	0.00	0.22	1.094	IO				0.85
58.667	0.00	0.22	1.092	IO				0.85
58.750	0.00	0.22	1.091	IO				0.85
58.833	0.00	0.22	1.089	IO				0.85
58.917	0.00	0.22	1.087	IO				0.85
59.000	0.00	0.22	1.086	IO				0.85
59.083	0.00	0.22	1.084	IO				0.85
59.167	0.00	0.22	1.083	IO				0.85
59.250	0.00	0.22	1.081	IO				0.84
59.333	0.00	0.22	1.080	IO				0.84

59.417	0.00	0.22	1.078	IO				0.84
59.500	0.00	0.22	1.077	IO				0.84
59.583	0.00	0.22	1.075	IO				0.84
59.667	0.00	0.22	1.074	IO				0.84
59.750	0.00	0.22	1.072	IO				0.84
59.833	0.00	0.22	1.071	IO				0.84
59.917	0.00	0.22	1.069	IO				0.84
60.000	0.00	0.22	1.068	IO				0.83
60.083	0.00	0.22	1.066	IO				0.83
60.167	0.00	0.22	1.065	IO				0.83
60.250	0.00	0.22	1.063	IO				0.83
60.333	0.00	0.22	1.062	IO				0.83
60.417	0.00	0.22	1.060	IO				0.83
60.500	0.00	0.22	1.059	IO				0.83
60.583	0.00	0.22	1.057	IO				0.83
60.667	0.00	0.22	1.056	IO				0.83
60.750	0.00	0.22	1.054	IO				0.82
60.833	0.00	0.22	1.053	IO				0.82
60.917	0.00	0.22	1.051	IO				0.82
61.000	0.00	0.22	1.050	IO				0.82
61.083	0.00	0.22	1.048	IO				0.82
61.167	0.00	0.22	1.047	IO				0.82
61.250	0.00	0.22	1.045	IO				0.82
61.333	0.00	0.22	1.044	IO				0.82
61.417	0.00	0.22	1.042	IO				0.82
61.500	0.00	0.22	1.041	IO				0.81
61.583	0.00	0.22	1.039	IO				0.81
61.667	0.00	0.22	1.038	IO				0.81
61.750	0.00	0.22	1.036	IO				0.81
61.833	0.00	0.22	1.035	IO				0.81
61.917	0.00	0.22	1.033	IO				0.81
62.000	0.00	0.22	1.032	IO				0.81
62.083	0.00	0.22	1.030	IO				0.81
62.167	0.00	0.21	1.029	IO				0.81
62.250	0.00	0.21	1.027	IO				0.81
62.333	0.00	0.21	1.026	IO				0.80
62.417	0.00	0.21	1.025	IO				0.80
62.500	0.00	0.21	1.023	IO				0.80
62.583	0.00	0.21	1.022	IO				0.80
62.667	0.00	0.21	1.020	IO				0.80
62.750	0.00	0.21	1.019	IO				0.80
62.833	0.00	0.21	1.017	IO				0.80
62.917	0.00	0.21	1.016	IO				0.80
63.000	0.00	0.21	1.014	IO				0.80
63.083	0.00	0.21	1.013	IO				0.79
63.167	0.00	0.21	1.011	IO				0.79
63.250	0.00	0.21	1.010	IO				0.79
63.333	0.00	0.21	1.008	IO				0.79
63.417	0.00	0.21	1.007	IO				0.79
63.500	0.00	0.21	1.005	IO				0.79
63.583	0.00	0.21	1.004	IO				0.79
63.667	0.00	0.21	1.002	IO				0.79
63.750	0.00	0.21	1.001	IO				0.79
63.833	0.00	0.21	1.000	IO				0.78
63.917	0.00	0.21	0.998	IO				0.78
64.000	0.00	0.21	0.997	IO				0.78
64.083	0.00	0.21	0.995	IO				0.78
64.167	0.00	0.21	0.994	IO				0.78
64.250	0.00	0.21	0.992	IO				0.78
64.333	0.00	0.21	0.991	IO				0.78
64.417	0.00	0.21	0.989	IO				0.78
64.500	0.00	0.21	0.988	IO				0.78
64.583	0.00	0.21	0.986	IO				0.77
64.667	0.00	0.21	0.985	IO				0.77
64.750	0.00	0.21	0.984	IO				0.77
64.833	0.00	0.21	0.982	IO				0.77
64.917	0.00	0.21	0.981	IO				0.77
65.000	0.00	0.21	0.979	IO				0.77
65.083	0.00	0.21	0.978	IO				0.77
65.167	0.00	0.21	0.976	IO				0.77
65.250	0.00	0.21	0.975	IO				0.77

65.333	0.00	0.21	0.973	IO				0.76
65.417	0.00	0.21	0.972	IO				0.76
65.500	0.00	0.21	0.971	IO				0.76
65.583	0.00	0.21	0.969	IO				0.76
65.667	0.00	0.21	0.968	IO				0.76
65.750	0.00	0.21	0.966	IO				0.76
65.833	0.00	0.21	0.965	IO				0.76
65.917	0.00	0.21	0.963	IO				0.76
66.000	0.00	0.21	0.962	IO				0.76
66.083	0.00	0.21	0.961	IO				0.76
66.167	0.00	0.21	0.959	IO				0.75
66.250	0.00	0.21	0.958	IO				0.75
66.333	0.00	0.21	0.956	IO				0.75
66.417	0.00	0.21	0.955	IO				0.75
66.500	0.00	0.21	0.953	IO				0.75
66.583	0.00	0.21	0.952	IO				0.75
66.667	0.00	0.21	0.951	IO				0.75
66.750	0.00	0.21	0.949	IO				0.75
66.833	0.00	0.21	0.948	IO				0.75
66.917	0.00	0.21	0.946	IO				0.74
67.000	0.00	0.21	0.945	IO				0.74
67.083	0.00	0.21	0.943	IO				0.74
67.167	0.00	0.21	0.942	IO				0.74
67.250	0.00	0.21	0.941	IO				0.74
67.333	0.00	0.21	0.939	IO				0.74
67.417	0.00	0.21	0.938	IO				0.74
67.500	0.00	0.21	0.936	IO				0.74
67.583	0.00	0.21	0.935	IO				0.74
67.667	0.00	0.20	0.934	IO				0.74
67.750	0.00	0.20	0.932	IO				0.73
67.833	0.00	0.20	0.931	IO				0.73
67.917	0.00	0.20	0.929	IO				0.73
68.000	0.00	0.20	0.928	IO				0.73
68.083	0.00	0.20	0.927	IO				0.73
68.167	0.00	0.20	0.925	IO				0.73
68.250	0.00	0.20	0.924	IO				0.73
68.333	0.00	0.20	0.922	IO				0.73
68.417	0.00	0.20	0.921	IO				0.73
68.500	0.00	0.20	0.919	IO				0.72
68.583	0.00	0.20	0.918	IO				0.72
68.667	0.00	0.20	0.917	IO				0.72
68.750	0.00	0.20	0.915	IO				0.72
68.833	0.00	0.20	0.914	IO				0.72
68.917	0.00	0.20	0.912	IO				0.72
69.000	0.00	0.20	0.911	IO				0.72
69.083	0.00	0.20	0.910	IO				0.72
69.167	0.00	0.20	0.908	IO				0.72
69.250	0.00	0.20	0.907	IO				0.72
69.333	0.00	0.20	0.906	IO				0.71
69.417	0.00	0.20	0.904	IO				0.71
69.500	0.00	0.20	0.903	IO				0.71
69.583	0.00	0.20	0.901	IO				0.71
69.667	0.00	0.20	0.900	IO				0.71
69.750	0.00	0.20	0.899	IO				0.71
69.833	0.00	0.20	0.897	IO				0.71
69.917	0.00	0.20	0.896	IO				0.71
70.000	0.00	0.20	0.894	IO				0.71
70.083	0.00	0.20	0.893	IO				0.71
70.167	0.00	0.20	0.892	IO				0.70
70.250	0.00	0.20	0.890	IO				0.70
70.333	0.00	0.20	0.889	IO				0.70
70.417	0.00	0.20	0.888	IO				0.70
70.500	0.00	0.20	0.886	IO				0.70
70.583	0.00	0.20	0.885	IO				0.70
70.667	0.00	0.20	0.883	IO				0.70
70.750	0.00	0.20	0.882	IO				0.70
70.833	0.00	0.20	0.881	IO				0.70
70.917	0.00	0.20	0.879	IO				0.70
71.000	0.00	0.20	0.878	IO				0.69
71.083	0.00	0.20	0.877	IO				0.69
71.167	0.00	0.20	0.875	IO				0.69

71.250	0.00	0.20	0.874	IO				0.69
71.333	0.00	0.20	0.872	IO				0.69
71.417	0.00	0.20	0.871	IO				0.69
71.500	0.00	0.20	0.870	IO				0.69
71.583	0.00	0.20	0.868	IO				0.69
71.667	0.00	0.20	0.867	IO				0.69
71.750	0.00	0.20	0.866	IO				0.69
71.833	0.00	0.20	0.864	IO				0.68
71.917	0.00	0.20	0.863	IO				0.68
72.000	0.00	0.20	0.862	IO				0.68
72.083	0.00	0.20	0.860	IO				0.68
72.167	0.00	0.20	0.859	IO				0.68
72.250	0.00	0.20	0.857	IO				0.68
72.333	0.00	0.20	0.856	IO				0.68
72.417	0.00	0.20	0.855	IO				0.68
72.500	0.00	0.20	0.853	IO				0.68
72.583	0.00	0.20	0.852	IO				0.67
72.667	0.00	0.20	0.851	IO				0.67
72.750	0.00	0.20	0.849	IO				0.67
72.833	0.00	0.20	0.848	IO				0.67
72.917	0.00	0.20	0.847	IO				0.67
73.000	0.00	0.20	0.845	IO				0.67
73.083	0.00	0.20	0.844	IO				0.67
73.167	0.00	0.20	0.843	IO				0.67
73.250	0.00	0.20	0.841	IO				0.67
73.333	0.00	0.20	0.840	IO				0.67
73.417	0.00	0.20	0.839	IO				0.66
73.500	0.00	0.19	0.837	IO				0.66
73.583	0.00	0.19	0.836	IO				0.66
73.667	0.00	0.19	0.834	IO				0.66
73.750	0.00	0.19	0.833	IO				0.66
73.833	0.00	0.19	0.832	IO				0.66
73.917	0.00	0.19	0.830	IO				0.66
74.000	0.00	0.19	0.829	IO				0.66
74.083	0.00	0.19	0.828	IO				0.66
74.167	0.00	0.19	0.826	IO				0.66
74.250	0.00	0.19	0.825	IO				0.66
74.333	0.00	0.19	0.824	IO				0.65
74.417	0.00	0.19	0.822	IO				0.65
74.500	0.00	0.19	0.821	IO				0.65
74.583	0.00	0.19	0.820	IO				0.65
74.667	0.00	0.19	0.818	IO				0.65
74.750	0.00	0.19	0.817	IO				0.65
74.833	0.00	0.19	0.816	IO				0.65
74.917	0.00	0.19	0.814	IO				0.65
75.000	0.00	0.19	0.813	IO				0.65
75.083	0.00	0.19	0.812	IO				0.65
75.167	0.00	0.19	0.811	IO				0.64
75.250	0.00	0.19	0.809	IO				0.64
75.333	0.00	0.19	0.808	IO				0.64
75.417	0.00	0.19	0.807	IO				0.64
75.500	0.00	0.19	0.805	IO				0.64
75.583	0.00	0.19	0.804	IO				0.64
75.667	0.00	0.19	0.803	IO				0.64
75.750	0.00	0.19	0.801	IO				0.64
75.833	0.00	0.19	0.800	IO				0.64
75.917	0.00	0.19	0.799	IO				0.64
76.000	0.00	0.19	0.797	IO				0.63
76.083	0.00	0.19	0.796	IO				0.63
76.167	0.00	0.19	0.795	IO				0.63
76.250	0.00	0.19	0.793	IO				0.63
76.333	0.00	0.19	0.792	IO				0.63
76.417	0.00	0.19	0.791	IO				0.63
76.500	0.00	0.19	0.789	IO				0.63
76.583	0.00	0.19	0.788	IO				0.63
76.667	0.00	0.19	0.787	IO				0.63
76.750	0.00	0.19	0.786	IO				0.63
76.833	0.00	0.19	0.784	IO				0.62
76.917	0.00	0.19	0.783	IO				0.62
77.000	0.00	0.19	0.782	IO				0.62
77.083	0.00	0.19	0.780	IO				0.62

77.167	0.00	0.19	0.779	IO				0.62
77.250	0.00	0.19	0.778	IO				0.62
77.333	0.00	0.19	0.776	IO				0.62
77.417	0.00	0.19	0.775	IO				0.62
77.500	0.00	0.19	0.774	IO				0.62
77.583	0.00	0.19	0.773	IO				0.62
77.667	0.00	0.19	0.771	IO				0.62
77.750	0.00	0.19	0.770	IO				0.61
77.833	0.00	0.19	0.769	IO				0.61
77.917	0.00	0.19	0.767	IO				0.61
78.000	0.00	0.19	0.766	IO				0.61
78.083	0.00	0.19	0.765	IO				0.61
78.167	0.00	0.19	0.763	IO				0.61
78.250	0.00	0.19	0.762	IO				0.61
78.333	0.00	0.19	0.761	IO				0.61
78.417	0.00	0.19	0.760	IO				0.61
78.500	0.00	0.19	0.758	IO				0.61
78.583	0.00	0.19	0.757	IO				0.60
78.667	0.00	0.19	0.756	IO				0.60
78.750	0.00	0.19	0.754	IO				0.60
78.833	0.00	0.19	0.753	IO				0.60
78.917	0.00	0.19	0.752	IO				0.60
79.000	0.00	0.19	0.751	IO				0.60
79.083	0.00	0.19	0.749	IO				0.60
79.167	0.00	0.19	0.748	IO				0.60
79.250	0.00	0.19	0.747	IO				0.60
79.333	0.00	0.19	0.746	IO				0.60
79.417	0.00	0.19	0.744	IO				0.60
79.500	0.00	0.19	0.743	IO				0.59
79.583	0.00	0.19	0.742	IO				0.59
79.667	0.00	0.18	0.740	IO				0.59
79.750	0.00	0.18	0.739	IO				0.59
79.833	0.00	0.18	0.738	IO				0.59
79.917	0.00	0.18	0.737	IO				0.59
80.000	0.00	0.18	0.735	IO				0.59
80.083	0.00	0.18	0.734	IO				0.59
80.167	0.00	0.18	0.733	IO				0.59
80.250	0.00	0.18	0.732	IO				0.59
80.333	0.00	0.18	0.730	IO				0.58
80.417	0.00	0.18	0.729	IO				0.58
80.500	0.00	0.18	0.728	IO				0.58
80.583	0.00	0.18	0.726	IO				0.58
80.667	0.00	0.18	0.725	IO				0.58
80.750	0.00	0.18	0.724	IO				0.58
80.833	0.00	0.18	0.723	IO				0.58
80.917	0.00	0.18	0.721	IO				0.58
81.000	0.00	0.18	0.720	IO				0.58
81.083	0.00	0.18	0.719	IO				0.58
81.167	0.00	0.18	0.718	IO				0.58
81.250	0.00	0.18	0.716	IO				0.57
81.333	0.00	0.18	0.715	IO				0.57
81.417	0.00	0.18	0.714	IO				0.57
81.500	0.00	0.18	0.713	IO				0.57
81.583	0.00	0.18	0.711	IO				0.57
81.667	0.00	0.18	0.710	IO				0.57
81.750	0.00	0.18	0.709	IO				0.57
81.833	0.00	0.18	0.708	IO				0.57
81.917	0.00	0.18	0.706	IO				0.57
82.000	0.00	0.18	0.705	IO				0.57
82.083	0.00	0.18	0.704	IO				0.57
82.167	0.00	0.18	0.703	IO				0.56
82.250	0.00	0.18	0.701	IO				0.56
82.333	0.00	0.18	0.700	IO				0.56
82.417	0.00	0.18	0.699	IO				0.56
82.500	0.00	0.18	0.698	IO				0.56
82.583	0.00	0.18	0.696	IO				0.56
82.667	0.00	0.18	0.695	IO				0.56
82.750	0.00	0.18	0.694	IO				0.56
82.833	0.00	0.18	0.693	IO				0.56
82.917	0.00	0.18	0.691	IO				0.56
83.000	0.00	0.18	0.690	IO				0.55

83.083	0.00	0.18	0.689	IO				0.55
83.167	0.00	0.18	0.688	IO				0.55
83.250	0.00	0.18	0.686	IO				0.55
83.333	0.00	0.18	0.685	IO				0.55
83.417	0.00	0.18	0.684	IO				0.55
83.500	0.00	0.18	0.683	IO				0.55
83.583	0.00	0.18	0.682	IO				0.55
83.667	0.00	0.18	0.680	IO				0.55
83.750	0.00	0.18	0.679	IO				0.55
83.833	0.00	0.18	0.678	IO				0.55
83.917	0.00	0.18	0.677	IO				0.54
84.000	0.00	0.18	0.675	IO				0.54
84.083	0.00	0.18	0.674	IO				0.54
84.167	0.00	0.18	0.673	IO				0.54
84.250	0.00	0.18	0.672	IO				0.54
84.333	0.00	0.18	0.670	IO				0.54
84.417	0.00	0.18	0.669	IO				0.54
84.500	0.00	0.18	0.668	IO				0.54
84.583	0.00	0.18	0.667	IO				0.54
84.667	0.00	0.18	0.666	IO				0.54
84.750	0.00	0.18	0.664	IO				0.54
84.833	0.00	0.18	0.663	IO				0.53
84.917	0.00	0.18	0.662	IO				0.53
85.000	0.00	0.18	0.661	IO				0.53
85.083	0.00	0.18	0.660	IO				0.53
85.167	0.00	0.18	0.658	IO				0.53
85.250	0.00	0.18	0.657	IO				0.53
85.333	0.00	0.18	0.656	IO				0.53
85.417	0.00	0.18	0.655	IO				0.53
85.500	0.00	0.18	0.653	IO				0.53
85.583	0.00	0.18	0.652	IO				0.53
85.667	0.00	0.18	0.651	IO				0.53
85.750	0.00	0.18	0.650	IO				0.53
85.833	0.00	0.18	0.649	IO				0.52
85.917	0.00	0.18	0.647	IO				0.52
86.000	0.00	0.18	0.646	IO				0.52
86.083	0.00	0.18	0.645	IO				0.52
86.167	0.00	0.17	0.644	IO				0.52
86.250	0.00	0.17	0.643	IO				0.52
86.333	0.00	0.17	0.641	IO				0.52
86.417	0.00	0.17	0.640	IO				0.52
86.500	0.00	0.17	0.639	IO				0.52
86.583	0.00	0.17	0.638	IO				0.52
86.667	0.00	0.17	0.637	IO				0.52
86.750	0.00	0.17	0.635	IO				0.51
86.833	0.00	0.17	0.634	IO				0.51
86.917	0.00	0.17	0.633	IO				0.51
87.000	0.00	0.17	0.632	IO				0.51
87.083	0.00	0.17	0.631	IO				0.51
87.167	0.00	0.17	0.629	IO				0.51
87.250	0.00	0.17	0.628	IO				0.51
87.333	0.00	0.17	0.627	IO				0.51
87.417	0.00	0.17	0.626	IO				0.51
87.500	0.00	0.17	0.625	IO				0.51
87.583	0.00	0.17	0.623	IO				0.51
87.667	0.00	0.17	0.622	IO				0.50
87.750	0.00	0.17	0.621	IO				0.50
87.833	0.00	0.17	0.620	IO				0.50
87.917	0.00	0.17	0.619	IO				0.50
88.000	0.00	0.17	0.617	IO				0.50
88.083	0.00	0.17	0.616	IO				0.50
88.167	0.00	0.17	0.615	IO				0.50
88.250	0.00	0.17	0.614	IO				0.50
88.333	0.00	0.17	0.613	IO				0.50
88.417	0.00	0.17	0.612	IO				0.50
88.500	0.00	0.17	0.610	IO				0.50
88.583	0.00	0.17	0.609	IO				0.49
88.667	0.00	0.17	0.608	IO				0.49
88.750	0.00	0.17	0.607	IO				0.49
88.833	0.00	0.17	0.606	IO				0.49
88.917	0.00	0.17	0.605	IO				0.49

89.000	0.00	0.17	0.603	IO				0.49
89.083	0.00	0.17	0.602	IO				0.49
89.167	0.00	0.17	0.601	IO				0.49
89.250	0.00	0.17	0.600	IO				0.49
89.333	0.00	0.17	0.599	IO				0.49
89.417	0.00	0.17	0.598	IO				0.49
89.500	0.00	0.17	0.596	IO				0.48
89.583	0.00	0.17	0.595	IO				0.48
89.667	0.00	0.17	0.594	IO				0.48
89.750	0.00	0.17	0.593	IO				0.48
89.833	0.00	0.17	0.592	IO				0.48
89.917	0.00	0.16	0.591	IO				0.48
90.000	0.00	0.16	0.590	IO				0.48
90.083	0.00	0.16	0.589	IO				0.48
90.167	0.00	0.16	0.587	IO				0.48
90.250	0.00	0.16	0.586	IO				0.48
90.333	0.00	0.16	0.585	IO				0.47
90.417	0.00	0.16	0.584	IO				0.47
90.500	0.00	0.16	0.583	IO				0.47
90.583	0.00	0.16	0.582	IO				0.47
90.667	0.00	0.16	0.581	IO				0.47
90.750	0.00	0.16	0.580	IO				0.47
90.833	0.00	0.16	0.578	IO				0.47
90.917	0.00	0.16	0.577	IO				0.47
91.000	0.00	0.16	0.576	IO				0.47
91.083	0.00	0.16	0.575	IO				0.47
91.167	0.00	0.16	0.574	IO				0.47
91.250	0.00	0.16	0.573	IO				0.47
91.333	0.00	0.16	0.572	IO				0.46
91.417	0.00	0.16	0.571	IO				0.46
91.500	0.00	0.16	0.570	IO				0.46
91.583	0.00	0.16	0.568	IO				0.46
91.667	0.00	0.16	0.567	IO				0.46
91.750	0.00	0.16	0.566	IO				0.46
91.833	0.00	0.16	0.565	IO				0.46
91.917	0.00	0.16	0.564	IO				0.46
92.000	0.00	0.16	0.563	IO				0.46
92.083	0.00	0.16	0.562	IO				0.46
92.167	0.00	0.16	0.561	IO				0.46
92.250	0.00	0.16	0.560	IO				0.45
92.333	0.00	0.16	0.559	IO				0.45
92.417	0.00	0.16	0.558	IO				0.45
92.500	0.00	0.16	0.557	IO				0.45
92.583	0.00	0.16	0.556	IO				0.45
92.667	0.00	0.15	0.554	IO				0.45
92.750	0.00	0.15	0.553	IO				0.45
92.833	0.00	0.15	0.552	IO				0.45
92.917	0.00	0.15	0.551	IO				0.45
93.000	0.00	0.15	0.550	IO				0.45
93.083	0.00	0.15	0.549	IO				0.45
93.167	0.00	0.15	0.548	IO				0.44
93.250	0.00	0.15	0.547	IO				0.44
93.333	0.00	0.15	0.546	IO				0.44
93.417	0.00	0.15	0.545	IO				0.44
93.500	0.00	0.15	0.544	IO				0.44
93.583	0.00	0.15	0.543	IO				0.44
93.667	0.00	0.15	0.542	IO				0.44
93.750	0.00	0.15	0.541	IO				0.44
93.833	0.00	0.15	0.540	IO				0.44
93.917	0.00	0.15	0.539	IO				0.44
94.000	0.00	0.15	0.538	IO				0.44
94.083	0.00	0.15	0.537	IO				0.44
94.167	0.00	0.15	0.536	IO				0.43
94.250	0.00	0.15	0.535	IO				0.43
94.333	0.00	0.15	0.534	IO				0.43
94.417	0.00	0.15	0.533	IO				0.43
94.500	0.00	0.15	0.531	IO				0.43
94.583	0.00	0.15	0.530	IO				0.43
94.667	0.00	0.15	0.529	IO				0.43
94.750	0.00	0.15	0.528	IO				0.43
94.833	0.00	0.15	0.527	IO				0.43

94.917	0.00	0.15	0.526	IO				0.43
95.000	0.00	0.15	0.525	IO				0.43
95.083	0.00	0.15	0.524	IO				0.43
95.167	0.00	0.15	0.523	IO				0.42
95.250	0.00	0.15	0.522	IO				0.42
95.333	0.00	0.15	0.521	IO				0.42
95.417	0.00	0.15	0.520	IO				0.42
95.500	0.00	0.15	0.519	IO				0.42
95.583	0.00	0.14	0.518	IO				0.42
95.667	0.00	0.14	0.517	IO				0.42
95.750	0.00	0.14	0.516	IO				0.42
95.833	0.00	0.14	0.515	IO				0.42
95.917	0.00	0.14	0.514	IO				0.42
96.000	0.00	0.14	0.513	IO				0.42
96.083	0.00	0.14	0.512	IO				0.42
96.167	0.00	0.14	0.511	IO				0.42
96.250	0.00	0.14	0.510	IO				0.41
96.333	0.00	0.14	0.509	IO				0.41
96.417	0.00	0.14	0.508	IO				0.41
96.500	0.00	0.14	0.508	IO				0.41
96.583	0.00	0.14	0.507	IO				0.41
96.667	0.00	0.14	0.506	IO				0.41
96.750	0.00	0.14	0.505	IO				0.41
96.833	0.00	0.14	0.504	IO				0.41
96.917	0.00	0.14	0.503	IO				0.41
97.000	0.00	0.14	0.502	IO				0.41
97.083	0.00	0.14	0.501	O				0.41
97.167	0.00	0.14	0.500	O				0.41
97.250	0.00	0.14	0.499	O				0.40
97.333	0.00	0.14	0.498	O				0.40
97.417	0.00	0.14	0.497	O				0.40
97.500	0.00	0.14	0.496	O				0.40
97.583	0.00	0.14	0.495	O				0.40
97.667	0.00	0.14	0.494	O				0.40
97.750	0.00	0.14	0.493	O				0.40
97.833	0.00	0.14	0.492	O				0.40
97.917	0.00	0.14	0.491	O				0.40
98.000	0.00	0.14	0.490	O				0.40
98.083	0.00	0.14	0.489	O				0.40
98.167	0.00	0.14	0.488	O				0.40
98.250	0.00	0.14	0.487	O				0.40
98.333	0.00	0.14	0.486	O				0.39
98.417	0.00	0.14	0.486	O				0.39
98.500	0.00	0.14	0.485	O				0.39
98.583	0.00	0.14	0.484	O				0.39
98.667	0.00	0.13	0.483	O				0.39
98.750	0.00	0.13	0.482	O				0.39
98.833	0.00	0.13	0.481	O				0.39
98.917	0.00	0.13	0.480	O				0.39
99.000	0.00	0.13	0.479	O				0.39
99.083	0.00	0.13	0.478	O				0.39
99.167	0.00	0.13	0.477	O				0.39
99.250	0.00	0.13	0.476	O				0.39
99.333	0.00	0.13	0.475	O				0.39
99.417	0.00	0.13	0.474	O				0.39
99.500	0.00	0.13	0.474	O				0.38
99.583	0.00	0.13	0.473	O				0.38
99.667	0.00	0.13	0.472	O				0.38
99.750	0.00	0.13	0.471	O				0.38
99.833	0.00	0.13	0.470	O				0.38
99.917	0.00	0.13	0.469	O				0.38
100.000	0.00	0.13	0.468	O				0.38
100.083	0.00	0.13	0.467	O				0.38
100.167	0.00	0.13	0.466	O				0.38
100.250	0.00	0.13	0.465	O				0.38
100.333	0.00	0.13	0.465	O				0.38
100.417	0.00	0.13	0.464	O				0.38
100.500	0.00	0.13	0.463	O				0.38
100.583	0.00	0.13	0.462	O				0.37
100.667	0.00	0.13	0.461	O				0.37
100.750	0.00	0.13	0.460	O				0.37

100.833	0.00	0.13	0.459	O	|	|	|	|	0.37
100.917	0.00	0.13	0.458	O	|	|	|	|	0.37
101.000	0.00	0.13	0.457	O	|	|	|	|	0.37
101.083	0.00	0.13	0.457	O	|	|	|	|	0.37
101.167	0.00	0.13	0.456	O	|	|	|	|	0.37
101.250	0.00	0.13	0.455	O	|	|	|	|	0.37
101.333	0.00	0.13	0.454	O	|	|	|	|	0.37
101.417	0.00	0.13	0.453	O	|	|	|	|	0.37
101.500	0.00	0.13	0.452	O	|	|	|	|	0.37
101.583	0.00	0.13	0.451	O	|	|	|	|	0.37
101.667	0.00	0.13	0.450	O	|	|	|	|	0.37
101.750	0.00	0.13	0.450	O	|	|	|	|	0.36
101.833	0.00	0.13	0.449	O	|	|	|	|	0.36
101.917	0.00	0.13	0.448	O	|	|	|	|	0.36
102.000	0.00	0.12	0.447	O	|	|	|	|	0.36
102.083	0.00	0.12	0.446	O	|	|	|	|	0.36
102.167	0.00	0.12	0.445	O	|	|	|	|	0.36
102.250	0.00	0.12	0.444	O	|	|	|	|	0.36
102.333	0.00	0.12	0.444	O	|	|	|	|	0.36
102.417	0.00	0.12	0.443	O	|	|	|	|	0.36
102.500	0.00	0.12	0.442	O	|	|	|	|	0.36
102.583	0.00	0.12	0.441	O	|	|	|	|	0.36
102.667	0.00	0.12	0.440	O	|	|	|	|	0.36
102.750	0.00	0.12	0.439	O	|	|	|	|	0.36
102.833	0.00	0.12	0.439	O	|	|	|	|	0.36
102.917	0.00	0.12	0.438	O	|	|	|	|	0.36
103.000	0.00	0.12	0.437	O	|	|	|	|	0.35
103.083	0.00	0.12	0.436	O	|	|	|	|	0.35
103.167	0.00	0.12	0.435	O	|	|	|	|	0.35
103.250	0.00	0.12	0.434	O	|	|	|	|	0.35
103.333	0.00	0.12	0.433	O	|	|	|	|	0.35
103.417	0.00	0.12	0.433	O	|	|	|	|	0.35
103.500	0.00	0.12	0.432	O	|	|	|	|	0.35
103.583	0.00	0.12	0.431	O	|	|	|	|	0.35
103.667	0.00	0.12	0.430	O	|	|	|	|	0.35
103.750	0.00	0.12	0.429	O	|	|	|	|	0.35
103.833	0.00	0.12	0.429	O	|	|	|	|	0.35
103.917	0.00	0.12	0.428	O	|	|	|	|	0.35
104.000	0.00	0.12	0.427	O	|	|	|	|	0.35
104.083	0.00	0.12	0.426	O	|	|	|	|	0.35
104.167	0.00	0.12	0.425	O	|	|	|	|	0.35
104.250	0.00	0.12	0.424	O	|	|	|	|	0.34
104.333	0.00	0.12	0.424	O	|	|	|	|	0.34
104.417	0.00	0.12	0.423	O	|	|	|	|	0.34
104.500	0.00	0.12	0.422	O	|	|	|	|	0.34
104.583	0.00	0.12	0.421	O	|	|	|	|	0.34
104.667	0.00	0.12	0.420	O	|	|	|	|	0.34
104.750	0.00	0.12	0.420	O	|	|	|	|	0.34
104.833	0.00	0.12	0.419	O	|	|	|	|	0.34
104.917	0.00	0.12	0.418	O	|	|	|	|	0.34
105.000	0.00	0.12	0.417	O	|	|	|	|	0.34
105.083	0.00	0.12	0.416	O	|	|	|	|	0.34
105.167	0.00	0.12	0.416	O	|	|	|	|	0.34
105.250	0.00	0.12	0.415	O	|	|	|	|	0.34
105.333	0.00	0.12	0.414	O	|	|	|	|	0.34
105.417	0.00	0.12	0.413	O	|	|	|	|	0.34
105.500	0.00	0.12	0.412	O	|	|	|	|	0.33
105.583	0.00	0.11	0.412	O	|	|	|	|	0.33
105.667	0.00	0.11	0.411	O	|	|	|	|	0.33
105.750	0.00	0.11	0.410	O	|	|	|	|	0.33
105.833	0.00	0.11	0.409	O	|	|	|	|	0.33
105.917	0.00	0.11	0.408	O	|	|	|	|	0.33
106.000	0.00	0.11	0.408	O	|	|	|	|	0.33
106.083	0.00	0.11	0.407	O	|	|	|	|	0.33
106.167	0.00	0.11	0.406	O	|	|	|	|	0.33
106.250	0.00	0.11	0.405	O	|	|	|	|	0.33
106.333	0.00	0.11	0.404	O	|	|	|	|	0.33
106.417	0.00	0.11	0.404	O	|	|	|	|	0.33
106.500	0.00	0.11	0.403	O	|	|	|	|	0.33
106.583	0.00	0.11	0.402	O	|	|	|	|	0.33
106.667	0.00	0.11	0.401	O	|	|	|	|	0.33

106.750	0.00	0.11	0.401	O	|	|	|	|	0.33
106.833	0.00	0.11	0.400	O	|	|	|	|	0.32
106.917	0.00	0.11	0.399	O	|	|	|	|	0.32
107.000	0.00	0.11	0.398	O	|	|	|	|	0.32
107.083	0.00	0.11	0.398	O	|	|	|	|	0.32
107.167	0.00	0.11	0.397	O	|	|	|	|	0.32
107.250	0.00	0.11	0.396	O	|	|	|	|	0.32
107.333	0.00	0.11	0.395	O	|	|	|	|	0.32
107.417	0.00	0.11	0.395	O	|	|	|	|	0.32
107.500	0.00	0.11	0.394	O	|	|	|	|	0.32
107.583	0.00	0.11	0.393	O	|	|	|	|	0.32
107.667	0.00	0.11	0.392	O	|	|	|	|	0.32
107.750	0.00	0.11	0.391	O	|	|	|	|	0.32
107.833	0.00	0.11	0.391	O	|	|	|	|	0.32
107.917	0.00	0.11	0.390	O	|	|	|	|	0.32
108.000	0.00	0.11	0.389	O	|	|	|	|	0.32
108.083	0.00	0.11	0.388	O	|	|	|	|	0.32
108.167	0.00	0.11	0.388	O	|	|	|	|	0.31
108.250	0.00	0.11	0.387	O	|	|	|	|	0.31
108.333	0.00	0.11	0.386	O	|	|	|	|	0.31
108.417	0.00	0.11	0.386	O	|	|	|	|	0.31
108.500	0.00	0.11	0.385	O	|	|	|	|	0.31
108.583	0.00	0.11	0.384	O	|	|	|	|	0.31
108.667	0.00	0.11	0.383	O	|	|	|	|	0.31
108.750	0.00	0.11	0.383	O	|	|	|	|	0.31
108.833	0.00	0.11	0.382	O	|	|	|	|	0.31
108.917	0.00	0.11	0.381	O	|	|	|	|	0.31
109.000	0.00	0.11	0.380	O	|	|	|	|	0.31
109.083	0.00	0.11	0.380	O	|	|	|	|	0.31
109.167	0.00	0.11	0.379	O	|	|	|	|	0.31
109.250	0.00	0.11	0.378	O	|	|	|	|	0.31
109.333	0.00	0.11	0.377	O	|	|	|	|	0.31
109.417	0.00	0.11	0.377	O	|	|	|	|	0.31
109.500	0.00	0.10	0.376	O	|	|	|	|	0.31
109.583	0.00	0.10	0.375	O	|	|	|	|	0.30
109.667	0.00	0.10	0.375	O	|	|	|	|	0.30
109.750	0.00	0.10	0.374	O	|	|	|	|	0.30
109.833	0.00	0.10	0.373	O	|	|	|	|	0.30
109.917	0.00	0.10	0.372	O	|	|	|	|	0.30
110.000	0.00	0.10	0.372	O	|	|	|	|	0.30
110.083	0.00	0.10	0.371	O	|	|	|	|	0.30
110.167	0.00	0.10	0.370	O	|	|	|	|	0.30
110.250	0.00	0.10	0.370	O	|	|	|	|	0.30
110.333	0.00	0.10	0.369	O	|	|	|	|	0.30
110.417	0.00	0.10	0.368	O	|	|	|	|	0.30
110.500	0.00	0.10	0.367	O	|	|	|	|	0.30
110.583	0.00	0.10	0.367	O	|	|	|	|	0.30
110.667	0.00	0.10	0.366	O	|	|	|	|	0.30
110.750	0.00	0.10	0.365	O	|	|	|	|	0.30
110.833	0.00	0.10	0.365	O	|	|	|	|	0.30
110.917	0.00	0.10	0.364	O	|	|	|	|	0.30
111.000	0.00	0.10	0.363	O	|	|	|	|	0.29
111.083	0.00	0.10	0.362	O	|	|	|	|	0.29
111.167	0.00	0.10	0.362	O	|	|	|	|	0.29
111.250	0.00	0.10	0.361	O	|	|	|	|	0.29
111.333	0.00	0.10	0.360	O	|	|	|	|	0.29
111.417	0.00	0.10	0.360	O	|	|	|	|	0.29
111.500	0.00	0.10	0.359	O	|	|	|	|	0.29
111.583	0.00	0.10	0.358	O	|	|	|	|	0.29
111.667	0.00	0.10	0.358	O	|	|	|	|	0.29
111.750	0.00	0.10	0.357	O	|	|	|	|	0.29
111.833	0.00	0.10	0.356	O	|	|	|	|	0.29
111.917	0.00	0.10	0.356	O	|	|	|	|	0.29
112.000	0.00	0.10	0.355	O	|	|	|	|	0.29
112.083	0.00	0.10	0.354	O	|	|	|	|	0.29
112.167	0.00	0.10	0.354	O	|	|	|	|	0.29
112.250	0.00	0.10	0.353	O	|	|	|	|	0.29
112.333	0.00	0.10	0.352	O	|	|	|	|	0.29
112.417	0.00	0.10	0.352	O	|	|	|	|	0.29
112.500	0.00	0.10	0.351	O	|	|	|	|	0.28
112.583	0.00	0.10	0.350	O	|	|	|	|	0.28

112.667	0.00	0.10	0.349	O	|	|	|	|	0.28
112.750	0.00	0.10	0.349	O	|	|	|	|	0.28
112.833	0.00	0.10	0.348	O	|	|	|	|	0.28
112.917	0.00	0.10	0.347	O	|	|	|	|	0.28
113.000	0.00	0.10	0.347	O	|	|	|	|	0.28
113.083	0.00	0.10	0.346	O	|	|	|	|	0.28
113.167	0.00	0.10	0.345	O	|	|	|	|	0.28
113.250	0.00	0.10	0.345	O	|	|	|	|	0.28
113.333	0.00	0.10	0.344	O	|	|	|	|	0.28
113.417	0.00	0.10	0.343	O	|	|	|	|	0.28
113.500	0.00	0.10	0.343	O	|	|	|	|	0.28
113.583	0.00	0.10	0.342	O	|	|	|	|	0.28
113.667	0.00	0.10	0.342	O	|	|	|	|	0.28
113.750	0.00	0.10	0.341	O	|	|	|	|	0.28
113.833	0.00	0.09	0.340	O	|	|	|	|	0.28
113.917	0.00	0.09	0.340	O	|	|	|	|	0.28
114.000	0.00	0.09	0.339	O	|	|	|	|	0.28
114.083	0.00	0.09	0.338	O	|	|	|	|	0.27
114.167	0.00	0.09	0.338	O	|	|	|	|	0.27
114.250	0.00	0.09	0.337	O	|	|	|	|	0.27
114.333	0.00	0.09	0.336	O	|	|	|	|	0.27
114.417	0.00	0.09	0.336	O	|	|	|	|	0.27
114.500	0.00	0.09	0.335	O	|	|	|	|	0.27
114.583	0.00	0.09	0.334	O	|	|	|	|	0.27
114.667	0.00	0.09	0.334	O	|	|	|	|	0.27
114.750	0.00	0.09	0.333	O	|	|	|	|	0.27
114.833	0.00	0.09	0.332	O	|	|	|	|	0.27
114.917	0.00	0.09	0.332	O	|	|	|	|	0.27
115.000	0.00	0.09	0.331	O	|	|	|	|	0.27
115.083	0.00	0.09	0.331	O	|	|	|	|	0.27
115.167	0.00	0.09	0.330	O	|	|	|	|	0.27
115.250	0.00	0.09	0.329	O	|	|	|	|	0.27
115.333	0.00	0.09	0.329	O	|	|	|	|	0.27
115.417	0.00	0.09	0.328	O	|	|	|	|	0.27
115.500	0.00	0.09	0.327	O	|	|	|	|	0.27
115.583	0.00	0.09	0.327	O	|	|	|	|	0.27
115.667	0.00	0.09	0.326	O	|	|	|	|	0.26
115.750	0.00	0.09	0.325	O	|	|	|	|	0.26
115.833	0.00	0.09	0.325	O	|	|	|	|	0.26
115.917	0.00	0.09	0.324	O	|	|	|	|	0.26
116.000	0.00	0.09	0.324	O	|	|	|	|	0.26
116.083	0.00	0.09	0.323	O	|	|	|	|	0.26
116.167	0.00	0.09	0.322	O	|	|	|	|	0.26
116.250	0.00	0.09	0.322	O	|	|	|	|	0.26
116.333	0.00	0.09	0.321	O	|	|	|	|	0.26
116.417	0.00	0.09	0.321	O	|	|	|	|	0.26
116.500	0.00	0.09	0.320	O	|	|	|	|	0.26
116.583	0.00	0.09	0.319	O	|	|	|	|	0.26
116.667	0.00	0.09	0.319	O	|	|	|	|	0.26
116.750	0.00	0.09	0.318	O	|	|	|	|	0.26
116.833	0.00	0.09	0.317	O	|	|	|	|	0.26
116.917	0.00	0.09	0.317	O	|	|	|	|	0.26
117.000	0.00	0.09	0.316	O	|	|	|	|	0.26
117.083	0.00	0.09	0.316	O	|	|	|	|	0.26
117.167	0.00	0.09	0.315	O	|	|	|	|	0.26
117.250	0.00	0.09	0.314	O	|	|	|	|	0.26
117.333	0.00	0.09	0.314	O	|	|	|	|	0.25
117.417	0.00	0.09	0.313	O	|	|	|	|	0.25
117.500	0.00	0.09	0.313	O	|	|	|	|	0.25
117.583	0.00	0.09	0.312	O	|	|	|	|	0.25
117.667	0.00	0.09	0.311	O	|	|	|	|	0.25
117.750	0.00	0.09	0.311	O	|	|	|	|	0.25
117.833	0.00	0.09	0.310	O	|	|	|	|	0.25
117.917	0.00	0.09	0.310	O	|	|	|	|	0.25
118.000	0.00	0.09	0.309	O	|	|	|	|	0.25
118.083	0.00	0.09	0.308	O	|	|	|	|	0.25
118.167	0.00	0.09	0.308	O	|	|	|	|	0.25
118.250	0.00	0.09	0.307	O	|	|	|	|	0.25
118.333	0.00	0.09	0.307	O	|	|	|	|	0.25
118.417	0.00	0.09	0.306	O	|	|	|	|	0.25
118.500	0.00	0.09	0.305	O	|	|	|	|	0.25

118.583	0.00	0.09	0.305	O	|	|	|	|	0.25
118.667	0.00	0.08	0.304	O	|	|	|	|	0.25
118.750	0.00	0.08	0.304	O	|	|	|	|	0.25
118.833	0.00	0.08	0.303	O	|	|	|	|	0.25
118.917	0.00	0.08	0.303	O	|	|	|	|	0.25
119.000	0.00	0.08	0.302	O	|	|	|	|	0.25
119.083	0.00	0.08	0.301	O	|	|	|	|	0.24
119.167	0.00	0.08	0.301	O	|	|	|	|	0.24
119.250	0.00	0.08	0.300	O	|	|	|	|	0.24
119.333	0.00	0.08	0.300	O	|	|	|	|	0.24
119.417	0.00	0.08	0.299	O	|	|	|	|	0.24
119.500	0.00	0.08	0.299	O	|	|	|	|	0.24
119.583	0.00	0.08	0.298	O	|	|	|	|	0.24
119.667	0.00	0.08	0.297	O	|	|	|	|	0.24
119.750	0.00	0.08	0.297	O	|	|	|	|	0.24
119.833	0.00	0.08	0.296	O	|	|	|	|	0.24
119.917	0.00	0.08	0.296	O	|	|	|	|	0.24
120.000	0.00	0.08	0.295	O	|	|	|	|	0.24
120.083	0.00	0.08	0.295	O	|	|	|	|	0.24
120.167	0.00	0.08	0.294	O	|	|	|	|	0.24
120.250	0.00	0.08	0.293	O	|	|	|	|	0.24
120.333	0.00	0.08	0.293	O	|	|	|	|	0.24
120.417	0.00	0.08	0.292	O	|	|	|	|	0.24
120.500	0.00	0.08	0.292	O	|	|	|	|	0.24
120.583	0.00	0.08	0.291	O	|	|	|	|	0.24
120.667	0.00	0.08	0.291	O	|	|	|	|	0.24
120.750	0.00	0.08	0.290	O	|	|	|	|	0.24
120.833	0.00	0.08	0.289	O	|	|	|	|	0.23
120.917	0.00	0.08	0.289	O	|	|	|	|	0.23
121.000	0.00	0.08	0.288	O	|	|	|	|	0.23
121.083	0.00	0.08	0.288	O	|	|	|	|	0.23
121.167	0.00	0.08	0.287	O	|	|	|	|	0.23
121.250	0.00	0.08	0.287	O	|	|	|	|	0.23
121.333	0.00	0.08	0.286	O	|	|	|	|	0.23
121.417	0.00	0.08	0.286	O	|	|	|	|	0.23
121.500	0.00	0.08	0.285	O	|	|	|	|	0.23
121.583	0.00	0.08	0.284	O	|	|	|	|	0.23
121.667	0.00	0.08	0.284	O	|	|	|	|	0.23
121.750	0.00	0.08	0.283	O	|	|	|	|	0.23
121.833	0.00	0.08	0.283	O	|	|	|	|	0.23
121.917	0.00	0.08	0.282	O	|	|	|	|	0.23
122.000	0.00	0.08	0.282	O	|	|	|	|	0.23
122.083	0.00	0.08	0.281	O	|	|	|	|	0.23
122.167	0.00	0.08	0.281	O	|	|	|	|	0.23
122.250	0.00	0.08	0.280	O	|	|	|	|	0.23
122.333	0.00	0.08	0.280	O	|	|	|	|	0.23
122.417	0.00	0.08	0.279	O	|	|	|	|	0.23
122.500	0.00	0.08	0.279	O	|	|	|	|	0.23
122.583	0.00	0.08	0.278	O	|	|	|	|	0.23
122.667	0.00	0.08	0.277	O	|	|	|	|	0.23
122.750	0.00	0.08	0.277	O	|	|	|	|	0.22
122.833	0.00	0.08	0.276	O	|	|	|	|	0.22
122.917	0.00	0.08	0.276	O	|	|	|	|	0.22
123.000	0.00	0.08	0.275	O	|	|	|	|	0.22
123.083	0.00	0.08	0.275	O	|	|	|	|	0.22
123.167	0.00	0.08	0.274	O	|	|	|	|	0.22
123.250	0.00	0.08	0.274	O	|	|	|	|	0.22
123.333	0.00	0.08	0.273	O	|	|	|	|	0.22
123.417	0.00	0.08	0.273	O	|	|	|	|	0.22
123.500	0.00	0.08	0.272	O	|	|	|	|	0.22
123.583	0.00	0.08	0.272	O	|	|	|	|	0.22
123.667	0.00	0.08	0.271	O	|	|	|	|	0.22
123.750	0.00	0.08	0.271	O	|	|	|	|	0.22
123.833	0.00	0.08	0.270	O	|	|	|	|	0.22
123.917	0.00	0.08	0.270	O	|	|	|	|	0.22
124.000	0.00	0.08	0.269	O	|	|	|	|	0.22
124.083	0.00	0.07	0.269	O	|	|	|	|	0.22
124.167	0.00	0.07	0.268	O	|	|	|	|	0.22
124.250	0.00	0.07	0.268	O	|	|	|	|	0.22
124.333	0.00	0.07	0.267	O	|	|	|	|	0.22
124.417	0.00	0.07	0.266	O	|	|	|	|	0.22

124.500	0.00	0.07	0.266	O	|	|	|	|	0.22
124.583	0.00	0.07	0.265	O	|	|	|	|	0.22
124.667	0.00	0.07	0.265	O	|	|	|	|	0.22
124.750	0.00	0.07	0.264	O	|	|	|	|	0.21
124.833	0.00	0.07	0.264	O	|	|	|	|	0.21
124.917	0.00	0.07	0.263	O	|	|	|	|	0.21
125.000	0.00	0.07	0.263	O	|	|	|	|	0.21
125.083	0.00	0.07	0.262	O	|	|	|	|	0.21
125.167	0.00	0.07	0.262	O	|	|	|	|	0.21
125.250	0.00	0.07	0.261	O	|	|	|	|	0.21
125.333	0.00	0.07	0.261	O	|	|	|	|	0.21
125.417	0.00	0.07	0.260	O	|	|	|	|	0.21
125.500	0.00	0.07	0.260	O	|	|	|	|	0.21
125.583	0.00	0.07	0.259	O	|	|	|	|	0.21
125.667	0.00	0.07	0.259	O	|	|	|	|	0.21
125.750	0.00	0.07	0.258	O	|	|	|	|	0.21
125.833	0.00	0.07	0.258	O	|	|	|	|	0.21
125.917	0.00	0.07	0.257	O	|	|	|	|	0.21
126.000	0.00	0.07	0.257	O	|	|	|	|	0.21
126.083	0.00	0.07	0.256	O	|	|	|	|	0.21
126.167	0.00	0.07	0.256	O	|	|	|	|	0.21
126.250	0.00	0.07	0.255	O	|	|	|	|	0.21
126.333	0.00	0.07	0.255	O	|	|	|	|	0.21
126.417	0.00	0.07	0.254	O	|	|	|	|	0.21
126.500	0.00	0.07	0.254	O	|	|	|	|	0.21
126.583	0.00	0.07	0.253	O	|	|	|	|	0.21
126.667	0.00	0.07	0.253	O	|	|	|	|	0.21
126.750	0.00	0.07	0.253	O	|	|	|	|	0.20
126.833	0.00	0.07	0.252	O	|	|	|	|	0.20
126.917	0.00	0.07	0.252	O	|	|	|	|	0.20
127.000	0.00	0.07	0.251	O	|	|	|	|	0.20
127.083	0.00	0.07	0.251	O	|	|	|	|	0.20
127.167	0.00	0.07	0.250	O	|	|	|	|	0.20
127.250	0.00	0.07	0.250	O	|	|	|	|	0.20
127.333	0.00	0.07	0.249	O	|	|	|	|	0.20
127.417	0.00	0.07	0.249	O	|	|	|	|	0.20
127.500	0.00	0.07	0.248	O	|	|	|	|	0.20
127.583	0.00	0.07	0.248	O	|	|	|	|	0.20
127.667	0.00	0.07	0.247	O	|	|	|	|	0.20
127.750	0.00	0.07	0.247	O	|	|	|	|	0.20
127.833	0.00	0.07	0.246	O	|	|	|	|	0.20
127.917	0.00	0.07	0.246	O	|	|	|	|	0.20
128.000	0.00	0.07	0.245	O	|	|	|	|	0.20
128.083	0.00	0.07	0.245	O	|	|	|	|	0.20
128.167	0.00	0.07	0.244	O	|	|	|	|	0.20
128.250	0.00	0.07	0.244	O	|	|	|	|	0.20
128.333	0.00	0.07	0.243	O	|	|	|	|	0.20
128.417	0.00	0.07	0.243	O	|	|	|	|	0.20
128.500	0.00	0.07	0.243	O	|	|	|	|	0.20
128.583	0.00	0.07	0.242	O	|	|	|	|	0.20
128.667	0.00	0.07	0.242	O	|	|	|	|	0.20
128.750	0.00	0.07	0.241	O	|	|	|	|	0.20
128.833	0.00	0.07	0.241	O	|	|	|	|	0.20
128.917	0.00	0.07	0.240	O	|	|	|	|	0.19
129.000	0.00	0.07	0.240	O	|	|	|	|	0.19
129.083	0.00	0.07	0.239	O	|	|	|	|	0.19
129.167	0.00	0.07	0.239	O	|	|	|	|	0.19
129.250	0.00	0.07	0.238	O	|	|	|	|	0.19
129.333	0.00	0.07	0.238	O	|	|	|	|	0.19
129.417	0.00	0.07	0.237	O	|	|	|	|	0.19
129.500	0.00	0.07	0.237	O	|	|	|	|	0.19
129.583	0.00	0.07	0.237	O	|	|	|	|	0.19
129.667	0.00	0.07	0.236	O	|	|	|	|	0.19
129.750	0.00	0.07	0.236	O	|	|	|	|	0.19
129.833	0.00	0.07	0.235	O	|	|	|	|	0.19
129.917	0.00	0.07	0.235	O	|	|	|	|	0.19
130.000	0.00	0.07	0.234	O	|	|	|	|	0.19
130.083	0.00	0.07	0.234	O	|	|	|	|	0.19
130.167	0.00	0.07	0.233	O	|	|	|	|	0.19
130.250	0.00	0.07	0.233	O	|	|	|	|	0.19
130.333	0.00	0.06	0.232	O	|	|	|	|	0.19

130.417	0.00	0.06	0.232	O	|	|	|	|	0.19
130.500	0.00	0.06	0.232	O	|	|	|	|	0.19
130.583	0.00	0.06	0.231	O	|	|	|	|	0.19
130.667	0.00	0.06	0.231	O	|	|	|	|	0.19
130.750	0.00	0.06	0.230	O	|	|	|	|	0.19
130.833	0.00	0.06	0.230	O	|	|	|	|	0.19
130.917	0.00	0.06	0.229	O	|	|	|	|	0.19
131.000	0.00	0.06	0.229	O	|	|	|	|	0.19
131.083	0.00	0.06	0.228	O	|	|	|	|	0.19
131.167	0.00	0.06	0.228	O	|	|	|	|	0.19
131.250	0.00	0.06	0.228	O	|	|	|	|	0.18
131.333	0.00	0.06	0.227	O	|	|	|	|	0.18
131.417	0.00	0.06	0.227	O	|	|	|	|	0.18
131.500	0.00	0.06	0.226	O	|	|	|	|	0.18
131.583	0.00	0.06	0.226	O	|	|	|	|	0.18
131.667	0.00	0.06	0.225	O	|	|	|	|	0.18
131.750	0.00	0.06	0.225	O	|	|	|	|	0.18
131.833	0.00	0.06	0.225	O	|	|	|	|	0.18
131.917	0.00	0.06	0.224	O	|	|	|	|	0.18
132.000	0.00	0.06	0.224	O	|	|	|	|	0.18
132.083	0.00	0.06	0.223	O	|	|	|	|	0.18
132.167	0.00	0.06	0.223	O	|	|	|	|	0.18
132.250	0.00	0.06	0.222	O	|	|	|	|	0.18
132.333	0.00	0.06	0.222	O	|	|	|	|	0.18
132.417	0.00	0.06	0.222	O	|	|	|	|	0.18
132.500	0.00	0.06	0.221	O	|	|	|	|	0.18
132.583	0.00	0.06	0.221	O	|	|	|	|	0.18
132.667	0.00	0.06	0.220	O	|	|	|	|	0.18
132.750	0.00	0.06	0.220	O	|	|	|	|	0.18
132.833	0.00	0.06	0.219	O	|	|	|	|	0.18
132.917	0.00	0.06	0.219	O	|	|	|	|	0.18
133.000	0.00	0.06	0.219	O	|	|	|	|	0.18
133.083	0.00	0.06	0.218	O	|	|	|	|	0.18
133.167	0.00	0.06	0.218	O	|	|	|	|	0.18
133.250	0.00	0.06	0.217	O	|	|	|	|	0.18
133.333	0.00	0.06	0.217	O	|	|	|	|	0.18
133.417	0.00	0.06	0.217	O	|	|	|	|	0.18
133.500	0.00	0.06	0.216	O	|	|	|	|	0.18
133.583	0.00	0.06	0.216	O	|	|	|	|	0.18
133.667	0.00	0.06	0.215	O	|	|	|	|	0.17
133.750	0.00	0.06	0.215	O	|	|	|	|	0.17
133.833	0.00	0.06	0.214	O	|	|	|	|	0.17
133.917	0.00	0.06	0.214	O	|	|	|	|	0.17
134.000	0.00	0.06	0.214	O	|	|	|	|	0.17
134.083	0.00	0.06	0.213	O	|	|	|	|	0.17
134.167	0.00	0.06	0.213	O	|	|	|	|	0.17
134.250	0.00	0.06	0.212	O	|	|	|	|	0.17
134.333	0.00	0.06	0.212	O	|	|	|	|	0.17
134.417	0.00	0.06	0.212	O	|	|	|	|	0.17
134.500	0.00	0.06	0.211	O	|	|	|	|	0.17
134.583	0.00	0.06	0.211	O	|	|	|	|	0.17
134.667	0.00	0.06	0.210	O	|	|	|	|	0.17
134.750	0.00	0.06	0.210	O	|	|	|	|	0.17
134.833	0.00	0.06	0.210	O	|	|	|	|	0.17
134.917	0.00	0.06	0.209	O	|	|	|	|	0.17
135.000	0.00	0.06	0.209	O	|	|	|	|	0.17
135.083	0.00	0.06	0.208	O	|	|	|	|	0.17
135.167	0.00	0.06	0.208	O	|	|	|	|	0.17
135.250	0.00	0.06	0.208	O	|	|	|	|	0.17
135.333	0.00	0.06	0.207	O	|	|	|	|	0.17
135.417	0.00	0.06	0.207	O	|	|	|	|	0.17
135.500	0.00	0.06	0.206	O	|	|	|	|	0.17
135.583	0.00	0.06	0.206	O	|	|	|	|	0.17
135.667	0.00	0.06	0.206	O	|	|	|	|	0.17
135.750	0.00	0.06	0.205	O	|	|	|	|	0.17
135.833	0.00	0.06	0.205	O	|	|	|	|	0.17
135.917	0.00	0.06	0.204	O	|	|	|	|	0.17
136.000	0.00	0.06	0.204	O	|	|	|	|	0.17
136.083	0.00	0.06	0.204	O	|	|	|	|	0.17
136.167	0.00	0.06	0.203	O	|	|	|	|	0.16
136.250	0.00	0.06	0.203	O	|	|	|	|	0.16

136.333	0.00	0.06	0.202	O	|	|	|	|	0.16
136.417	0.00	0.06	0.202	O	|	|	|	|	0.16
136.500	0.00	0.06	0.202	O	|	|	|	|	0.16
136.583	0.00	0.06	0.201	O	|	|	|	|	0.16
136.667	0.00	0.06	0.201	O	|	|	|	|	0.16
136.750	0.00	0.06	0.200	O	|	|	|	|	0.16
136.833	0.00	0.06	0.200	O	|	|	|	|	0.16
136.917	0.00	0.06	0.200	O	|	|	|	|	0.16
137.000	0.00	0.06	0.199	O	|	|	|	|	0.16
137.083	0.00	0.06	0.199	O	|	|	|	|	0.16
137.167	0.00	0.06	0.199	O	|	|	|	|	0.16
137.250	0.00	0.06	0.198	O	|	|	|	|	0.16
137.333	0.00	0.06	0.198	O	|	|	|	|	0.16
137.417	0.00	0.06	0.197	O	|	|	|	|	0.16
137.500	0.00	0.06	0.197	O	|	|	|	|	0.16
137.583	0.00	0.05	0.197	O	|	|	|	|	0.16
137.667	0.00	0.05	0.196	O	|	|	|	|	0.16
137.750	0.00	0.05	0.196	O	|	|	|	|	0.16
137.833	0.00	0.05	0.196	O	|	|	|	|	0.16
137.917	0.00	0.05	0.195	O	|	|	|	|	0.16
138.000	0.00	0.05	0.195	O	|	|	|	|	0.16
138.083	0.00	0.05	0.194	O	|	|	|	|	0.16
138.167	0.00	0.05	0.194	O	|	|	|	|	0.16
138.250	0.00	0.05	0.194	O	|	|	|	|	0.16
138.333	0.00	0.05	0.193	O	|	|	|	|	0.16
138.417	0.00	0.05	0.193	O	|	|	|	|	0.16
138.500	0.00	0.05	0.193	O	|	|	|	|	0.16
138.583	0.00	0.05	0.192	O	|	|	|	|	0.16
138.667	0.00	0.05	0.192	O	|	|	|	|	0.16
138.750	0.00	0.05	0.191	O	|	|	|	|	0.16
138.833	0.00	0.05	0.191	O	|	|	|	|	0.16
138.917	0.00	0.05	0.191	O	|	|	|	|	0.15
139.000	0.00	0.05	0.190	O	|	|	|	|	0.15
139.083	0.00	0.05	0.190	O	|	|	|	|	0.15
139.167	0.00	0.05	0.190	O	|	|	|	|	0.15
139.250	0.00	0.05	0.189	O	|	|	|	|	0.15
139.333	0.00	0.05	0.189	O	|	|	|	|	0.15
139.417	0.00	0.05	0.189	O	|	|	|	|	0.15
139.500	0.00	0.05	0.188	O	|	|	|	|	0.15
139.583	0.00	0.05	0.188	O	|	|	|	|	0.15
139.667	0.00	0.05	0.187	O	|	|	|	|	0.15
139.750	0.00	0.05	0.187	O	|	|	|	|	0.15
139.833	0.00	0.05	0.187	O	|	|	|	|	0.15
139.917	0.00	0.05	0.186	O	|	|	|	|	0.15
140.000	0.00	0.05	0.186	O	|	|	|	|	0.15
140.083	0.00	0.05	0.186	O	|	|	|	|	0.15
140.167	0.00	0.05	0.185	O	|	|	|	|	0.15
140.250	0.00	0.05	0.185	O	|	|	|	|	0.15
140.333	0.00	0.05	0.185	O	|	|	|	|	0.15
140.417	0.00	0.05	0.184	O	|	|	|	|	0.15
140.500	0.00	0.05	0.184	O	|	|	|	|	0.15
140.583	0.00	0.05	0.184	O	|	|	|	|	0.15
140.667	0.00	0.05	0.183	O	|	|	|	|	0.15
140.750	0.00	0.05	0.183	O	|	|	|	|	0.15
140.833	0.00	0.05	0.182	O	|	|	|	|	0.15
140.917	0.00	0.05	0.182	O	|	|	|	|	0.15
141.000	0.00	0.05	0.182	O	|	|	|	|	0.15
141.083	0.00	0.05	0.181	O	|	|	|	|	0.15
141.167	0.00	0.05	0.181	O	|	|	|	|	0.15
141.250	0.00	0.05	0.181	O	|	|	|	|	0.15
141.333	0.00	0.05	0.180	O	|	|	|	|	0.15
141.417	0.00	0.05	0.180	O	|	|	|	|	0.15
141.500	0.00	0.05	0.180	O	|	|	|	|	0.15
141.583	0.00	0.05	0.179	O	|	|	|	|	0.15
141.667	0.00	0.05	0.179	O	|	|	|	|	0.15
141.750	0.00	0.05	0.179	O	|	|	|	|	0.14
141.833	0.00	0.05	0.178	O	|	|	|	|	0.14
141.917	0.00	0.05	0.178	O	|	|	|	|	0.14
142.000	0.00	0.05	0.178	O	|	|	|	|	0.14
142.083	0.00	0.05	0.177	O	|	|	|	|	0.14
142.167	0.00	0.05	0.177	O	|	|	|	|	0.14

142.250	0.00	0.05	0.177	O	|	|	|	|	0.14
142.333	0.00	0.05	0.176	O	|	|	|	|	0.14
142.417	0.00	0.05	0.176	O	|	|	|	|	0.14
142.500	0.00	0.05	0.176	O	|	|	|	|	0.14
142.583	0.00	0.05	0.175	O	|	|	|	|	0.14
142.667	0.00	0.05	0.175	O	|	|	|	|	0.14
142.750	0.00	0.05	0.175	O	|	|	|	|	0.14
142.833	0.00	0.05	0.174	O	|	|	|	|	0.14
142.917	0.00	0.05	0.174	O	|	|	|	|	0.14
143.000	0.00	0.05	0.174	O	|	|	|	|	0.14
143.083	0.00	0.05	0.173	O	|	|	|	|	0.14
143.167	0.00	0.05	0.173	O	|	|	|	|	0.14
143.250	0.00	0.05	0.173	O	|	|	|	|	0.14
143.333	0.00	0.05	0.172	O	|	|	|	|	0.14
143.417	0.00	0.05	0.172	O	|	|	|	|	0.14
143.500	0.00	0.05	0.172	O	|	|	|	|	0.14
143.583	0.00	0.05	0.171	O	|	|	|	|	0.14
143.667	0.00	0.05	0.171	O	|	|	|	|	0.14
143.750	0.00	0.05	0.171	O	|	|	|	|	0.14
143.833	0.00	0.05	0.170	O	|	|	|	|	0.14
143.917	0.00	0.05	0.170	O	|	|	|	|	0.14
144.000	0.00	0.05	0.170	O	|	|	|	|	0.14
144.083	0.00	0.05	0.169	O	|	|	|	|	0.14
144.167	0.00	0.05	0.169	O	|	|	|	|	0.14
144.250	0.00	0.05	0.169	O	|	|	|	|	0.14
144.333	0.00	0.05	0.168	O	|	|	|	|	0.14
144.417	0.00	0.05	0.168	O	|	|	|	|	0.14
144.500	0.00	0.05	0.168	O	|	|	|	|	0.14
144.583	0.00	0.05	0.167	O	|	|	|	|	0.14
144.667	0.00	0.05	0.167	O	|	|	|	|	0.14
144.750	0.00	0.05	0.167	O	|	|	|	|	0.14
144.833	0.00	0.05	0.166	O	|	|	|	|	0.14
144.917	0.00	0.05	0.166	O	|	|	|	|	0.13
145.000	0.00	0.05	0.166	O	|	|	|	|	0.13
145.083	0.00	0.05	0.165	O	|	|	|	|	0.13
145.167	0.00	0.05	0.165	O	|	|	|	|	0.13
145.250	0.00	0.05	0.165	O	|	|	|	|	0.13
145.333	0.00	0.05	0.164	O	|	|	|	|	0.13
145.417	0.00	0.05	0.164	O	|	|	|	|	0.13
145.500	0.00	0.05	0.164	O	|	|	|	|	0.13
145.583	0.00	0.05	0.164	O	|	|	|	|	0.13
145.667	0.00	0.05	0.163	O	|	|	|	|	0.13
145.750	0.00	0.05	0.163	O	|	|	|	|	0.13
145.833	0.00	0.05	0.163	O	|	|	|	|	0.13
145.917	0.00	0.05	0.162	O	|	|	|	|	0.13
146.000	0.00	0.05	0.162	O	|	|	|	|	0.13
146.083	0.00	0.05	0.162	O	|	|	|	|	0.13
146.167	0.00	0.05	0.161	O	|	|	|	|	0.13
146.250	0.00	0.04	0.161	O	|	|	|	|	0.13
146.333	0.00	0.04	0.161	O	|	|	|	|	0.13
146.417	0.00	0.04	0.160	O	|	|	|	|	0.13
146.500	0.00	0.04	0.160	O	|	|	|	|	0.13
146.583	0.00	0.04	0.160	O	|	|	|	|	0.13
146.667	0.00	0.04	0.159	O	|	|	|	|	0.13
146.750	0.00	0.04	0.159	O	|	|	|	|	0.13
146.833	0.00	0.04	0.159	O	|	|	|	|	0.13
146.917	0.00	0.04	0.159	O	|	|	|	|	0.13
147.000	0.00	0.04	0.158	O	|	|	|	|	0.13
147.083	0.00	0.04	0.158	O	|	|	|	|	0.13
147.167	0.00	0.04	0.158	O	|	|	|	|	0.13
147.250	0.00	0.04	0.157	O	|	|	|	|	0.13
147.333	0.00	0.04	0.157	O	|	|	|	|	0.13
147.417	0.00	0.04	0.157	O	|	|	|	|	0.13
147.500	0.00	0.04	0.156	O	|	|	|	|	0.13
147.583	0.00	0.04	0.156	O	|	|	|	|	0.13
147.667	0.00	0.04	0.156	O	|	|	|	|	0.13
147.750	0.00	0.04	0.156	O	|	|	|	|	0.13
147.833	0.00	0.04	0.155	O	|	|	|	|	0.13
147.917	0.00	0.04	0.155	O	|	|	|	|	0.13
148.000	0.00	0.04	0.155	O	|	|	|	|	0.13
148.083	0.00	0.04	0.154	O	|	|	|	|	0.13

148.167	0.00	0.04	0.154	O	|	|	|	|	0.13
148.250	0.00	0.04	0.154	O	|	|	|	|	0.12
148.333	0.00	0.04	0.153	O	|	|	|	|	0.12
148.417	0.00	0.04	0.153	O	|	|	|	|	0.12
148.500	0.00	0.04	0.153	O	|	|	|	|	0.12
148.583	0.00	0.04	0.153	O	|	|	|	|	0.12
148.667	0.00	0.04	0.152	O	|	|	|	|	0.12
148.750	0.00	0.04	0.152	O	|	|	|	|	0.12
148.833	0.00	0.04	0.152	O	|	|	|	|	0.12
148.917	0.00	0.04	0.151	O	|	|	|	|	0.12
149.000	0.00	0.04	0.151	O	|	|	|	|	0.12
149.083	0.00	0.04	0.151	O	|	|	|	|	0.12
149.167	0.00	0.04	0.151	O	|	|	|	|	0.12
149.250	0.00	0.04	0.150	O	|	|	|	|	0.12
149.333	0.00	0.04	0.150	O	|	|	|	|	0.12
149.417	0.00	0.04	0.150	O	|	|	|	|	0.12
149.500	0.00	0.04	0.149	O	|	|	|	|	0.12
149.583	0.00	0.04	0.149	O	|	|	|	|	0.12
149.667	0.00	0.04	0.149	O	|	|	|	|	0.12
149.750	0.00	0.04	0.149	O	|	|	|	|	0.12
149.833	0.00	0.04	0.148	O	|	|	|	|	0.12
149.917	0.00	0.04	0.148	O	|	|	|	|	0.12
150.000	0.00	0.04	0.148	O	|	|	|	|	0.12
150.083	0.00	0.04	0.147	O	|	|	|	|	0.12
150.167	0.00	0.04	0.147	O	|	|	|	|	0.12
150.250	0.00	0.04	0.147	O	|	|	|	|	0.12
150.333	0.00	0.04	0.147	O	|	|	|	|	0.12
150.417	0.00	0.04	0.146	O	|	|	|	|	0.12
150.500	0.00	0.04	0.146	O	|	|	|	|	0.12
150.583	0.00	0.04	0.146	O	|	|	|	|	0.12
150.667	0.00	0.04	0.145	O	|	|	|	|	0.12
150.750	0.00	0.04	0.145	O	|	|	|	|	0.12
150.833	0.00	0.04	0.145	O	|	|	|	|	0.12
150.917	0.00	0.04	0.145	O	|	|	|	|	0.12
151.000	0.00	0.04	0.144	O	|	|	|	|	0.12
151.083	0.00	0.04	0.144	O	|	|	|	|	0.12
151.167	0.00	0.04	0.144	O	|	|	|	|	0.12
151.250	0.00	0.04	0.143	O	|	|	|	|	0.12
151.333	0.00	0.04	0.143	O	|	|	|	|	0.12
151.417	0.00	0.04	0.143	O	|	|	|	|	0.12
151.500	0.00	0.04	0.143	O	|	|	|	|	0.12
151.583	0.00	0.04	0.142	O	|	|	|	|	0.12
151.667	0.00	0.04	0.142	O	|	|	|	|	0.12
151.750	0.00	0.04	0.142	O	|	|	|	|	0.12
151.833	0.00	0.04	0.142	O	|	|	|	|	0.11
151.917	0.00	0.04	0.141	O	|	|	|	|	0.11
152.000	0.00	0.04	0.141	O	|	|	|	|	0.11
152.083	0.00	0.04	0.141	O	|	|	|	|	0.11
152.167	0.00	0.04	0.140	O	|	|	|	|	0.11
152.250	0.00	0.04	0.140	O	|	|	|	|	0.11
152.333	0.00	0.04	0.140	O	|	|	|	|	0.11
152.417	0.00	0.04	0.140	O	|	|	|	|	0.11
152.500	0.00	0.04	0.139	O	|	|	|	|	0.11
152.583	0.00	0.04	0.139	O	|	|	|	|	0.11
152.667	0.00	0.04	0.139	O	|	|	|	|	0.11
152.750	0.00	0.04	0.139	O	|	|	|	|	0.11
152.833	0.00	0.04	0.138	O	|	|	|	|	0.11
152.917	0.00	0.04	0.138	O	|	|	|	|	0.11
153.000	0.00	0.04	0.138	O	|	|	|	|	0.11
153.083	0.00	0.04	0.138	O	|	|	|	|	0.11
153.167	0.00	0.04	0.137	O	|	|	|	|	0.11
153.250	0.00	0.04	0.137	O	|	|	|	|	0.11
153.333	0.00	0.04	0.137	O	|	|	|	|	0.11
153.417	0.00	0.04	0.136	O	|	|	|	|	0.11
153.500	0.00	0.04	0.136	O	|	|	|	|	0.11
153.583	0.00	0.04	0.136	O	|	|	|	|	0.11
153.667	0.00	0.04	0.136	O	|	|	|	|	0.11
153.750	0.00	0.04	0.135	O	|	|	|	|	0.11
153.833	0.00	0.04	0.135	O	|	|	|	|	0.11
153.917	0.00	0.04	0.135	O	|	|	|	|	0.11
154.000	0.00	0.04	0.135	O	|	|	|	|	0.11

154.083	0.00	0.04	0.134	O	|	|	|	|	0.11
154.167	0.00	0.04	0.134	O	|	|	|	|	0.11
154.250	0.00	0.04	0.134	O	|	|	|	|	0.11
154.333	0.00	0.04	0.134	O	|	|	|	|	0.11
154.417	0.00	0.04	0.133	O	|	|	|	|	0.11
154.500	0.00	0.04	0.133	O	|	|	|	|	0.11
154.583	0.00	0.04	0.133	O	|	|	|	|	0.11
154.667	0.00	0.04	0.133	O	|	|	|	|	0.11
154.750	0.00	0.04	0.132	O	|	|	|	|	0.11
154.833	0.00	0.04	0.132	O	|	|	|	|	0.11
154.917	0.00	0.04	0.132	O	|	|	|	|	0.11
155.000	0.00	0.04	0.132	O	|	|	|	|	0.11
155.083	0.00	0.04	0.131	O	|	|	|	|	0.11
155.167	0.00	0.04	0.131	O	|	|	|	|	0.11
155.250	0.00	0.04	0.131	O	|	|	|	|	0.11
155.333	0.00	0.04	0.131	O	|	|	|	|	0.11
155.417	0.00	0.04	0.130	O	|	|	|	|	0.11
155.500	0.00	0.04	0.130	O	|	|	|	|	0.11
155.583	0.00	0.04	0.130	O	|	|	|	|	0.11
155.667	0.00	0.04	0.130	O	|	|	|	|	0.11
155.750	0.00	0.04	0.129	O	|	|	|	|	0.10
155.833	0.00	0.04	0.129	O	|	|	|	|	0.10
155.917	0.00	0.04	0.129	O	|	|	|	|	0.10
156.000	0.00	0.04	0.129	O	|	|	|	|	0.10
156.083	0.00	0.04	0.128	O	|	|	|	|	0.10
156.167	0.00	0.04	0.128	O	|	|	|	|	0.10
156.250	0.00	0.04	0.128	O	|	|	|	|	0.10
156.333	0.00	0.04	0.128	O	|	|	|	|	0.10
156.417	0.00	0.04	0.127	O	|	|	|	|	0.10
156.500	0.00	0.04	0.127	O	|	|	|	|	0.10
156.583	0.00	0.04	0.127	O	|	|	|	|	0.10
156.667	0.00	0.04	0.127	O	|	|	|	|	0.10
156.750	0.00	0.04	0.126	O	|	|	|	|	0.10
156.833	0.00	0.04	0.126	O	|	|	|	|	0.10
156.917	0.00	0.04	0.126	O	|	|	|	|	0.10
157.000	0.00	0.04	0.126	O	|	|	|	|	0.10
157.083	0.00	0.04	0.125	O	|	|	|	|	0.10
157.167	0.00	0.03	0.125	O	|	|	|	|	0.10
157.250	0.00	0.03	0.125	O	|	|	|	|	0.10
157.333	0.00	0.03	0.125	O	|	|	|	|	0.10
157.417	0.00	0.03	0.124	O	|	|	|	|	0.10
157.500	0.00	0.03	0.124	O	|	|	|	|	0.10
157.583	0.00	0.03	0.124	O	|	|	|	|	0.10
157.667	0.00	0.03	0.124	O	|	|	|	|	0.10
157.750	0.00	0.03	0.123	O	|	|	|	|	0.10
157.833	0.00	0.03	0.123	O	|	|	|	|	0.10
157.917	0.00	0.03	0.123	O	|	|	|	|	0.10
158.000	0.00	0.03	0.123	O	|	|	|	|	0.10
158.083	0.00	0.03	0.123	O	|	|	|	|	0.10
158.167	0.00	0.03	0.122	O	|	|	|	|	0.10
158.250	0.00	0.03	0.122	O	|	|	|	|	0.10
158.333	0.00	0.03	0.122	O	|	|	|	|	0.10
158.417	0.00	0.03	0.122	O	|	|	|	|	0.10
158.500	0.00	0.03	0.121	O	|	|	|	|	0.10
158.583	0.00	0.03	0.121	O	|	|	|	|	0.10
158.667	0.00	0.03	0.121	O	|	|	|	|	0.10
158.750	0.00	0.03	0.121	O	|	|	|	|	0.10
158.833	0.00	0.03	0.120	O	|	|	|	|	0.10
158.917	0.00	0.03	0.120	O	|	|	|	|	0.10
159.000	0.00	0.03	0.120	O	|	|	|	|	0.10
159.083	0.00	0.03	0.120	O	|	|	|	|	0.10
159.167	0.00	0.03	0.120	O	|	|	|	|	0.10
159.250	0.00	0.03	0.119	O	|	|	|	|	0.10
159.333	0.00	0.03	0.119	O	|	|	|	|	0.10
159.417	0.00	0.03	0.119	O	|	|	|	|	0.10
159.500	0.00	0.03	0.119	O	|	|	|	|	0.10
159.583	0.00	0.03	0.118	O	|	|	|	|	0.10
159.667	0.00	0.03	0.118	O	|	|	|	|	0.10
159.750	0.00	0.03	0.118	O	|	|	|	|	0.10
159.833	0.00	0.03	0.118	O	|	|	|	|	0.10
159.917	0.00	0.03	0.117	O	|	|	|	|	0.10

160.000	0.00	0.03	0.117	O	|	|	|	|	0.10
160.083	0.00	0.03	0.117	O	|	|	|	|	0.09
160.167	0.00	0.03	0.117	O	|	|	|	|	0.09
160.250	0.00	0.03	0.117	O	|	|	|	|	0.09
160.333	0.00	0.03	0.116	O	|	|	|	|	0.09
160.417	0.00	0.03	0.116	O	|	|	|	|	0.09
160.500	0.00	0.03	0.116	O	|	|	|	|	0.09
160.583	0.00	0.03	0.116	O	|	|	|	|	0.09
160.667	0.00	0.03	0.115	O	|	|	|	|	0.09
160.750	0.00	0.03	0.115	O	|	|	|	|	0.09
160.833	0.00	0.03	0.115	O	|	|	|	|	0.09
160.917	0.00	0.03	0.115	O	|	|	|	|	0.09
161.000	0.00	0.03	0.115	O	|	|	|	|	0.09
161.083	0.00	0.03	0.114	O	|	|	|	|	0.09
161.167	0.00	0.03	0.114	O	|	|	|	|	0.09
161.250	0.00	0.03	0.114	O	|	|	|	|	0.09
161.333	0.00	0.03	0.114	O	|	|	|	|	0.09
161.417	0.00	0.03	0.113	O	|	|	|	|	0.09
161.500	0.00	0.03	0.113	O	|	|	|	|	0.09
161.583	0.00	0.03	0.113	O	|	|	|	|	0.09
161.667	0.00	0.03	0.113	O	|	|	|	|	0.09
161.750	0.00	0.03	0.113	O	|	|	|	|	0.09
161.833	0.00	0.03	0.112	O	|	|	|	|	0.09
161.917	0.00	0.03	0.112	O	|	|	|	|	0.09
162.000	0.00	0.03	0.112	O	|	|	|	|	0.09
162.083	0.00	0.03	0.112	O	|	|	|	|	0.09
162.167	0.00	0.03	0.112	O	|	|	|	|	0.09
162.250	0.00	0.03	0.111	O	|	|	|	|	0.09
162.333	0.00	0.03	0.111	O	|	|	|	|	0.09
162.417	0.00	0.03	0.111	O	|	|	|	|	0.09
162.500	0.00	0.03	0.111	O	|	|	|	|	0.09
162.583	0.00	0.03	0.110	O	|	|	|	|	0.09
162.667	0.00	0.03	0.110	O	|	|	|	|	0.09
162.750	0.00	0.03	0.110	O	|	|	|	|	0.09
162.833	0.00	0.03	0.110	O	|	|	|	|	0.09
162.917	0.00	0.03	0.110	O	|	|	|	|	0.09
163.000	0.00	0.03	0.109	O	|	|	|	|	0.09
163.083	0.00	0.03	0.109	O	|	|	|	|	0.09
163.167	0.00	0.03	0.109	O	|	|	|	|	0.09
163.250	0.00	0.03	0.109	O	|	|	|	|	0.09
163.333	0.00	0.03	0.109	O	|	|	|	|	0.09
163.417	0.00	0.03	0.108	O	|	|	|	|	0.09
163.500	0.00	0.03	0.108	O	|	|	|	|	0.09
163.583	0.00	0.03	0.108	O	|	|	|	|	0.09
163.667	0.00	0.03	0.108	O	|	|	|	|	0.09
163.750	0.00	0.03	0.108	O	|	|	|	|	0.09
163.833	0.00	0.03	0.107	O	|	|	|	|	0.09
163.917	0.00	0.03	0.107	O	|	|	|	|	0.09
164.000	0.00	0.03	0.107	O	|	|	|	|	0.09
164.083	0.00	0.03	0.107	O	|	|	|	|	0.09
164.167	0.00	0.03	0.106	O	|	|	|	|	0.09
164.250	0.00	0.03	0.106	O	|	|	|	|	0.09
164.333	0.00	0.03	0.106	O	|	|	|	|	0.09
164.417	0.00	0.03	0.106	O	|	|	|	|	0.09
164.500	0.00	0.03	0.106	O	|	|	|	|	0.09
164.583	0.00	0.03	0.105	O	|	|	|	|	0.09
164.667	0.00	0.03	0.105	O	|	|	|	|	0.09
164.750	0.00	0.03	0.105	O	|	|	|	|	0.09
164.833	0.00	0.03	0.105	O	|	|	|	|	0.09
164.917	0.00	0.03	0.105	O	|	|	|	|	0.08
165.000	0.00	0.03	0.104	O	|	|	|	|	0.08
165.083	0.00	0.03	0.104	O	|	|	|	|	0.08
165.167	0.00	0.03	0.104	O	|	|	|	|	0.08
165.250	0.00	0.03	0.104	O	|	|	|	|	0.08
165.333	0.00	0.03	0.104	O	|	|	|	|	0.08
165.417	0.00	0.03	0.103	O	|	|	|	|	0.08
165.500	0.00	0.03	0.103	O	|	|	|	|	0.08
165.583	0.00	0.03	0.103	O	|	|	|	|	0.08
165.667	0.00	0.03	0.103	O	|	|	|	|	0.08
165.750	0.00	0.03	0.103	O	|	|	|	|	0.08
165.833	0.00	0.03	0.102	O	|	|	|	|	0.08

165.917	0.00	0.03	0.102	O					0.08
166.000	0.00	0.03	0.102	O					0.08
166.083	0.00	0.03	0.102	O					0.08
166.167	0.00	0.03	0.102	O					0.08
166.250	0.00	0.03	0.101	O					0.08
166.333	0.00	0.03	0.101	O					0.08
166.417	0.00	0.03	0.101	O					0.08
166.500	0.00	0.03	0.101	O					0.08
166.583	0.00	0.03	0.101	O					0.08
166.667	0.00	0.03	0.101	O					0.08
166.750	0.00	0.03	0.100	O					0.08
166.833	0.00	0.03	0.100	O					0.08
166.917	0.00	0.03	0.100	O					0.08
167.000	0.00	0.03	0.100	O					0.08
167.083	0.00	0.03	0.100	O					0.08
167.167	0.00	0.03	0.099	O					0.08
167.250	0.00	0.03	0.099	O					0.08
167.333	0.00	0.03	0.099	O					0.08
167.417	0.00	0.03	0.099	O					0.08
167.500	0.00	0.03	0.099	O					0.08
167.583	0.00	0.03	0.098	O					0.08
167.667	0.00	0.03	0.098	O					0.08
167.750	0.00	0.03	0.098	O					0.08
167.833	0.00	0.03	0.098	O					0.08
167.917	0.00	0.03	0.098	O					0.08
168.000	0.00	0.03	0.097	O					0.08
168.083	0.00	0.03	0.097	O					0.08
168.167	0.00	0.03	0.097	O					0.08
168.250	0.00	0.03	0.097	O					0.08
168.333	0.00	0.03	0.097	O					0.08
168.417	0.00	0.03	0.097	O					0.08
168.500	0.00	0.03	0.096	O					0.08
168.583	0.00	0.03	0.096	O					0.08
168.667	0.00	0.03	0.096	O					0.08
168.750	0.00	0.03	0.096	O					0.08
168.833	0.00	0.03	0.096	O					0.08
168.917	0.00	0.03	0.095	O					0.08
169.000	0.00	0.03	0.095	O					0.08
169.083	0.00	0.03	0.095	O					0.08
169.167	0.00	0.03	0.095	O					0.08
169.250	0.00	0.03	0.095	O					0.08
169.333	0.00	0.03	0.095	O					0.08
169.417	0.00	0.03	0.094	O					0.08
169.500	0.00	0.03	0.094	O					0.08
169.583	0.00	0.03	0.094	O					0.08
169.667	0.00	0.03	0.094	O					0.08
169.750	0.00	0.03	0.094	O					0.08
169.833	0.00	0.03	0.093	O					0.08
169.917	0.00	0.03	0.093	O					0.08
170.000	0.00	0.03	0.093	O					0.08
170.083	0.00	0.03	0.093	O					0.08
170.167	0.00	0.03	0.093	O					0.08
170.250	0.00	0.03	0.093	O					0.08
170.333	0.00	0.03	0.092	O					0.07
170.417	0.00	0.03	0.092	O					0.07
170.500	0.00	0.03	0.092	O					0.07
170.583	0.00	0.03	0.092	O					0.07
170.667	0.00	0.03	0.092	O					0.07
170.750	0.00	0.03	0.091	O					0.07
170.833	0.00	0.03	0.091	O					0.07
170.917	0.00	0.03	0.091	O					0.07
171.000	0.00	0.03	0.091	O					0.07
171.083	0.00	0.03	0.091	O					0.07
171.167	0.00	0.03	0.091	O					0.07
171.250	0.00	0.03	0.090	O					0.07
171.333	0.00	0.03	0.090	O					0.07
171.417	0.00	0.03	0.090	O					0.07
171.500	0.00	0.03	0.090	O					0.07
171.583	0.00	0.03	0.090	O					0.07
171.667	0.00	0.03	0.090	O					0.07
171.750	0.00	0.02	0.089	O					0.07

171.833	0.00	0.02	0.089	O	|	|	|	|	0.07
171.917	0.00	0.02	0.089	O	|	|	|	|	0.07
172.000	0.00	0.02	0.089	O	|	|	|	|	0.07
172.083	0.00	0.02	0.089	O	|	|	|	|	0.07
172.167	0.00	0.02	0.089	O	|	|	|	|	0.07
172.250	0.00	0.02	0.088	O	|	|	|	|	0.07
172.333	0.00	0.02	0.088	O	|	|	|	|	0.07
172.417	0.00	0.02	0.088	O	|	|	|	|	0.07
172.500	0.00	0.02	0.088	O	|	|	|	|	0.07
172.583	0.00	0.02	0.088	O	|	|	|	|	0.07
172.667	0.00	0.02	0.088	O	|	|	|	|	0.07
172.750	0.00	0.02	0.087	O	|	|	|	|	0.07
172.833	0.00	0.02	0.087	O	|	|	|	|	0.07
172.917	0.00	0.02	0.087	O	|	|	|	|	0.07
173.000	0.00	0.02	0.087	O	|	|	|	|	0.07
173.083	0.00	0.02	0.087	O	|	|	|	|	0.07
173.167	0.00	0.02	0.087	O	|	|	|	|	0.07
173.250	0.00	0.02	0.086	O	|	|	|	|	0.07
173.333	0.00	0.02	0.086	O	|	|	|	|	0.07
173.417	0.00	0.02	0.086	O	|	|	|	|	0.07
173.500	0.00	0.02	0.086	O	|	|	|	|	0.07
173.583	0.00	0.02	0.086	O	|	|	|	|	0.07
173.667	0.00	0.02	0.086	O	|	|	|	|	0.07
173.750	0.00	0.02	0.085	O	|	|	|	|	0.07
173.833	0.00	0.02	0.085	O	|	|	|	|	0.07
173.917	0.00	0.02	0.085	O	|	|	|	|	0.07
174.000	0.00	0.02	0.085	O	|	|	|	|	0.07
174.083	0.00	0.02	0.085	O	|	|	|	|	0.07
174.167	0.00	0.02	0.085	O	|	|	|	|	0.07
174.250	0.00	0.02	0.084	O	|	|	|	|	0.07
174.333	0.00	0.02	0.084	O	|	|	|	|	0.07
174.417	0.00	0.02	0.084	O	|	|	|	|	0.07
174.500	0.00	0.02	0.084	O	|	|	|	|	0.07
174.583	0.00	0.02	0.084	O	|	|	|	|	0.07
174.667	0.00	0.02	0.084	O	|	|	|	|	0.07
174.750	0.00	0.02	0.083	O	|	|	|	|	0.07
174.833	0.00	0.02	0.083	O	|	|	|	|	0.07
174.917	0.00	0.02	0.083	O	|	|	|	|	0.07
175.000	0.00	0.02	0.083	O	|	|	|	|	0.07
175.083	0.00	0.02	0.083	O	|	|	|	|	0.07
175.167	0.00	0.02	0.083	O	|	|	|	|	0.07
175.250	0.00	0.02	0.082	O	|	|	|	|	0.07
175.333	0.00	0.02	0.082	O	|	|	|	|	0.07
175.417	0.00	0.02	0.082	O	|	|	|	|	0.07
175.500	0.00	0.02	0.082	O	|	|	|	|	0.07
175.583	0.00	0.02	0.082	O	|	|	|	|	0.07
175.667	0.00	0.02	0.082	O	|	|	|	|	0.07
175.750	0.00	0.02	0.082	O	|	|	|	|	0.07
175.833	0.00	0.02	0.081	O	|	|	|	|	0.07
175.917	0.00	0.02	0.081	O	|	|	|	|	0.07
176.000	0.00	0.02	0.081	O	|	|	|	|	0.07
176.083	0.00	0.02	0.081	O	|	|	|	|	0.07
176.167	0.00	0.02	0.081	O	|	|	|	|	0.07
176.250	0.00	0.02	0.081	O	|	|	|	|	0.07
176.333	0.00	0.02	0.080	O	|	|	|	|	0.07
176.417	0.00	0.02	0.080	O	|	|	|	|	0.07
176.500	0.00	0.02	0.080	O	|	|	|	|	0.07
176.583	0.00	0.02	0.080	O	|	|	|	|	0.06
176.667	0.00	0.02	0.080	O	|	|	|	|	0.06
176.750	0.00	0.02	0.080	O	|	|	|	|	0.06
176.833	0.00	0.02	0.079	O	|	|	|	|	0.06
176.917	0.00	0.02	0.079	O	|	|	|	|	0.06
177.000	0.00	0.02	0.079	O	|	|	|	|	0.06
177.083	0.00	0.02	0.079	O	|	|	|	|	0.06
177.167	0.00	0.02	0.079	O	|	|	|	|	0.06
177.250	0.00	0.02	0.079	O	|	|	|	|	0.06
177.333	0.00	0.02	0.079	O	|	|	|	|	0.06
177.417	0.00	0.02	0.078	O	|	|	|	|	0.06
177.500	0.00	0.02	0.078	O	|	|	|	|	0.06
177.583	0.00	0.02	0.078	O	|	|	|	|	0.06
177.667	0.00	0.02	0.078	O	|	|	|	|	0.06

177.750	0.00	0.02	0.078	O	|	|	|	|	0.06
177.833	0.00	0.02	0.078	O	|	|	|	|	0.06
177.917	0.00	0.02	0.078	O	|	|	|	|	0.06
178.000	0.00	0.02	0.077	O	|	|	|	|	0.06
178.083	0.00	0.02	0.077	O	|	|	|	|	0.06
178.167	0.00	0.02	0.077	O	|	|	|	|	0.06
178.250	0.00	0.02	0.077	O	|	|	|	|	0.06
178.333	0.00	0.02	0.077	O	|	|	|	|	0.06
178.417	0.00	0.02	0.077	O	|	|	|	|	0.06
178.500	0.00	0.02	0.077	O	|	|	|	|	0.06
178.583	0.00	0.02	0.076	O	|	|	|	|	0.06
178.667	0.00	0.02	0.076	O	|	|	|	|	0.06
178.750	0.00	0.02	0.076	O	|	|	|	|	0.06
178.833	0.00	0.02	0.076	O	|	|	|	|	0.06
178.917	0.00	0.02	0.076	O	|	|	|	|	0.06
179.000	0.00	0.02	0.076	O	|	|	|	|	0.06
179.083	0.00	0.02	0.075	O	|	|	|	|	0.06
179.167	0.00	0.02	0.075	O	|	|	|	|	0.06
179.250	0.00	0.02	0.075	O	|	|	|	|	0.06
179.333	0.00	0.02	0.075	O	|	|	|	|	0.06
179.417	0.00	0.02	0.075	O	|	|	|	|	0.06
179.500	0.00	0.02	0.075	O	|	|	|	|	0.06
179.583	0.00	0.02	0.075	O	|	|	|	|	0.06
179.667	0.00	0.02	0.074	O	|	|	|	|	0.06
179.750	0.00	0.02	0.074	O	|	|	|	|	0.06
179.833	0.00	0.02	0.074	O	|	|	|	|	0.06
179.917	0.00	0.02	0.074	O	|	|	|	|	0.06
180.000	0.00	0.02	0.074	O	|	|	|	|	0.06
180.083	0.00	0.02	0.074	O	|	|	|	|	0.06
180.167	0.00	0.02	0.074	O	|	|	|	|	0.06
180.250	0.00	0.02	0.073	O	|	|	|	|	0.06
180.333	0.00	0.02	0.073	O	|	|	|	|	0.06
180.417	0.00	0.02	0.073	O	|	|	|	|	0.06
180.500	0.00	0.02	0.073	O	|	|	|	|	0.06
180.583	0.00	0.02	0.073	O	|	|	|	|	0.06
180.667	0.00	0.02	0.073	O	|	|	|	|	0.06
180.750	0.00	0.02	0.073	O	|	|	|	|	0.06
180.833	0.00	0.02	0.072	O	|	|	|	|	0.06
180.917	0.00	0.02	0.072	O	|	|	|	|	0.06
181.000	0.00	0.02	0.072	O	|	|	|	|	0.06
181.083	0.00	0.02	0.072	O	|	|	|	|	0.06
181.167	0.00	0.02	0.072	O	|	|	|	|	0.06
181.250	0.00	0.02	0.072	O	|	|	|	|	0.06
181.333	0.00	0.02	0.072	O	|	|	|	|	0.06
181.417	0.00	0.02	0.072	O	|	|	|	|	0.06
181.500	0.00	0.02	0.071	O	|	|	|	|	0.06
181.583	0.00	0.02	0.071	O	|	|	|	|	0.06
181.667	0.00	0.02	0.071	O	|	|	|	|	0.06
181.750	0.00	0.02	0.071	O	|	|	|	|	0.06
181.833	0.00	0.02	0.071	O	|	|	|	|	0.06
181.917	0.00	0.02	0.071	O	|	|	|	|	0.06
182.000	0.00	0.02	0.071	O	|	|	|	|	0.06
182.083	0.00	0.02	0.070	O	|	|	|	|	0.06
182.167	0.00	0.02	0.070	O	|	|	|	|	0.06
182.250	0.00	0.02	0.070	O	|	|	|	|	0.06
182.333	0.00	0.02	0.070	O	|	|	|	|	0.06
182.417	0.00	0.02	0.070	O	|	|	|	|	0.06
182.500	0.00	0.02	0.070	O	|	|	|	|	0.06
182.583	0.00	0.02	0.070	O	|	|	|	|	0.06
182.667	0.00	0.02	0.069	O	|	|	|	|	0.06
182.750	0.00	0.02	0.069	O	|	|	|	|	0.06
182.833	0.00	0.02	0.069	O	|	|	|	|	0.06
182.917	0.00	0.02	0.069	O	|	|	|	|	0.06
183.000	0.00	0.02	0.069	O	|	|	|	|	0.06
183.083	0.00	0.02	0.069	O	|	|	|	|	0.06
183.167	0.00	0.02	0.069	O	|	|	|	|	0.06
183.250	0.00	0.02	0.069	O	|	|	|	|	0.06
183.333	0.00	0.02	0.068	O	|	|	|	|	0.06
183.417	0.00	0.02	0.068	O	|	|	|	|	0.06
183.500	0.00	0.02	0.068	O	|	|	|	|	0.06
183.583	0.00	0.02	0.068	O	|	|	|	|	0.06

183.667	0.00	0.02	0.068	O	|	|	|	|	0.06
183.750	0.00	0.02	0.068	O	|	|	|	|	0.06
183.833	0.00	0.02	0.068	O	|	|	|	|	0.05
183.917	0.00	0.02	0.068	O	|	|	|	|	0.05
184.000	0.00	0.02	0.067	O	|	|	|	|	0.05
184.083	0.00	0.02	0.067	O	|	|	|	|	0.05
184.167	0.00	0.02	0.067	O	|	|	|	|	0.05
184.250	0.00	0.02	0.067	O	|	|	|	|	0.05
184.333	0.00	0.02	0.067	O	|	|	|	|	0.05
184.417	0.00	0.02	0.067	O	|	|	|	|	0.05
184.500	0.00	0.02	0.067	O	|	|	|	|	0.05
184.583	0.00	0.02	0.066	O	|	|	|	|	0.05
184.667	0.00	0.02	0.066	O	|	|	|	|	0.05
184.750	0.00	0.02	0.066	O	|	|	|	|	0.05
184.833	0.00	0.02	0.066	O	|	|	|	|	0.05
184.917	0.00	0.02	0.066	O	|	|	|	|	0.05
185.000	0.00	0.02	0.066	O	|	|	|	|	0.05
185.083	0.00	0.02	0.066	O	|	|	|	|	0.05
185.167	0.00	0.02	0.066	O	|	|	|	|	0.05
185.250	0.00	0.02	0.065	O	|	|	|	|	0.05
185.333	0.00	0.02	0.065	O	|	|	|	|	0.05
185.417	0.00	0.02	0.065	O	|	|	|	|	0.05
185.500	0.00	0.02	0.065	O	|	|	|	|	0.05
185.583	0.00	0.02	0.065	O	|	|	|	|	0.05
185.667	0.00	0.02	0.065	O	|	|	|	|	0.05
185.750	0.00	0.02	0.065	O	|	|	|	|	0.05
185.833	0.00	0.02	0.065	O	|	|	|	|	0.05
185.917	0.00	0.02	0.064	O	|	|	|	|	0.05
186.000	0.00	0.02	0.064	O	|	|	|	|	0.05
186.083	0.00	0.02	0.064	O	|	|	|	|	0.05
186.167	0.00	0.02	0.064	O	|	|	|	|	0.05
186.250	0.00	0.02	0.064	O	|	|	|	|	0.05
186.333	0.00	0.02	0.064	O	|	|	|	|	0.05
186.417	0.00	0.02	0.064	O	|	|	|	|	0.05
186.500	0.00	0.02	0.064	O	|	|	|	|	0.05
186.583	0.00	0.02	0.063	O	|	|	|	|	0.05
186.667	0.00	0.02	0.063	O	|	|	|	|	0.05
186.750	0.00	0.02	0.063	O	|	|	|	|	0.05
186.833	0.00	0.02	0.063	O	|	|	|	|	0.05
186.917	0.00	0.02	0.063	O	|	|	|	|	0.05
187.000	0.00	0.02	0.063	O	|	|	|	|	0.05
187.083	0.00	0.02	0.063	O	|	|	|	|	0.05
187.167	0.00	0.02	0.063	O	|	|	|	|	0.05
187.250	0.00	0.02	0.063	O	|	|	|	|	0.05
187.333	0.00	0.02	0.062	O	|	|	|	|	0.05
187.417	0.00	0.02	0.062	O	|	|	|	|	0.05
187.500	0.00	0.02	0.062	O	|	|	|	|	0.05
187.583	0.00	0.02	0.062	O	|	|	|	|	0.05
187.667	0.00	0.02	0.062	O	|	|	|	|	0.05
187.750	0.00	0.02	0.062	O	|	|	|	|	0.05
187.833	0.00	0.02	0.062	O	|	|	|	|	0.05
187.917	0.00	0.02	0.062	O	|	|	|	|	0.05
188.000	0.00	0.02	0.061	O	|	|	|	|	0.05
188.083	0.00	0.02	0.061	O	|	|	|	|	0.05
188.167	0.00	0.02	0.061	O	|	|	|	|	0.05
188.250	0.00	0.02	0.061	O	|	|	|	|	0.05
188.333	0.00	0.02	0.061	O	|	|	|	|	0.05
188.417	0.00	0.02	0.061	O	|	|	|	|	0.05
188.500	0.00	0.02	0.061	O	|	|	|	|	0.05
188.583	0.00	0.02	0.061	O	|	|	|	|	0.05
188.667	0.00	0.02	0.061	O	|	|	|	|	0.05
188.750	0.00	0.02	0.060	O	|	|	|	|	0.05
188.833	0.00	0.02	0.060	O	|	|	|	|	0.05
188.917	0.00	0.02	0.060	O	|	|	|	|	0.05
189.000	0.00	0.02	0.060	O	|	|	|	|	0.05
189.083	0.00	0.02	0.060	O	|	|	|	|	0.05
189.167	0.00	0.02	0.060	O	|	|	|	|	0.05
189.250	0.00	0.02	0.060	O	|	|	|	|	0.05
189.333	0.00	0.02	0.060	O	|	|	|	|	0.05
189.417	0.00	0.02	0.059	O	|	|	|	|	0.05
189.500	0.00	0.02	0.059	O	|	|	|	|	0.05

189.583	0.00	0.02	0.059	O	|	|	|	|	0.05
189.667	0.00	0.02	0.059	O	|	|	|	|	0.05
189.750	0.00	0.02	0.059	O	|	|	|	|	0.05
189.833	0.00	0.02	0.059	O	|	|	|	|	0.05
189.917	0.00	0.02	0.059	O	|	|	|	|	0.05
190.000	0.00	0.02	0.059	O	|	|	|	|	0.05
190.083	0.00	0.02	0.059	O	|	|	|	|	0.05
190.167	0.00	0.02	0.058	O	|	|	|	|	0.05
190.250	0.00	0.02	0.058	O	|	|	|	|	0.05
190.333	0.00	0.02	0.058	O	|	|	|	|	0.05
190.417	0.00	0.02	0.058	O	|	|	|	|	0.05
190.500	0.00	0.02	0.058	O	|	|	|	|	0.05
190.583	0.00	0.02	0.058	O	|	|	|	|	0.05
190.667	0.00	0.02	0.058	O	|	|	|	|	0.05
190.750	0.00	0.02	0.058	O	|	|	|	|	0.05
190.833	0.00	0.02	0.058	O	|	|	|	|	0.05
190.917	0.00	0.02	0.057	O	|	|	|	|	0.05
191.000	0.00	0.02	0.057	O	|	|	|	|	0.05
191.083	0.00	0.02	0.057	O	|	|	|	|	0.05
191.167	0.00	0.02	0.057	O	|	|	|	|	0.05
191.250	0.00	0.02	0.057	O	|	|	|	|	0.05
191.333	0.00	0.02	0.057	O	|	|	|	|	0.05
191.417	0.00	0.02	0.057	O	|	|	|	|	0.05
191.500	0.00	0.02	0.057	O	|	|	|	|	0.05
191.583	0.00	0.02	0.057	O	|	|	|	|	0.05
191.667	0.00	0.02	0.056	O	|	|	|	|	0.05
191.750	0.00	0.02	0.056	O	|	|	|	|	0.05
191.833	0.00	0.02	0.056	O	|	|	|	|	0.05
191.917	0.00	0.02	0.056	O	|	|	|	|	0.05
192.000	0.00	0.02	0.056	O	|	|	|	|	0.05
192.083	0.00	0.02	0.056	O	|	|	|	|	0.05
192.167	0.00	0.02	0.056	O	|	|	|	|	0.05
192.250	0.00	0.02	0.056	O	|	|	|	|	0.05
192.333	0.00	0.02	0.056	O	|	|	|	|	0.05
192.417	0.00	0.02	0.055	O	|	|	|	|	0.05
192.500	0.00	0.02	0.055	O	|	|	|	|	0.04
192.583	0.00	0.02	0.055	O	|	|	|	|	0.04
192.667	0.00	0.02	0.055	O	|	|	|	|	0.04
192.750	0.00	0.02	0.055	O	|	|	|	|	0.04
192.833	0.00	0.02	0.055	O	|	|	|	|	0.04
192.917	0.00	0.02	0.055	O	|	|	|	|	0.04
193.000	0.00	0.02	0.055	O	|	|	|	|	0.04
193.083	0.00	0.02	0.055	O	|	|	|	|	0.04
193.167	0.00	0.02	0.055	O	|	|	|	|	0.04
193.250	0.00	0.02	0.054	O	|	|	|	|	0.04
193.333	0.00	0.02	0.054	O	|	|	|	|	0.04
193.417	0.00	0.02	0.054	O	|	|	|	|	0.04
193.500	0.00	0.02	0.054	O	|	|	|	|	0.04
193.583	0.00	0.02	0.054	O	|	|	|	|	0.04
193.667	0.00	0.02	0.054	O	|	|	|	|	0.04
193.750	0.00	0.02	0.054	O	|	|	|	|	0.04
193.833	0.00	0.01	0.054	O	|	|	|	|	0.04
193.917	0.00	0.01	0.054	O	|	|	|	|	0.04
194.000	0.00	0.01	0.053	O	|	|	|	|	0.04
194.083	0.00	0.01	0.053	O	|	|	|	|	0.04
194.167	0.00	0.01	0.053	O	|	|	|	|	0.04
194.250	0.00	0.01	0.053	O	|	|	|	|	0.04
194.333	0.00	0.01	0.053	O	|	|	|	|	0.04
194.417	0.00	0.01	0.053	O	|	|	|	|	0.04
194.500	0.00	0.01	0.053	O	|	|	|	|	0.04
194.583	0.00	0.01	0.053	O	|	|	|	|	0.04
194.667	0.00	0.01	0.053	O	|	|	|	|	0.04
194.750	0.00	0.01	0.053	O	|	|	|	|	0.04
194.833	0.00	0.01	0.052	O	|	|	|	|	0.04
194.917	0.00	0.01	0.052	O	|	|	|	|	0.04
195.000	0.00	0.01	0.052	O	|	|	|	|	0.04
195.083	0.00	0.01	0.052	O	|	|	|	|	0.04
195.167	0.00	0.01	0.052	O	|	|	|	|	0.04
195.250	0.00	0.01	0.052	O	|	|	|	|	0.04
195.333	0.00	0.01	0.052	O	|	|	|	|	0.04
195.417	0.00	0.01	0.052	O	|	|	|	|	0.04

195.500	0.00	0.01	0.052	O	|	|	|	|	0.04
195.583	0.00	0.01	0.052	O	|	|	|	|	0.04
195.667	0.00	0.01	0.051	O	|	|	|	|	0.04
195.750	0.00	0.01	0.051	O	|	|	|	|	0.04
195.833	0.00	0.01	0.051	O	|	|	|	|	0.04
195.917	0.00	0.01	0.051	O	|	|	|	|	0.04
196.000	0.00	0.01	0.051	O	|	|	|	|	0.04
196.083	0.00	0.01	0.051	O	|	|	|	|	0.04
196.167	0.00	0.01	0.051	O	|	|	|	|	0.04
196.250	0.00	0.01	0.051	O	|	|	|	|	0.04
196.333	0.00	0.01	0.051	O	|	|	|	|	0.04
196.417	0.00	0.01	0.051	O	|	|	|	|	0.04
196.500	0.00	0.01	0.050	O	|	|	|	|	0.04
196.583	0.00	0.01	0.050	O	|	|	|	|	0.04
196.667	0.00	0.01	0.050	O	|	|	|	|	0.04
196.750	0.00	0.01	0.050	O	|	|	|	|	0.04
196.833	0.00	0.01	0.050	O	|	|	|	|	0.04
196.917	0.00	0.01	0.050	O	|	|	|	|	0.04
197.000	0.00	0.01	0.050	O	|	|	|	|	0.04
197.083	0.00	0.01	0.050	O	|	|	|	|	0.04
197.167	0.00	0.01	0.050	O	|	|	|	|	0.04
197.250	0.00	0.01	0.050	O	|	|	|	|	0.04
197.333	0.00	0.01	0.050	O	|	|	|	|	0.04
197.417	0.00	0.01	0.049	O	|	|	|	|	0.04
197.500	0.00	0.01	0.049	O	|	|	|	|	0.04
197.583	0.00	0.01	0.049	O	|	|	|	|	0.04
197.667	0.00	0.01	0.049	O	|	|	|	|	0.04
197.750	0.00	0.01	0.049	O	|	|	|	|	0.04
197.833	0.00	0.01	0.049	O	|	|	|	|	0.04
197.917	0.00	0.01	0.049	O	|	|	|	|	0.04
198.000	0.00	0.01	0.049	O	|	|	|	|	0.04
198.083	0.00	0.01	0.049	O	|	|	|	|	0.04
198.167	0.00	0.01	0.049	O	|	|	|	|	0.04
198.250	0.00	0.01	0.048	O	|	|	|	|	0.04
198.333	0.00	0.01	0.048	O	|	|	|	|	0.04
198.417	0.00	0.01	0.048	O	|	|	|	|	0.04
198.500	0.00	0.01	0.048	O	|	|	|	|	0.04
198.583	0.00	0.01	0.048	O	|	|	|	|	0.04
198.667	0.00	0.01	0.048	O	|	|	|	|	0.04
198.750	0.00	0.01	0.048	O	|	|	|	|	0.04
198.833	0.00	0.01	0.048	O	|	|	|	|	0.04
198.917	0.00	0.01	0.048	O	|	|	|	|	0.04
199.000	0.00	0.01	0.048	O	|	|	|	|	0.04
199.083	0.00	0.01	0.048	O	|	|	|	|	0.04
199.167	0.00	0.01	0.047	O	|	|	|	|	0.04
199.250	0.00	0.01	0.047	O	|	|	|	|	0.04
199.333	0.00	0.01	0.047	O	|	|	|	|	0.04
199.417	0.00	0.01	0.047	O	|	|	|	|	0.04
199.500	0.00	0.01	0.047	O	|	|	|	|	0.04
199.583	0.00	0.01	0.047	O	|	|	|	|	0.04
199.667	0.00	0.01	0.047	O	|	|	|	|	0.04
199.750	0.00	0.01	0.047	O	|	|	|	|	0.04
199.833	0.00	0.01	0.047	O	|	|	|	|	0.04
199.917	0.00	0.01	0.047	O	|	|	|	|	0.04
200.000	0.00	0.01	0.047	O	|	|	|	|	0.04
200.083	0.00	0.01	0.046	O	|	|	|	|	0.04
200.167	0.00	0.01	0.046	O	|	|	|	|	0.04
200.250	0.00	0.01	0.046	O	|	|	|	|	0.04
200.333	0.00	0.01	0.046	O	|	|	|	|	0.04
200.417	0.00	0.01	0.046	O	|	|	|	|	0.04
200.500	0.00	0.01	0.046	O	|	|	|	|	0.04
200.583	0.00	0.01	0.046	O	|	|	|	|	0.04
200.667	0.00	0.01	0.046	O	|	|	|	|	0.04
200.750	0.00	0.01	0.046	O	|	|	|	|	0.04
200.833	0.00	0.01	0.046	O	|	|	|	|	0.04
200.917	0.00	0.01	0.046	O	|	|	|	|	0.04
201.000	0.00	0.01	0.046	O	|	|	|	|	0.04
201.083	0.00	0.01	0.045	O	|	|	|	|	0.04
201.167	0.00	0.01	0.045	O	|	|	|	|	0.04
201.250	0.00	0.01	0.045	O	|	|	|	|	0.04
201.333	0.00	0.01	0.045	O	|	|	|	|	0.04

201.417	0.00	0.01	0.045	O	|	|	|	|	0.04
201.500	0.00	0.01	0.045	O	|	|	|	|	0.04
201.583	0.00	0.01	0.045	O	|	|	|	|	0.04
201.667	0.00	0.01	0.045	O	|	|	|	|	0.04
201.750	0.00	0.01	0.045	O	|	|	|	|	0.04
201.833	0.00	0.01	0.045	O	|	|	|	|	0.04
201.917	0.00	0.01	0.045	O	|	|	|	|	0.04
202.000	0.00	0.01	0.044	O	|	|	|	|	0.04
202.083	0.00	0.01	0.044	O	|	|	|	|	0.04
202.167	0.00	0.01	0.044	O	|	|	|	|	0.04
202.250	0.00	0.01	0.044	O	|	|	|	|	0.04
202.333	0.00	0.01	0.044	O	|	|	|	|	0.04
202.417	0.00	0.01	0.044	O	|	|	|	|	0.04
202.500	0.00	0.01	0.044	O	|	|	|	|	0.04
202.583	0.00	0.01	0.044	O	|	|	|	|	0.04
202.667	0.00	0.01	0.044	O	|	|	|	|	0.04
202.750	0.00	0.01	0.044	O	|	|	|	|	0.04
202.833	0.00	0.01	0.044	O	|	|	|	|	0.04
202.917	0.00	0.01	0.044	O	|	|	|	|	0.04
203.000	0.00	0.01	0.043	O	|	|	|	|	0.04
203.083	0.00	0.01	0.043	O	|	|	|	|	0.04
203.167	0.00	0.01	0.043	O	|	|	|	|	0.04
203.250	0.00	0.01	0.043	O	|	|	|	|	0.04
203.333	0.00	0.01	0.043	O	|	|	|	|	0.04
203.417	0.00	0.01	0.043	O	|	|	|	|	0.03
203.500	0.00	0.01	0.043	O	|	|	|	|	0.03
203.583	0.00	0.01	0.043	O	|	|	|	|	0.03
203.667	0.00	0.01	0.043	O	|	|	|	|	0.03
203.750	0.00	0.01	0.043	O	|	|	|	|	0.03
203.833	0.00	0.01	0.043	O	|	|	|	|	0.03
203.917	0.00	0.01	0.043	O	|	|	|	|	0.03
204.000	0.00	0.01	0.042	O	|	|	|	|	0.03
204.083	0.00	0.01	0.042	O	|	|	|	|	0.03
204.167	0.00	0.01	0.042	O	|	|	|	|	0.03
204.250	0.00	0.01	0.042	O	|	|	|	|	0.03
204.333	0.00	0.01	0.042	O	|	|	|	|	0.03
204.417	0.00	0.01	0.042	O	|	|	|	|	0.03
204.500	0.00	0.01	0.042	O	|	|	|	|	0.03
204.583	0.00	0.01	0.042	O	|	|	|	|	0.03
204.667	0.00	0.01	0.042	O	|	|	|	|	0.03
204.750	0.00	0.01	0.042	O	|	|	|	|	0.03
204.833	0.00	0.01	0.042	O	|	|	|	|	0.03
204.917	0.00	0.01	0.042	O	|	|	|	|	0.03
205.000	0.00	0.01	0.042	O	|	|	|	|	0.03
205.083	0.00	0.01	0.041	O	|	|	|	|	0.03
205.167	0.00	0.01	0.041	O	|	|	|	|	0.03
205.250	0.00	0.01	0.041	O	|	|	|	|	0.03
205.333	0.00	0.01	0.041	O	|	|	|	|	0.03
205.417	0.00	0.01	0.041	O	|	|	|	|	0.03
205.500	0.00	0.01	0.041	O	|	|	|	|	0.03
205.583	0.00	0.01	0.041	O	|	|	|	|	0.03
205.667	0.00	0.01	0.041	O	|	|	|	|	0.03
205.750	0.00	0.01	0.041	O	|	|	|	|	0.03
205.833	0.00	0.01	0.041	O	|	|	|	|	0.03
205.917	0.00	0.01	0.041	O	|	|	|	|	0.03
206.000	0.00	0.01	0.041	O	|	|	|	|	0.03
206.083	0.00	0.01	0.040	O	|	|	|	|	0.03
206.167	0.00	0.01	0.040	O	|	|	|	|	0.03
206.250	0.00	0.01	0.040	O	|	|	|	|	0.03
206.333	0.00	0.01	0.040	O	|	|	|	|	0.03
206.417	0.00	0.01	0.040	O	|	|	|	|	0.03
206.500	0.00	0.01	0.040	O	|	|	|	|	0.03
206.583	0.00	0.01	0.040	O	|	|	|	|	0.03
206.667	0.00	0.01	0.040	O	|	|	|	|	0.03
206.750	0.00	0.01	0.040	O	|	|	|	|	0.03
206.833	0.00	0.01	0.040	O	|	|	|	|	0.03
206.917	0.00	0.01	0.040	O	|	|	|	|	0.03
207.000	0.00	0.01	0.040	O	|	|	|	|	0.03
207.083	0.00	0.01	0.040	O	|	|	|	|	0.03
207.167	0.00	0.01	0.039	O	|	|	|	|	0.03
207.250	0.00	0.01	0.039	O	|	|	|	|	0.03

207.333	0.00	0.01	0.039	O					0.03
207.417	0.00	0.01	0.039	O					0.03
207.500	0.00	0.01	0.039	O					0.03
207.583	0.00	0.01	0.039	O					0.03
207.667	0.00	0.01	0.039	O					0.03
207.750	0.00	0.01	0.039	O					0.03
207.833	0.00	0.01	0.039	O					0.03
207.917	0.00	0.01	0.039	O					0.03
208.000	0.00	0.01	0.039	O					0.03
208.083	0.00	0.01	0.039	O					0.03
208.167	0.00	0.01	0.039	O					0.03
208.250	0.00	0.01	0.039	O					0.03
208.333	0.00	0.01	0.038	O					0.03
208.417	0.00	0.01	0.038	O					0.03
208.500	0.00	0.01	0.038	O					0.03
208.583	0.00	0.01	0.038	O					0.03
208.667	0.00	0.01	0.038	O					0.03
208.750	0.00	0.01	0.038	O					0.03
208.833	0.00	0.01	0.038	O					0.03
208.917	0.00	0.01	0.038	O					0.03
209.000	0.00	0.01	0.038	O					0.03
209.083	0.00	0.01	0.038	O					0.03
209.167	0.00	0.01	0.038	O					0.03
209.250	0.00	0.01	0.038	O					0.03
209.333	0.00	0.01	0.038	O					0.03
209.417	0.00	0.01	0.037	O					0.03
209.500	0.00	0.01	0.037	O					0.03
209.583	0.00	0.01	0.037	O					0.03
209.667	0.00	0.01	0.037	O					0.03
209.750	0.00	0.01	0.037	O					0.03
209.833	0.00	0.01	0.037	O					0.03
209.917	0.00	0.01	0.037	O					0.03
210.000	0.00	0.01	0.037	O					0.03
210.083	0.00	0.01	0.037	O					0.03
210.167	0.00	0.01	0.037	O					0.03
210.250	0.00	0.01	0.037	O					0.03
210.333	0.00	0.01	0.037	O					0.03
210.417	0.00	0.01	0.037	O					0.03
210.500	0.00	0.01	0.037	O					0.03
210.583	0.00	0.01	0.036	O					0.03
210.667	0.00	0.01	0.036	O					0.03
210.750	0.00	0.01	0.036	O					0.03
210.833	0.00	0.01	0.036	O					0.03
210.917	0.00	0.01	0.036	O					0.03
211.000	0.00	0.01	0.036	O					0.03
211.083	0.00	0.01	0.036	O					0.03
211.167	0.00	0.01	0.036	O					0.03
211.250	0.00	0.01	0.036	O					0.03
211.333	0.00	0.01	0.036	O					0.03
211.417	0.00	0.01	0.036	O					0.03
211.500	0.00	0.01	0.036	O					0.03
211.583	0.00	0.01	0.036	O					0.03
211.667	0.00	0.01	0.036	O					0.03
211.750	0.00	0.01	0.036	O					0.03
211.833	0.00	0.01	0.035	O					0.03
211.917	0.00	0.01	0.035	O					0.03
212.000	0.00	0.01	0.035	O					0.03
212.083	0.00	0.01	0.035	O					0.03
212.167	0.00	0.01	0.035	O					0.03
212.250	0.00	0.01	0.035	O					0.03
212.333	0.00	0.01	0.035	O					0.03
212.417	0.00	0.01	0.035	O					0.03
212.500	0.00	0.01	0.035	O					0.03
212.583	0.00	0.01	0.035	O					0.03
212.667	0.00	0.01	0.035	O					0.03
212.750	0.00	0.01	0.035	O					0.03
212.833	0.00	0.01	0.035	O					0.03
212.917	0.00	0.01	0.035	O					0.03
213.000	0.00	0.01	0.035	O					0.03
213.083	0.00	0.01	0.034	O					0.03
213.167	0.00	0.01	0.034	O					0.03

213.250	0.00	0.01	0.034	O	|	|	|	|	0.03
213.333	0.00	0.01	0.034	O	|	|	|	|	0.03
213.417	0.00	0.01	0.034	O	|	|	|	|	0.03
213.500	0.00	0.01	0.034	O	|	|	|	|	0.03
213.583	0.00	0.01	0.034	O	|	|	|	|	0.03
213.667	0.00	0.01	0.034	O	|	|	|	|	0.03
213.750	0.00	0.01	0.034	O	|	|	|	|	0.03
213.833	0.00	0.01	0.034	O	|	|	|	|	0.03
213.917	0.00	0.01	0.034	O	|	|	|	|	0.03
214.000	0.00	0.01	0.034	O	|	|	|	|	0.03
214.083	0.00	0.01	0.034	O	|	|	|	|	0.03
214.167	0.00	0.01	0.034	O	|	|	|	|	0.03
214.250	0.00	0.01	0.034	O	|	|	|	|	0.03
214.333	0.00	0.01	0.033	O	|	|	|	|	0.03
214.417	0.00	0.01	0.033	O	|	|	|	|	0.03
214.500	0.00	0.01	0.033	O	|	|	|	|	0.03
214.583	0.00	0.01	0.033	O	|	|	|	|	0.03
214.667	0.00	0.01	0.033	O	|	|	|	|	0.03
214.750	0.00	0.01	0.033	O	|	|	|	|	0.03
214.833	0.00	0.01	0.033	O	|	|	|	|	0.03
214.917	0.00	0.01	0.033	O	|	|	|	|	0.03
215.000	0.00	0.01	0.033	O	|	|	|	|	0.03
215.083	0.00	0.01	0.033	O	|	|	|	|	0.03
215.167	0.00	0.01	0.033	O	|	|	|	|	0.03
215.250	0.00	0.01	0.033	O	|	|	|	|	0.03
215.333	0.00	0.01	0.033	O	|	|	|	|	0.03
215.417	0.00	0.01	0.033	O	|	|	|	|	0.03
215.500	0.00	0.01	0.033	O	|	|	|	|	0.03
215.583	0.00	0.01	0.033	O	|	|	|	|	0.03
215.667	0.00	0.01	0.032	O	|	|	|	|	0.03
215.750	0.00	0.01	0.032	O	|	|	|	|	0.03
215.833	0.00	0.01	0.032	O	|	|	|	|	0.03
215.917	0.00	0.01	0.032	O	|	|	|	|	0.03
216.000	0.00	0.01	0.032	O	|	|	|	|	0.03
216.083	0.00	0.01	0.032	O	|	|	|	|	0.03
216.167	0.00	0.01	0.032	O	|	|	|	|	0.03
216.250	0.00	0.01	0.032	O	|	|	|	|	0.03
216.333	0.00	0.01	0.032	O	|	|	|	|	0.03
216.417	0.00	0.01	0.032	O	|	|	|	|	0.03
216.500	0.00	0.01	0.032	O	|	|	|	|	0.03
216.583	0.00	0.01	0.032	O	|	|	|	|	0.03
216.667	0.00	0.01	0.032	O	|	|	|	|	0.03
216.750	0.00	0.01	0.032	O	|	|	|	|	0.03
216.833	0.00	0.01	0.032	O	|	|	|	|	0.03
216.917	0.00	0.01	0.032	O	|	|	|	|	0.03
217.000	0.00	0.01	0.031	O	|	|	|	|	0.03
217.083	0.00	0.01	0.031	O	|	|	|	|	0.03
217.167	0.00	0.01	0.031	O	|	|	|	|	0.03
217.250	0.00	0.01	0.031	O	|	|	|	|	0.03
217.333	0.00	0.01	0.031	O	|	|	|	|	0.03
217.417	0.00	0.01	0.031	O	|	|	|	|	0.03
217.500	0.00	0.01	0.031	O	|	|	|	|	0.03
217.583	0.00	0.01	0.031	O	|	|	|	|	0.03
217.667	0.00	0.01	0.031	O	|	|	|	|	0.03
217.750	0.00	0.01	0.031	O	|	|	|	|	0.03
217.833	0.00	0.01	0.031	O	|	|	|	|	0.03
217.917	0.00	0.01	0.031	O	|	|	|	|	0.03
218.000	0.00	0.01	0.031	O	|	|	|	|	0.02
218.083	0.00	0.01	0.031	O	|	|	|	|	0.02
218.167	0.00	0.01	0.031	O	|	|	|	|	0.02
218.250	0.00	0.01	0.031	O	|	|	|	|	0.02
218.333	0.00	0.01	0.031	O	|	|	|	|	0.02
218.417	0.00	0.01	0.030	O	|	|	|	|	0.02
218.500	0.00	0.01	0.030	O	|	|	|	|	0.02
218.583	0.00	0.01	0.030	O	|	|	|	|	0.02
218.667	0.00	0.01	0.030	O	|	|	|	|	0.02
218.750	0.00	0.01	0.030	O	|	|	|	|	0.02
218.833	0.00	0.01	0.030	O	|	|	|	|	0.02
218.917	0.00	0.01	0.030	O	|	|	|	|	0.02
219.000	0.00	0.01	0.030	O	|	|	|	|	0.02
219.083	0.00	0.01	0.030	O	|	|	|	|	0.02

219.167	0.00	0.01	0.030	O	|	|	|	|	0.02
219.250	0.00	0.01	0.030	O	|	|	|	|	0.02
219.333	0.00	0.01	0.030	O	|	|	|	|	0.02
219.417	0.00	0.01	0.030	O	|	|	|	|	0.02
219.500	0.00	0.01	0.030	O	|	|	|	|	0.02
219.583	0.00	0.01	0.030	O	|	|	|	|	0.02
219.667	0.00	0.01	0.030	O	|	|	|	|	0.02
219.750	0.00	0.01	0.030	O	|	|	|	|	0.02
219.833	0.00	0.01	0.029	O	|	|	|	|	0.02
219.917	0.00	0.01	0.029	O	|	|	|	|	0.02
220.000	0.00	0.01	0.029	O	|	|	|	|	0.02
220.083	0.00	0.01	0.029	O	|	|	|	|	0.02
220.167	0.00	0.01	0.029	O	|	|	|	|	0.02
220.250	0.00	0.01	0.029	O	|	|	|	|	0.02
220.333	0.00	0.01	0.029	O	|	|	|	|	0.02
220.417	0.00	0.01	0.029	O	|	|	|	|	0.02
220.500	0.00	0.01	0.029	O	|	|	|	|	0.02
220.583	0.00	0.01	0.029	O	|	|	|	|	0.02
220.667	0.00	0.01	0.029	O	|	|	|	|	0.02
220.750	0.00	0.01	0.029	O	|	|	|	|	0.02
220.833	0.00	0.01	0.029	O	|	|	|	|	0.02
220.917	0.00	0.01	0.029	O	|	|	|	|	0.02
221.000	0.00	0.01	0.029	O	|	|	|	|	0.02
221.083	0.00	0.01	0.029	O	|	|	|	|	0.02
221.167	0.00	0.01	0.029	O	|	|	|	|	0.02
221.250	0.00	0.01	0.029	O	|	|	|	|	0.02
221.333	0.00	0.01	0.028	O	|	|	|	|	0.02
221.417	0.00	0.01	0.028	O	|	|	|	|	0.02
221.500	0.00	0.01	0.028	O	|	|	|	|	0.02
221.583	0.00	0.01	0.028	O	|	|	|	|	0.02
221.667	0.00	0.01	0.028	O	|	|	|	|	0.02
221.750	0.00	0.01	0.028	O	|	|	|	|	0.02
221.833	0.00	0.01	0.028	O	|	|	|	|	0.02
221.917	0.00	0.01	0.028	O	|	|	|	|	0.02
222.000	0.00	0.01	0.028	O	|	|	|	|	0.02
222.083	0.00	0.01	0.028	O	|	|	|	|	0.02
222.167	0.00	0.01	0.028	O	|	|	|	|	0.02
222.250	0.00	0.01	0.028	O	|	|	|	|	0.02
222.333	0.00	0.01	0.028	O	|	|	|	|	0.02
222.417	0.00	0.01	0.028	O	|	|	|	|	0.02
222.500	0.00	0.01	0.028	O	|	|	|	|	0.02
222.583	0.00	0.01	0.028	O	|	|	|	|	0.02
222.667	0.00	0.01	0.028	O	|	|	|	|	0.02
222.750	0.00	0.01	0.028	O	|	|	|	|	0.02
222.833	0.00	0.01	0.028	O	|	|	|	|	0.02
222.917	0.00	0.01	0.027	O	|	|	|	|	0.02
223.000	0.00	0.01	0.027	O	|	|	|	|	0.02
223.083	0.00	0.01	0.027	O	|	|	|	|	0.02
223.167	0.00	0.01	0.027	O	|	|	|	|	0.02
223.250	0.00	0.01	0.027	O	|	|	|	|	0.02
223.333	0.00	0.01	0.027	O	|	|	|	|	0.02
223.417	0.00	0.01	0.027	O	|	|	|	|	0.02
223.500	0.00	0.01	0.027	O	|	|	|	|	0.02
223.583	0.00	0.01	0.027	O	|	|	|	|	0.02
223.667	0.00	0.01	0.027	O	|	|	|	|	0.02
223.750	0.00	0.01	0.027	O	|	|	|	|	0.02
223.833	0.00	0.01	0.027	O	|	|	|	|	0.02
223.917	0.00	0.01	0.027	O	|	|	|	|	0.02
224.000	0.00	0.01	0.027	O	|	|	|	|	0.02
224.083	0.00	0.01	0.027	O	|	|	|	|	0.02
224.167	0.00	0.01	0.027	O	|	|	|	|	0.02
224.250	0.00	0.01	0.027	O	|	|	|	|	0.02
224.333	0.00	0.01	0.027	O	|	|	|	|	0.02
224.417	0.00	0.01	0.027	O	|	|	|	|	0.02
224.500	0.00	0.01	0.026	O	|	|	|	|	0.02
224.583	0.00	0.01	0.026	O	|	|	|	|	0.02
224.667	0.00	0.01	0.026	O	|	|	|	|	0.02
224.750	0.00	0.01	0.026	O	|	|	|	|	0.02
224.833	0.00	0.01	0.026	O	|	|	|	|	0.02
224.917	0.00	0.01	0.026	O	|	|	|	|	0.02
225.000	0.00	0.01	0.026	O	|	|	|	|	0.02

225.083	0.00	0.01	0.026	O	|	|	|	|	0.02
225.167	0.00	0.01	0.026	O	|	|	|	|	0.02
225.250	0.00	0.01	0.026	O	|	|	|	|	0.02
225.333	0.00	0.01	0.026	O	|	|	|	|	0.02
225.417	0.00	0.01	0.026	O	|	|	|	|	0.02
225.500	0.00	0.01	0.026	O	|	|	|	|	0.02
225.583	0.00	0.01	0.026	O	|	|	|	|	0.02
225.667	0.00	0.01	0.026	O	|	|	|	|	0.02
225.750	0.00	0.01	0.026	O	|	|	|	|	0.02
225.833	0.00	0.01	0.026	O	|	|	|	|	0.02
225.917	0.00	0.01	0.026	O	|	|	|	|	0.02
226.000	0.00	0.01	0.026	O	|	|	|	|	0.02
226.083	0.00	0.01	0.026	O	|	|	|	|	0.02
226.167	0.00	0.01	0.025	O	|	|	|	|	0.02
226.250	0.00	0.01	0.025	O	|	|	|	|	0.02
226.333	0.00	0.01	0.025	O	|	|	|	|	0.02
226.417	0.00	0.01	0.025	O	|	|	|	|	0.02
226.500	0.00	0.01	0.025	O	|	|	|	|	0.02
226.583	0.00	0.01	0.025	O	|	|	|	|	0.02
226.667	0.00	0.01	0.025	O	|	|	|	|	0.02
226.750	0.00	0.01	0.025	O	|	|	|	|	0.02
226.833	0.00	0.01	0.025	O	|	|	|	|	0.02
226.917	0.00	0.01	0.025	O	|	|	|	|	0.02
227.000	0.00	0.01	0.025	O	|	|	|	|	0.02
227.083	0.00	0.01	0.025	O	|	|	|	|	0.02
227.167	0.00	0.01	0.025	O	|	|	|	|	0.02
227.250	0.00	0.01	0.025	O	|	|	|	|	0.02
227.333	0.00	0.01	0.025	O	|	|	|	|	0.02
227.417	0.00	0.01	0.025	O	|	|	|	|	0.02
227.500	0.00	0.01	0.025	O	|	|	|	|	0.02
227.583	0.00	0.01	0.025	O	|	|	|	|	0.02
227.667	0.00	0.01	0.025	O	|	|	|	|	0.02
227.750	0.00	0.01	0.025	O	|	|	|	|	0.02
227.833	0.00	0.01	0.025	O	|	|	|	|	0.02
227.917	0.00	0.01	0.024	O	|	|	|	|	0.02
228.000	0.00	0.01	0.024	O	|	|	|	|	0.02
228.083	0.00	0.01	0.024	O	|	|	|	|	0.02
228.167	0.00	0.01	0.024	O	|	|	|	|	0.02
228.250	0.00	0.01	0.024	O	|	|	|	|	0.02
228.333	0.00	0.01	0.024	O	|	|	|	|	0.02
228.417	0.00	0.01	0.024	O	|	|	|	|	0.02
228.500	0.00	0.01	0.024	O	|	|	|	|	0.02
228.583	0.00	0.01	0.024	O	|	|	|	|	0.02
228.667	0.00	0.01	0.024	O	|	|	|	|	0.02
228.750	0.00	0.01	0.024	O	|	|	|	|	0.02
228.833	0.00	0.01	0.024	O	|	|	|	|	0.02
228.917	0.00	0.01	0.024	O	|	|	|	|	0.02
229.000	0.00	0.01	0.024	O	|	|	|	|	0.02
229.083	0.00	0.01	0.024	O	|	|	|	|	0.02
229.167	0.00	0.01	0.024	O	|	|	|	|	0.02
229.250	0.00	0.01	0.024	O	|	|	|	|	0.02
229.333	0.00	0.01	0.024	O	|	|	|	|	0.02
229.417	0.00	0.01	0.024	O	|	|	|	|	0.02
229.500	0.00	0.01	0.024	O	|	|	|	|	0.02
229.583	0.00	0.01	0.024	O	|	|	|	|	0.02
229.667	0.00	0.01	0.023	O	|	|	|	|	0.02
229.750	0.00	0.01	0.023	O	|	|	|	|	0.02
229.833	0.00	0.01	0.023	O	|	|	|	|	0.02
229.917	0.00	0.01	0.023	O	|	|	|	|	0.02
230.000	0.00	0.01	0.023	O	|	|	|	|	0.02
230.083	0.00	0.01	0.023	O	|	|	|	|	0.02
230.167	0.00	0.01	0.023	O	|	|	|	|	0.02
230.250	0.00	0.01	0.023	O	|	|	|	|	0.02
230.333	0.00	0.01	0.023	O	|	|	|	|	0.02
230.417	0.00	0.01	0.023	O	|	|	|	|	0.02
230.500	0.00	0.01	0.023	O	|	|	|	|	0.02
230.583	0.00	0.01	0.023	O	|	|	|	|	0.02
230.667	0.00	0.01	0.023	O	|	|	|	|	0.02
230.750	0.00	0.01	0.023	O	|	|	|	|	0.02
230.833	0.00	0.01	0.023	O	|	|	|	|	0.02
230.917	0.00	0.01	0.023	O	|	|	|	|	0.02

231.000	0.00	0.01	0.023	O	|	|	|	|	0.02
231.083	0.00	0.01	0.023	O	|	|	|	|	0.02
231.167	0.00	0.01	0.023	O	|	|	|	|	0.02
231.250	0.00	0.01	0.023	O	|	|	|	|	0.02
231.333	0.00	0.01	0.023	O	|	|	|	|	0.02
231.417	0.00	0.01	0.023	O	|	|	|	|	0.02
231.500	0.00	0.01	0.023	O	|	|	|	|	0.02
231.583	0.00	0.01	0.022	O	|	|	|	|	0.02
231.667	0.00	0.01	0.022	O	|	|	|	|	0.02
231.750	0.00	0.01	0.022	O	|	|	|	|	0.02
231.833	0.00	0.01	0.022	O	|	|	|	|	0.02
231.917	0.00	0.01	0.022	O	|	|	|	|	0.02
232.000	0.00	0.01	0.022	O	|	|	|	|	0.02
232.083	0.00	0.01	0.022	O	|	|	|	|	0.02
232.167	0.00	0.01	0.022	O	|	|	|	|	0.02
232.250	0.00	0.01	0.022	O	|	|	|	|	0.02
232.333	0.00	0.01	0.022	O	|	|	|	|	0.02
232.417	0.00	0.01	0.022	O	|	|	|	|	0.02
232.500	0.00	0.01	0.022	O	|	|	|	|	0.02
232.583	0.00	0.01	0.022	O	|	|	|	|	0.02
232.667	0.00	0.01	0.022	O	|	|	|	|	0.02
232.750	0.00	0.01	0.022	O	|	|	|	|	0.02
232.833	0.00	0.01	0.022	O	|	|	|	|	0.02
232.917	0.00	0.01	0.022	O	|	|	|	|	0.02
233.000	0.00	0.01	0.022	O	|	|	|	|	0.02
233.083	0.00	0.01	0.022	O	|	|	|	|	0.02
233.167	0.00	0.01	0.022	O	|	|	|	|	0.02
233.250	0.00	0.01	0.022	O	|	|	|	|	0.02
233.333	0.00	0.01	0.022	O	|	|	|	|	0.02
233.417	0.00	0.01	0.022	O	|	|	|	|	0.02
233.500	0.00	0.01	0.022	O	|	|	|	|	0.02
233.583	0.00	0.01	0.021	O	|	|	|	|	0.02
233.667	0.00	0.01	0.021	O	|	|	|	|	0.02
233.750	0.00	0.01	0.021	O	|	|	|	|	0.02
233.833	0.00	0.01	0.021	O	|	|	|	|	0.02
233.917	0.00	0.01	0.021	O	|	|	|	|	0.02
234.000	0.00	0.01	0.021	O	|	|	|	|	0.02
234.083	0.00	0.01	0.021	O	|	|	|	|	0.02
234.167	0.00	0.01	0.021	O	|	|	|	|	0.02
234.250	0.00	0.01	0.021	O	|	|	|	|	0.02
234.333	0.00	0.01	0.021	O	|	|	|	|	0.02
234.417	0.00	0.01	0.021	O	|	|	|	|	0.02
234.500	0.00	0.01	0.021	O	|	|	|	|	0.02
234.583	0.00	0.01	0.021	O	|	|	|	|	0.02
234.667	0.00	0.01	0.021	O	|	|	|	|	0.02
234.750	0.00	0.01	0.021	O	|	|	|	|	0.02
234.833	0.00	0.01	0.021	O	|	|	|	|	0.02
234.917	0.00	0.01	0.021	O	|	|	|	|	0.02
235.000	0.00	0.01	0.021	O	|	|	|	|	0.02
235.083	0.00	0.01	0.021	O	|	|	|	|	0.02
235.167	0.00	0.01	0.021	O	|	|	|	|	0.02
235.250	0.00	0.01	0.021	O	|	|	|	|	0.02
235.333	0.00	0.01	0.021	O	|	|	|	|	0.02
235.417	0.00	0.01	0.021	O	|	|	|	|	0.02
235.500	0.00	0.01	0.021	O	|	|	|	|	0.02
235.583	0.00	0.01	0.020	O	|	|	|	|	0.02
235.667	0.00	0.01	0.020	O	|	|	|	|	0.02
235.750	0.00	0.01	0.020	O	|	|	|	|	0.02
235.833	0.00	0.01	0.020	O	|	|	|	|	0.02
235.917	0.00	0.01	0.020	O	|	|	|	|	0.02
236.000	0.00	0.01	0.020	O	|	|	|	|	0.02
236.083	0.00	0.01	0.020	O	|	|	|	|	0.02
236.167	0.00	0.01	0.020	O	|	|	|	|	0.02
236.250	0.00	0.01	0.020	O	|	|	|	|	0.02
236.333	0.00	0.01	0.020	O	|	|	|	|	0.02
236.417	0.00	0.01	0.020	O	|	|	|	|	0.02
236.500	0.00	0.01	0.020	O	|	|	|	|	0.02
236.583	0.00	0.01	0.020	O	|	|	|	|	0.02
236.667	0.00	0.01	0.020	O	|	|	|	|	0.02
236.750	0.00	0.01	0.020	O	|	|	|	|	0.02
236.833	0.00	0.01	0.020	O	|	|	|	|	0.02

236.917	0.00	0.01	0.020	O	|	|	|	|	0.02
237.000	0.00	0.01	0.020	O	|	|	|	|	0.02
237.083	0.00	0.01	0.020	O	|	|	|	|	0.02
237.167	0.00	0.01	0.020	O	|	|	|	|	0.02
237.250	0.00	0.01	0.020	O	|	|	|	|	0.02
237.333	0.00	0.01	0.020	O	|	|	|	|	0.02
237.417	0.00	0.01	0.020	O	|	|	|	|	0.02
237.500	0.00	0.01	0.020	O	|	|	|	|	0.02
237.583	0.00	0.01	0.020	O	|	|	|	|	0.02
237.667	0.00	0.01	0.020	O	|	|	|	|	0.02
237.750	0.00	0.01	0.019	O	|	|	|	|	0.02
237.833	0.00	0.01	0.019	O	|	|	|	|	0.02
237.917	0.00	0.01	0.019	O	|	|	|	|	0.02
238.000	0.00	0.01	0.019	O	|	|	|	|	0.02
238.083	0.00	0.01	0.019	O	|	|	|	|	0.02
238.167	0.00	0.01	0.019	O	|	|	|	|	0.02
238.250	0.00	0.01	0.019	O	|	|	|	|	0.02
238.333	0.00	0.01	0.019	O	|	|	|	|	0.02
238.417	0.00	0.01	0.019	O	|	|	|	|	0.02
238.500	0.00	0.01	0.019	O	|	|	|	|	0.02
238.583	0.00	0.01	0.019	O	|	|	|	|	0.02
238.667	0.00	0.01	0.019	O	|	|	|	|	0.02
238.750	0.00	0.01	0.019	O	|	|	|	|	0.02
238.833	0.00	0.01	0.019	O	|	|	|	|	0.02
238.917	0.00	0.01	0.019	O	|	|	|	|	0.02
239.000	0.00	0.01	0.019	O	|	|	|	|	0.02
239.083	0.00	0.01	0.019	O	|	|	|	|	0.02
239.167	0.00	0.01	0.019	O	|	|	|	|	0.02
239.250	0.00	0.01	0.019	O	|	|	|	|	0.02
239.333	0.00	0.01	0.019	O	|	|	|	|	0.02
239.417	0.00	0.01	0.019	O	|	|	|	|	0.02
239.500	0.00	0.01	0.019	O	|	|	|	|	0.02
239.583	0.00	0.01	0.019	O	|	|	|	|	0.02
239.667	0.00	0.01	0.019	O	|	|	|	|	0.02
239.750	0.00	0.01	0.019	O	|	|	|	|	0.02
239.833	0.00	0.01	0.019	O	|	|	|	|	0.02
239.917	0.00	0.01	0.019	O	|	|	|	|	0.02
240.000	0.00	0.01	0.019	O	|	|	|	|	0.02
240.083	0.00	0.01	0.018	O	|	|	|	|	0.01
240.167	0.00	0.01	0.018	O	|	|	|	|	0.01
240.250	0.00	0.01	0.018	O	|	|	|	|	0.01
240.333	0.00	0.01	0.018	O	|	|	|	|	0.01
240.417	0.00	0.01	0.018	O	|	|	|	|	0.01
240.500	0.00	0.01	0.018	O	|	|	|	|	0.01
240.583	0.00	0.01	0.018	O	|	|	|	|	0.01
240.667	0.00	0.01	0.018	O	|	|	|	|	0.01
240.750	0.00	0.01	0.018	O	|	|	|	|	0.01
240.833	0.00	0.01	0.018	O	|	|	|	|	0.01
240.917	0.00	0.01	0.018	O	|	|	|	|	0.01
241.000	0.00	0.01	0.018	O	|	|	|	|	0.01
241.083	0.00	0.01	0.018	O	|	|	|	|	0.01
241.167	0.00	0.01	0.018	O	|	|	|	|	0.01
241.250	0.00	0.01	0.018	O	|	|	|	|	0.01
241.333	0.00	0.01	0.018	O	|	|	|	|	0.01
241.417	0.00	0.01	0.018	O	|	|	|	|	0.01
241.500	0.00	0.00	0.018	O	|	|	|	|	0.01
241.583	0.00	0.00	0.018	O	|	|	|	|	0.01
241.667	0.00	0.00	0.018	O	|	|	|	|	0.01
241.750	0.00	0.00	0.018	O	|	|	|	|	0.01
241.833	0.00	0.00	0.018	O	|	|	|	|	0.01
241.917	0.00	0.00	0.018	O	|	|	|	|	0.01
242.000	0.00	0.00	0.018	O	|	|	|	|	0.01
242.083	0.00	0.00	0.018	O	|	|	|	|	0.01
242.167	0.00	0.00	0.018	O	|	|	|	|	0.01
242.250	0.00	0.00	0.018	O	|	|	|	|	0.01
242.333	0.00	0.00	0.018	O	|	|	|	|	0.01
242.417	0.00	0.00	0.018	O	|	|	|	|	0.01
242.500	0.00	0.00	0.017	O	|	|	|	|	0.01
242.583	0.00	0.00	0.017	O	|	|	|	|	0.01
242.667	0.00	0.00	0.017	O	|	|	|	|	0.01
242.750	0.00	0.00	0.017	O	|	|	|	|	0.01

242.833	0.00	0.00	0.017	O	|	|	|	|	0.01
242.917	0.00	0.00	0.017	O	|	|	|	|	0.01
243.000	0.00	0.00	0.017	O	|	|	|	|	0.01
243.083	0.00	0.00	0.017	O	|	|	|	|	0.01
243.167	0.00	0.00	0.017	O	|	|	|	|	0.01
243.250	0.00	0.00	0.017	O	|	|	|	|	0.01
243.333	0.00	0.00	0.017	O	|	|	|	|	0.01
243.417	0.00	0.00	0.017	O	|	|	|	|	0.01
243.500	0.00	0.00	0.017	O	|	|	|	|	0.01
243.583	0.00	0.00	0.017	O	|	|	|	|	0.01
243.667	0.00	0.00	0.017	O	|	|	|	|	0.01
243.750	0.00	0.00	0.017	O	|	|	|	|	0.01
243.833	0.00	0.00	0.017	O	|	|	|	|	0.01
243.917	0.00	0.00	0.017	O	|	|	|	|	0.01
244.000	0.00	0.00	0.017	O	|	|	|	|	0.01
244.083	0.00	0.00	0.017	O	|	|	|	|	0.01
244.167	0.00	0.00	0.017	O	|	|	|	|	0.01
244.250	0.00	0.00	0.017	O	|	|	|	|	0.01
244.333	0.00	0.00	0.017	O	|	|	|	|	0.01
244.417	0.00	0.00	0.017	O	|	|	|	|	0.01
244.500	0.00	0.00	0.017	O	|	|	|	|	0.01
244.583	0.00	0.00	0.017	O	|	|	|	|	0.01
244.667	0.00	0.00	0.017	O	|	|	|	|	0.01
244.750	0.00	0.00	0.017	O	|	|	|	|	0.01
244.833	0.00	0.00	0.017	O	|	|	|	|	0.01
244.917	0.00	0.00	0.017	O	|	|	|	|	0.01
245.000	0.00	0.00	0.016	O	|	|	|	|	0.01
245.083	0.00	0.00	0.016	O	|	|	|	|	0.01
245.167	0.00	0.00	0.016	O	|	|	|	|	0.01
245.250	0.00	0.00	0.016	O	|	|	|	|	0.01
245.333	0.00	0.00	0.016	O	|	|	|	|	0.01
245.417	0.00	0.00	0.016	O	|	|	|	|	0.01
245.500	0.00	0.00	0.016	O	|	|	|	|	0.01
245.583	0.00	0.00	0.016	O	|	|	|	|	0.01
245.667	0.00	0.00	0.016	O	|	|	|	|	0.01
245.750	0.00	0.00	0.016	O	|	|	|	|	0.01
245.833	0.00	0.00	0.016	O	|	|	|	|	0.01
245.917	0.00	0.00	0.016	O	|	|	|	|	0.01
246.000	0.00	0.00	0.016	O	|	|	|	|	0.01
246.083	0.00	0.00	0.016	O	|	|	|	|	0.01
246.167	0.00	0.00	0.016	O	|	|	|	|	0.01
246.250	0.00	0.00	0.016	O	|	|	|	|	0.01
246.333	0.00	0.00	0.016	O	|	|	|	|	0.01
246.417	0.00	0.00	0.016	O	|	|	|	|	0.01
246.500	0.00	0.00	0.016	O	|	|	|	|	0.01
246.583	0.00	0.00	0.016	O	|	|	|	|	0.01
246.667	0.00	0.00	0.016	O	|	|	|	|	0.01
246.750	0.00	0.00	0.016	O	|	|	|	|	0.01
246.833	0.00	0.00	0.016	O	|	|	|	|	0.01
246.917	0.00	0.00	0.016	O	|	|	|	|	0.01
247.000	0.00	0.00	0.016	O	|	|	|	|	0.01
247.083	0.00	0.00	0.016	O	|	|	|	|	0.01
247.167	0.00	0.00	0.016	O	|	|	|	|	0.01
247.250	0.00	0.00	0.016	O	|	|	|	|	0.01
247.333	0.00	0.00	0.016	O	|	|	|	|	0.01
247.417	0.00	0.00	0.016	O	|	|	|	|	0.01
247.500	0.00	0.00	0.016	O	|	|	|	|	0.01
247.583	0.00	0.00	0.016	O	|	|	|	|	0.01
247.667	0.00	0.00	0.016	O	|	|	|	|	0.01
247.750	0.00	0.00	0.015	O	|	|	|	|	0.01
247.833	0.00	0.00	0.015	O	|	|	|	|	0.01
247.917	0.00	0.00	0.015	O	|	|	|	|	0.01
248.000	0.00	0.00	0.015	O	|	|	|	|	0.01
248.083	0.00	0.00	0.015	O	|	|	|	|	0.01
248.167	0.00	0.00	0.015	O	|	|	|	|	0.01
248.250	0.00	0.00	0.015	O	|	|	|	|	0.01
248.333	0.00	0.00	0.015	O	|	|	|	|	0.01
248.417	0.00	0.00	0.015	O	|	|	|	|	0.01
248.500	0.00	0.00	0.015	O	|	|	|	|	0.01
248.583	0.00	0.00	0.015	O	|	|	|	|	0.01
248.667	0.00	0.00	0.015	O	|	|	|	|	0.01

248.750	0.00	0.00	0.015	O	|	|	|	|	0.01
248.833	0.00	0.00	0.015	O	|	|	|	|	0.01
248.917	0.00	0.00	0.015	O	|	|	|	|	0.01
249.000	0.00	0.00	0.015	O	|	|	|	|	0.01
249.083	0.00	0.00	0.015	O	|	|	|	|	0.01
249.167	0.00	0.00	0.015	O	|	|	|	|	0.01
249.250	0.00	0.00	0.015	O	|	|	|	|	0.01
249.333	0.00	0.00	0.015	O	|	|	|	|	0.01
249.417	0.00	0.00	0.015	O	|	|	|	|	0.01
249.500	0.00	0.00	0.015	O	|	|	|	|	0.01
249.583	0.00	0.00	0.015	O	|	|	|	|	0.01
249.667	0.00	0.00	0.015	O	|	|	|	|	0.01
249.750	0.00	0.00	0.015	O	|	|	|	|	0.01
249.833	0.00	0.00	0.015	O	|	|	|	|	0.01
249.917	0.00	0.00	0.015	O	|	|	|	|	0.01
250.000	0.00	0.00	0.015	O	|	|	|	|	0.01
250.083	0.00	0.00	0.015	O	|	|	|	|	0.01
250.167	0.00	0.00	0.015	O	|	|	|	|	0.01
250.250	0.00	0.00	0.015	O	|	|	|	|	0.01
250.333	0.00	0.00	0.015	O	|	|	|	|	0.01
250.417	0.00	0.00	0.015	O	|	|	|	|	0.01
250.500	0.00	0.00	0.015	O	|	|	|	|	0.01
250.583	0.00	0.00	0.014	O	|	|	|	|	0.01
250.667	0.00	0.00	0.014	O	|	|	|	|	0.01
250.750	0.00	0.00	0.014	O	|	|	|	|	0.01
250.833	0.00	0.00	0.014	O	|	|	|	|	0.01
250.917	0.00	0.00	0.014	O	|	|	|	|	0.01
251.000	0.00	0.00	0.014	O	|	|	|	|	0.01
251.083	0.00	0.00	0.014	O	|	|	|	|	0.01
251.167	0.00	0.00	0.014	O	|	|	|	|	0.01
251.250	0.00	0.00	0.014	O	|	|	|	|	0.01
251.333	0.00	0.00	0.014	O	|	|	|	|	0.01
251.417	0.00	0.00	0.014	O	|	|	|	|	0.01
251.500	0.00	0.00	0.014	O	|	|	|	|	0.01
251.583	0.00	0.00	0.014	O	|	|	|	|	0.01
251.667	0.00	0.00	0.014	O	|	|	|	|	0.01
251.750	0.00	0.00	0.014	O	|	|	|	|	0.01
251.833	0.00	0.00	0.014	O	|	|	|	|	0.01
251.917	0.00	0.00	0.014	O	|	|	|	|	0.01
252.000	0.00	0.00	0.014	O	|	|	|	|	0.01
252.083	0.00	0.00	0.014	O	|	|	|	|	0.01
252.167	0.00	0.00	0.014	O	|	|	|	|	0.01
252.250	0.00	0.00	0.014	O	|	|	|	|	0.01
252.333	0.00	0.00	0.014	O	|	|	|	|	0.01
252.417	0.00	0.00	0.014	O	|	|	|	|	0.01
252.500	0.00	0.00	0.014	O	|	|	|	|	0.01
252.583	0.00	0.00	0.014	O	|	|	|	|	0.01
252.667	0.00	0.00	0.014	O	|	|	|	|	0.01
252.750	0.00	0.00	0.014	O	|	|	|	|	0.01
252.833	0.00	0.00	0.014	O	|	|	|	|	0.01
252.917	0.00	0.00	0.014	O	|	|	|	|	0.01
253.000	0.00	0.00	0.014	O	|	|	|	|	0.01
253.083	0.00	0.00	0.014	O	|	|	|	|	0.01
253.167	0.00	0.00	0.014	O	|	|	|	|	0.01
253.250	0.00	0.00	0.014	O	|	|	|	|	0.01
253.333	0.00	0.00	0.014	O	|	|	|	|	0.01
253.417	0.00	0.00	0.014	O	|	|	|	|	0.01
253.500	0.00	0.00	0.014	O	|	|	|	|	0.01
253.583	0.00	0.00	0.014	O	|	|	|	|	0.01
253.667	0.00	0.00	0.014	O	|	|	|	|	0.01
253.750	0.00	0.00	0.013	O	|	|	|	|	0.01
253.833	0.00	0.00	0.013	O	|	|	|	|	0.01
253.917	0.00	0.00	0.013	O	|	|	|	|	0.01
254.000	0.00	0.00	0.013	O	|	|	|	|	0.01
254.083	0.00	0.00	0.013	O	|	|	|	|	0.01
254.167	0.00	0.00	0.013	O	|	|	|	|	0.01
254.250	0.00	0.00	0.013	O	|	|	|	|	0.01
254.333	0.00	0.00	0.013	O	|	|	|	|	0.01
254.417	0.00	0.00	0.013	O	|	|	|	|	0.01
254.500	0.00	0.00	0.013	O	|	|	|	|	0.01
254.583	0.00	0.00	0.013	O	|	|	|	|	0.01

254.667	0.00	0.00	0.013	O	|	|	|	|	0.01
254.750	0.00	0.00	0.013	O	|	|	|	|	0.01
254.833	0.00	0.00	0.013	O	|	|	|	|	0.01
254.917	0.00	0.00	0.013	O	|	|	|	|	0.01
255.000	0.00	0.00	0.013	O	|	|	|	|	0.01
255.083	0.00	0.00	0.013	O	|	|	|	|	0.01
255.167	0.00	0.00	0.013	O	|	|	|	|	0.01
255.250	0.00	0.00	0.013	O	|	|	|	|	0.01
255.333	0.00	0.00	0.013	O	|	|	|	|	0.01
255.417	0.00	0.00	0.013	O	|	|	|	|	0.01
255.500	0.00	0.00	0.013	O	|	|	|	|	0.01
255.583	0.00	0.00	0.013	O	|	|	|	|	0.01
255.667	0.00	0.00	0.013	O	|	|	|	|	0.01
255.750	0.00	0.00	0.013	O	|	|	|	|	0.01
255.833	0.00	0.00	0.013	O	|	|	|	|	0.01
255.917	0.00	0.00	0.013	O	|	|	|	|	0.01
256.000	0.00	0.00	0.013	O	|	|	|	|	0.01
256.083	0.00	0.00	0.013	O	|	|	|	|	0.01
256.167	0.00	0.00	0.013	O	|	|	|	|	0.01
256.250	0.00	0.00	0.013	O	|	|	|	|	0.01
256.333	0.00	0.00	0.013	O	|	|	|	|	0.01
256.417	0.00	0.00	0.013	O	|	|	|	|	0.01
256.500	0.00	0.00	0.013	O	|	|	|	|	0.01
256.583	0.00	0.00	0.013	O	|	|	|	|	0.01
256.667	0.00	0.00	0.013	O	|	|	|	|	0.01
256.750	0.00	0.00	0.013	O	|	|	|	|	0.01
256.833	0.00	0.00	0.013	O	|	|	|	|	0.01
256.917	0.00	0.00	0.013	O	|	|	|	|	0.01
257.000	0.00	0.00	0.013	O	|	|	|	|	0.01
257.083	0.00	0.00	0.012	O	|	|	|	|	0.01
257.167	0.00	0.00	0.012	O	|	|	|	|	0.01
257.250	0.00	0.00	0.012	O	|	|	|	|	0.01
257.333	0.00	0.00	0.012	O	|	|	|	|	0.01
257.417	0.00	0.00	0.012	O	|	|	|	|	0.01
257.500	0.00	0.00	0.012	O	|	|	|	|	0.01
257.583	0.00	0.00	0.012	O	|	|	|	|	0.01
257.667	0.00	0.00	0.012	O	|	|	|	|	0.01
257.750	0.00	0.00	0.012	O	|	|	|	|	0.01
257.833	0.00	0.00	0.012	O	|	|	|	|	0.01
257.917	0.00	0.00	0.012	O	|	|	|	|	0.01
258.000	0.00	0.00	0.012	O	|	|	|	|	0.01
258.083	0.00	0.00	0.012	O	|	|	|	|	0.01
258.167	0.00	0.00	0.012	O	|	|	|	|	0.01
258.250	0.00	0.00	0.012	O	|	|	|	|	0.01
258.333	0.00	0.00	0.012	O	|	|	|	|	0.01
258.417	0.00	0.00	0.012	O	|	|	|	|	0.01
258.500	0.00	0.00	0.012	O	|	|	|	|	0.01
258.583	0.00	0.00	0.012	O	|	|	|	|	0.01
258.667	0.00	0.00	0.012	O	|	|	|	|	0.01
258.750	0.00	0.00	0.012	O	|	|	|	|	0.01
258.833	0.00	0.00	0.012	O	|	|	|	|	0.01
258.917	0.00	0.00	0.012	O	|	|	|	|	0.01
259.000	0.00	0.00	0.012	O	|	|	|	|	0.01
259.083	0.00	0.00	0.012	O	|	|	|	|	0.01
259.167	0.00	0.00	0.012	O	|	|	|	|	0.01
259.250	0.00	0.00	0.012	O	|	|	|	|	0.01
259.333	0.00	0.00	0.012	O	|	|	|	|	0.01
259.417	0.00	0.00	0.012	O	|	|	|	|	0.01
259.500	0.00	0.00	0.012	O	|	|	|	|	0.01
259.583	0.00	0.00	0.012	O	|	|	|	|	0.01
259.667	0.00	0.00	0.012	O	|	|	|	|	0.01
259.750	0.00	0.00	0.012	O	|	|	|	|	0.01
259.833	0.00	0.00	0.012	O	|	|	|	|	0.01
259.917	0.00	0.00	0.012	O	|	|	|	|	0.01
260.000	0.00	0.00	0.012	O	|	|	|	|	0.01
260.083	0.00	0.00	0.012	O	|	|	|	|	0.01
260.167	0.00	0.00	0.012	O	|	|	|	|	0.01
260.250	0.00	0.00	0.012	O	|	|	|	|	0.01
260.333	0.00	0.00	0.012	O	|	|	|	|	0.01
260.417	0.00	0.00	0.012	O	|	|	|	|	0.01
260.500	0.00	0.00	0.012	O	|	|	|	|	0.01

260.583	0.00	0.00	0.012	O	|	|	|	|	0.01
260.667	0.00	0.00	0.011	O	|	|	|	|	0.01
260.750	0.00	0.00	0.011	O	|	|	|	|	0.01
260.833	0.00	0.00	0.011	O	|	|	|	|	0.01
260.917	0.00	0.00	0.011	O	|	|	|	|	0.01
261.000	0.00	0.00	0.011	O	|	|	|	|	0.01
261.083	0.00	0.00	0.011	O	|	|	|	|	0.01
261.167	0.00	0.00	0.011	O	|	|	|	|	0.01
261.250	0.00	0.00	0.011	O	|	|	|	|	0.01
261.333	0.00	0.00	0.011	O	|	|	|	|	0.01
261.417	0.00	0.00	0.011	O	|	|	|	|	0.01
261.500	0.00	0.00	0.011	O	|	|	|	|	0.01
261.583	0.00	0.00	0.011	O	|	|	|	|	0.01
261.667	0.00	0.00	0.011	O	|	|	|	|	0.01
261.750	0.00	0.00	0.011	O	|	|	|	|	0.01
261.833	0.00	0.00	0.011	O	|	|	|	|	0.01
261.917	0.00	0.00	0.011	O	|	|	|	|	0.01
262.000	0.00	0.00	0.011	O	|	|	|	|	0.01
262.083	0.00	0.00	0.011	O	|	|	|	|	0.01
262.167	0.00	0.00	0.011	O	|	|	|	|	0.01
262.250	0.00	0.00	0.011	O	|	|	|	|	0.01
262.333	0.00	0.00	0.011	O	|	|	|	|	0.01
262.417	0.00	0.00	0.011	O	|	|	|	|	0.01
262.500	0.00	0.00	0.011	O	|	|	|	|	0.01
262.583	0.00	0.00	0.011	O	|	|	|	|	0.01
262.667	0.00	0.00	0.011	O	|	|	|	|	0.01
262.750	0.00	0.00	0.011	O	|	|	|	|	0.01
262.833	0.00	0.00	0.011	O	|	|	|	|	0.01
262.917	0.00	0.00	0.011	O	|	|	|	|	0.01
263.000	0.00	0.00	0.011	O	|	|	|	|	0.01
263.083	0.00	0.00	0.011	O	|	|	|	|	0.01
263.167	0.00	0.00	0.011	O	|	|	|	|	0.01
263.250	0.00	0.00	0.011	O	|	|	|	|	0.01
263.333	0.00	0.00	0.011	O	|	|	|	|	0.01
263.417	0.00	0.00	0.011	O	|	|	|	|	0.01
263.500	0.00	0.00	0.011	O	|	|	|	|	0.01
263.583	0.00	0.00	0.011	O	|	|	|	|	0.01
263.667	0.00	0.00	0.011	O	|	|	|	|	0.01
263.750	0.00	0.00	0.011	O	|	|	|	|	0.01
263.833	0.00	0.00	0.011	O	|	|	|	|	0.01
263.917	0.00	0.00	0.011	O	|	|	|	|	0.01
264.000	0.00	0.00	0.011	O	|	|	|	|	0.01
264.083	0.00	0.00	0.011	O	|	|	|	|	0.01
264.167	0.00	0.00	0.011	O	|	|	|	|	0.01
264.250	0.00	0.00	0.011	O	|	|	|	|	0.01
264.333	0.00	0.00	0.011	O	|	|	|	|	0.01
264.417	0.00	0.00	0.011	O	|	|	|	|	0.01
264.500	0.00	0.00	0.011	O	|	|	|	|	0.01
264.583	0.00	0.00	0.010	O	|	|	|	|	0.01
264.667	0.00	0.00	0.010	O	|	|	|	|	0.01
264.750	0.00	0.00	0.010	O	|	|	|	|	0.01
264.833	0.00	0.00	0.010	O	|	|	|	|	0.01
264.917	0.00	0.00	0.010	O	|	|	|	|	0.01
265.000	0.00	0.00	0.010	O	|	|	|	|	0.01
265.083	0.00	0.00	0.010	O	|	|	|	|	0.01
265.167	0.00	0.00	0.010	O	|	|	|	|	0.01
265.250	0.00	0.00	0.010	O	|	|	|	|	0.01
265.333	0.00	0.00	0.010	O	|	|	|	|	0.01
265.417	0.00	0.00	0.010	O	|	|	|	|	0.01
265.500	0.00	0.00	0.010	O	|	|	|	|	0.01
265.583	0.00	0.00	0.010	O	|	|	|	|	0.01
265.667	0.00	0.00	0.010	O	|	|	|	|	0.01
265.750	0.00	0.00	0.010	O	|	|	|	|	0.01
265.833	0.00	0.00	0.010	O	|	|	|	|	0.01
265.917	0.00	0.00	0.010	O	|	|	|	|	0.01
266.000	0.00	0.00	0.010	O	|	|	|	|	0.01
266.083	0.00	0.00	0.010	O	|	|	|	|	0.01
266.167	0.00	0.00	0.010	O	|	|	|	|	0.01
266.250	0.00	0.00	0.010	O	|	|	|	|	0.01
266.333	0.00	0.00	0.010	O	|	|	|	|	0.01
266.417	0.00	0.00	0.010	O	|	|	|	|	0.01

266.500	0.00	0.00	0.010	O	|	|	|	|	0.01
266.583	0.00	0.00	0.010	O	|	|	|	|	0.01
266.667	0.00	0.00	0.010	O	|	|	|	|	0.01
266.750	0.00	0.00	0.010	O	|	|	|	|	0.01
266.833	0.00	0.00	0.010	O	|	|	|	|	0.01
266.917	0.00	0.00	0.010	O	|	|	|	|	0.01
267.000	0.00	0.00	0.010	O	|	|	|	|	0.01
267.083	0.00	0.00	0.010	O	|	|	|	|	0.01
267.167	0.00	0.00	0.010	O	|	|	|	|	0.01
267.250	0.00	0.00	0.010	O	|	|	|	|	0.01
267.333	0.00	0.00	0.010	O	|	|	|	|	0.01
267.417	0.00	0.00	0.010	O	|	|	|	|	0.01
267.500	0.00	0.00	0.010	O	|	|	|	|	0.01
267.583	0.00	0.00	0.010	O	|	|	|	|	0.01
267.667	0.00	0.00	0.010	O	|	|	|	|	0.01
267.750	0.00	0.00	0.010	O	|	|	|	|	0.01
267.833	0.00	0.00	0.010	O	|	|	|	|	0.01
267.917	0.00	0.00	0.010	O	|	|	|	|	0.01
268.000	0.00	0.00	0.010	O	|	|	|	|	0.01
268.083	0.00	0.00	0.010	O	|	|	|	|	0.01
268.167	0.00	0.00	0.010	O	|	|	|	|	0.01
268.250	0.00	0.00	0.010	O	|	|	|	|	0.01
268.333	0.00	0.00	0.010	O	|	|	|	|	0.01
268.417	0.00	0.00	0.010	O	|	|	|	|	0.01
268.500	0.00	0.00	0.010	O	|	|	|	|	0.01
268.583	0.00	0.00	0.010	O	|	|	|	|	0.01
268.667	0.00	0.00	0.010	O	|	|	|	|	0.01
268.750	0.00	0.00	0.010	O	|	|	|	|	0.01
268.833	0.00	0.00	0.010	O	|	|	|	|	0.01
268.917	0.00	0.00	0.009	O	|	|	|	|	0.01
269.000	0.00	0.00	0.009	O	|	|	|	|	0.01
269.083	0.00	0.00	0.009	O	|	|	|	|	0.01
269.167	0.00	0.00	0.009	O	|	|	|	|	0.01
269.250	0.00	0.00	0.009	O	|	|	|	|	0.01
269.333	0.00	0.00	0.009	O	|	|	|	|	0.01
269.417	0.00	0.00	0.009	O	|	|	|	|	0.01
269.500	0.00	0.00	0.009	O	|	|	|	|	0.01
269.583	0.00	0.00	0.009	O	|	|	|	|	0.01
269.667	0.00	0.00	0.009	O	|	|	|	|	0.01
269.750	0.00	0.00	0.009	O	|	|	|	|	0.01
269.833	0.00	0.00	0.009	O	|	|	|	|	0.01
269.917	0.00	0.00	0.009	O	|	|	|	|	0.01
270.000	0.00	0.00	0.009	O	|	|	|	|	0.01
270.083	0.00	0.00	0.009	O	|	|	|	|	0.01
270.167	0.00	0.00	0.009	O	|	|	|	|	0.01
270.250	0.00	0.00	0.009	O	|	|	|	|	0.01
270.333	0.00	0.00	0.009	O	|	|	|	|	0.01
270.417	0.00	0.00	0.009	O	|	|	|	|	0.01
270.500	0.00	0.00	0.009	O	|	|	|	|	0.01
270.583	0.00	0.00	0.009	O	|	|	|	|	0.01
270.667	0.00	0.00	0.009	O	|	|	|	|	0.01
270.750	0.00	0.00	0.009	O	|	|	|	|	0.01
270.833	0.00	0.00	0.009	O	|	|	|	|	0.01
270.917	0.00	0.00	0.009	O	|	|	|	|	0.01
271.000	0.00	0.00	0.009	O	|	|	|	|	0.01
271.083	0.00	0.00	0.009	O	|	|	|	|	0.01
271.167	0.00	0.00	0.009	O	|	|	|	|	0.01
271.250	0.00	0.00	0.009	O	|	|	|	|	0.01
271.333	0.00	0.00	0.009	O	|	|	|	|	0.01
271.417	0.00	0.00	0.009	O	|	|	|	|	0.01
271.500	0.00	0.00	0.009	O	|	|	|	|	0.01
271.583	0.00	0.00	0.009	O	|	|	|	|	0.01
271.667	0.00	0.00	0.009	O	|	|	|	|	0.01
271.750	0.00	0.00	0.009	O	|	|	|	|	0.01
271.833	0.00	0.00	0.009	O	|	|	|	|	0.01
271.917	0.00	0.00	0.009	O	|	|	|	|	0.01
272.000	0.00	0.00	0.009	O	|	|	|	|	0.01
272.083	0.00	0.00	0.009	O	|	|	|	|	0.01
272.167	0.00	0.00	0.009	O	|	|	|	|	0.01
272.250	0.00	0.00	0.009	O	|	|	|	|	0.01
272.333	0.00	0.00	0.009	O	|	|	|	|	0.01

272.417	0.00	0.00	0.009	O	|	|	|	|	0.01
272.500	0.00	0.00	0.009	O	|	|	|	|	0.01
272.583	0.00	0.00	0.009	O	|	|	|	|	0.01
272.667	0.00	0.00	0.009	O	|	|	|	|	0.01
272.750	0.00	0.00	0.009	O	|	|	|	|	0.01
272.833	0.00	0.00	0.009	O	|	|	|	|	0.01
272.917	0.00	0.00	0.009	O	|	|	|	|	0.01
273.000	0.00	0.00	0.009	O	|	|	|	|	0.01
273.083	0.00	0.00	0.009	O	|	|	|	|	0.01
273.167	0.00	0.00	0.009	O	|	|	|	|	0.01
273.250	0.00	0.00	0.009	O	|	|	|	|	0.01
273.333	0.00	0.00	0.009	O	|	|	|	|	0.01
273.417	0.00	0.00	0.009	O	|	|	|	|	0.01
273.500	0.00	0.00	0.009	O	|	|	|	|	0.01
273.583	0.00	0.00	0.009	O	|	|	|	|	0.01
273.667	0.00	0.00	0.009	O	|	|	|	|	0.01
273.750	0.00	0.00	0.008	O	|	|	|	|	0.01
273.833	0.00	0.00	0.008	O	|	|	|	|	0.01
273.917	0.00	0.00	0.008	O	|	|	|	|	0.01
274.000	0.00	0.00	0.008	O	|	|	|	|	0.01
274.083	0.00	0.00	0.008	O	|	|	|	|	0.01
274.167	0.00	0.00	0.008	O	|	|	|	|	0.01
274.250	0.00	0.00	0.008	O	|	|	|	|	0.01
274.333	0.00	0.00	0.008	O	|	|	|	|	0.01
274.417	0.00	0.00	0.008	O	|	|	|	|	0.01
274.500	0.00	0.00	0.008	O	|	|	|	|	0.01
274.583	0.00	0.00	0.008	O	|	|	|	|	0.01
274.667	0.00	0.00	0.008	O	|	|	|	|	0.01
274.750	0.00	0.00	0.008	O	|	|	|	|	0.01
274.833	0.00	0.00	0.008	O	|	|	|	|	0.01
274.917	0.00	0.00	0.008	O	|	|	|	|	0.01
275.000	0.00	0.00	0.008	O	|	|	|	|	0.01
275.083	0.00	0.00	0.008	O	|	|	|	|	0.01
275.167	0.00	0.00	0.008	O	|	|	|	|	0.01
275.250	0.00	0.00	0.008	O	|	|	|	|	0.01
275.333	0.00	0.00	0.008	O	|	|	|	|	0.01
275.417	0.00	0.00	0.008	O	|	|	|	|	0.01
275.500	0.00	0.00	0.008	O	|	|	|	|	0.01
275.583	0.00	0.00	0.008	O	|	|	|	|	0.01
275.667	0.00	0.00	0.008	O	|	|	|	|	0.01
275.750	0.00	0.00	0.008	O	|	|	|	|	0.01
275.833	0.00	0.00	0.008	O	|	|	|	|	0.01
275.917	0.00	0.00	0.008	O	|	|	|	|	0.01
276.000	0.00	0.00	0.008	O	|	|	|	|	0.01
276.083	0.00	0.00	0.008	O	|	|	|	|	0.01
276.167	0.00	0.00	0.008	O	|	|	|	|	0.01
276.250	0.00	0.00	0.008	O	|	|	|	|	0.01
276.333	0.00	0.00	0.008	O	|	|	|	|	0.01
276.417	0.00	0.00	0.008	O	|	|	|	|	0.01
276.500	0.00	0.00	0.008	O	|	|	|	|	0.01
276.583	0.00	0.00	0.008	O	|	|	|	|	0.01
276.667	0.00	0.00	0.008	O	|	|	|	|	0.01
276.750	0.00	0.00	0.008	O	|	|	|	|	0.01
276.833	0.00	0.00	0.008	O	|	|	|	|	0.01
276.917	0.00	0.00	0.008	O	|	|	|	|	0.01
277.000	0.00	0.00	0.008	O	|	|	|	|	0.01
277.083	0.00	0.00	0.008	O	|	|	|	|	0.01
277.167	0.00	0.00	0.008	O	|	|	|	|	0.01
277.250	0.00	0.00	0.008	O	|	|	|	|	0.01
277.333	0.00	0.00	0.008	O	|	|	|	|	0.01
277.417	0.00	0.00	0.008	O	|	|	|	|	0.01
277.500	0.00	0.00	0.008	O	|	|	|	|	0.01
277.583	0.00	0.00	0.008	O	|	|	|	|	0.01
277.667	0.00	0.00	0.008	O	|	|	|	|	0.01
277.750	0.00	0.00	0.008	O	|	|	|	|	0.01
277.833	0.00	0.00	0.008	O	|	|	|	|	0.01
277.917	0.00	0.00	0.008	O	|	|	|	|	0.01
278.000	0.00	0.00	0.008	O	|	|	|	|	0.01
278.083	0.00	0.00	0.008	O	|	|	|	|	0.01
278.167	0.00	0.00	0.008	O	|	|	|	|	0.01
278.250	0.00	0.00	0.008	O	|	|	|	|	0.01

278.333	0.00	0.00	0.008	O	|	|	|	|	0.01
278.417	0.00	0.00	0.008	O	|	|	|	|	0.01
278.500	0.00	0.00	0.008	O	|	|	|	|	0.01
278.583	0.00	0.00	0.008	O	|	|	|	|	0.01
278.667	0.00	0.00	0.008	O	|	|	|	|	0.01
278.750	0.00	0.00	0.008	O	|	|	|	|	0.01
278.833	0.00	0.00	0.008	O	|	|	|	|	0.01
278.917	0.00	0.00	0.008	O	|	|	|	|	0.01
279.000	0.00	0.00	0.008	O	|	|	|	|	0.01
279.083	0.00	0.00	0.008	O	|	|	|	|	0.01
279.167	0.00	0.00	0.007	O	|	|	|	|	0.01
279.250	0.00	0.00	0.007	O	|	|	|	|	0.01
279.333	0.00	0.00	0.007	O	|	|	|	|	0.01
279.417	0.00	0.00	0.007	O	|	|	|	|	0.01
279.500	0.00	0.00	0.007	O	|	|	|	|	0.01
279.583	0.00	0.00	0.007	O	|	|	|	|	0.01
279.667	0.00	0.00	0.007	O	|	|	|	|	0.01
279.750	0.00	0.00	0.007	O	|	|	|	|	0.01
279.833	0.00	0.00	0.007	O	|	|	|	|	0.01
279.917	0.00	0.00	0.007	O	|	|	|	|	0.01
280.000	0.00	0.00	0.007	O	|	|	|	|	0.01
280.083	0.00	0.00	0.007	O	|	|	|	|	0.01
280.167	0.00	0.00	0.007	O	|	|	|	|	0.01
280.250	0.00	0.00	0.007	O	|	|	|	|	0.01
280.333	0.00	0.00	0.007	O	|	|	|	|	0.01
280.417	0.00	0.00	0.007	O	|	|	|	|	0.01
280.500	0.00	0.00	0.007	O	|	|	|	|	0.01
280.583	0.00	0.00	0.007	O	|	|	|	|	0.01
280.667	0.00	0.00	0.007	O	|	|	|	|	0.01
280.750	0.00	0.00	0.007	O	|	|	|	|	0.01
280.833	0.00	0.00	0.007	O	|	|	|	|	0.01
280.917	0.00	0.00	0.007	O	|	|	|	|	0.01
281.000	0.00	0.00	0.007	O	|	|	|	|	0.01
281.083	0.00	0.00	0.007	O	|	|	|	|	0.01
281.167	0.00	0.00	0.007	O	|	|	|	|	0.01
281.250	0.00	0.00	0.007	O	|	|	|	|	0.01
281.333	0.00	0.00	0.007	O	|	|	|	|	0.01
281.417	0.00	0.00	0.007	O	|	|	|	|	0.01
281.500	0.00	0.00	0.007	O	|	|	|	|	0.01
281.583	0.00	0.00	0.007	O	|	|	|	|	0.01
281.667	0.00	0.00	0.007	O	|	|	|	|	0.01
281.750	0.00	0.00	0.007	O	|	|	|	|	0.01
281.833	0.00	0.00	0.007	O	|	|	|	|	0.01
281.917	0.00	0.00	0.007	O	|	|	|	|	0.01
282.000	0.00	0.00	0.007	O	|	|	|	|	0.01
282.083	0.00	0.00	0.007	O	|	|	|	|	0.01
282.167	0.00	0.00	0.007	O	|	|	|	|	0.01
282.250	0.00	0.00	0.007	O	|	|	|	|	0.01
282.333	0.00	0.00	0.007	O	|	|	|	|	0.01
282.417	0.00	0.00	0.007	O	|	|	|	|	0.01
282.500	0.00	0.00	0.007	O	|	|	|	|	0.01
282.583	0.00	0.00	0.007	O	|	|	|	|	0.01
282.667	0.00	0.00	0.007	O	|	|	|	|	0.01
282.750	0.00	0.00	0.007	O	|	|	|	|	0.01
282.833	0.00	0.00	0.007	O	|	|	|	|	0.01
282.917	0.00	0.00	0.007	O	|	|	|	|	0.01
283.000	0.00	0.00	0.007	O	|	|	|	|	0.01
283.083	0.00	0.00	0.007	O	|	|	|	|	0.01
283.167	0.00	0.00	0.007	O	|	|	|	|	0.01
283.250	0.00	0.00	0.007	O	|	|	|	|	0.01
283.333	0.00	0.00	0.007	O	|	|	|	|	0.01
283.417	0.00	0.00	0.007	O	|	|	|	|	0.01
283.500	0.00	0.00	0.007	O	|	|	|	|	0.01
283.583	0.00	0.00	0.007	O	|	|	|	|	0.01
283.667	0.00	0.00	0.007	O	|	|	|	|	0.01
283.750	0.00	0.00	0.007	O	|	|	|	|	0.01
283.833	0.00	0.00	0.007	O	|	|	|	|	0.01
283.917	0.00	0.00	0.007	O	|	|	|	|	0.01
284.000	0.00	0.00	0.007	O	|	|	|	|	0.01
284.083	0.00	0.00	0.007	O	|	|	|	|	0.01
284.167	0.00	0.00	0.007	O	|	|	|	|	0.01

284.250	0.00	0.00	0.007	O	|	|	|	|	0.01
284.333	0.00	0.00	0.007	O	|	|	|	|	0.01
284.417	0.00	0.00	0.007	O	|	|	|	|	0.01
284.500	0.00	0.00	0.007	O	|	|	|	|	0.01
284.583	0.00	0.00	0.007	O	|	|	|	|	0.01
284.667	0.00	0.00	0.007	O	|	|	|	|	0.01
284.750	0.00	0.00	0.007	O	|	|	|	|	0.01
284.833	0.00	0.00	0.007	O	|	|	|	|	0.01
284.917	0.00	0.00	0.007	O	|	|	|	|	0.01
285.000	0.00	0.00	0.007	O	|	|	|	|	0.01
285.083	0.00	0.00	0.007	O	|	|	|	|	0.01
285.167	0.00	0.00	0.007	O	|	|	|	|	0.01
285.250	0.00	0.00	0.007	O	|	|	|	|	0.01
285.333	0.00	0.00	0.007	O	|	|	|	|	0.01
285.417	0.00	0.00	0.006	O	|	|	|	|	0.01
285.500	0.00	0.00	0.006	O	|	|	|	|	0.01
285.583	0.00	0.00	0.006	O	|	|	|	|	0.01
285.667	0.00	0.00	0.006	O	|	|	|	|	0.01
285.750	0.00	0.00	0.006	O	|	|	|	|	0.01
285.833	0.00	0.00	0.006	O	|	|	|	|	0.01
285.917	0.00	0.00	0.006	O	|	|	|	|	0.01
286.000	0.00	0.00	0.006	O	|	|	|	|	0.01
286.083	0.00	0.00	0.006	O	|	|	|	|	0.01
286.167	0.00	0.00	0.006	O	|	|	|	|	0.01
286.250	0.00	0.00	0.006	O	|	|	|	|	0.01
286.333	0.00	0.00	0.006	O	|	|	|	|	0.01
286.417	0.00	0.00	0.006	O	|	|	|	|	0.01
286.500	0.00	0.00	0.006	O	|	|	|	|	0.01
286.583	0.00	0.00	0.006	O	|	|	|	|	0.01
286.667	0.00	0.00	0.006	O	|	|	|	|	0.01
286.750	0.00	0.00	0.006	O	|	|	|	|	0.01
286.833	0.00	0.00	0.006	O	|	|	|	|	0.01
286.917	0.00	0.00	0.006	O	|	|	|	|	0.01
287.000	0.00	0.00	0.006	O	|	|	|	|	0.01
287.083	0.00	0.00	0.006	O	|	|	|	|	0.01
287.167	0.00	0.00	0.006	O	|	|	|	|	0.01
287.250	0.00	0.00	0.006	O	|	|	|	|	0.01
287.333	0.00	0.00	0.006	O	|	|	|	|	0.01
287.417	0.00	0.00	0.006	O	|	|	|	|	0.01
287.500	0.00	0.00	0.006	O	|	|	|	|	0.01
287.583	0.00	0.00	0.006	O	|	|	|	|	0.01
287.667	0.00	0.00	0.006	O	|	|	|	|	0.01
287.750	0.00	0.00	0.006	O	|	|	|	|	0.00
287.833	0.00	0.00	0.006	O	|	|	|	|	0.00
287.917	0.00	0.00	0.006	O	|	|	|	|	0.00
288.000	0.00	0.00	0.006	O	|	|	|	|	0.00
288.083	0.00	0.00	0.006	O	|	|	|	|	0.00
288.167	0.00	0.00	0.006	O	|	|	|	|	0.00
288.250	0.00	0.00	0.006	O	|	|	|	|	0.00
288.333	0.00	0.00	0.006	O	|	|	|	|	0.00
288.417	0.00	0.00	0.006	O	|	|	|	|	0.00
288.500	0.00	0.00	0.006	O	|	|	|	|	0.00
288.583	0.00	0.00	0.006	O	|	|	|	|	0.00
288.667	0.00	0.00	0.006	O	|	|	|	|	0.00
288.750	0.00	0.00	0.006	O	|	|	|	|	0.00
288.833	0.00	0.00	0.006	O	|	|	|	|	0.00
288.917	0.00	0.00	0.006	O	|	|	|	|	0.00
289.000	0.00	0.00	0.006	O	|	|	|	|	0.00
289.083	0.00	0.00	0.006	O	|	|	|	|	0.00
289.167	0.00	0.00	0.006	O	|	|	|	|	0.00
289.250	0.00	0.00	0.006	O	|	|	|	|	0.00
289.333	0.00	0.00	0.006	O	|	|	|	|	0.00
289.417	0.00	0.00	0.006	O	|	|	|	|	0.00
289.500	0.00	0.00	0.006	O	|	|	|	|	0.00
289.583	0.00	0.00	0.006	O	|	|	|	|	0.00
289.667	0.00	0.00	0.006	O	|	|	|	|	0.00
289.750	0.00	0.00	0.006	O	|	|	|	|	0.00
289.833	0.00	0.00	0.006	O	|	|	|	|	0.00
289.917	0.00	0.00	0.006	O	|	|	|	|	0.00
290.000	0.00	0.00	0.006	O	|	|	|	|	0.00
290.083	0.00	0.00	0.006	O	|	|	|	|	0.00

290.167	0.00	0.00	0.006	O	|	|	|	|	0.00
290.250	0.00	0.00	0.006	O	|	|	|	|	0.00
290.333	0.00	0.00	0.006	O	|	|	|	|	0.00
290.417	0.00	0.00	0.006	O	|	|	|	|	0.00
290.500	0.00	0.00	0.006	O	|	|	|	|	0.00
290.583	0.00	0.00	0.006	O	|	|	|	|	0.00
290.667	0.00	0.00	0.006	O	|	|	|	|	0.00
290.750	0.00	0.00	0.006	O	|	|	|	|	0.00
290.833	0.00	0.00	0.006	O	|	|	|	|	0.00
290.917	0.00	0.00	0.006	O	|	|	|	|	0.00
291.000	0.00	0.00	0.006	O	|	|	|	|	0.00
291.083	0.00	0.00	0.006	O	|	|	|	|	0.00
291.167	0.00	0.00	0.006	O	|	|	|	|	0.00
291.250	0.00	0.00	0.006	O	|	|	|	|	0.00
291.333	0.00	0.00	0.006	O	|	|	|	|	0.00
291.417	0.00	0.00	0.006	O	|	|	|	|	0.00
291.500	0.00	0.00	0.006	O	|	|	|	|	0.00
291.583	0.00	0.00	0.006	O	|	|	|	|	0.00
291.667	0.00	0.00	0.006	O	|	|	|	|	0.00
291.750	0.00	0.00	0.006	O	|	|	|	|	0.00
291.833	0.00	0.00	0.006	O	|	|	|	|	0.00
291.917	0.00	0.00	0.006	O	|	|	|	|	0.00
292.000	0.00	0.00	0.006	O	|	|	|	|	0.00
292.083	0.00	0.00	0.006	O	|	|	|	|	0.00
292.167	0.00	0.00	0.006	O	|	|	|	|	0.00
292.250	0.00	0.00	0.006	O	|	|	|	|	0.00
292.333	0.00	0.00	0.006	O	|	|	|	|	0.00
292.417	0.00	0.00	0.006	O	|	|	|	|	0.00
292.500	0.00	0.00	0.006	O	|	|	|	|	0.00
292.583	0.00	0.00	0.005	O	|	|	|	|	0.00
292.667	0.00	0.00	0.005	O	|	|	|	|	0.00
292.750	0.00	0.00	0.005	O	|	|	|	|	0.00
292.833	0.00	0.00	0.005	O	|	|	|	|	0.00
292.917	0.00	0.00	0.005	O	|	|	|	|	0.00
293.000	0.00	0.00	0.005	O	|	|	|	|	0.00
293.083	0.00	0.00	0.005	O	|	|	|	|	0.00
293.167	0.00	0.00	0.005	O	|	|	|	|	0.00
293.250	0.00	0.00	0.005	O	|	|	|	|	0.00
293.333	0.00	0.00	0.005	O	|	|	|	|	0.00
293.417	0.00	0.00	0.005	O	|	|	|	|	0.00
293.500	0.00	0.00	0.005	O	|	|	|	|	0.00
293.583	0.00	0.00	0.005	O	|	|	|	|	0.00
293.667	0.00	0.00	0.005	O	|	|	|	|	0.00
293.750	0.00	0.00	0.005	O	|	|	|	|	0.00
293.833	0.00	0.00	0.005	O	|	|	|	|	0.00
293.917	0.00	0.00	0.005	O	|	|	|	|	0.00
294.000	0.00	0.00	0.005	O	|	|	|	|	0.00
294.083	0.00	0.00	0.005	O	|	|	|	|	0.00
294.167	0.00	0.00	0.005	O	|	|	|	|	0.00
294.250	0.00	0.00	0.005	O	|	|	|	|	0.00
294.333	0.00	0.00	0.005	O	|	|	|	|	0.00
294.417	0.00	0.00	0.005	O	|	|	|	|	0.00
294.500	0.00	0.00	0.005	O	|	|	|	|	0.00
294.583	0.00	0.00	0.005	O	|	|	|	|	0.00
294.667	0.00	0.00	0.005	O	|	|	|	|	0.00
294.750	0.00	0.00	0.005	O	|	|	|	|	0.00
294.833	0.00	0.00	0.005	O	|	|	|	|	0.00
294.917	0.00	0.00	0.005	O	|	|	|	|	0.00
295.000	0.00	0.00	0.005	O	|	|	|	|	0.00
295.083	0.00	0.00	0.005	O	|	|	|	|	0.00
295.167	0.00	0.00	0.005	O	|	|	|	|	0.00
295.250	0.00	0.00	0.005	O	|	|	|	|	0.00
295.333	0.00	0.00	0.005	O	|	|	|	|	0.00
295.417	0.00	0.00	0.005	O	|	|	|	|	0.00
295.500	0.00	0.00	0.005	O	|	|	|	|	0.00
295.583	0.00	0.00	0.005	O	|	|	|	|	0.00
295.667	0.00	0.00	0.005	O	|	|	|	|	0.00
295.750	0.00	0.00	0.005	O	|	|	|	|	0.00
295.833	0.00	0.00	0.005	O	|	|	|	|	0.00
295.917	0.00	0.00	0.005	O	|	|	|	|	0.00
296.000	0.00	0.00	0.005	O	|	|	|	|	0.00

296.083	0.00	0.00	0.005	O	|	|	|	|	0.00
296.167	0.00	0.00	0.005	O	|	|	|	|	0.00
296.250	0.00	0.00	0.005	O	|	|	|	|	0.00
296.333	0.00	0.00	0.005	O	|	|	|	|	0.00
296.417	0.00	0.00	0.005	O	|	|	|	|	0.00
296.500	0.00	0.00	0.005	O	|	|	|	|	0.00
296.583	0.00	0.00	0.005	O	|	|	|	|	0.00
296.667	0.00	0.00	0.005	O	|	|	|	|	0.00
296.750	0.00	0.00	0.005	O	|	|	|	|	0.00
296.833	0.00	0.00	0.005	O	|	|	|	|	0.00
296.917	0.00	0.00	0.005	O	|	|	|	|	0.00
297.000	0.00	0.00	0.005	O	|	|	|	|	0.00
297.083	0.00	0.00	0.005	O	|	|	|	|	0.00
297.167	0.00	0.00	0.005	O	|	|	|	|	0.00
297.250	0.00	0.00	0.005	O	|	|	|	|	0.00
297.333	0.00	0.00	0.005	O	|	|	|	|	0.00
297.417	0.00	0.00	0.005	O	|	|	|	|	0.00
297.500	0.00	0.00	0.005	O	|	|	|	|	0.00
297.583	0.00	0.00	0.005	O	|	|	|	|	0.00
297.667	0.00	0.00	0.005	O	|	|	|	|	0.00
297.750	0.00	0.00	0.005	O	|	|	|	|	0.00
297.833	0.00	0.00	0.005	O	|	|	|	|	0.00
297.917	0.00	0.00	0.005	O	|	|	|	|	0.00
298.000	0.00	0.00	0.005	O	|	|	|	|	0.00
298.083	0.00	0.00	0.005	O	|	|	|	|	0.00
298.167	0.00	0.00	0.005	O	|	|	|	|	0.00
298.250	0.00	0.00	0.005	O	|	|	|	|	0.00
298.333	0.00	0.00	0.005	O	|	|	|	|	0.00
298.417	0.00	0.00	0.005	O	|	|	|	|	0.00
298.500	0.00	0.00	0.005	O	|	|	|	|	0.00
298.583	0.00	0.00	0.005	O	|	|	|	|	0.00
298.667	0.00	0.00	0.005	O	|	|	|	|	0.00
298.750	0.00	0.00	0.005	O	|	|	|	|	0.00
298.833	0.00	0.00	0.005	O	|	|	|	|	0.00
298.917	0.00	0.00	0.005	O	|	|	|	|	0.00
299.000	0.00	0.00	0.005	O	|	|	|	|	0.00
299.083	0.00	0.00	0.005	O	|	|	|	|	0.00
299.167	0.00	0.00	0.005	O	|	|	|	|	0.00
299.250	0.00	0.00	0.005	O	|	|	|	|	0.00
299.333	0.00	0.00	0.005	O	|	|	|	|	0.00
299.417	0.00	0.00	0.005	O	|	|	|	|	0.00
299.500	0.00	0.00	0.005	O	|	|	|	|	0.00
299.583	0.00	0.00	0.005	O	|	|	|	|	0.00
299.667	0.00	0.00	0.005	O	|	|	|	|	0.00
299.750	0.00	0.00	0.005	O	|	|	|	|	0.00
299.833	0.00	0.00	0.005	O	|	|	|	|	0.00
299.917	0.00	0.00	0.005	O	|	|	|	|	0.00
300.000	0.00	0.00	0.005	O	|	|	|	|	0.00
300.083	0.00	0.00	0.005	O	|	|	|	|	0.00
300.167	0.00	0.00	0.005	O	|	|	|	|	0.00
300.250	0.00	0.00	0.005	O	|	|	|	|	0.00
300.333	0.00	0.00	0.005	O	|	|	|	|	0.00
300.417	0.00	0.00	0.005	O	|	|	|	|	0.00
300.500	0.00	0.00	0.005	O	|	|	|	|	0.00
300.583	0.00	0.00	0.005	O	|	|	|	|	0.00
300.667	0.00	0.00	0.005	O	|	|	|	|	0.00
300.750	0.00	0.00	0.005	O	|	|	|	|	0.00
300.833	0.00	0.00	0.005	O	|	|	|	|	0.00
300.917	0.00	0.00	0.005	O	|	|	|	|	0.00
301.000	0.00	0.00	0.005	O	|	|	|	|	0.00
301.083	0.00	0.00	0.005	O	|	|	|	|	0.00
301.167	0.00	0.00	0.005	O	|	|	|	|	0.00
301.250	0.00	0.00	0.005	O	|	|	|	|	0.00
301.333	0.00	0.00	0.004	O	|	|	|	|	0.00
301.417	0.00	0.00	0.004	O	|	|	|	|	0.00
301.500	0.00	0.00	0.004	O	|	|	|	|	0.00
301.583	0.00	0.00	0.004	O	|	|	|	|	0.00
301.667	0.00	0.00	0.004	O	|	|	|	|	0.00
301.750	0.00	0.00	0.004	O	|	|	|	|	0.00
301.833	0.00	0.00	0.004	O	|	|	|	|	0.00
301.917	0.00	0.00	0.004	O	|	|	|	|	0.00

302.000	0.00	0.00	0.004	O					0.00
302.083	0.00	0.00	0.004	O					0.00
302.167	0.00	0.00	0.004	O					0.00
302.250	0.00	0.00	0.004	O					0.00
302.333	0.00	0.00	0.004	O					0.00
302.417	0.00	0.00	0.004	O					0.00
302.500	0.00	0.00	0.004	O					0.00
302.583	0.00	0.00	0.004	O					0.00
302.667	0.00	0.00	0.004	O					0.00
302.750	0.00	0.00	0.004	O					0.00
302.833	0.00	0.00	0.004	O					0.00
302.917	0.00	0.00	0.004	O					0.00
303.000	0.00	0.00	0.004	O					0.00
303.083	0.00	0.00	0.004	O					0.00
303.167	0.00	0.00	0.004	O					0.00
303.250	0.00	0.00	0.004	O					0.00
303.333	0.00	0.00	0.004	O					0.00
303.417	0.00	0.00	0.004	O					0.00
303.500	0.00	0.00	0.004	O					0.00
303.583	0.00	0.00	0.004	O					0.00
303.667	0.00	0.00	0.004	O					0.00
303.750	0.00	0.00	0.004	O					0.00
303.833	0.00	0.00	0.004	O					0.00
303.917	0.00	0.00	0.004	O					0.00
304.000	0.00	0.00	0.004	O					0.00
304.083	0.00	0.00	0.004	O					0.00
304.167	0.00	0.00	0.004	O					0.00
304.250	0.00	0.00	0.004	O					0.00
304.333	0.00	0.00	0.004	O					0.00
304.417	0.00	0.00	0.004	O					0.00
304.500	0.00	0.00	0.004	O					0.00
304.583	0.00	0.00	0.004	O					0.00
304.667	0.00	0.00	0.004	O					0.00
304.750	0.00	0.00	0.004	O					0.00
304.833	0.00	0.00	0.004	O					0.00
304.917	0.00	0.00	0.004	O					0.00
305.000	0.00	0.00	0.004	O					0.00
305.083	0.00	0.00	0.004	O					0.00
305.167	0.00	0.00	0.004	O					0.00
305.250	0.00	0.00	0.004	O					0.00
305.333	0.00	0.00	0.004	O					0.00
305.417	0.00	0.00	0.004	O					0.00
305.500	0.00	0.00	0.004	O					0.00
305.583	0.00	0.00	0.004	O					0.00
305.667	0.00	0.00	0.004	O					0.00
305.750	0.00	0.00	0.004	O					0.00
305.833	0.00	0.00	0.004	O					0.00
305.917	0.00	0.00	0.004	O					0.00
306.000	0.00	0.00	0.004	O					0.00
306.083	0.00	0.00	0.004	O					0.00
306.167	0.00	0.00	0.004	O					0.00
306.250	0.00	0.00	0.004	O					0.00
306.333	0.00	0.00	0.004	O					0.00
306.417	0.00	0.00	0.004	O					0.00
306.500	0.00	0.00	0.004	O					0.00
306.583	0.00	0.00	0.004	O					0.00
306.667	0.00	0.00	0.004	O					0.00
306.750	0.00	0.00	0.004	O					0.00
306.833	0.00	0.00	0.004	O					0.00
306.917	0.00	0.00	0.004	O					0.00
307.000	0.00	0.00	0.004	O					0.00
307.083	0.00	0.00	0.004	O					0.00
307.167	0.00	0.00	0.004	O					0.00
307.250	0.00	0.00	0.004	O					0.00
307.333	0.00	0.00	0.004	O					0.00
307.417	0.00	0.00	0.004	O					0.00
307.500	0.00	0.00	0.004	O					0.00
307.583	0.00	0.00	0.004	O					0.00
307.667	0.00	0.00	0.004	O					0.00
307.750	0.00	0.00	0.004	O					0.00
307.833	0.00	0.00	0.004	O					0.00

307.917	0.00	0.00	0.004	O	|	|	|	0.00
308.000	0.00	0.00	0.004	O	|	|	|	0.00
308.083	0.00	0.00	0.004	O	|	|	|	0.00
308.167	0.00	0.00	0.004	O	|	|	|	0.00
308.250	0.00	0.00	0.004	O	|	|	|	0.00
308.333	0.00	0.00	0.004	O	|	|	|	0.00
308.417	0.00	0.00	0.004	O	|	|	|	0.00
308.500	0.00	0.00	0.004	O	|	|	|	0.00
308.583	0.00	0.00	0.004	O	|	|	|	0.00
308.667	0.00	0.00	0.004	O	|	|	|	0.00
308.750	0.00	0.00	0.004	O	|	|	|	0.00
308.833	0.00	0.00	0.004	O	|	|	|	0.00
308.917	0.00	0.00	0.004	O	|	|	|	0.00
309.000	0.00	0.00	0.004	O	|	|	|	0.00
309.083	0.00	0.00	0.004	O	|	|	|	0.00
309.167	0.00	0.00	0.004	O	|	|	|	0.00
309.250	0.00	0.00	0.004	O	|	|	|	0.00
309.333	0.00	0.00	0.004	O	|	|	|	0.00
309.417	0.00	0.00	0.004	O	|	|	|	0.00
309.500	0.00	0.00	0.004	O	|	|	|	0.00
309.583	0.00	0.00	0.004	O	|	|	|	0.00
309.667	0.00	0.00	0.004	O	|	|	|	0.00
309.750	0.00	0.00	0.004	O	|	|	|	0.00
309.833	0.00	0.00	0.004	O	|	|	|	0.00
309.917	0.00	0.00	0.004	O	|	|	|	0.00
310.000	0.00	0.00	0.004	O	|	|	|	0.00
310.083	0.00	0.00	0.004	O	|	|	|	0.00
310.167	0.00	0.00	0.004	O	|	|	|	0.00
310.250	0.00	0.00	0.004	O	|	|	|	0.00
310.333	0.00	0.00	0.004	O	|	|	|	0.00
310.417	0.00	0.00	0.004	O	|	|	|	0.00
310.500	0.00	0.00	0.004	O	|	|	|	0.00
310.583	0.00	0.00	0.004	O	|	|	|	0.00
310.667	0.00	0.00	0.004	O	|	|	|	0.00
310.750	0.00	0.00	0.004	O	|	|	|	0.00
310.833	0.00	0.00	0.004	O	|	|	|	0.00
310.917	0.00	0.00	0.004	O	|	|	|	0.00
311.000	0.00	0.00	0.004	O	|	|	|	0.00
311.083	0.00	0.00	0.004	O	|	|	|	0.00
311.167	0.00	0.00	0.004	O	|	|	|	0.00
311.250	0.00	0.00	0.004	O	|	|	|	0.00

Remaining water in basin = 0.00 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 3735
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.298 (CFS)
Total volume = 2.208 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

APPENDIX G.4: ONSITE BASIN ROUTING CALCULATIONS – 100-YEAR, 1-HOUR STORM DURATION

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014
Study date: 10/28/21

HEMET 30 ONSITE BASIN A ROUTING
100-YEAR, 1-HOUR ROUTING ANALYSIS
FILENAME: BASINA1100

Program License Serial Number 6279

********** HYDROGRAPH INFORMATION **********

From study/file name: ARA1POST1100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 15
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 61.227 (CFS)
Total volume = 1.894 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 15
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.500	0.616	0.172	0.615	0.617
1.500	1.965	0.312	1.964	1.966
2.500	3.433	15.406	3.380	3.486
3.500	5.020	37.934	4.889	5.151

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 15.3 30.61 45.92 61.23	Depth (Ft.)
0.083	4.33	0.00	0.015	O I	0.01
0.167	8.29	0.02	0.058	O I	0.05

0.250	10.26	0.03	0.122	O	I	|	|	|	0.10
0.333	11.54	0.05	0.197	O	I	|	|	|	0.16
0.417	13.00	0.08	0.281	O	I	|	|	|	0.23
0.500	15.29	0.11	0.378	O	I	|	|	|	0.31
0.583	17.89	0.14	0.491	O	I	|	|	|	0.40
0.667	21.30	0.17	0.625	O	I	|	|	|	0.51
0.750	29.13	0.19	0.797	O	I	|	|	|	0.63
0.833	61.23	0.22	1.107	O	I	|	|	|	0.86
0.917	50.42	0.26	1.490	O	I	|	|	|	1.15
1.000	21.37	0.29	1.735	O	I	|	|	|	1.33
1.083	9.15	0.30	1.838	O	I	|	|	|	1.41
1.167	1.47	0.30	1.873	O	I	|	|	|	1.43
1.250	0.36	0.30	1.877	O	I	|	|	|	1.43
1.333	0.00	0.30	1.876	O	I	|	|	|	1.43
1.417	0.00	0.30	1.874	O	I	|	|	|	1.43
1.500	0.00	0.30	1.872	O	I	|	|	|	1.43
1.583	0.00	0.30	1.870	O	I	|	|	|	1.43
1.667	0.00	0.30	1.868	O	I	|	|	|	1.43
1.750	0.00	0.30	1.866	O	I	|	|	|	1.43
1.833	0.00	0.30	1.864	O	I	|	|	|	1.42
1.917	0.00	0.30	1.861	O	I	|	|	|	1.42
2.000	0.00	0.30	1.859	O	I	|	|	|	1.42
2.083	0.00	0.30	1.857	O	I	|	|	|	1.42
2.167	0.00	0.30	1.855	O	I	|	|	|	1.42
2.250	0.00	0.30	1.853	O	I	|	|	|	1.42
2.333	0.00	0.30	1.851	O	I	|	|	|	1.42
2.417	0.00	0.30	1.849	O	I	|	|	|	1.41
2.500	0.00	0.30	1.847	O	I	|	|	|	1.41
2.583	0.00	0.30	1.845	O	I	|	|	|	1.41
2.667	0.00	0.30	1.843	O	I	|	|	|	1.41
2.750	0.00	0.30	1.841	O	I	|	|	|	1.41
2.833	0.00	0.30	1.839	O	I	|	|	|	1.41
2.917	0.00	0.30	1.837	O	I	|	|	|	1.40
3.000	0.00	0.30	1.835	O	I	|	|	|	1.40
3.083	0.00	0.30	1.833	O	I	|	|	|	1.40
3.167	0.00	0.30	1.831	O	I	|	|	|	1.40
3.250	0.00	0.30	1.828	O	I	|	|	|	1.40
3.333	0.00	0.30	1.826	O	I	|	|	|	1.40
3.417	0.00	0.30	1.824	O	I	|	|	|	1.40
3.500	0.00	0.30	1.822	O	I	|	|	|	1.39
3.583	0.00	0.30	1.820	O	I	|	|	|	1.39
3.667	0.00	0.30	1.818	O	I	|	|	|	1.39
3.750	0.00	0.30	1.816	O	I	|	|	|	1.39
3.833	0.00	0.30	1.814	O	I	|	|	|	1.39
3.917	0.00	0.30	1.812	O	I	|	|	|	1.39
4.000	0.00	0.30	1.810	O	I	|	|	|	1.39
4.083	0.00	0.30	1.808	O	I	|	|	|	1.38
4.167	0.00	0.30	1.806	O	I	|	|	|	1.38
4.250	0.00	0.30	1.804	O	I	|	|	|	1.38
4.333	0.00	0.30	1.802	O	I	|	|	|	1.38
4.417	0.00	0.29	1.800	O	I	|	|	|	1.38
4.500	0.00	0.29	1.798	O	I	|	|	|	1.38
4.583	0.00	0.29	1.796	O	I	|	|	|	1.37
4.667	0.00	0.29	1.794	O	I	|	|	|	1.37
4.750	0.00	0.29	1.792	O	I	|	|	|	1.37
4.833	0.00	0.29	1.790	O	I	|	|	|	1.37
4.917	0.00	0.29	1.788	O	I	|	|	|	1.37
5.000	0.00	0.29	1.786	O	I	|	|	|	1.37
5.083	0.00	0.29	1.784	O	I	|	|	|	1.37
5.167	0.00	0.29	1.782	O	I	|	|	|	1.36
5.250	0.00	0.29	1.780	O	I	|	|	|	1.36
5.333	0.00	0.29	1.778	O	I	|	|	|	1.36
5.417	0.00	0.29	1.776	O	I	|	|	|	1.36
5.500	0.00	0.29	1.774	O	I	|	|	|	1.36
5.583	0.00	0.29	1.772	O	I	|	|	|	1.36
5.667	0.00	0.29	1.770	O	I	|	|	|	1.36
5.750	0.00	0.29	1.768	O	I	|	|	|	1.35
5.833	0.00	0.29	1.766	O	I	|	|	|	1.35
5.917	0.00	0.29	1.764	O	I	|	|	|	1.35
6.000	0.00	0.29	1.762	O	I	|	|	|	1.35
6.083	0.00	0.29	1.760	O	I	|	|	|	1.35

6.167	0.00	0.29	1.758	O					1.35
6.250	0.00	0.29	1.756	O					1.34
6.333	0.00	0.29	1.754	O					1.34
6.417	0.00	0.29	1.752	O					1.34
6.500	0.00	0.29	1.750	O					1.34
6.583	0.00	0.29	1.748	O					1.34
6.667	0.00	0.29	1.746	O					1.34
6.750	0.00	0.29	1.744	O					1.34
6.833	0.00	0.29	1.742	O					1.33
6.917	0.00	0.29	1.740	O					1.33
7.000	0.00	0.29	1.738	O					1.33
7.083	0.00	0.29	1.736	O					1.33
7.167	0.00	0.29	1.734	O					1.33
7.250	0.00	0.29	1.732	O					1.33
7.333	0.00	0.29	1.730	O					1.33
7.417	0.00	0.29	1.728	O					1.32
7.500	0.00	0.29	1.726	O					1.32
7.583	0.00	0.29	1.724	O					1.32
7.667	0.00	0.29	1.722	O					1.32
7.750	0.00	0.29	1.720	O					1.32
7.833	0.00	0.29	1.718	O					1.32
7.917	0.00	0.29	1.716	O					1.32
8.000	0.00	0.29	1.714	O					1.31
8.083	0.00	0.29	1.712	O					1.31
8.167	0.00	0.29	1.710	O					1.31
8.250	0.00	0.29	1.708	O					1.31
8.333	0.00	0.29	1.706	O					1.31
8.417	0.00	0.28	1.704	O					1.31
8.500	0.00	0.28	1.702	O					1.31
8.583	0.00	0.28	1.700	O					1.30
8.667	0.00	0.28	1.698	O					1.30
8.750	0.00	0.28	1.696	O					1.30
8.833	0.00	0.28	1.694	O					1.30
8.917	0.00	0.28	1.692	O					1.30
9.000	0.00	0.28	1.690	O					1.30
9.083	0.00	0.28	1.688	O					1.29
9.167	0.00	0.28	1.686	O					1.29
9.250	0.00	0.28	1.685	O					1.29
9.333	0.00	0.28	1.683	O					1.29
9.417	0.00	0.28	1.681	O					1.29
9.500	0.00	0.28	1.679	O					1.29
9.583	0.00	0.28	1.677	O					1.29
9.667	0.00	0.28	1.675	O					1.28
9.750	0.00	0.28	1.673	O					1.28
9.833	0.00	0.28	1.671	O					1.28
9.917	0.00	0.28	1.669	O					1.28
10.000	0.00	0.28	1.667	O					1.28
10.083	0.00	0.28	1.665	O					1.28
10.167	0.00	0.28	1.663	O					1.28
10.250	0.00	0.28	1.661	O					1.27
10.333	0.00	0.28	1.659	O					1.27
10.417	0.00	0.28	1.657	O					1.27
10.500	0.00	0.28	1.655	O					1.27
10.583	0.00	0.28	1.654	O					1.27
10.667	0.00	0.28	1.652	O					1.27
10.750	0.00	0.28	1.650	O					1.27
10.833	0.00	0.28	1.648	O					1.26
10.917	0.00	0.28	1.646	O					1.26
11.000	0.00	0.28	1.644	O					1.26
11.083	0.00	0.28	1.642	O					1.26
11.167	0.00	0.28	1.640	O					1.26
11.250	0.00	0.28	1.638	O					1.26
11.333	0.00	0.28	1.636	O					1.26
11.417	0.00	0.28	1.634	O					1.25
11.500	0.00	0.28	1.632	O					1.25
11.583	0.00	0.28	1.631	O					1.25
11.667	0.00	0.28	1.629	O					1.25
11.750	0.00	0.28	1.627	O					1.25
11.833	0.00	0.28	1.625	O					1.25
11.917	0.00	0.28	1.623	O					1.25
12.000	0.00	0.28	1.621	O					1.24

12.083	0.00	0.28	1.619	O				1.24
12.167	0.00	0.28	1.617	O				1.24
12.250	0.00	0.28	1.615	O				1.24
12.333	0.00	0.28	1.613	O				1.24
12.417	0.00	0.28	1.611	O				1.24
12.500	0.00	0.28	1.610	O				1.24
12.583	0.00	0.27	1.608	O				1.24
12.667	0.00	0.27	1.606	O				1.23
12.750	0.00	0.27	1.604	O				1.23
12.833	0.00	0.27	1.602	O				1.23
12.917	0.00	0.27	1.600	O				1.23
13.000	0.00	0.27	1.598	O				1.23
13.083	0.00	0.27	1.596	O				1.23
13.167	0.00	0.27	1.594	O				1.23
13.250	0.00	0.27	1.593	O				1.22
13.333	0.00	0.27	1.591	O				1.22
13.417	0.00	0.27	1.589	O				1.22
13.500	0.00	0.27	1.587	O				1.22
13.583	0.00	0.27	1.585	O				1.22
13.667	0.00	0.27	1.583	O				1.22
13.750	0.00	0.27	1.581	O				1.22
13.833	0.00	0.27	1.579	O				1.21
13.917	0.00	0.27	1.578	O				1.21
14.000	0.00	0.27	1.576	O				1.21
14.083	0.00	0.27	1.574	O				1.21
14.167	0.00	0.27	1.572	O				1.21
14.250	0.00	0.27	1.570	O				1.21
14.333	0.00	0.27	1.568	O				1.21
14.417	0.00	0.27	1.566	O				1.20
14.500	0.00	0.27	1.565	O				1.20
14.583	0.00	0.27	1.563	O				1.20
14.667	0.00	0.27	1.561	O				1.20
14.750	0.00	0.27	1.559	O				1.20
14.833	0.00	0.27	1.557	O				1.20
14.917	0.00	0.27	1.555	O				1.20
15.000	0.00	0.27	1.553	O				1.19
15.083	0.00	0.27	1.552	O				1.19
15.167	0.00	0.27	1.550	O				1.19
15.250	0.00	0.27	1.548	O				1.19
15.333	0.00	0.27	1.546	O				1.19
15.417	0.00	0.27	1.544	O				1.19
15.500	0.00	0.27	1.542	O				1.19
15.583	0.00	0.27	1.540	O				1.19
15.667	0.00	0.27	1.539	O				1.18
15.750	0.00	0.27	1.537	O				1.18
15.833	0.00	0.27	1.535	O				1.18
15.917	0.00	0.27	1.533	O				1.18
16.000	0.00	0.27	1.531	O				1.18
16.083	0.00	0.27	1.529	O				1.18
16.167	0.00	0.27	1.528	O				1.18
16.250	0.00	0.27	1.526	O				1.17
16.333	0.00	0.27	1.524	O				1.17
16.417	0.00	0.27	1.522	O				1.17
16.500	0.00	0.27	1.520	O				1.17
16.583	0.00	0.27	1.518	O				1.17
16.667	0.00	0.27	1.517	O				1.17
16.750	0.00	0.27	1.515	O				1.17
16.833	0.00	0.27	1.513	O				1.16
16.917	0.00	0.26	1.511	O				1.16
17.000	0.00	0.26	1.509	O				1.16
17.083	0.00	0.26	1.507	O				1.16
17.167	0.00	0.26	1.506	O				1.16
17.250	0.00	0.26	1.504	O				1.16
17.333	0.00	0.26	1.502	O				1.16
17.417	0.00	0.26	1.500	O				1.16
17.500	0.00	0.26	1.498	O				1.15
17.583	0.00	0.26	1.496	O				1.15
17.667	0.00	0.26	1.495	O				1.15
17.750	0.00	0.26	1.493	O				1.15
17.833	0.00	0.26	1.491	O				1.15
17.917	0.00	0.26	1.489	O				1.15

18.000	0.00	0.26	1.487	O					1.15
18.083	0.00	0.26	1.486	O					1.14
18.167	0.00	0.26	1.484	O					1.14
18.250	0.00	0.26	1.482	O					1.14
18.333	0.00	0.26	1.480	O					1.14
18.417	0.00	0.26	1.478	O					1.14
18.500	0.00	0.26	1.477	O					1.14
18.583	0.00	0.26	1.475	O					1.14
18.667	0.00	0.26	1.473	O					1.14
18.750	0.00	0.26	1.471	O					1.13
18.833	0.00	0.26	1.469	O					1.13
18.917	0.00	0.26	1.468	O					1.13
19.000	0.00	0.26	1.466	O					1.13
19.083	0.00	0.26	1.464	O					1.13
19.167	0.00	0.26	1.462	O					1.13
19.250	0.00	0.26	1.460	O					1.13
19.333	0.00	0.26	1.459	O					1.12
19.417	0.00	0.26	1.457	O					1.12
19.500	0.00	0.26	1.455	O					1.12
19.583	0.00	0.26	1.453	O					1.12
19.667	0.00	0.26	1.452	O					1.12
19.750	0.00	0.26	1.450	O					1.12
19.833	0.00	0.26	1.448	O					1.12
19.917	0.00	0.26	1.446	O					1.12
20.000	0.00	0.26	1.444	O					1.11
20.083	0.00	0.26	1.443	O					1.11
20.167	0.00	0.26	1.441	O					1.11
20.250	0.00	0.26	1.439	O					1.11
20.333	0.00	0.26	1.437	O					1.11
20.417	0.00	0.26	1.436	O					1.11
20.500	0.00	0.26	1.434	O					1.11
20.583	0.00	0.26	1.432	O					1.10
20.667	0.00	0.26	1.430	O					1.10
20.750	0.00	0.26	1.428	O					1.10
20.833	0.00	0.26	1.427	O					1.10
20.917	0.00	0.26	1.425	O					1.10
21.000	0.00	0.26	1.423	O					1.10
21.083	0.00	0.26	1.421	O					1.10
21.167	0.00	0.26	1.420	O					1.10
21.250	0.00	0.26	1.418	O					1.09
21.333	0.00	0.26	1.416	O					1.09
21.417	0.00	0.25	1.414	O					1.09
21.500	0.00	0.25	1.413	O					1.09
21.583	0.00	0.25	1.411	O					1.09
21.667	0.00	0.25	1.409	O					1.09
21.750	0.00	0.25	1.407	O					1.09
21.833	0.00	0.25	1.406	O					1.09
21.917	0.00	0.25	1.404	O					1.08
22.000	0.00	0.25	1.402	O					1.08
22.083	0.00	0.25	1.400	O					1.08
22.167	0.00	0.25	1.399	O					1.08
22.250	0.00	0.25	1.397	O					1.08
22.333	0.00	0.25	1.395	O					1.08
22.417	0.00	0.25	1.393	O					1.08
22.500	0.00	0.25	1.392	O					1.08
22.583	0.00	0.25	1.390	O					1.07
22.667	0.00	0.25	1.388	O					1.07
22.750	0.00	0.25	1.386	O					1.07
22.833	0.00	0.25	1.385	O					1.07
22.917	0.00	0.25	1.383	O					1.07
23.000	0.00	0.25	1.381	O					1.07
23.083	0.00	0.25	1.380	O					1.07
23.167	0.00	0.25	1.378	O					1.06
23.250	0.00	0.25	1.376	O					1.06
23.333	0.00	0.25	1.374	O					1.06
23.417	0.00	0.25	1.373	O					1.06
23.500	0.00	0.25	1.371	O					1.06
23.583	0.00	0.25	1.369	O					1.06
23.667	0.00	0.25	1.367	O					1.06
23.750	0.00	0.25	1.366	O					1.06
23.833	0.00	0.25	1.364	O					1.05

23.917	0.00	0.25	1.362	O					1.05
24.000	0.00	0.25	1.361	O					1.05
24.083	0.00	0.25	1.359	O					1.05
24.167	0.00	0.25	1.357	O					1.05
24.250	0.00	0.25	1.355	O					1.05
24.333	0.00	0.25	1.354	O					1.05
24.417	0.00	0.25	1.352	O					1.05
24.500	0.00	0.25	1.350	O					1.04
24.583	0.00	0.25	1.349	O					1.04
24.667	0.00	0.25	1.347	O					1.04
24.750	0.00	0.25	1.345	O					1.04
24.833	0.00	0.25	1.343	O					1.04
24.917	0.00	0.25	1.342	O					1.04
25.000	0.00	0.25	1.340	O					1.04
25.083	0.00	0.25	1.338	O					1.04
25.167	0.00	0.25	1.337	O					1.03
25.250	0.00	0.25	1.335	O					1.03
25.333	0.00	0.25	1.333	O					1.03
25.417	0.00	0.25	1.332	O					1.03
25.500	0.00	0.25	1.330	O					1.03
25.583	0.00	0.25	1.328	O					1.03
25.667	0.00	0.25	1.327	O					1.03
25.750	0.00	0.25	1.325	O					1.03
25.833	0.00	0.25	1.323	O					1.02
25.917	0.00	0.25	1.321	O					1.02
26.000	0.00	0.25	1.320	O					1.02
26.083	0.00	0.24	1.318	O					1.02
26.167	0.00	0.24	1.316	O					1.02
26.250	0.00	0.24	1.315	O					1.02
26.333	0.00	0.24	1.313	O					1.02
26.417	0.00	0.24	1.311	O					1.02
26.500	0.00	0.24	1.310	O					1.01
26.583	0.00	0.24	1.308	O					1.01
26.667	0.00	0.24	1.306	O					1.01
26.750	0.00	0.24	1.305	O					1.01
26.833	0.00	0.24	1.303	O					1.01
26.917	0.00	0.24	1.301	O					1.01
27.000	0.00	0.24	1.300	O					1.01
27.083	0.00	0.24	1.298	O					1.01
27.167	0.00	0.24	1.296	O					1.00
27.250	0.00	0.24	1.295	O					1.00
27.333	0.00	0.24	1.293	O					1.00
27.417	0.00	0.24	1.291	O					1.00
27.500	0.00	0.24	1.290	O					1.00
27.583	0.00	0.24	1.288	O					1.00
27.667	0.00	0.24	1.286	O					1.00
27.750	0.00	0.24	1.285	O					1.00
27.833	0.00	0.24	1.283	O					0.99
27.917	0.00	0.24	1.281	O					0.99
28.000	0.00	0.24	1.280	O					0.99
28.083	0.00	0.24	1.278	O					0.99
28.167	0.00	0.24	1.276	O					0.99
28.250	0.00	0.24	1.275	O					0.99
28.333	0.00	0.24	1.273	O					0.99
28.417	0.00	0.24	1.271	O					0.99
28.500	0.00	0.24	1.270	O					0.98
28.583	0.00	0.24	1.268	O					0.98
28.667	0.00	0.24	1.266	O					0.98
28.750	0.00	0.24	1.265	O					0.98
28.833	0.00	0.24	1.263	O					0.98
28.917	0.00	0.24	1.261	O					0.98
29.000	0.00	0.24	1.260	O					0.98
29.083	0.00	0.24	1.258	O					0.98
29.167	0.00	0.24	1.256	O					0.97
29.250	0.00	0.24	1.255	O					0.97
29.333	0.00	0.24	1.253	O					0.97
29.417	0.00	0.24	1.252	O					0.97
29.500	0.00	0.24	1.250	O					0.97
29.583	0.00	0.24	1.248	O					0.97
29.667	0.00	0.24	1.247	O					0.97
29.750	0.00	0.24	1.245	O					0.97

29.833	0.00	0.24	1.243	O				0.97
29.917	0.00	0.24	1.242	O				0.96
30.000	0.00	0.24	1.240	O				0.96
30.083	0.00	0.24	1.238	O				0.96
30.167	0.00	0.24	1.237	O				0.96
30.250	0.00	0.24	1.235	O				0.96
30.333	0.00	0.24	1.234	O				0.96
30.417	0.00	0.24	1.232	O				0.96
30.500	0.00	0.24	1.230	O				0.96
30.583	0.00	0.24	1.229	O				0.95
30.667	0.00	0.24	1.227	O				0.95
30.750	0.00	0.24	1.225	O				0.95
30.833	0.00	0.24	1.224	O				0.95
30.917	0.00	0.23	1.222	O				0.95
31.000	0.00	0.23	1.221	O				0.95
31.083	0.00	0.23	1.219	O				0.95
31.167	0.00	0.23	1.217	O				0.95
31.250	0.00	0.23	1.216	O				0.94
31.333	0.00	0.23	1.214	O				0.94
31.417	0.00	0.23	1.213	O				0.94
31.500	0.00	0.23	1.211	O				0.94
31.583	0.00	0.23	1.209	O				0.94
31.667	0.00	0.23	1.208	O				0.94
31.750	0.00	0.23	1.206	O				0.94
31.833	0.00	0.23	1.205	O				0.94
31.917	0.00	0.23	1.203	O				0.94
32.000	0.00	0.23	1.201	O				0.93
32.083	0.00	0.23	1.200	O				0.93
32.167	0.00	0.23	1.198	O				0.93
32.250	0.00	0.23	1.197	O				0.93
32.333	0.00	0.23	1.195	O				0.93
32.417	0.00	0.23	1.193	O				0.93
32.500	0.00	0.23	1.192	O				0.93
32.583	0.00	0.23	1.190	O				0.93
32.667	0.00	0.23	1.189	O				0.92
32.750	0.00	0.23	1.187	O				0.92
32.833	0.00	0.23	1.185	O				0.92
32.917	0.00	0.23	1.184	O				0.92
33.000	0.00	0.23	1.182	O				0.92
33.083	0.00	0.23	1.181	O				0.92
33.167	0.00	0.23	1.179	O				0.92
33.250	0.00	0.23	1.177	O				0.92
33.333	0.00	0.23	1.176	O				0.91
33.417	0.00	0.23	1.174	O				0.91
33.500	0.00	0.23	1.173	O				0.91
33.583	0.00	0.23	1.171	O				0.91
33.667	0.00	0.23	1.169	O				0.91
33.750	0.00	0.23	1.168	O				0.91
33.833	0.00	0.23	1.166	O				0.91
33.917	0.00	0.23	1.165	O				0.91
34.000	0.00	0.23	1.163	O				0.91
34.083	0.00	0.23	1.162	O				0.90
34.167	0.00	0.23	1.160	O				0.90
34.250	0.00	0.23	1.158	O				0.90
34.333	0.00	0.23	1.157	O				0.90
34.417	0.00	0.23	1.155	O				0.90
34.500	0.00	0.23	1.154	O				0.90
34.583	0.00	0.23	1.152	O				0.90
34.667	0.00	0.23	1.151	O				0.90
34.750	0.00	0.23	1.149	O				0.90
34.833	0.00	0.23	1.147	O				0.89
34.917	0.00	0.23	1.146	O				0.89
35.000	0.00	0.23	1.144	O				0.89
35.083	0.00	0.23	1.143	O				0.89
35.167	0.00	0.23	1.141	O				0.89
35.250	0.00	0.23	1.140	O				0.89
35.333	0.00	0.23	1.138	O				0.89
35.417	0.00	0.23	1.137	O				0.89
35.500	0.00	0.23	1.135	O				0.88
35.583	0.00	0.23	1.133	O				0.88
35.667	0.00	0.23	1.132	O				0.88

35.750	0.00	0.23	1.130	O				0.88
35.833	0.00	0.23	1.129	O				0.88
35.917	0.00	0.23	1.127	O				0.88
36.000	0.00	0.22	1.126	O				0.88
36.083	0.00	0.22	1.124	O				0.88
36.167	0.00	0.22	1.123	O				0.88
36.250	0.00	0.22	1.121	O				0.87
36.333	0.00	0.22	1.119	O				0.87
36.417	0.00	0.22	1.118	O				0.87
36.500	0.00	0.22	1.116	O				0.87
36.583	0.00	0.22	1.115	O				0.87
36.667	0.00	0.22	1.113	O				0.87
36.750	0.00	0.22	1.112	O				0.87
36.833	0.00	0.22	1.110	O				0.87
36.917	0.00	0.22	1.109	O				0.87
37.000	0.00	0.22	1.107	O				0.86
37.083	0.00	0.22	1.106	O				0.86
37.167	0.00	0.22	1.104	O				0.86
37.250	0.00	0.22	1.103	O				0.86
37.333	0.00	0.22	1.101	O				0.86
37.417	0.00	0.22	1.100	O				0.86
37.500	0.00	0.22	1.098	O				0.86
37.583	0.00	0.22	1.096	O				0.86
37.667	0.00	0.22	1.095	O				0.86
37.750	0.00	0.22	1.093	O				0.85
37.833	0.00	0.22	1.092	O				0.85
37.917	0.00	0.22	1.090	O				0.85
38.000	0.00	0.22	1.089	O				0.85
38.083	0.00	0.22	1.087	O				0.85
38.167	0.00	0.22	1.086	O				0.85
38.250	0.00	0.22	1.084	O				0.85
38.333	0.00	0.22	1.083	O				0.85
38.417	0.00	0.22	1.081	O				0.84
38.500	0.00	0.22	1.080	O				0.84
38.583	0.00	0.22	1.078	O				0.84
38.667	0.00	0.22	1.077	O				0.84
38.750	0.00	0.22	1.075	O				0.84
38.833	0.00	0.22	1.074	O				0.84
38.917	0.00	0.22	1.072	O				0.84
39.000	0.00	0.22	1.071	O				0.84
39.083	0.00	0.22	1.069	O				0.84
39.167	0.00	0.22	1.068	O				0.83
39.250	0.00	0.22	1.066	O				0.83
39.333	0.00	0.22	1.065	O				0.83
39.417	0.00	0.22	1.063	O				0.83
39.500	0.00	0.22	1.062	O				0.83
39.583	0.00	0.22	1.060	O				0.83
39.667	0.00	0.22	1.059	O				0.83
39.750	0.00	0.22	1.057	O				0.83
39.833	0.00	0.22	1.056	O				0.83
39.917	0.00	0.22	1.054	O				0.82
40.000	0.00	0.22	1.053	O				0.82
40.083	0.00	0.22	1.051	O				0.82
40.167	0.00	0.22	1.050	O				0.82
40.250	0.00	0.22	1.048	O				0.82
40.333	0.00	0.22	1.047	O				0.82
40.417	0.00	0.22	1.045	O				0.82
40.500	0.00	0.22	1.044	O				0.82
40.583	0.00	0.22	1.042	O				0.82
40.667	0.00	0.22	1.041	O				0.81
40.750	0.00	0.22	1.039	O				0.81
40.833	0.00	0.22	1.038	O				0.81
40.917	0.00	0.22	1.036	O				0.81
41.000	0.00	0.22	1.035	O				0.81
41.083	0.00	0.22	1.033	O				0.81
41.167	0.00	0.22	1.032	O				0.81
41.250	0.00	0.21	1.030	O				0.81
41.333	0.00	0.21	1.029	O				0.81
41.417	0.00	0.21	1.027	O				0.80
41.500	0.00	0.21	1.026	O				0.80
41.583	0.00	0.21	1.024	O				0.80

41.667	0.00	0.21	1.023	O	|	|	|	|	0.80
41.750	0.00	0.21	1.021	O	|	|	|	|	0.80
41.833	0.00	0.21	1.020	O	|	|	|	|	0.80
41.917	0.00	0.21	1.018	O	|	|	|	|	0.80
42.000	0.00	0.21	1.017	O	|	|	|	|	0.80
42.083	0.00	0.21	1.016	O	|	|	|	|	0.80
42.167	0.00	0.21	1.014	O	|	|	|	|	0.80
42.250	0.00	0.21	1.013	O	|	|	|	|	0.79
42.333	0.00	0.21	1.011	O	|	|	|	|	0.79
42.417	0.00	0.21	1.010	O	|	|	|	|	0.79
42.500	0.00	0.21	1.008	O	|	|	|	|	0.79
42.583	0.00	0.21	1.007	O	|	|	|	|	0.79
42.667	0.00	0.21	1.005	O	|	|	|	|	0.79
42.750	0.00	0.21	1.004	O	|	|	|	|	0.79
42.833	0.00	0.21	1.002	O	|	|	|	|	0.79
42.917	0.00	0.21	1.001	O	|	|	|	|	0.79
43.000	0.00	0.21	0.999	O	|	|	|	|	0.78
43.083	0.00	0.21	0.998	O	|	|	|	|	0.78
43.167	0.00	0.21	0.996	O	|	|	|	|	0.78
43.250	0.00	0.21	0.995	O	|	|	|	|	0.78
43.333	0.00	0.21	0.994	O	|	|	|	|	0.78
43.417	0.00	0.21	0.992	O	|	|	|	|	0.78
43.500	0.00	0.21	0.991	O	|	|	|	|	0.78
43.583	0.00	0.21	0.989	O	|	|	|	|	0.78
43.667	0.00	0.21	0.988	O	|	|	|	|	0.78
43.750	0.00	0.21	0.986	O	|	|	|	|	0.77
43.833	0.00	0.21	0.985	O	|	|	|	|	0.77
43.917	0.00	0.21	0.983	O	|	|	|	|	0.77
44.000	0.00	0.21	0.982	O	|	|	|	|	0.77
44.083	0.00	0.21	0.981	O	|	|	|	|	0.77
44.167	0.00	0.21	0.979	O	|	|	|	|	0.77
44.250	0.00	0.21	0.978	O	|	|	|	|	0.77
44.333	0.00	0.21	0.976	O	|	|	|	|	0.77
44.417	0.00	0.21	0.975	O	|	|	|	|	0.77
44.500	0.00	0.21	0.973	O	|	|	|	|	0.76
44.583	0.00	0.21	0.972	O	|	|	|	|	0.76
44.667	0.00	0.21	0.970	O	|	|	|	|	0.76
44.750	0.00	0.21	0.969	O	|	|	|	|	0.76
44.833	0.00	0.21	0.968	O	|	|	|	|	0.76
44.917	0.00	0.21	0.966	O	|	|	|	|	0.76
45.000	0.00	0.21	0.965	O	|	|	|	|	0.76
45.083	0.00	0.21	0.963	O	|	|	|	|	0.76
45.167	0.00	0.21	0.962	O	|	|	|	|	0.76
45.250	0.00	0.21	0.960	O	|	|	|	|	0.76
45.333	0.00	0.21	0.959	O	|	|	|	|	0.75
45.417	0.00	0.21	0.958	O	|	|	|	|	0.75
45.500	0.00	0.21	0.956	O	|	|	|	|	0.75
45.583	0.00	0.21	0.955	O	|	|	|	|	0.75
45.667	0.00	0.21	0.953	O	|	|	|	|	0.75
45.750	0.00	0.21	0.952	O	|	|	|	|	0.75
45.833	0.00	0.21	0.950	O	|	|	|	|	0.75
45.917	0.00	0.21	0.949	O	|	|	|	|	0.75
46.000	0.00	0.21	0.948	O	|	|	|	|	0.75
46.083	0.00	0.21	0.946	O	|	|	|	|	0.74
46.167	0.00	0.21	0.945	O	|	|	|	|	0.74
46.250	0.00	0.21	0.943	O	|	|	|	|	0.74
46.333	0.00	0.21	0.942	O	|	|	|	|	0.74
46.417	0.00	0.21	0.940	O	|	|	|	|	0.74
46.500	0.00	0.21	0.939	O	|	|	|	|	0.74
46.583	0.00	0.21	0.938	O	|	|	|	|	0.74
46.667	0.00	0.21	0.936	O	|	|	|	|	0.74
46.750	0.00	0.21	0.935	O	|	|	|	|	0.74
46.833	0.00	0.20	0.933	O	|	|	|	|	0.74
46.917	0.00	0.20	0.932	O	|	|	|	|	0.73
47.000	0.00	0.20	0.931	O	|	|	|	|	0.73
47.083	0.00	0.20	0.929	O	|	|	|	|	0.73
47.167	0.00	0.20	0.928	O	|	|	|	|	0.73
47.250	0.00	0.20	0.926	O	|	|	|	|	0.73
47.333	0.00	0.20	0.925	O	|	|	|	|	0.73
47.417	0.00	0.20	0.924	O	|	|	|	|	0.73
47.500	0.00	0.20	0.922	O	|	|	|	|	0.73

47.583	0.00	0.20	0.921	O	|	|	|	|	0.73
47.667	0.00	0.20	0.919	O	|	|	|	|	0.72
47.750	0.00	0.20	0.918	O	|	|	|	|	0.72
47.833	0.00	0.20	0.917	O	|	|	|	|	0.72
47.917	0.00	0.20	0.915	O	|	|	|	|	0.72
48.000	0.00	0.20	0.914	O	|	|	|	|	0.72
48.083	0.00	0.20	0.912	O	|	|	|	|	0.72
48.167	0.00	0.20	0.911	O	|	|	|	|	0.72
48.250	0.00	0.20	0.910	O	|	|	|	|	0.72
48.333	0.00	0.20	0.908	O	|	|	|	|	0.72
48.417	0.00	0.20	0.907	O	|	|	|	|	0.72
48.500	0.00	0.20	0.905	O	|	|	|	|	0.71
48.583	0.00	0.20	0.904	O	|	|	|	|	0.71
48.667	0.00	0.20	0.903	O	|	|	|	|	0.71
48.750	0.00	0.20	0.901	O	|	|	|	|	0.71
48.833	0.00	0.20	0.900	O	|	|	|	|	0.71
48.917	0.00	0.20	0.898	O	|	|	|	|	0.71
49.000	0.00	0.20	0.897	O	|	|	|	|	0.71
49.083	0.00	0.20	0.896	O	|	|	|	|	0.71
49.167	0.00	0.20	0.894	O	|	|	|	|	0.71
49.250	0.00	0.20	0.893	O	|	|	|	|	0.71
49.333	0.00	0.20	0.892	O	|	|	|	|	0.70
49.417	0.00	0.20	0.890	O	|	|	|	|	0.70
49.500	0.00	0.20	0.889	O	|	|	|	|	0.70
49.583	0.00	0.20	0.887	O	|	|	|	|	0.70
49.667	0.00	0.20	0.886	O	|	|	|	|	0.70
49.750	0.00	0.20	0.885	O	|	|	|	|	0.70
49.833	0.00	0.20	0.883	O	|	|	|	|	0.70
49.917	0.00	0.20	0.882	O	|	|	|	|	0.70
50.000	0.00	0.20	0.880	O	|	|	|	|	0.70
50.083	0.00	0.20	0.879	O	|	|	|	|	0.70
50.167	0.00	0.20	0.878	O	|	|	|	|	0.69
50.250	0.00	0.20	0.876	O	|	|	|	|	0.69
50.333	0.00	0.20	0.875	O	|	|	|	|	0.69
50.417	0.00	0.20	0.874	O	|	|	|	|	0.69
50.500	0.00	0.20	0.872	O	|	|	|	|	0.69
50.583	0.00	0.20	0.871	O	|	|	|	|	0.69
50.667	0.00	0.20	0.870	O	|	|	|	|	0.69
50.750	0.00	0.20	0.868	O	|	|	|	|	0.69
50.833	0.00	0.20	0.867	O	|	|	|	|	0.69
50.917	0.00	0.20	0.865	O	|	|	|	|	0.68
51.000	0.00	0.20	0.864	O	|	|	|	|	0.68
51.083	0.00	0.20	0.863	O	|	|	|	|	0.68
51.167	0.00	0.20	0.861	O	|	|	|	|	0.68
51.250	0.00	0.20	0.860	O	|	|	|	|	0.68
51.333	0.00	0.20	0.859	O	|	|	|	|	0.68
51.417	0.00	0.20	0.857	O	|	|	|	|	0.68
51.500	0.00	0.20	0.856	O	|	|	|	|	0.68
51.583	0.00	0.20	0.855	O	|	|	|	|	0.68
51.667	0.00	0.20	0.853	O	|	|	|	|	0.68
51.750	0.00	0.20	0.852	O	|	|	|	|	0.67
51.833	0.00	0.20	0.851	O	|	|	|	|	0.67
51.917	0.00	0.20	0.849	O	|	|	|	|	0.67
52.000	0.00	0.20	0.848	O	|	|	|	|	0.67
52.083	0.00	0.20	0.846	O	|	|	|	|	0.67
52.167	0.00	0.20	0.845	O	|	|	|	|	0.67
52.250	0.00	0.20	0.844	O	|	|	|	|	0.67
52.333	0.00	0.20	0.842	O	|	|	|	|	0.67
52.417	0.00	0.20	0.841	O	|	|	|	|	0.67
52.500	0.00	0.20	0.840	O	|	|	|	|	0.67
52.583	0.00	0.20	0.838	O	|	|	|	|	0.66
52.667	0.00	0.19	0.837	O	|	|	|	|	0.66
52.750	0.00	0.19	0.836	O	|	|	|	|	0.66
52.833	0.00	0.19	0.834	O	|	|	|	|	0.66
52.917	0.00	0.19	0.833	O	|	|	|	|	0.66
53.000	0.00	0.19	0.832	O	|	|	|	|	0.66
53.083	0.00	0.19	0.830	O	|	|	|	|	0.66
53.167	0.00	0.19	0.829	O	|	|	|	|	0.66
53.250	0.00	0.19	0.828	O	|	|	|	|	0.66
53.333	0.00	0.19	0.826	O	|	|	|	|	0.66
53.417	0.00	0.19	0.825	O	|	|	|	|	0.65

53.500	0.00	0.19	0.824	O	|	|	|	|	0.65
53.583	0.00	0.19	0.822	O	|	|	|	|	0.65
53.667	0.00	0.19	0.821	O	|	|	|	|	0.65
53.750	0.00	0.19	0.820	O	|	|	|	|	0.65
53.833	0.00	0.19	0.818	O	|	|	|	|	0.65
53.917	0.00	0.19	0.817	O	|	|	|	|	0.65
54.000	0.00	0.19	0.816	O	|	|	|	|	0.65
54.083	0.00	0.19	0.814	O	|	|	|	|	0.65
54.167	0.00	0.19	0.813	O	|	|	|	|	0.65
54.250	0.00	0.19	0.812	O	|	|	|	|	0.65
54.333	0.00	0.19	0.810	O	|	|	|	|	0.64
54.417	0.00	0.19	0.809	O	|	|	|	|	0.64
54.500	0.00	0.19	0.808	O	|	|	|	|	0.64
54.583	0.00	0.19	0.806	O	|	|	|	|	0.64
54.667	0.00	0.19	0.805	O	|	|	|	|	0.64
54.750	0.00	0.19	0.804	O	|	|	|	|	0.64
54.833	0.00	0.19	0.802	O	|	|	|	|	0.64
54.917	0.00	0.19	0.801	O	|	|	|	|	0.64
55.000	0.00	0.19	0.800	O	|	|	|	|	0.64
55.083	0.00	0.19	0.798	O	|	|	|	|	0.64
55.167	0.00	0.19	0.797	O	|	|	|	|	0.63
55.250	0.00	0.19	0.796	O	|	|	|	|	0.63
55.333	0.00	0.19	0.795	O	|	|	|	|	0.63
55.417	0.00	0.19	0.793	O	|	|	|	|	0.63
55.500	0.00	0.19	0.792	O	|	|	|	|	0.63
55.583	0.00	0.19	0.791	O	|	|	|	|	0.63
55.667	0.00	0.19	0.789	O	|	|	|	|	0.63
55.750	0.00	0.19	0.788	O	|	|	|	|	0.63
55.833	0.00	0.19	0.787	O	|	|	|	|	0.63
55.917	0.00	0.19	0.785	O	|	|	|	|	0.63
56.000	0.00	0.19	0.784	O	|	|	|	|	0.62
56.083	0.00	0.19	0.783	O	|	|	|	|	0.62
56.167	0.00	0.19	0.781	O	|	|	|	|	0.62
56.250	0.00	0.19	0.780	O	|	|	|	|	0.62
56.333	0.00	0.19	0.779	O	|	|	|	|	0.62
56.417	0.00	0.19	0.778	O	|	|	|	|	0.62
56.500	0.00	0.19	0.776	O	|	|	|	|	0.62
56.583	0.00	0.19	0.775	O	|	|	|	|	0.62
56.667	0.00	0.19	0.774	O	|	|	|	|	0.62
56.750	0.00	0.19	0.772	O	|	|	|	|	0.62
56.833	0.00	0.19	0.771	O	|	|	|	|	0.61
56.917	0.00	0.19	0.770	O	|	|	|	|	0.61
57.000	0.00	0.19	0.769	O	|	|	|	|	0.61
57.083	0.00	0.19	0.767	O	|	|	|	|	0.61
57.167	0.00	0.19	0.766	O	|	|	|	|	0.61
57.250	0.00	0.19	0.765	O	|	|	|	|	0.61
57.333	0.00	0.19	0.763	O	|	|	|	|	0.61
57.417	0.00	0.19	0.762	O	|	|	|	|	0.61
57.500	0.00	0.19	0.761	O	|	|	|	|	0.61
57.583	0.00	0.19	0.759	O	|	|	|	|	0.61
57.667	0.00	0.19	0.758	O	|	|	|	|	0.61
57.750	0.00	0.19	0.757	O	|	|	|	|	0.60
57.833	0.00	0.19	0.756	O	|	|	|	|	0.60
57.917	0.00	0.19	0.754	O	|	|	|	|	0.60
58.000	0.00	0.19	0.753	O	|	|	|	|	0.60
58.083	0.00	0.19	0.752	O	|	|	|	|	0.60
58.167	0.00	0.19	0.750	O	|	|	|	|	0.60
58.250	0.00	0.19	0.749	O	|	|	|	|	0.60
58.333	0.00	0.19	0.748	O	|	|	|	|	0.60
58.417	0.00	0.19	0.747	O	|	|	|	|	0.60
58.500	0.00	0.19	0.745	O	|	|	|	|	0.60
58.583	0.00	0.19	0.744	O	|	|	|	|	0.59
58.667	0.00	0.19	0.743	O	|	|	|	|	0.59
58.750	0.00	0.19	0.742	O	|	|	|	|	0.59
58.833	0.00	0.18	0.740	O	|	|	|	|	0.59
58.917	0.00	0.18	0.739	O	|	|	|	|	0.59
59.000	0.00	0.18	0.738	O	|	|	|	|	0.59
59.083	0.00	0.18	0.736	O	|	|	|	|	0.59
59.167	0.00	0.18	0.735	O	|	|	|	|	0.59
59.250	0.00	0.18	0.734	O	|	|	|	|	0.59
59.333	0.00	0.18	0.733	O	|	|	|	|	0.59

59.417	0.00	0.18	0.731	O	|	|	|	|	0.59
59.500	0.00	0.18	0.730	O	|	|	|	|	0.58
59.583	0.00	0.18	0.729	O	|	|	|	|	0.58
59.667	0.00	0.18	0.728	O	|	|	|	|	0.58
59.750	0.00	0.18	0.726	O	|	|	|	|	0.58
59.833	0.00	0.18	0.725	O	|	|	|	|	0.58
59.917	0.00	0.18	0.724	O	|	|	|	|	0.58
60.000	0.00	0.18	0.723	O	|	|	|	|	0.58
60.083	0.00	0.18	0.721	O	|	|	|	|	0.58
60.167	0.00	0.18	0.720	O	|	|	|	|	0.58
60.250	0.00	0.18	0.719	O	|	|	|	|	0.58
60.333	0.00	0.18	0.717	O	|	|	|	|	0.58
60.417	0.00	0.18	0.716	O	|	|	|	|	0.57
60.500	0.00	0.18	0.715	O	|	|	|	|	0.57
60.583	0.00	0.18	0.714	O	|	|	|	|	0.57
60.667	0.00	0.18	0.712	O	|	|	|	|	0.57
60.750	0.00	0.18	0.711	O	|	|	|	|	0.57
60.833	0.00	0.18	0.710	O	|	|	|	|	0.57
60.917	0.00	0.18	0.709	O	|	|	|	|	0.57
61.000	0.00	0.18	0.707	O	|	|	|	|	0.57
61.083	0.00	0.18	0.706	O	|	|	|	|	0.57
61.167	0.00	0.18	0.705	O	|	|	|	|	0.57
61.250	0.00	0.18	0.704	O	|	|	|	|	0.57
61.333	0.00	0.18	0.702	O	|	|	|	|	0.56
61.417	0.00	0.18	0.701	O	|	|	|	|	0.56
61.500	0.00	0.18	0.700	O	|	|	|	|	0.56
61.583	0.00	0.18	0.699	O	|	|	|	|	0.56
61.667	0.00	0.18	0.697	O	|	|	|	|	0.56
61.750	0.00	0.18	0.696	O	|	|	|	|	0.56
61.833	0.00	0.18	0.695	O	|	|	|	|	0.56
61.917	0.00	0.18	0.694	O	|	|	|	|	0.56
62.000	0.00	0.18	0.693	O	|	|	|	|	0.56
62.083	0.00	0.18	0.691	O	|	|	|	|	0.56
62.167	0.00	0.18	0.690	O	|	|	|	|	0.55
62.250	0.00	0.18	0.689	O	|	|	|	|	0.55
62.333	0.00	0.18	0.688	O	|	|	|	|	0.55
62.417	0.00	0.18	0.686	O	|	|	|	|	0.55
62.500	0.00	0.18	0.685	O	|	|	|	|	0.55
62.583	0.00	0.18	0.684	O	|	|	|	|	0.55
62.667	0.00	0.18	0.683	O	|	|	|	|	0.55
62.750	0.00	0.18	0.681	O	|	|	|	|	0.55
62.833	0.00	0.18	0.680	O	|	|	|	|	0.55
62.917	0.00	0.18	0.679	O	|	|	|	|	0.55
63.000	0.00	0.18	0.678	O	|	|	|	|	0.55
63.083	0.00	0.18	0.676	O	|	|	|	|	0.54
63.167	0.00	0.18	0.675	O	|	|	|	|	0.54
63.250	0.00	0.18	0.674	O	|	|	|	|	0.54
63.333	0.00	0.18	0.673	O	|	|	|	|	0.54
63.417	0.00	0.18	0.672	O	|	|	|	|	0.54
63.500	0.00	0.18	0.670	O	|	|	|	|	0.54
63.583	0.00	0.18	0.669	O	|	|	|	|	0.54
63.667	0.00	0.18	0.668	O	|	|	|	|	0.54
63.750	0.00	0.18	0.667	O	|	|	|	|	0.54
63.833	0.00	0.18	0.665	O	|	|	|	|	0.54
63.917	0.00	0.18	0.664	O	|	|	|	|	0.54
64.000	0.00	0.18	0.663	O	|	|	|	|	0.53
64.083	0.00	0.18	0.662	O	|	|	|	|	0.53
64.167	0.00	0.18	0.661	O	|	|	|	|	0.53
64.250	0.00	0.18	0.659	O	|	|	|	|	0.53
64.333	0.00	0.18	0.658	O	|	|	|	|	0.53
64.417	0.00	0.18	0.657	O	|	|	|	|	0.53
64.500	0.00	0.18	0.656	O	|	|	|	|	0.53
64.583	0.00	0.18	0.655	O	|	|	|	|	0.53
64.667	0.00	0.18	0.653	O	|	|	|	|	0.53
64.750	0.00	0.18	0.652	O	|	|	|	|	0.53
64.833	0.00	0.18	0.651	O	|	|	|	|	0.53
64.917	0.00	0.18	0.650	O	|	|	|	|	0.52
65.000	0.00	0.18	0.648	O	|	|	|	|	0.52
65.083	0.00	0.18	0.647	O	|	|	|	|	0.52
65.167	0.00	0.18	0.646	O	|	|	|	|	0.52
65.250	0.00	0.17	0.645	O	|	|	|	|	0.52

65.333	0.00	0.17	0.644	O				0.52
65.417	0.00	0.17	0.642	O				0.52
65.500	0.00	0.17	0.641	O				0.52
65.583	0.00	0.17	0.640	O				0.52
65.667	0.00	0.17	0.639	O				0.52
65.750	0.00	0.17	0.638	O				0.52
65.833	0.00	0.17	0.636	O				0.52
65.917	0.00	0.17	0.635	O				0.51
66.000	0.00	0.17	0.634	O				0.51
66.083	0.00	0.17	0.633	O				0.51
66.167	0.00	0.17	0.632	O				0.51
66.250	0.00	0.17	0.630	O				0.51
66.333	0.00	0.17	0.629	O				0.51
66.417	0.00	0.17	0.628	O				0.51
66.500	0.00	0.17	0.627	O				0.51
66.583	0.00	0.17	0.626	O				0.51
66.667	0.00	0.17	0.624	O				0.51
66.750	0.00	0.17	0.623	O				0.51
66.833	0.00	0.17	0.622	O				0.50
66.917	0.00	0.17	0.621	O				0.50
67.000	0.00	0.17	0.620	O				0.50
67.083	0.00	0.17	0.619	O				0.50
67.167	0.00	0.17	0.617	O				0.50
67.250	0.00	0.17	0.616	O				0.50
67.333	0.00	0.17	0.615	O				0.50
67.417	0.00	0.17	0.614	O				0.50
67.500	0.00	0.17	0.613	O				0.50
67.583	0.00	0.17	0.611	O				0.50
67.667	0.00	0.17	0.610	O				0.50
67.750	0.00	0.17	0.609	O				0.49
67.833	0.00	0.17	0.608	O				0.49
67.917	0.00	0.17	0.607	O				0.49
68.000	0.00	0.17	0.606	O				0.49
68.083	0.00	0.17	0.604	O				0.49
68.167	0.00	0.17	0.603	O				0.49
68.250	0.00	0.17	0.602	O				0.49
68.333	0.00	0.17	0.601	O				0.49
68.417	0.00	0.17	0.600	O				0.49
68.500	0.00	0.17	0.599	O				0.49
68.583	0.00	0.17	0.598	O				0.48
68.667	0.00	0.17	0.596	O				0.48
68.750	0.00	0.17	0.595	O				0.48
68.833	0.00	0.17	0.594	O				0.48
68.917	0.00	0.17	0.593	O				0.48
69.000	0.00	0.17	0.592	O				0.48
69.083	0.00	0.16	0.591	O				0.48
69.167	0.00	0.16	0.590	O				0.48
69.250	0.00	0.16	0.588	O				0.48
69.333	0.00	0.16	0.587	O				0.48
69.417	0.00	0.16	0.586	O				0.48
69.500	0.00	0.16	0.585	O				0.47
69.583	0.00	0.16	0.584	O				0.47
69.667	0.00	0.16	0.583	O				0.47
69.750	0.00	0.16	0.582	O				0.47
69.833	0.00	0.16	0.581	O				0.47
69.917	0.00	0.16	0.579	O				0.47
70.000	0.00	0.16	0.578	O				0.47
70.083	0.00	0.16	0.577	O				0.47
70.167	0.00	0.16	0.576	O				0.47
70.250	0.00	0.16	0.575	O				0.47
70.333	0.00	0.16	0.574	O				0.47
70.417	0.00	0.16	0.573	O				0.46
70.500	0.00	0.16	0.572	O				0.46
70.583	0.00	0.16	0.571	O				0.46
70.667	0.00	0.16	0.569	O				0.46
70.750	0.00	0.16	0.568	O				0.46
70.833	0.00	0.16	0.567	O				0.46
70.917	0.00	0.16	0.566	O				0.46
71.000	0.00	0.16	0.565	O				0.46
71.083	0.00	0.16	0.564	O				0.46
71.167	0.00	0.16	0.563	O				0.46

71.250	0.00	0.16	0.562	O	|	|	|	|	0.46
71.333	0.00	0.16	0.561	O	|	|	|	|	0.46
71.417	0.00	0.16	0.560	O	|	|	|	|	0.45
71.500	0.00	0.16	0.559	O	|	|	|	|	0.45
71.583	0.00	0.16	0.558	O	|	|	|	|	0.45
71.667	0.00	0.16	0.556	O	|	|	|	|	0.45
71.750	0.00	0.16	0.555	O	|	|	|	|	0.45
71.833	0.00	0.15	0.554	O	|	|	|	|	0.45
71.917	0.00	0.15	0.553	O	|	|	|	|	0.45
72.000	0.00	0.15	0.552	O	|	|	|	|	0.45
72.083	0.00	0.15	0.551	O	|	|	|	|	0.45
72.167	0.00	0.15	0.550	O	|	|	|	|	0.45
72.250	0.00	0.15	0.549	O	|	|	|	|	0.45
72.333	0.00	0.15	0.548	O	|	|	|	|	0.44
72.417	0.00	0.15	0.547	O	|	|	|	|	0.44
72.500	0.00	0.15	0.546	O	|	|	|	|	0.44
72.583	0.00	0.15	0.545	O	|	|	|	|	0.44
72.667	0.00	0.15	0.544	O	|	|	|	|	0.44
72.750	0.00	0.15	0.543	O	|	|	|	|	0.44
72.833	0.00	0.15	0.542	O	|	|	|	|	0.44
72.917	0.00	0.15	0.541	O	|	|	|	|	0.44
73.000	0.00	0.15	0.540	O	|	|	|	|	0.44
73.083	0.00	0.15	0.539	O	|	|	|	|	0.44
73.167	0.00	0.15	0.538	O	|	|	|	|	0.44
73.250	0.00	0.15	0.537	O	|	|	|	|	0.44
73.333	0.00	0.15	0.535	O	|	|	|	|	0.43
73.417	0.00	0.15	0.534	O	|	|	|	|	0.43
73.500	0.00	0.15	0.533	O	|	|	|	|	0.43
73.583	0.00	0.15	0.532	O	|	|	|	|	0.43
73.667	0.00	0.15	0.531	O	|	|	|	|	0.43
73.750	0.00	0.15	0.530	O	|	|	|	|	0.43
73.833	0.00	0.15	0.529	O	|	|	|	|	0.43
73.917	0.00	0.15	0.528	O	|	|	|	|	0.43
74.000	0.00	0.15	0.527	O	|	|	|	|	0.43
74.083	0.00	0.15	0.526	O	|	|	|	|	0.43
74.167	0.00	0.15	0.525	O	|	|	|	|	0.43
74.250	0.00	0.15	0.524	O	|	|	|	|	0.43
74.333	0.00	0.15	0.523	O	|	|	|	|	0.42
74.417	0.00	0.15	0.522	O	|	|	|	|	0.42
74.500	0.00	0.15	0.521	O	|	|	|	|	0.42
74.583	0.00	0.15	0.520	O	|	|	|	|	0.42
74.667	0.00	0.14	0.519	O	|	|	|	|	0.42
74.750	0.00	0.14	0.518	O	|	|	|	|	0.42
74.833	0.00	0.14	0.517	O	|	|	|	|	0.42
74.917	0.00	0.14	0.516	O	|	|	|	|	0.42
75.000	0.00	0.14	0.515	O	|	|	|	|	0.42
75.083	0.00	0.14	0.514	O	|	|	|	|	0.42
75.167	0.00	0.14	0.513	O	|	|	|	|	0.42
75.250	0.00	0.14	0.512	O	|	|	|	|	0.42
75.333	0.00	0.14	0.511	O	|	|	|	|	0.42
75.417	0.00	0.14	0.510	O	|	|	|	|	0.41
75.500	0.00	0.14	0.509	O	|	|	|	|	0.41
75.583	0.00	0.14	0.508	O	|	|	|	|	0.41
75.667	0.00	0.14	0.507	O	|	|	|	|	0.41
75.750	0.00	0.14	0.506	O	|	|	|	|	0.41
75.833	0.00	0.14	0.505	O	|	|	|	|	0.41
75.917	0.00	0.14	0.504	O	|	|	|	|	0.41
76.000	0.00	0.14	0.504	O	|	|	|	|	0.41
76.083	0.00	0.14	0.503	O	|	|	|	|	0.41
76.167	0.00	0.14	0.502	O	|	|	|	|	0.41
76.250	0.00	0.14	0.501	O	|	|	|	|	0.41
76.333	0.00	0.14	0.500	O	|	|	|	|	0.41
76.417	0.00	0.14	0.499	O	|	|	|	|	0.40
76.500	0.00	0.14	0.498	O	|	|	|	|	0.40
76.583	0.00	0.14	0.497	O	|	|	|	|	0.40
76.667	0.00	0.14	0.496	O	|	|	|	|	0.40
76.750	0.00	0.14	0.495	O	|	|	|	|	0.40
76.833	0.00	0.14	0.494	O	|	|	|	|	0.40
76.917	0.00	0.14	0.493	O	|	|	|	|	0.40
77.000	0.00	0.14	0.492	O	|	|	|	|	0.40
77.083	0.00	0.14	0.491	O	|	|	|	|	0.40

77.167	0.00	0.14	0.490	O	|	|	|	|	0.40
77.250	0.00	0.14	0.489	O	|	|	|	|	0.40
77.333	0.00	0.14	0.488	O	|	|	|	|	0.40
77.417	0.00	0.14	0.487	O	|	|	|	|	0.40
77.500	0.00	0.14	0.486	O	|	|	|	|	0.39
77.583	0.00	0.14	0.485	O	|	|	|	|	0.39
77.667	0.00	0.14	0.485	O	|	|	|	|	0.39
77.750	0.00	0.14	0.484	O	|	|	|	|	0.39
77.833	0.00	0.13	0.483	O	|	|	|	|	0.39
77.917	0.00	0.13	0.482	O	|	|	|	|	0.39
78.000	0.00	0.13	0.481	O	|	|	|	|	0.39
78.083	0.00	0.13	0.480	O	|	|	|	|	0.39
78.167	0.00	0.13	0.479	O	|	|	|	|	0.39
78.250	0.00	0.13	0.478	O	|	|	|	|	0.39
78.333	0.00	0.13	0.477	O	|	|	|	|	0.39
78.417	0.00	0.13	0.476	O	|	|	|	|	0.39
78.500	0.00	0.13	0.475	O	|	|	|	|	0.39
78.583	0.00	0.13	0.474	O	|	|	|	|	0.39
78.667	0.00	0.13	0.473	O	|	|	|	|	0.38
78.750	0.00	0.13	0.473	O	|	|	|	|	0.38
78.833	0.00	0.13	0.472	O	|	|	|	|	0.38
78.917	0.00	0.13	0.471	O	|	|	|	|	0.38
79.000	0.00	0.13	0.470	O	|	|	|	|	0.38
79.083	0.00	0.13	0.469	O	|	|	|	|	0.38
79.167	0.00	0.13	0.468	O	|	|	|	|	0.38
79.250	0.00	0.13	0.467	O	|	|	|	|	0.38
79.333	0.00	0.13	0.466	O	|	|	|	|	0.38
79.417	0.00	0.13	0.465	O	|	|	|	|	0.38
79.500	0.00	0.13	0.464	O	|	|	|	|	0.38
79.583	0.00	0.13	0.464	O	|	|	|	|	0.38
79.667	0.00	0.13	0.463	O	|	|	|	|	0.38
79.750	0.00	0.13	0.462	O	|	|	|	|	0.37
79.833	0.00	0.13	0.461	O	|	|	|	|	0.37
79.917	0.00	0.13	0.460	O	|	|	|	|	0.37
80.000	0.00	0.13	0.459	O	|	|	|	|	0.37
80.083	0.00	0.13	0.458	O	|	|	|	|	0.37
80.167	0.00	0.13	0.457	O	|	|	|	|	0.37
80.250	0.00	0.13	0.456	O	|	|	|	|	0.37
80.333	0.00	0.13	0.456	O	|	|	|	|	0.37
80.417	0.00	0.13	0.455	O	|	|	|	|	0.37
80.500	0.00	0.13	0.454	O	|	|	|	|	0.37
80.583	0.00	0.13	0.453	O	|	|	|	|	0.37
80.667	0.00	0.13	0.452	O	|	|	|	|	0.37
80.750	0.00	0.13	0.451	O	|	|	|	|	0.37
80.833	0.00	0.13	0.450	O	|	|	|	|	0.37
80.917	0.00	0.13	0.450	O	|	|	|	|	0.36
81.000	0.00	0.13	0.449	O	|	|	|	|	0.36
81.083	0.00	0.13	0.448	O	|	|	|	|	0.36
81.167	0.00	0.12	0.447	O	|	|	|	|	0.36
81.250	0.00	0.12	0.446	O	|	|	|	|	0.36
81.333	0.00	0.12	0.445	O	|	|	|	|	0.36
81.417	0.00	0.12	0.444	O	|	|	|	|	0.36
81.500	0.00	0.12	0.444	O	|	|	|	|	0.36
81.583	0.00	0.12	0.443	O	|	|	|	|	0.36
81.667	0.00	0.12	0.442	O	|	|	|	|	0.36
81.750	0.00	0.12	0.441	O	|	|	|	|	0.36
81.833	0.00	0.12	0.440	O	|	|	|	|	0.36
81.917	0.00	0.12	0.439	O	|	|	|	|	0.36
82.000	0.00	0.12	0.438	O	|	|	|	|	0.36
82.083	0.00	0.12	0.438	O	|	|	|	|	0.36
82.167	0.00	0.12	0.437	O	|	|	|	|	0.35
82.250	0.00	0.12	0.436	O	|	|	|	|	0.35
82.333	0.00	0.12	0.435	O	|	|	|	|	0.35
82.417	0.00	0.12	0.434	O	|	|	|	|	0.35
82.500	0.00	0.12	0.433	O	|	|	|	|	0.35
82.583	0.00	0.12	0.433	O	|	|	|	|	0.35
82.667	0.00	0.12	0.432	O	|	|	|	|	0.35
82.750	0.00	0.12	0.431	O	|	|	|	|	0.35
82.833	0.00	0.12	0.430	O	|	|	|	|	0.35
82.917	0.00	0.12	0.429	O	|	|	|	|	0.35
83.000	0.00	0.12	0.428	O	|	|	|	|	0.35

83.083	0.00	0.12	0.428	O	|	|	|	|	0.35
83.167	0.00	0.12	0.427	O	|	|	|	|	0.35
83.250	0.00	0.12	0.426	O	|	|	|	|	0.35
83.333	0.00	0.12	0.425	O	|	|	|	|	0.35
83.417	0.00	0.12	0.424	O	|	|	|	|	0.34
83.500	0.00	0.12	0.424	O	|	|	|	|	0.34
83.583	0.00	0.12	0.423	O	|	|	|	|	0.34
83.667	0.00	0.12	0.422	O	|	|	|	|	0.34
83.750	0.00	0.12	0.421	O	|	|	|	|	0.34
83.833	0.00	0.12	0.420	O	|	|	|	|	0.34
83.917	0.00	0.12	0.419	O	|	|	|	|	0.34
84.000	0.00	0.12	0.419	O	|	|	|	|	0.34
84.083	0.00	0.12	0.418	O	|	|	|	|	0.34
84.167	0.00	0.12	0.417	O	|	|	|	|	0.34
84.250	0.00	0.12	0.416	O	|	|	|	|	0.34
84.333	0.00	0.12	0.415	O	|	|	|	|	0.34
84.417	0.00	0.12	0.415	O	|	|	|	|	0.34
84.500	0.00	0.12	0.414	O	|	|	|	|	0.34
84.583	0.00	0.12	0.413	O	|	|	|	|	0.34
84.667	0.00	0.12	0.412	O	|	|	|	|	0.33
84.750	0.00	0.11	0.411	O	|	|	|	|	0.33
84.833	0.00	0.11	0.411	O	|	|	|	|	0.33
84.917	0.00	0.11	0.410	O	|	|	|	|	0.33
85.000	0.00	0.11	0.409	O	|	|	|	|	0.33
85.083	0.00	0.11	0.408	O	|	|	|	|	0.33
85.167	0.00	0.11	0.408	O	|	|	|	|	0.33
85.250	0.00	0.11	0.407	O	|	|	|	|	0.33
85.333	0.00	0.11	0.406	O	|	|	|	|	0.33
85.417	0.00	0.11	0.405	O	|	|	|	|	0.33
85.500	0.00	0.11	0.404	O	|	|	|	|	0.33
85.583	0.00	0.11	0.404	O	|	|	|	|	0.33
85.667	0.00	0.11	0.403	O	|	|	|	|	0.33
85.750	0.00	0.11	0.402	O	|	|	|	|	0.33
85.833	0.00	0.11	0.401	O	|	|	|	|	0.33
85.917	0.00	0.11	0.401	O	|	|	|	|	0.33
86.000	0.00	0.11	0.400	O	|	|	|	|	0.32
86.083	0.00	0.11	0.399	O	|	|	|	|	0.32
86.167	0.00	0.11	0.398	O	|	|	|	|	0.32
86.250	0.00	0.11	0.397	O	|	|	|	|	0.32
86.333	0.00	0.11	0.397	O	|	|	|	|	0.32
86.417	0.00	0.11	0.396	O	|	|	|	|	0.32
86.500	0.00	0.11	0.395	O	|	|	|	|	0.32
86.583	0.00	0.11	0.394	O	|	|	|	|	0.32
86.667	0.00	0.11	0.394	O	|	|	|	|	0.32
86.750	0.00	0.11	0.393	O	|	|	|	|	0.32
86.833	0.00	0.11	0.392	O	|	|	|	|	0.32
86.917	0.00	0.11	0.391	O	|	|	|	|	0.32
87.000	0.00	0.11	0.391	O	|	|	|	|	0.32
87.083	0.00	0.11	0.390	O	|	|	|	|	0.32
87.167	0.00	0.11	0.389	O	|	|	|	|	0.32
87.250	0.00	0.11	0.388	O	|	|	|	|	0.32
87.333	0.00	0.11	0.388	O	|	|	|	|	0.31
87.417	0.00	0.11	0.387	O	|	|	|	|	0.31
87.500	0.00	0.11	0.386	O	|	|	|	|	0.31
87.583	0.00	0.11	0.385	O	|	|	|	|	0.31
87.667	0.00	0.11	0.385	O	|	|	|	|	0.31
87.750	0.00	0.11	0.384	O	|	|	|	|	0.31
87.833	0.00	0.11	0.383	O	|	|	|	|	0.31
87.917	0.00	0.11	0.382	O	|	|	|	|	0.31
88.000	0.00	0.11	0.382	O	|	|	|	|	0.31
88.083	0.00	0.11	0.381	O	|	|	|	|	0.31
88.167	0.00	0.11	0.380	O	|	|	|	|	0.31
88.250	0.00	0.11	0.380	O	|	|	|	|	0.31
88.333	0.00	0.11	0.379	O	|	|	|	|	0.31
88.417	0.00	0.11	0.378	O	|	|	|	|	0.31
88.500	0.00	0.11	0.377	O	|	|	|	|	0.31
88.583	0.00	0.11	0.377	O	|	|	|	|	0.31
88.667	0.00	0.10	0.376	O	|	|	|	|	0.31
88.750	0.00	0.10	0.375	O	|	|	|	|	0.30
88.833	0.00	0.10	0.374	O	|	|	|	|	0.30
88.917	0.00	0.10	0.374	O	|	|	|	|	0.30

89.000	0.00	0.10	0.373	O	|	|	|	|	0.30
89.083	0.00	0.10	0.372	O	|	|	|	|	0.30
89.167	0.00	0.10	0.372	O	|	|	|	|	0.30
89.250	0.00	0.10	0.371	O	|	|	|	|	0.30
89.333	0.00	0.10	0.370	O	|	|	|	|	0.30
89.417	0.00	0.10	0.369	O	|	|	|	|	0.30
89.500	0.00	0.10	0.369	O	|	|	|	|	0.30
89.583	0.00	0.10	0.368	O	|	|	|	|	0.30
89.667	0.00	0.10	0.367	O	|	|	|	|	0.30
89.750	0.00	0.10	0.367	O	|	|	|	|	0.30
89.833	0.00	0.10	0.366	O	|	|	|	|	0.30
89.917	0.00	0.10	0.365	O	|	|	|	|	0.30
90.000	0.00	0.10	0.365	O	|	|	|	|	0.30
90.083	0.00	0.10	0.364	O	|	|	|	|	0.30
90.167	0.00	0.10	0.363	O	|	|	|	|	0.29
90.250	0.00	0.10	0.362	O	|	|	|	|	0.29
90.333	0.00	0.10	0.362	O	|	|	|	|	0.29
90.417	0.00	0.10	0.361	O	|	|	|	|	0.29
90.500	0.00	0.10	0.360	O	|	|	|	|	0.29
90.583	0.00	0.10	0.360	O	|	|	|	|	0.29
90.667	0.00	0.10	0.359	O	|	|	|	|	0.29
90.750	0.00	0.10	0.358	O	|	|	|	|	0.29
90.833	0.00	0.10	0.358	O	|	|	|	|	0.29
90.917	0.00	0.10	0.357	O	|	|	|	|	0.29
91.000	0.00	0.10	0.356	O	|	|	|	|	0.29
91.083	0.00	0.10	0.356	O	|	|	|	|	0.29
91.167	0.00	0.10	0.355	O	|	|	|	|	0.29
91.250	0.00	0.10	0.354	O	|	|	|	|	0.29
91.333	0.00	0.10	0.353	O	|	|	|	|	0.29
91.417	0.00	0.10	0.353	O	|	|	|	|	0.29
91.500	0.00	0.10	0.352	O	|	|	|	|	0.29
91.583	0.00	0.10	0.351	O	|	|	|	|	0.29
91.667	0.00	0.10	0.351	O	|	|	|	|	0.28
91.750	0.00	0.10	0.350	O	|	|	|	|	0.28
91.833	0.00	0.10	0.349	O	|	|	|	|	0.28
91.917	0.00	0.10	0.349	O	|	|	|	|	0.28
92.000	0.00	0.10	0.348	O	|	|	|	|	0.28
92.083	0.00	0.10	0.347	O	|	|	|	|	0.28
92.167	0.00	0.10	0.347	O	|	|	|	|	0.28
92.250	0.00	0.10	0.346	O	|	|	|	|	0.28
92.333	0.00	0.10	0.345	O	|	|	|	|	0.28
92.417	0.00	0.10	0.345	O	|	|	|	|	0.28
92.500	0.00	0.10	0.344	O	|	|	|	|	0.28
92.583	0.00	0.10	0.343	O	|	|	|	|	0.28
92.667	0.00	0.10	0.343	O	|	|	|	|	0.28
92.750	0.00	0.10	0.342	O	|	|	|	|	0.28
92.833	0.00	0.10	0.341	O	|	|	|	|	0.28
92.917	0.00	0.10	0.341	O	|	|	|	|	0.28
93.000	0.00	0.09	0.340	O	|	|	|	|	0.28
93.083	0.00	0.09	0.339	O	|	|	|	|	0.28
93.167	0.00	0.09	0.339	O	|	|	|	|	0.28
93.250	0.00	0.09	0.338	O	|	|	|	|	0.27
93.333	0.00	0.09	0.338	O	|	|	|	|	0.27
93.417	0.00	0.09	0.337	O	|	|	|	|	0.27
93.500	0.00	0.09	0.336	O	|	|	|	|	0.27
93.583	0.00	0.09	0.336	O	|	|	|	|	0.27
93.667	0.00	0.09	0.335	O	|	|	|	|	0.27
93.750	0.00	0.09	0.334	O	|	|	|	|	0.27
93.833	0.00	0.09	0.334	O	|	|	|	|	0.27
93.917	0.00	0.09	0.333	O	|	|	|	|	0.27
94.000	0.00	0.09	0.332	O	|	|	|	|	0.27
94.083	0.00	0.09	0.332	O	|	|	|	|	0.27
94.167	0.00	0.09	0.331	O	|	|	|	|	0.27
94.250	0.00	0.09	0.330	O	|	|	|	|	0.27
94.333	0.00	0.09	0.330	O	|	|	|	|	0.27
94.417	0.00	0.09	0.329	O	|	|	|	|	0.27
94.500	0.00	0.09	0.329	O	|	|	|	|	0.27
94.583	0.00	0.09	0.328	O	|	|	|	|	0.27
94.667	0.00	0.09	0.327	O	|	|	|	|	0.27
94.750	0.00	0.09	0.327	O	|	|	|	|	0.27
94.833	0.00	0.09	0.326	O	|	|	|	|	0.26

94.917	0.00	0.09	0.325	O					0.26
95.000	0.00	0.09	0.325	O					0.26
95.083	0.00	0.09	0.324	O					0.26
95.167	0.00	0.09	0.324	O					0.26
95.250	0.00	0.09	0.323	O					0.26
95.333	0.00	0.09	0.322	O					0.26
95.417	0.00	0.09	0.322	O					0.26
95.500	0.00	0.09	0.321	O					0.26
95.583	0.00	0.09	0.320	O					0.26
95.667	0.00	0.09	0.320	O					0.26
95.750	0.00	0.09	0.319	O					0.26
95.833	0.00	0.09	0.319	O					0.26
95.917	0.00	0.09	0.318	O					0.26
96.000	0.00	0.09	0.317	O					0.26
96.083	0.00	0.09	0.317	O					0.26
96.167	0.00	0.09	0.316	O					0.26
96.250	0.00	0.09	0.316	O					0.26
96.333	0.00	0.09	0.315	O					0.26
96.417	0.00	0.09	0.314	O					0.26
96.500	0.00	0.09	0.314	O					0.25
96.583	0.00	0.09	0.313	O					0.25
96.667	0.00	0.09	0.313	O					0.25
96.750	0.00	0.09	0.312	O					0.25
96.833	0.00	0.09	0.311	O					0.25
96.917	0.00	0.09	0.311	O					0.25
97.000	0.00	0.09	0.310	O					0.25
97.083	0.00	0.09	0.310	O					0.25
97.167	0.00	0.09	0.309	O					0.25
97.250	0.00	0.09	0.308	O					0.25
97.333	0.00	0.09	0.308	O					0.25
97.417	0.00	0.09	0.307	O					0.25
97.500	0.00	0.09	0.307	O					0.25
97.583	0.00	0.09	0.306	O					0.25
97.667	0.00	0.09	0.305	O					0.25
97.750	0.00	0.09	0.305	O					0.25
97.833	0.00	0.08	0.304	O					0.25
97.917	0.00	0.08	0.304	O					0.25
98.000	0.00	0.08	0.303	O					0.25
98.083	0.00	0.08	0.302	O					0.25
98.167	0.00	0.08	0.302	O					0.25
98.250	0.00	0.08	0.301	O					0.24
98.333	0.00	0.08	0.301	O					0.24
98.417	0.00	0.08	0.300	O					0.24
98.500	0.00	0.08	0.300	O					0.24
98.583	0.00	0.08	0.299	O					0.24
98.667	0.00	0.08	0.298	O					0.24
98.750	0.00	0.08	0.298	O					0.24
98.833	0.00	0.08	0.297	O					0.24
98.917	0.00	0.08	0.297	O					0.24
99.000	0.00	0.08	0.296	O					0.24
99.083	0.00	0.08	0.296	O					0.24
99.167	0.00	0.08	0.295	O					0.24
99.250	0.00	0.08	0.294	O					0.24
99.333	0.00	0.08	0.294	O					0.24
99.417	0.00	0.08	0.293	O					0.24
99.500	0.00	0.08	0.293	O					0.24
99.583	0.00	0.08	0.292	O					0.24
99.667	0.00	0.08	0.292	O					0.24
99.750	0.00	0.08	0.291	O					0.24
99.833	0.00	0.08	0.291	O					0.24
99.917	0.00	0.08	0.290	O					0.24
100.000	0.00	0.08	0.289	O					0.23
100.083	0.00	0.08	0.289	O					0.23
100.167	0.00	0.08	0.288	O					0.23
100.250	0.00	0.08	0.288	O					0.23
100.333	0.00	0.08	0.287	O					0.23
100.417	0.00	0.08	0.287	O					0.23
100.500	0.00	0.08	0.286	O					0.23
100.583	0.00	0.08	0.286	O					0.23
100.667	0.00	0.08	0.285	O					0.23
100.750	0.00	0.08	0.284	O					0.23

100.833	0.00	0.08	0.284	O	|	|	|	|	0.23
100.917	0.00	0.08	0.283	O	|	|	|	|	0.23
101.000	0.00	0.08	0.283	O	|	|	|	|	0.23
101.083	0.00	0.08	0.282	O	|	|	|	|	0.23
101.167	0.00	0.08	0.282	O	|	|	|	|	0.23
101.250	0.00	0.08	0.281	O	|	|	|	|	0.23
101.333	0.00	0.08	0.281	O	|	|	|	|	0.23
101.417	0.00	0.08	0.280	O	|	|	|	|	0.23
101.500	0.00	0.08	0.280	O	|	|	|	|	0.23
101.583	0.00	0.08	0.279	O	|	|	|	|	0.23
101.667	0.00	0.08	0.278	O	|	|	|	|	0.23
101.750	0.00	0.08	0.278	O	|	|	|	|	0.23
101.833	0.00	0.08	0.277	O	|	|	|	|	0.23
101.917	0.00	0.08	0.277	O	|	|	|	|	0.22
102.000	0.00	0.08	0.276	O	|	|	|	|	0.22
102.083	0.00	0.08	0.276	O	|	|	|	|	0.22
102.167	0.00	0.08	0.275	O	|	|	|	|	0.22
102.250	0.00	0.08	0.275	O	|	|	|	|	0.22
102.333	0.00	0.08	0.274	O	|	|	|	|	0.22
102.417	0.00	0.08	0.274	O	|	|	|	|	0.22
102.500	0.00	0.08	0.273	O	|	|	|	|	0.22
102.583	0.00	0.08	0.273	O	|	|	|	|	0.22
102.667	0.00	0.08	0.272	O	|	|	|	|	0.22
102.750	0.00	0.08	0.272	O	|	|	|	|	0.22
102.833	0.00	0.08	0.271	O	|	|	|	|	0.22
102.917	0.00	0.08	0.271	O	|	|	|	|	0.22
103.000	0.00	0.08	0.270	O	|	|	|	|	0.22
103.083	0.00	0.08	0.270	O	|	|	|	|	0.22
103.167	0.00	0.08	0.269	O	|	|	|	|	0.22
103.250	0.00	0.07	0.268	O	|	|	|	|	0.22
103.333	0.00	0.07	0.268	O	|	|	|	|	0.22
103.417	0.00	0.07	0.267	O	|	|	|	|	0.22
103.500	0.00	0.07	0.267	O	|	|	|	|	0.22
103.583	0.00	0.07	0.266	O	|	|	|	|	0.22
103.667	0.00	0.07	0.266	O	|	|	|	|	0.22
103.750	0.00	0.07	0.265	O	|	|	|	|	0.22
103.833	0.00	0.07	0.265	O	|	|	|	|	0.22
103.917	0.00	0.07	0.264	O	|	|	|	|	0.21
104.000	0.00	0.07	0.264	O	|	|	|	|	0.21
104.083	0.00	0.07	0.263	O	|	|	|	|	0.21
104.167	0.00	0.07	0.263	O	|	|	|	|	0.21
104.250	0.00	0.07	0.262	O	|	|	|	|	0.21
104.333	0.00	0.07	0.262	O	|	|	|	|	0.21
104.417	0.00	0.07	0.261	O	|	|	|	|	0.21
104.500	0.00	0.07	0.261	O	|	|	|	|	0.21
104.583	0.00	0.07	0.260	O	|	|	|	|	0.21
104.667	0.00	0.07	0.260	O	|	|	|	|	0.21
104.750	0.00	0.07	0.259	O	|	|	|	|	0.21
104.833	0.00	0.07	0.259	O	|	|	|	|	0.21
104.917	0.00	0.07	0.258	O	|	|	|	|	0.21
105.000	0.00	0.07	0.258	O	|	|	|	|	0.21
105.083	0.00	0.07	0.257	O	|	|	|	|	0.21
105.167	0.00	0.07	0.257	O	|	|	|	|	0.21
105.250	0.00	0.07	0.256	O	|	|	|	|	0.21
105.333	0.00	0.07	0.256	O	|	|	|	|	0.21
105.417	0.00	0.07	0.255	O	|	|	|	|	0.21
105.500	0.00	0.07	0.255	O	|	|	|	|	0.21
105.583	0.00	0.07	0.254	O	|	|	|	|	0.21
105.667	0.00	0.07	0.254	O	|	|	|	|	0.21
105.750	0.00	0.07	0.253	O	|	|	|	|	0.21
105.833	0.00	0.07	0.253	O	|	|	|	|	0.21
105.917	0.00	0.07	0.252	O	|	|	|	|	0.20
106.000	0.00	0.07	0.252	O	|	|	|	|	0.20
106.083	0.00	0.07	0.251	O	|	|	|	|	0.20
106.167	0.00	0.07	0.251	O	|	|	|	|	0.20
106.250	0.00	0.07	0.251	O	|	|	|	|	0.20
106.333	0.00	0.07	0.250	O	|	|	|	|	0.20
106.417	0.00	0.07	0.250	O	|	|	|	|	0.20
106.500	0.00	0.07	0.249	O	|	|	|	|	0.20
106.583	0.00	0.07	0.249	O	|	|	|	|	0.20
106.667	0.00	0.07	0.248	O	|	|	|	|	0.20

106.750	0.00	0.07	0.248	O	|	|	|	|	0.20
106.833	0.00	0.07	0.247	O	|	|	|	|	0.20
106.917	0.00	0.07	0.247	O	|	|	|	|	0.20
107.000	0.00	0.07	0.246	O	|	|	|	|	0.20
107.083	0.00	0.07	0.246	O	|	|	|	|	0.20
107.167	0.00	0.07	0.245	O	|	|	|	|	0.20
107.250	0.00	0.07	0.245	O	|	|	|	|	0.20
107.333	0.00	0.07	0.244	O	|	|	|	|	0.20
107.417	0.00	0.07	0.244	O	|	|	|	|	0.20
107.500	0.00	0.07	0.243	O	|	|	|	|	0.20
107.583	0.00	0.07	0.243	O	|	|	|	|	0.20
107.667	0.00	0.07	0.242	O	|	|	|	|	0.20
107.750	0.00	0.07	0.242	O	|	|	|	|	0.20
107.833	0.00	0.07	0.242	O	|	|	|	|	0.20
107.917	0.00	0.07	0.241	O	|	|	|	|	0.20
108.000	0.00	0.07	0.241	O	|	|	|	|	0.20
108.083	0.00	0.07	0.240	O	|	|	|	|	0.19
108.167	0.00	0.07	0.240	O	|	|	|	|	0.19
108.250	0.00	0.07	0.239	O	|	|	|	|	0.19
108.333	0.00	0.07	0.239	O	|	|	|	|	0.19
108.417	0.00	0.07	0.238	O	|	|	|	|	0.19
108.500	0.00	0.07	0.238	O	|	|	|	|	0.19
108.583	0.00	0.07	0.237	O	|	|	|	|	0.19
108.667	0.00	0.07	0.237	O	|	|	|	|	0.19
108.750	0.00	0.07	0.236	O	|	|	|	|	0.19
108.833	0.00	0.07	0.236	O	|	|	|	|	0.19
108.917	0.00	0.07	0.236	O	|	|	|	|	0.19
109.000	0.00	0.07	0.235	O	|	|	|	|	0.19
109.083	0.00	0.07	0.235	O	|	|	|	|	0.19
109.167	0.00	0.07	0.234	O	|	|	|	|	0.19
109.250	0.00	0.07	0.234	O	|	|	|	|	0.19
109.333	0.00	0.07	0.233	O	|	|	|	|	0.19
109.417	0.00	0.07	0.233	O	|	|	|	|	0.19
109.500	0.00	0.06	0.232	O	|	|	|	|	0.19
109.583	0.00	0.06	0.232	O	|	|	|	|	0.19
109.667	0.00	0.06	0.232	O	|	|	|	|	0.19
109.750	0.00	0.06	0.231	O	|	|	|	|	0.19
109.833	0.00	0.06	0.231	O	|	|	|	|	0.19
109.917	0.00	0.06	0.230	O	|	|	|	|	0.19
110.000	0.00	0.06	0.230	O	|	|	|	|	0.19
110.083	0.00	0.06	0.229	O	|	|	|	|	0.19
110.167	0.00	0.06	0.229	O	|	|	|	|	0.19
110.250	0.00	0.06	0.228	O	|	|	|	|	0.19
110.333	0.00	0.06	0.228	O	|	|	|	|	0.19
110.417	0.00	0.06	0.228	O	|	|	|	|	0.18
110.500	0.00	0.06	0.227	O	|	|	|	|	0.18
110.583	0.00	0.06	0.227	O	|	|	|	|	0.18
110.667	0.00	0.06	0.226	O	|	|	|	|	0.18
110.750	0.00	0.06	0.226	O	|	|	|	|	0.18
110.833	0.00	0.06	0.225	O	|	|	|	|	0.18
110.917	0.00	0.06	0.225	O	|	|	|	|	0.18
111.000	0.00	0.06	0.225	O	|	|	|	|	0.18
111.083	0.00	0.06	0.224	O	|	|	|	|	0.18
111.167	0.00	0.06	0.224	O	|	|	|	|	0.18
111.250	0.00	0.06	0.223	O	|	|	|	|	0.18
111.333	0.00	0.06	0.223	O	|	|	|	|	0.18
111.417	0.00	0.06	0.222	O	|	|	|	|	0.18
111.500	0.00	0.06	0.222	O	|	|	|	|	0.18
111.583	0.00	0.06	0.222	O	|	|	|	|	0.18
111.667	0.00	0.06	0.221	O	|	|	|	|	0.18
111.750	0.00	0.06	0.221	O	|	|	|	|	0.18
111.833	0.00	0.06	0.220	O	|	|	|	|	0.18
111.917	0.00	0.06	0.220	O	|	|	|	|	0.18
112.000	0.00	0.06	0.219	O	|	|	|	|	0.18
112.083	0.00	0.06	0.219	O	|	|	|	|	0.18
112.167	0.00	0.06	0.219	O	|	|	|	|	0.18
112.250	0.00	0.06	0.218	O	|	|	|	|	0.18
112.333	0.00	0.06	0.218	O	|	|	|	|	0.18
112.417	0.00	0.06	0.217	O	|	|	|	|	0.18
112.500	0.00	0.06	0.217	O	|	|	|	|	0.18
112.583	0.00	0.06	0.216	O	|	|	|	|	0.18

112.667	0.00	0.06	0.216	O	|	|	|	|	0.18
112.750	0.00	0.06	0.216	O	|	|	|	|	0.18
112.833	0.00	0.06	0.215	O	|	|	|	|	0.17
112.917	0.00	0.06	0.215	O	|	|	|	|	0.17
113.000	0.00	0.06	0.214	O	|	|	|	|	0.17
113.083	0.00	0.06	0.214	O	|	|	|	|	0.17
113.167	0.00	0.06	0.214	O	|	|	|	|	0.17
113.250	0.00	0.06	0.213	O	|	|	|	|	0.17
113.333	0.00	0.06	0.213	O	|	|	|	|	0.17
113.417	0.00	0.06	0.212	O	|	|	|	|	0.17
113.500	0.00	0.06	0.212	O	|	|	|	|	0.17
113.583	0.00	0.06	0.212	O	|	|	|	|	0.17
113.667	0.00	0.06	0.211	O	|	|	|	|	0.17
113.750	0.00	0.06	0.211	O	|	|	|	|	0.17
113.833	0.00	0.06	0.210	O	|	|	|	|	0.17
113.917	0.00	0.06	0.210	O	|	|	|	|	0.17
114.000	0.00	0.06	0.210	O	|	|	|	|	0.17
114.083	0.00	0.06	0.209	O	|	|	|	|	0.17
114.167	0.00	0.06	0.209	O	|	|	|	|	0.17
114.250	0.00	0.06	0.208	O	|	|	|	|	0.17
114.333	0.00	0.06	0.208	O	|	|	|	|	0.17
114.417	0.00	0.06	0.207	O	|	|	|	|	0.17
114.500	0.00	0.06	0.207	O	|	|	|	|	0.17
114.583	0.00	0.06	0.207	O	|	|	|	|	0.17
114.667	0.00	0.06	0.206	O	|	|	|	|	0.17
114.750	0.00	0.06	0.206	O	|	|	|	|	0.17
114.833	0.00	0.06	0.206	O	|	|	|	|	0.17
114.917	0.00	0.06	0.205	O	|	|	|	|	0.17
115.000	0.00	0.06	0.205	O	|	|	|	|	0.17
115.083	0.00	0.06	0.204	O	|	|	|	|	0.17
115.167	0.00	0.06	0.204	O	|	|	|	|	0.17
115.250	0.00	0.06	0.204	O	|	|	|	|	0.17
115.333	0.00	0.06	0.203	O	|	|	|	|	0.16
115.417	0.00	0.06	0.203	O	|	|	|	|	0.16
115.500	0.00	0.06	0.202	O	|	|	|	|	0.16
115.583	0.00	0.06	0.202	O	|	|	|	|	0.16
115.667	0.00	0.06	0.202	O	|	|	|	|	0.16
115.750	0.00	0.06	0.201	O	|	|	|	|	0.16
115.833	0.00	0.06	0.201	O	|	|	|	|	0.16
115.917	0.00	0.06	0.200	O	|	|	|	|	0.16
116.000	0.00	0.06	0.200	O	|	|	|	|	0.16
116.083	0.00	0.06	0.200	O	|	|	|	|	0.16
116.167	0.00	0.06	0.199	O	|	|	|	|	0.16
116.250	0.00	0.06	0.199	O	|	|	|	|	0.16
116.333	0.00	0.06	0.199	O	|	|	|	|	0.16
116.417	0.00	0.06	0.198	O	|	|	|	|	0.16
116.500	0.00	0.06	0.198	O	|	|	|	|	0.16
116.583	0.00	0.06	0.197	O	|	|	|	|	0.16
116.667	0.00	0.06	0.197	O	|	|	|	|	0.16
116.750	0.00	0.05	0.197	O	|	|	|	|	0.16
116.833	0.00	0.05	0.196	O	|	|	|	|	0.16
116.917	0.00	0.05	0.196	O	|	|	|	|	0.16
117.000	0.00	0.05	0.195	O	|	|	|	|	0.16
117.083	0.00	0.05	0.195	O	|	|	|	|	0.16
117.167	0.00	0.05	0.195	O	|	|	|	|	0.16
117.250	0.00	0.05	0.194	O	|	|	|	|	0.16
117.333	0.00	0.05	0.194	O	|	|	|	|	0.16
117.417	0.00	0.05	0.194	O	|	|	|	|	0.16
117.500	0.00	0.05	0.193	O	|	|	|	|	0.16
117.583	0.00	0.05	0.193	O	|	|	|	|	0.16
117.667	0.00	0.05	0.193	O	|	|	|	|	0.16
117.750	0.00	0.05	0.192	O	|	|	|	|	0.16
117.833	0.00	0.05	0.192	O	|	|	|	|	0.16
117.917	0.00	0.05	0.191	O	|	|	|	|	0.16
118.000	0.00	0.05	0.191	O	|	|	|	|	0.16
118.083	0.00	0.05	0.191	O	|	|	|	|	0.15
118.167	0.00	0.05	0.190	O	|	|	|	|	0.15
118.250	0.00	0.05	0.190	O	|	|	|	|	0.15
118.333	0.00	0.05	0.190	O	|	|	|	|	0.15
118.417	0.00	0.05	0.189	O	|	|	|	|	0.15
118.500	0.00	0.05	0.189	O	|	|	|	|	0.15

118.583	0.00	0.05	0.188	O	|	|	|	|	0.15
118.667	0.00	0.05	0.188	O	|	|	|	|	0.15
118.750	0.00	0.05	0.188	O	|	|	|	|	0.15
118.833	0.00	0.05	0.187	O	|	|	|	|	0.15
118.917	0.00	0.05	0.187	O	|	|	|	|	0.15
119.000	0.00	0.05	0.187	O	|	|	|	|	0.15
119.083	0.00	0.05	0.186	O	|	|	|	|	0.15
119.167	0.00	0.05	0.186	O	|	|	|	|	0.15
119.250	0.00	0.05	0.186	O	|	|	|	|	0.15
119.333	0.00	0.05	0.185	O	|	|	|	|	0.15
119.417	0.00	0.05	0.185	O	|	|	|	|	0.15
119.500	0.00	0.05	0.185	O	|	|	|	|	0.15
119.583	0.00	0.05	0.184	O	|	|	|	|	0.15
119.667	0.00	0.05	0.184	O	|	|	|	|	0.15
119.750	0.00	0.05	0.183	O	|	|	|	|	0.15
119.833	0.00	0.05	0.183	O	|	|	|	|	0.15
119.917	0.00	0.05	0.183	O	|	|	|	|	0.15
120.000	0.00	0.05	0.182	O	|	|	|	|	0.15
120.083	0.00	0.05	0.182	O	|	|	|	|	0.15
120.167	0.00	0.05	0.182	O	|	|	|	|	0.15
120.250	0.00	0.05	0.181	O	|	|	|	|	0.15
120.333	0.00	0.05	0.181	O	|	|	|	|	0.15
120.417	0.00	0.05	0.181	O	|	|	|	|	0.15
120.500	0.00	0.05	0.180	O	|	|	|	|	0.15
120.583	0.00	0.05	0.180	O	|	|	|	|	0.15
120.667	0.00	0.05	0.180	O	|	|	|	|	0.15
120.750	0.00	0.05	0.179	O	|	|	|	|	0.15
120.833	0.00	0.05	0.179	O	|	|	|	|	0.15
120.917	0.00	0.05	0.179	O	|	|	|	|	0.14
121.000	0.00	0.05	0.178	O	|	|	|	|	0.14
121.083	0.00	0.05	0.178	O	|	|	|	|	0.14
121.167	0.00	0.05	0.178	O	|	|	|	|	0.14
121.250	0.00	0.05	0.177	O	|	|	|	|	0.14
121.333	0.00	0.05	0.177	O	|	|	|	|	0.14
121.417	0.00	0.05	0.177	O	|	|	|	|	0.14
121.500	0.00	0.05	0.176	O	|	|	|	|	0.14
121.583	0.00	0.05	0.176	O	|	|	|	|	0.14
121.667	0.00	0.05	0.176	O	|	|	|	|	0.14
121.750	0.00	0.05	0.175	O	|	|	|	|	0.14
121.833	0.00	0.05	0.175	O	|	|	|	|	0.14
121.917	0.00	0.05	0.175	O	|	|	|	|	0.14
122.000	0.00	0.05	0.174	O	|	|	|	|	0.14
122.083	0.00	0.05	0.174	O	|	|	|	|	0.14
122.167	0.00	0.05	0.174	O	|	|	|	|	0.14
122.250	0.00	0.05	0.173	O	|	|	|	|	0.14
122.333	0.00	0.05	0.173	O	|	|	|	|	0.14
122.417	0.00	0.05	0.173	O	|	|	|	|	0.14
122.500	0.00	0.05	0.172	O	|	|	|	|	0.14
122.583	0.00	0.05	0.172	O	|	|	|	|	0.14
122.667	0.00	0.05	0.172	O	|	|	|	|	0.14
122.750	0.00	0.05	0.171	O	|	|	|	|	0.14
122.833	0.00	0.05	0.171	O	|	|	|	|	0.14
122.917	0.00	0.05	0.171	O	|	|	|	|	0.14
123.000	0.00	0.05	0.170	O	|	|	|	|	0.14
123.083	0.00	0.05	0.170	O	|	|	|	|	0.14
123.167	0.00	0.05	0.170	O	|	|	|	|	0.14
123.250	0.00	0.05	0.169	O	|	|	|	|	0.14
123.333	0.00	0.05	0.169	O	|	|	|	|	0.14
123.417	0.00	0.05	0.169	O	|	|	|	|	0.14
123.500	0.00	0.05	0.168	O	|	|	|	|	0.14
123.583	0.00	0.05	0.168	O	|	|	|	|	0.14
123.667	0.00	0.05	0.168	O	|	|	|	|	0.14
123.750	0.00	0.05	0.167	O	|	|	|	|	0.14
123.833	0.00	0.05	0.167	O	|	|	|	|	0.14
123.917	0.00	0.05	0.167	O	|	|	|	|	0.14
124.000	0.00	0.05	0.166	O	|	|	|	|	0.14
124.083	0.00	0.05	0.166	O	|	|	|	|	0.13
124.167	0.00	0.05	0.166	O	|	|	|	|	0.13
124.250	0.00	0.05	0.165	O	|	|	|	|	0.13
124.333	0.00	0.05	0.165	O	|	|	|	|	0.13
124.417	0.00	0.05	0.165	O	|	|	|	|	0.13

124.500	0.00	0.05	0.164	O					0.13
124.583	0.00	0.05	0.164	O					0.13
124.667	0.00	0.05	0.164	O					0.13
124.750	0.00	0.05	0.163	O					0.13
124.833	0.00	0.05	0.163	O					0.13
124.917	0.00	0.05	0.163	O					0.13
125.000	0.00	0.05	0.163	O					0.13
125.083	0.00	0.05	0.162	O					0.13
125.167	0.00	0.05	0.162	O					0.13
125.250	0.00	0.05	0.162	O					0.13
125.333	0.00	0.05	0.161	O					0.13
125.417	0.00	0.04	0.161	O					0.13
125.500	0.00	0.04	0.161	O					0.13
125.583	0.00	0.04	0.160	O					0.13
125.667	0.00	0.04	0.160	O					0.13
125.750	0.00	0.04	0.160	O					0.13
125.833	0.00	0.04	0.159	O					0.13
125.917	0.00	0.04	0.159	O					0.13
126.000	0.00	0.04	0.159	O					0.13
126.083	0.00	0.04	0.159	O					0.13
126.167	0.00	0.04	0.158	O					0.13
126.250	0.00	0.04	0.158	O					0.13
126.333	0.00	0.04	0.158	O					0.13
126.417	0.00	0.04	0.157	O					0.13
126.500	0.00	0.04	0.157	O					0.13
126.583	0.00	0.04	0.157	O					0.13
126.667	0.00	0.04	0.156	O					0.13
126.750	0.00	0.04	0.156	O					0.13
126.833	0.00	0.04	0.156	O					0.13
126.917	0.00	0.04	0.156	O					0.13
127.000	0.00	0.04	0.155	O					0.13
127.083	0.00	0.04	0.155	O					0.13
127.167	0.00	0.04	0.155	O					0.13
127.250	0.00	0.04	0.154	O					0.13
127.333	0.00	0.04	0.154	O					0.13
127.417	0.00	0.04	0.154	O					0.12
127.500	0.00	0.04	0.153	O					0.12
127.583	0.00	0.04	0.153	O					0.12
127.667	0.00	0.04	0.153	O					0.12
127.750	0.00	0.04	0.153	O					0.12
127.833	0.00	0.04	0.152	O					0.12
127.917	0.00	0.04	0.152	O					0.12
128.000	0.00	0.04	0.152	O					0.12
128.083	0.00	0.04	0.151	O					0.12
128.167	0.00	0.04	0.151	O					0.12
128.250	0.00	0.04	0.151	O					0.12
128.333	0.00	0.04	0.151	O					0.12
128.417	0.00	0.04	0.150	O					0.12
128.500	0.00	0.04	0.150	O					0.12
128.583	0.00	0.04	0.150	O					0.12
128.667	0.00	0.04	0.149	O					0.12
128.750	0.00	0.04	0.149	O					0.12
128.833	0.00	0.04	0.149	O					0.12
128.917	0.00	0.04	0.148	O					0.12
129.000	0.00	0.04	0.148	O					0.12
129.083	0.00	0.04	0.148	O					0.12
129.167	0.00	0.04	0.148	O					0.12
129.250	0.00	0.04	0.147	O					0.12
129.333	0.00	0.04	0.147	O					0.12
129.417	0.00	0.04	0.147	O					0.12
129.500	0.00	0.04	0.147	O					0.12
129.583	0.00	0.04	0.146	O					0.12
129.667	0.00	0.04	0.146	O					0.12
129.750	0.00	0.04	0.146	O					0.12
129.833	0.00	0.04	0.145	O					0.12
129.917	0.00	0.04	0.145	O					0.12
130.000	0.00	0.04	0.145	O					0.12
130.083	0.00	0.04	0.145	O					0.12
130.167	0.00	0.04	0.144	O					0.12
130.250	0.00	0.04	0.144	O					0.12
130.333	0.00	0.04	0.144	O					0.12

130.417	0.00	0.04	0.143	O	|	|	|	|	0.12
130.500	0.00	0.04	0.143	O	|	|	|	|	0.12
130.583	0.00	0.04	0.143	O	|	|	|	|	0.12
130.667	0.00	0.04	0.143	O	|	|	|	|	0.12
130.750	0.00	0.04	0.142	O	|	|	|	|	0.12
130.833	0.00	0.04	0.142	O	|	|	|	|	0.12
130.917	0.00	0.04	0.142	O	|	|	|	|	0.12
131.000	0.00	0.04	0.142	O	|	|	|	|	0.11
131.083	0.00	0.04	0.141	O	|	|	|	|	0.11
131.167	0.00	0.04	0.141	O	|	|	|	|	0.11
131.250	0.00	0.04	0.141	O	|	|	|	|	0.11
131.333	0.00	0.04	0.140	O	|	|	|	|	0.11
131.417	0.00	0.04	0.140	O	|	|	|	|	0.11
131.500	0.00	0.04	0.140	O	|	|	|	|	0.11
131.583	0.00	0.04	0.140	O	|	|	|	|	0.11
131.667	0.00	0.04	0.139	O	|	|	|	|	0.11
131.750	0.00	0.04	0.139	O	|	|	|	|	0.11
131.833	0.00	0.04	0.139	O	|	|	|	|	0.11
131.917	0.00	0.04	0.139	O	|	|	|	|	0.11
132.000	0.00	0.04	0.138	O	|	|	|	|	0.11
132.083	0.00	0.04	0.138	O	|	|	|	|	0.11
132.167	0.00	0.04	0.138	O	|	|	|	|	0.11
132.250	0.00	0.04	0.137	O	|	|	|	|	0.11
132.333	0.00	0.04	0.137	O	|	|	|	|	0.11
132.417	0.00	0.04	0.137	O	|	|	|	|	0.11
132.500	0.00	0.04	0.137	O	|	|	|	|	0.11
132.583	0.00	0.04	0.136	O	|	|	|	|	0.11
132.667	0.00	0.04	0.136	O	|	|	|	|	0.11
132.750	0.00	0.04	0.136	O	|	|	|	|	0.11
132.833	0.00	0.04	0.136	O	|	|	|	|	0.11
132.917	0.00	0.04	0.135	O	|	|	|	|	0.11
133.000	0.00	0.04	0.135	O	|	|	|	|	0.11
133.083	0.00	0.04	0.135	O	|	|	|	|	0.11
133.167	0.00	0.04	0.135	O	|	|	|	|	0.11
133.250	0.00	0.04	0.134	O	|	|	|	|	0.11
133.333	0.00	0.04	0.134	O	|	|	|	|	0.11
133.417	0.00	0.04	0.134	O	|	|	|	|	0.11
133.500	0.00	0.04	0.134	O	|	|	|	|	0.11
133.583	0.00	0.04	0.133	O	|	|	|	|	0.11
133.667	0.00	0.04	0.133	O	|	|	|	|	0.11
133.750	0.00	0.04	0.133	O	|	|	|	|	0.11
133.833	0.00	0.04	0.133	O	|	|	|	|	0.11
133.917	0.00	0.04	0.132	O	|	|	|	|	0.11
134.000	0.00	0.04	0.132	O	|	|	|	|	0.11
134.083	0.00	0.04	0.132	O	|	|	|	|	0.11
134.167	0.00	0.04	0.132	O	|	|	|	|	0.11
134.250	0.00	0.04	0.131	O	|	|	|	|	0.11
134.333	0.00	0.04	0.131	O	|	|	|	|	0.11
134.417	0.00	0.04	0.131	O	|	|	|	|	0.11
134.500	0.00	0.04	0.131	O	|	|	|	|	0.11
134.583	0.00	0.04	0.130	O	|	|	|	|	0.11
134.667	0.00	0.04	0.130	O	|	|	|	|	0.11
134.750	0.00	0.04	0.130	O	|	|	|	|	0.11
134.833	0.00	0.04	0.130	O	|	|	|	|	0.11
134.917	0.00	0.04	0.129	O	|	|	|	|	0.10
135.000	0.00	0.04	0.129	O	|	|	|	|	0.10
135.083	0.00	0.04	0.129	O	|	|	|	|	0.10
135.167	0.00	0.04	0.129	O	|	|	|	|	0.10
135.250	0.00	0.04	0.128	O	|	|	|	|	0.10
135.333	0.00	0.04	0.128	O	|	|	|	|	0.10
135.417	0.00	0.04	0.128	O	|	|	|	|	0.10
135.500	0.00	0.04	0.128	O	|	|	|	|	0.10
135.583	0.00	0.04	0.127	O	|	|	|	|	0.10
135.667	0.00	0.04	0.127	O	|	|	|	|	0.10
135.750	0.00	0.04	0.127	O	|	|	|	|	0.10
135.833	0.00	0.04	0.127	O	|	|	|	|	0.10
135.917	0.00	0.04	0.126	O	|	|	|	|	0.10
136.000	0.00	0.04	0.126	O	|	|	|	|	0.10
136.083	0.00	0.04	0.126	O	|	|	|	|	0.10
136.167	0.00	0.04	0.126	O	|	|	|	|	0.10
136.250	0.00	0.04	0.125	O	|	|	|	|	0.10

136.333	0.00	0.03	0.125	O					0.10
136.417	0.00	0.03	0.125	O					0.10
136.500	0.00	0.03	0.125	O					0.10
136.583	0.00	0.03	0.124	O					0.10
136.667	0.00	0.03	0.124	O					0.10
136.750	0.00	0.03	0.124	O					0.10
136.833	0.00	0.03	0.124	O					0.10
136.917	0.00	0.03	0.123	O					0.10
137.000	0.00	0.03	0.123	O					0.10
137.083	0.00	0.03	0.123	O					0.10
137.167	0.00	0.03	0.123	O					0.10
137.250	0.00	0.03	0.123	O					0.10
137.333	0.00	0.03	0.122	O					0.10
137.417	0.00	0.03	0.122	O					0.10
137.500	0.00	0.03	0.122	O					0.10
137.583	0.00	0.03	0.122	O					0.10
137.667	0.00	0.03	0.121	O					0.10
137.750	0.00	0.03	0.121	O					0.10
137.833	0.00	0.03	0.121	O					0.10
137.917	0.00	0.03	0.121	O					0.10
138.000	0.00	0.03	0.120	O					0.10
138.083	0.00	0.03	0.120	O					0.10
138.167	0.00	0.03	0.120	O					0.10
138.250	0.00	0.03	0.120	O					0.10
138.333	0.00	0.03	0.119	O					0.10
138.417	0.00	0.03	0.119	O					0.10
138.500	0.00	0.03	0.119	O					0.10
138.583	0.00	0.03	0.119	O					0.10
138.667	0.00	0.03	0.119	O					0.10
138.750	0.00	0.03	0.118	O					0.10
138.833	0.00	0.03	0.118	O					0.10
138.917	0.00	0.03	0.118	O					0.10
139.000	0.00	0.03	0.118	O					0.10
139.083	0.00	0.03	0.117	O					0.10
139.167	0.00	0.03	0.117	O					0.10
139.250	0.00	0.03	0.117	O					0.09
139.333	0.00	0.03	0.117	O					0.09
139.417	0.00	0.03	0.117	O					0.09
139.500	0.00	0.03	0.116	O					0.09
139.583	0.00	0.03	0.116	O					0.09
139.667	0.00	0.03	0.116	O					0.09
139.750	0.00	0.03	0.116	O					0.09
139.833	0.00	0.03	0.115	O					0.09
139.917	0.00	0.03	0.115	O					0.09
140.000	0.00	0.03	0.115	O					0.09
140.083	0.00	0.03	0.115	O					0.09
140.167	0.00	0.03	0.115	O					0.09
140.250	0.00	0.03	0.114	O					0.09
140.333	0.00	0.03	0.114	O					0.09
140.417	0.00	0.03	0.114	O					0.09
140.500	0.00	0.03	0.114	O					0.09
140.583	0.00	0.03	0.113	O					0.09
140.667	0.00	0.03	0.113	O					0.09
140.750	0.00	0.03	0.113	O					0.09
140.833	0.00	0.03	0.113	O					0.09
140.917	0.00	0.03	0.113	O					0.09
141.000	0.00	0.03	0.112	O					0.09
141.083	0.00	0.03	0.112	O					0.09
141.167	0.00	0.03	0.112	O					0.09
141.250	0.00	0.03	0.112	O					0.09
141.333	0.00	0.03	0.111	O					0.09
141.417	0.00	0.03	0.111	O					0.09
141.500	0.00	0.03	0.111	O					0.09
141.583	0.00	0.03	0.111	O					0.09
141.667	0.00	0.03	0.111	O					0.09
141.750	0.00	0.03	0.110	O					0.09
141.833	0.00	0.03	0.110	O					0.09
141.917	0.00	0.03	0.110	O					0.09
142.000	0.00	0.03	0.110	O					0.09
142.083	0.00	0.03	0.110	O					0.09
142.167	0.00	0.03	0.109	O					0.09

142.250	0.00	0.03	0.109	O	|	|	|	|	0.09
142.333	0.00	0.03	0.109	O	|	|	|	|	0.09
142.417	0.00	0.03	0.109	O	|	|	|	|	0.09
142.500	0.00	0.03	0.109	O	|	|	|	|	0.09
142.583	0.00	0.03	0.108	O	|	|	|	|	0.09
142.667	0.00	0.03	0.108	O	|	|	|	|	0.09
142.750	0.00	0.03	0.108	O	|	|	|	|	0.09
142.833	0.00	0.03	0.108	O	|	|	|	|	0.09
142.917	0.00	0.03	0.107	O	|	|	|	|	0.09
143.000	0.00	0.03	0.107	O	|	|	|	|	0.09
143.083	0.00	0.03	0.107	O	|	|	|	|	0.09
143.167	0.00	0.03	0.107	O	|	|	|	|	0.09
143.250	0.00	0.03	0.107	O	|	|	|	|	0.09
143.333	0.00	0.03	0.106	O	|	|	|	|	0.09
143.417	0.00	0.03	0.106	O	|	|	|	|	0.09
143.500	0.00	0.03	0.106	O	|	|	|	|	0.09
143.583	0.00	0.03	0.106	O	|	|	|	|	0.09
143.667	0.00	0.03	0.106	O	|	|	|	|	0.09
143.750	0.00	0.03	0.105	O	|	|	|	|	0.09
143.833	0.00	0.03	0.105	O	|	|	|	|	0.09
143.917	0.00	0.03	0.105	O	|	|	|	|	0.09
144.000	0.00	0.03	0.105	O	|	|	|	|	0.09
144.083	0.00	0.03	0.105	O	|	|	|	|	0.08
144.167	0.00	0.03	0.104	O	|	|	|	|	0.08
144.250	0.00	0.03	0.104	O	|	|	|	|	0.08
144.333	0.00	0.03	0.104	O	|	|	|	|	0.08
144.417	0.00	0.03	0.104	O	|	|	|	|	0.08
144.500	0.00	0.03	0.104	O	|	|	|	|	0.08
144.583	0.00	0.03	0.103	O	|	|	|	|	0.08
144.667	0.00	0.03	0.103	O	|	|	|	|	0.08
144.750	0.00	0.03	0.103	O	|	|	|	|	0.08
144.833	0.00	0.03	0.103	O	|	|	|	|	0.08
144.917	0.00	0.03	0.103	O	|	|	|	|	0.08
145.000	0.00	0.03	0.102	O	|	|	|	|	0.08
145.083	0.00	0.03	0.102	O	|	|	|	|	0.08
145.167	0.00	0.03	0.102	O	|	|	|	|	0.08
145.250	0.00	0.03	0.102	O	|	|	|	|	0.08
145.333	0.00	0.03	0.102	O	|	|	|	|	0.08
145.417	0.00	0.03	0.101	O	|	|	|	|	0.08
145.500	0.00	0.03	0.101	O	|	|	|	|	0.08
145.583	0.00	0.03	0.101	O	|	|	|	|	0.08
145.667	0.00	0.03	0.101	O	|	|	|	|	0.08
145.750	0.00	0.03	0.101	O	|	|	|	|	0.08
145.833	0.00	0.03	0.100	O	|	|	|	|	0.08
145.917	0.00	0.03	0.100	O	|	|	|	|	0.08
146.000	0.00	0.03	0.100	O	|	|	|	|	0.08
146.083	0.00	0.03	0.100	O	|	|	|	|	0.08
146.167	0.00	0.03	0.100	O	|	|	|	|	0.08
146.250	0.00	0.03	0.100	O	|	|	|	|	0.08
146.333	0.00	0.03	0.099	O	|	|	|	|	0.08
146.417	0.00	0.03	0.099	O	|	|	|	|	0.08
146.500	0.00	0.03	0.099	O	|	|	|	|	0.08
146.583	0.00	0.03	0.099	O	|	|	|	|	0.08
146.667	0.00	0.03	0.099	O	|	|	|	|	0.08
146.750	0.00	0.03	0.098	O	|	|	|	|	0.08
146.833	0.00	0.03	0.098	O	|	|	|	|	0.08
146.917	0.00	0.03	0.098	O	|	|	|	|	0.08
147.000	0.00	0.03	0.098	O	|	|	|	|	0.08
147.083	0.00	0.03	0.098	O	|	|	|	|	0.08
147.167	0.00	0.03	0.097	O	|	|	|	|	0.08
147.250	0.00	0.03	0.097	O	|	|	|	|	0.08
147.333	0.00	0.03	0.097	O	|	|	|	|	0.08
147.417	0.00	0.03	0.097	O	|	|	|	|	0.08
147.500	0.00	0.03	0.097	O	|	|	|	|	0.08
147.583	0.00	0.03	0.097	O	|	|	|	|	0.08
147.667	0.00	0.03	0.096	O	|	|	|	|	0.08
147.750	0.00	0.03	0.096	O	|	|	|	|	0.08
147.833	0.00	0.03	0.096	O	|	|	|	|	0.08
147.917	0.00	0.03	0.096	O	|	|	|	|	0.08
148.000	0.00	0.03	0.096	O	|	|	|	|	0.08
148.083	0.00	0.03	0.095	O	|	|	|	|	0.08

148.167	0.00	0.03	0.095	O	|	|	|	|	0.08
148.250	0.00	0.03	0.095	O	|	|	|	|	0.08
148.333	0.00	0.03	0.095	O	|	|	|	|	0.08
148.417	0.00	0.03	0.095	O	|	|	|	|	0.08
148.500	0.00	0.03	0.095	O	|	|	|	|	0.08
148.583	0.00	0.03	0.094	O	|	|	|	|	0.08
148.667	0.00	0.03	0.094	O	|	|	|	|	0.08
148.750	0.00	0.03	0.094	O	|	|	|	|	0.08
148.833	0.00	0.03	0.094	O	|	|	|	|	0.08
148.917	0.00	0.03	0.094	O	|	|	|	|	0.08
149.000	0.00	0.03	0.093	O	|	|	|	|	0.08
149.083	0.00	0.03	0.093	O	|	|	|	|	0.08
149.167	0.00	0.03	0.093	O	|	|	|	|	0.08
149.250	0.00	0.03	0.093	O	|	|	|	|	0.08
149.333	0.00	0.03	0.093	O	|	|	|	|	0.08
149.417	0.00	0.03	0.093	O	|	|	|	|	0.08
149.500	0.00	0.03	0.092	O	|	|	|	|	0.07
149.583	0.00	0.03	0.092	O	|	|	|	|	0.07
149.667	0.00	0.03	0.092	O	|	|	|	|	0.07
149.750	0.00	0.03	0.092	O	|	|	|	|	0.07
149.833	0.00	0.03	0.092	O	|	|	|	|	0.07
149.917	0.00	0.03	0.091	O	|	|	|	|	0.07
150.000	0.00	0.03	0.091	O	|	|	|	|	0.07
150.083	0.00	0.03	0.091	O	|	|	|	|	0.07
150.167	0.00	0.03	0.091	O	|	|	|	|	0.07
150.250	0.00	0.03	0.091	O	|	|	|	|	0.07
150.333	0.00	0.03	0.091	O	|	|	|	|	0.07
150.417	0.00	0.03	0.090	O	|	|	|	|	0.07
150.500	0.00	0.03	0.090	O	|	|	|	|	0.07
150.583	0.00	0.03	0.090	O	|	|	|	|	0.07
150.667	0.00	0.03	0.090	O	|	|	|	|	0.07
150.750	0.00	0.03	0.090	O	|	|	|	|	0.07
150.833	0.00	0.03	0.090	O	|	|	|	|	0.07
150.917	0.00	0.02	0.089	O	|	|	|	|	0.07
151.000	0.00	0.02	0.089	O	|	|	|	|	0.07
151.083	0.00	0.02	0.089	O	|	|	|	|	0.07
151.167	0.00	0.02	0.089	O	|	|	|	|	0.07
151.250	0.00	0.02	0.089	O	|	|	|	|	0.07
151.333	0.00	0.02	0.089	O	|	|	|	|	0.07
151.417	0.00	0.02	0.088	O	|	|	|	|	0.07
151.500	0.00	0.02	0.088	O	|	|	|	|	0.07
151.583	0.00	0.02	0.088	O	|	|	|	|	0.07
151.667	0.00	0.02	0.088	O	|	|	|	|	0.07
151.750	0.00	0.02	0.088	O	|	|	|	|	0.07
151.833	0.00	0.02	0.088	O	|	|	|	|	0.07
151.917	0.00	0.02	0.087	O	|	|	|	|	0.07
152.000	0.00	0.02	0.087	O	|	|	|	|	0.07
152.083	0.00	0.02	0.087	O	|	|	|	|	0.07
152.167	0.00	0.02	0.087	O	|	|	|	|	0.07
152.250	0.00	0.02	0.087	O	|	|	|	|	0.07
152.333	0.00	0.02	0.087	O	|	|	|	|	0.07
152.417	0.00	0.02	0.086	O	|	|	|	|	0.07
152.500	0.00	0.02	0.086	O	|	|	|	|	0.07
152.583	0.00	0.02	0.086	O	|	|	|	|	0.07
152.667	0.00	0.02	0.086	O	|	|	|	|	0.07
152.750	0.00	0.02	0.086	O	|	|	|	|	0.07
152.833	0.00	0.02	0.086	O	|	|	|	|	0.07
152.917	0.00	0.02	0.085	O	|	|	|	|	0.07
153.000	0.00	0.02	0.085	O	|	|	|	|	0.07
153.083	0.00	0.02	0.085	O	|	|	|	|	0.07
153.167	0.00	0.02	0.085	O	|	|	|	|	0.07
153.250	0.00	0.02	0.085	O	|	|	|	|	0.07
153.333	0.00	0.02	0.085	O	|	|	|	|	0.07
153.417	0.00	0.02	0.084	O	|	|	|	|	0.07
153.500	0.00	0.02	0.084	O	|	|	|	|	0.07
153.583	0.00	0.02	0.084	O	|	|	|	|	0.07
153.667	0.00	0.02	0.084	O	|	|	|	|	0.07
153.750	0.00	0.02	0.084	O	|	|	|	|	0.07
153.833	0.00	0.02	0.084	O	|	|	|	|	0.07
153.917	0.00	0.02	0.083	O	|	|	|	|	0.07
154.000	0.00	0.02	0.083	O	|	|	|	|	0.07

154.083	0.00	0.02	0.083	O	|	|	|	|	0.07
154.167	0.00	0.02	0.083	O	|	|	|	|	0.07
154.250	0.00	0.02	0.083	O	|	|	|	|	0.07
154.333	0.00	0.02	0.083	O	|	|	|	|	0.07
154.417	0.00	0.02	0.082	O	|	|	|	|	0.07
154.500	0.00	0.02	0.082	O	|	|	|	|	0.07
154.583	0.00	0.02	0.082	O	|	|	|	|	0.07
154.667	0.00	0.02	0.082	O	|	|	|	|	0.07
154.750	0.00	0.02	0.082	O	|	|	|	|	0.07
154.833	0.00	0.02	0.082	O	|	|	|	|	0.07
154.917	0.00	0.02	0.081	O	|	|	|	|	0.07
155.000	0.00	0.02	0.081	O	|	|	|	|	0.07
155.083	0.00	0.02	0.081	O	|	|	|	|	0.07
155.167	0.00	0.02	0.081	O	|	|	|	|	0.07
155.250	0.00	0.02	0.081	O	|	|	|	|	0.07
155.333	0.00	0.02	0.081	O	|	|	|	|	0.07
155.417	0.00	0.02	0.081	O	|	|	|	|	0.07
155.500	0.00	0.02	0.080	O	|	|	|	|	0.07
155.583	0.00	0.02	0.080	O	|	|	|	|	0.07
155.667	0.00	0.02	0.080	O	|	|	|	|	0.07
155.750	0.00	0.02	0.080	O	|	|	|	|	0.06
155.833	0.00	0.02	0.080	O	|	|	|	|	0.06
155.917	0.00	0.02	0.080	O	|	|	|	|	0.06
156.000	0.00	0.02	0.079	O	|	|	|	|	0.06
156.083	0.00	0.02	0.079	O	|	|	|	|	0.06
156.167	0.00	0.02	0.079	O	|	|	|	|	0.06
156.250	0.00	0.02	0.079	O	|	|	|	|	0.06
156.333	0.00	0.02	0.079	O	|	|	|	|	0.06
156.417	0.00	0.02	0.079	O	|	|	|	|	0.06
156.500	0.00	0.02	0.079	O	|	|	|	|	0.06
156.583	0.00	0.02	0.078	O	|	|	|	|	0.06
156.667	0.00	0.02	0.078	O	|	|	|	|	0.06
156.750	0.00	0.02	0.078	O	|	|	|	|	0.06
156.833	0.00	0.02	0.078	O	|	|	|	|	0.06
156.917	0.00	0.02	0.078	O	|	|	|	|	0.06
157.000	0.00	0.02	0.078	O	|	|	|	|	0.06
157.083	0.00	0.02	0.078	O	|	|	|	|	0.06
157.167	0.00	0.02	0.077	O	|	|	|	|	0.06
157.250	0.00	0.02	0.077	O	|	|	|	|	0.06
157.333	0.00	0.02	0.077	O	|	|	|	|	0.06
157.417	0.00	0.02	0.077	O	|	|	|	|	0.06
157.500	0.00	0.02	0.077	O	|	|	|	|	0.06
157.583	0.00	0.02	0.077	O	|	|	|	|	0.06
157.667	0.00	0.02	0.076	O	|	|	|	|	0.06
157.750	0.00	0.02	0.076	O	|	|	|	|	0.06
157.833	0.00	0.02	0.076	O	|	|	|	|	0.06
157.917	0.00	0.02	0.076	O	|	|	|	|	0.06
158.000	0.00	0.02	0.076	O	|	|	|	|	0.06
158.083	0.00	0.02	0.076	O	|	|	|	|	0.06
158.167	0.00	0.02	0.076	O	|	|	|	|	0.06
158.250	0.00	0.02	0.075	O	|	|	|	|	0.06
158.333	0.00	0.02	0.075	O	|	|	|	|	0.06
158.417	0.00	0.02	0.075	O	|	|	|	|	0.06
158.500	0.00	0.02	0.075	O	|	|	|	|	0.06
158.583	0.00	0.02	0.075	O	|	|	|	|	0.06
158.667	0.00	0.02	0.075	O	|	|	|	|	0.06
158.750	0.00	0.02	0.075	O	|	|	|	|	0.06
158.833	0.00	0.02	0.074	O	|	|	|	|	0.06
158.917	0.00	0.02	0.074	O	|	|	|	|	0.06
159.000	0.00	0.02	0.074	O	|	|	|	|	0.06
159.083	0.00	0.02	0.074	O	|	|	|	|	0.06
159.167	0.00	0.02	0.074	O	|	|	|	|	0.06
159.250	0.00	0.02	0.074	O	|	|	|	|	0.06
159.333	0.00	0.02	0.074	O	|	|	|	|	0.06
159.417	0.00	0.02	0.073	O	|	|	|	|	0.06
159.500	0.00	0.02	0.073	O	|	|	|	|	0.06
159.583	0.00	0.02	0.073	O	|	|	|	|	0.06
159.667	0.00	0.02	0.073	O	|	|	|	|	0.06
159.750	0.00	0.02	0.073	O	|	|	|	|	0.06
159.833	0.00	0.02	0.073	O	|	|	|	|	0.06
159.917	0.00	0.02	0.073	O	|	|	|	|	0.06

160.000	0.00	0.02	0.072	O	|	|	|	0.06
160.083	0.00	0.02	0.072	O	|	|	|	0.06
160.167	0.00	0.02	0.072	O	|	|	|	0.06
160.250	0.00	0.02	0.072	O	|	|	|	0.06
160.333	0.00	0.02	0.072	O	|	|	|	0.06
160.417	0.00	0.02	0.072	O	|	|	|	0.06
160.500	0.00	0.02	0.072	O	|	|	|	0.06
160.583	0.00	0.02	0.072	O	|	|	|	0.06
160.667	0.00	0.02	0.071	O	|	|	|	0.06
160.750	0.00	0.02	0.071	O	|	|	|	0.06
160.833	0.00	0.02	0.071	O	|	|	|	0.06
160.917	0.00	0.02	0.071	O	|	|	|	0.06
161.000	0.00	0.02	0.071	O	|	|	|	0.06
161.083	0.00	0.02	0.071	O	|	|	|	0.06
161.167	0.00	0.02	0.071	O	|	|	|	0.06
161.250	0.00	0.02	0.070	O	|	|	|	0.06
161.333	0.00	0.02	0.070	O	|	|	|	0.06
161.417	0.00	0.02	0.070	O	|	|	|	0.06
161.500	0.00	0.02	0.070	O	|	|	|	0.06
161.583	0.00	0.02	0.070	O	|	|	|	0.06
161.667	0.00	0.02	0.070	O	|	|	|	0.06
161.750	0.00	0.02	0.070	O	|	|	|	0.06
161.833	0.00	0.02	0.069	O	|	|	|	0.06
161.917	0.00	0.02	0.069	O	|	|	|	0.06
162.000	0.00	0.02	0.069	O	|	|	|	0.06
162.083	0.00	0.02	0.069	O	|	|	|	0.06
162.167	0.00	0.02	0.069	O	|	|	|	0.06
162.250	0.00	0.02	0.069	O	|	|	|	0.06
162.333	0.00	0.02	0.069	O	|	|	|	0.06
162.417	0.00	0.02	0.069	O	|	|	|	0.06
162.500	0.00	0.02	0.068	O	|	|	|	0.06
162.583	0.00	0.02	0.068	O	|	|	|	0.06
162.667	0.00	0.02	0.068	O	|	|	|	0.06
162.750	0.00	0.02	0.068	O	|	|	|	0.06
162.833	0.00	0.02	0.068	O	|	|	|	0.06
162.917	0.00	0.02	0.068	O	|	|	|	0.05
163.000	0.00	0.02	0.068	O	|	|	|	0.05
163.083	0.00	0.02	0.067	O	|	|	|	0.05
163.167	0.00	0.02	0.067	O	|	|	|	0.05
163.250	0.00	0.02	0.067	O	|	|	|	0.05
163.333	0.00	0.02	0.067	O	|	|	|	0.05
163.417	0.00	0.02	0.067	O	|	|	|	0.05
163.500	0.00	0.02	0.067	O	|	|	|	0.05
163.583	0.00	0.02	0.067	O	|	|	|	0.05
163.667	0.00	0.02	0.067	O	|	|	|	0.05
163.750	0.00	0.02	0.066	O	|	|	|	0.05
163.833	0.00	0.02	0.066	O	|	|	|	0.05
163.917	0.00	0.02	0.066	O	|	|	|	0.05
164.000	0.00	0.02	0.066	O	|	|	|	0.05
164.083	0.00	0.02	0.066	O	|	|	|	0.05
164.167	0.00	0.02	0.066	O	|	|	|	0.05
164.250	0.00	0.02	0.066	O	|	|	|	0.05
164.333	0.00	0.02	0.066	O	|	|	|	0.05
164.417	0.00	0.02	0.065	O	|	|	|	0.05
164.500	0.00	0.02	0.065	O	|	|	|	0.05
164.583	0.00	0.02	0.065	O	|	|	|	0.05
164.667	0.00	0.02	0.065	O	|	|	|	0.05
164.750	0.00	0.02	0.065	O	|	|	|	0.05
164.833	0.00	0.02	0.065	O	|	|	|	0.05
164.917	0.00	0.02	0.065	O	|	|	|	0.05
165.000	0.00	0.02	0.065	O	|	|	|	0.05
165.083	0.00	0.02	0.064	O	|	|	|	0.05
165.167	0.00	0.02	0.064	O	|	|	|	0.05
165.250	0.00	0.02	0.064	O	|	|	|	0.05
165.333	0.00	0.02	0.064	O	|	|	|	0.05
165.417	0.00	0.02	0.064	O	|	|	|	0.05
165.500	0.00	0.02	0.064	O	|	|	|	0.05
165.583	0.00	0.02	0.064	O	|	|	|	0.05
165.667	0.00	0.02	0.064	O	|	|	|	0.05
165.750	0.00	0.02	0.063	O	|	|	|	0.05
165.833	0.00	0.02	0.063	O	|	|	|	0.05

165.917	0.00	0.02	0.063	O	|	|	|	|	0.05
166.000	0.00	0.02	0.063	O	|	|	|	|	0.05
166.083	0.00	0.02	0.063	O	|	|	|	|	0.05
166.167	0.00	0.02	0.063	O	|	|	|	|	0.05
166.250	0.00	0.02	0.063	O	|	|	|	|	0.05
166.333	0.00	0.02	0.063	O	|	|	|	|	0.05
166.417	0.00	0.02	0.062	O	|	|	|	|	0.05
166.500	0.00	0.02	0.062	O	|	|	|	|	0.05
166.583	0.00	0.02	0.062	O	|	|	|	|	0.05
166.667	0.00	0.02	0.062	O	|	|	|	|	0.05
166.750	0.00	0.02	0.062	O	|	|	|	|	0.05
166.833	0.00	0.02	0.062	O	|	|	|	|	0.05
166.917	0.00	0.02	0.062	O	|	|	|	|	0.05
167.000	0.00	0.02	0.062	O	|	|	|	|	0.05
167.083	0.00	0.02	0.062	O	|	|	|	|	0.05
167.167	0.00	0.02	0.061	O	|	|	|	|	0.05
167.250	0.00	0.02	0.061	O	|	|	|	|	0.05
167.333	0.00	0.02	0.061	O	|	|	|	|	0.05
167.417	0.00	0.02	0.061	O	|	|	|	|	0.05
167.500	0.00	0.02	0.061	O	|	|	|	|	0.05
167.583	0.00	0.02	0.061	O	|	|	|	|	0.05
167.667	0.00	0.02	0.061	O	|	|	|	|	0.05
167.750	0.00	0.02	0.061	O	|	|	|	|	0.05
167.833	0.00	0.02	0.060	O	|	|	|	|	0.05
167.917	0.00	0.02	0.060	O	|	|	|	|	0.05
168.000	0.00	0.02	0.060	O	|	|	|	|	0.05
168.083	0.00	0.02	0.060	O	|	|	|	|	0.05
168.167	0.00	0.02	0.060	O	|	|	|	|	0.05
168.250	0.00	0.02	0.060	O	|	|	|	|	0.05
168.333	0.00	0.02	0.060	O	|	|	|	|	0.05
168.417	0.00	0.02	0.060	O	|	|	|	|	0.05
168.500	0.00	0.02	0.060	O	|	|	|	|	0.05
168.583	0.00	0.02	0.059	O	|	|	|	|	0.05
168.667	0.00	0.02	0.059	O	|	|	|	|	0.05
168.750	0.00	0.02	0.059	O	|	|	|	|	0.05
168.833	0.00	0.02	0.059	O	|	|	|	|	0.05
168.917	0.00	0.02	0.059	O	|	|	|	|	0.05
169.000	0.00	0.02	0.059	O	|	|	|	|	0.05
169.083	0.00	0.02	0.059	O	|	|	|	|	0.05
169.167	0.00	0.02	0.059	O	|	|	|	|	0.05
169.250	0.00	0.02	0.059	O	|	|	|	|	0.05
169.333	0.00	0.02	0.058	O	|	|	|	|	0.05
169.417	0.00	0.02	0.058	O	|	|	|	|	0.05
169.500	0.00	0.02	0.058	O	|	|	|	|	0.05
169.583	0.00	0.02	0.058	O	|	|	|	|	0.05
169.667	0.00	0.02	0.058	O	|	|	|	|	0.05
169.750	0.00	0.02	0.058	O	|	|	|	|	0.05
169.833	0.00	0.02	0.058	O	|	|	|	|	0.05
169.917	0.00	0.02	0.058	O	|	|	|	|	0.05
170.000	0.00	0.02	0.058	O	|	|	|	|	0.05
170.083	0.00	0.02	0.057	O	|	|	|	|	0.05
170.167	0.00	0.02	0.057	O	|	|	|	|	0.05
170.250	0.00	0.02	0.057	O	|	|	|	|	0.05
170.333	0.00	0.02	0.057	O	|	|	|	|	0.05
170.417	0.00	0.02	0.057	O	|	|	|	|	0.05
170.500	0.00	0.02	0.057	O	|	|	|	|	0.05
170.583	0.00	0.02	0.057	O	|	|	|	|	0.05
170.667	0.00	0.02	0.057	O	|	|	|	|	0.05
170.750	0.00	0.02	0.057	O	|	|	|	|	0.05
170.833	0.00	0.02	0.056	O	|	|	|	|	0.05
170.917	0.00	0.02	0.056	O	|	|	|	|	0.05
171.000	0.00	0.02	0.056	O	|	|	|	|	0.05
171.083	0.00	0.02	0.056	O	|	|	|	|	0.05
171.167	0.00	0.02	0.056	O	|	|	|	|	0.05
171.250	0.00	0.02	0.056	O	|	|	|	|	0.05
171.333	0.00	0.02	0.056	O	|	|	|	|	0.05
171.417	0.00	0.02	0.056	O	|	|	|	|	0.05
171.500	0.00	0.02	0.056	O	|	|	|	|	0.05
171.583	0.00	0.02	0.055	O	|	|	|	|	0.05
171.667	0.00	0.02	0.055	O	|	|	|	|	0.04
171.750	0.00	0.02	0.055	O	|	|	|	|	0.04

171.833	0.00	0.02	0.055	O	|	|	|	|	0.04
171.917	0.00	0.02	0.055	O	|	|	|	|	0.04
172.000	0.00	0.02	0.055	O	|	|	|	|	0.04
172.083	0.00	0.02	0.055	O	|	|	|	|	0.04
172.167	0.00	0.02	0.055	O	|	|	|	|	0.04
172.250	0.00	0.02	0.055	O	|	|	|	|	0.04
172.333	0.00	0.02	0.055	O	|	|	|	|	0.04
172.417	0.00	0.02	0.054	O	|	|	|	|	0.04
172.500	0.00	0.02	0.054	O	|	|	|	|	0.04
172.583	0.00	0.02	0.054	O	|	|	|	|	0.04
172.667	0.00	0.02	0.054	O	|	|	|	|	0.04
172.750	0.00	0.02	0.054	O	|	|	|	|	0.04
172.833	0.00	0.02	0.054	O	|	|	|	|	0.04
172.917	0.00	0.02	0.054	O	|	|	|	|	0.04
173.000	0.00	0.01	0.054	O	|	|	|	|	0.04
173.083	0.00	0.01	0.054	O	|	|	|	|	0.04
173.167	0.00	0.01	0.053	O	|	|	|	|	0.04
173.250	0.00	0.01	0.053	O	|	|	|	|	0.04
173.333	0.00	0.01	0.053	O	|	|	|	|	0.04
173.417	0.00	0.01	0.053	O	|	|	|	|	0.04
173.500	0.00	0.01	0.053	O	|	|	|	|	0.04
173.583	0.00	0.01	0.053	O	|	|	|	|	0.04
173.667	0.00	0.01	0.053	O	|	|	|	|	0.04
173.750	0.00	0.01	0.053	O	|	|	|	|	0.04
173.833	0.00	0.01	0.053	O	|	|	|	|	0.04
173.917	0.00	0.01	0.053	O	|	|	|	|	0.04
174.000	0.00	0.01	0.052	O	|	|	|	|	0.04
174.083	0.00	0.01	0.052	O	|	|	|	|	0.04
174.167	0.00	0.01	0.052	O	|	|	|	|	0.04
174.250	0.00	0.01	0.052	O	|	|	|	|	0.04
174.333	0.00	0.01	0.052	O	|	|	|	|	0.04
174.417	0.00	0.01	0.052	O	|	|	|	|	0.04
174.500	0.00	0.01	0.052	O	|	|	|	|	0.04
174.583	0.00	0.01	0.052	O	|	|	|	|	0.04
174.667	0.00	0.01	0.052	O	|	|	|	|	0.04
174.750	0.00	0.01	0.052	O	|	|	|	|	0.04
174.833	0.00	0.01	0.051	O	|	|	|	|	0.04
174.917	0.00	0.01	0.051	O	|	|	|	|	0.04
175.000	0.00	0.01	0.051	O	|	|	|	|	0.04
175.083	0.00	0.01	0.051	O	|	|	|	|	0.04
175.167	0.00	0.01	0.051	O	|	|	|	|	0.04
175.250	0.00	0.01	0.051	O	|	|	|	|	0.04
175.333	0.00	0.01	0.051	O	|	|	|	|	0.04
175.417	0.00	0.01	0.051	O	|	|	|	|	0.04
175.500	0.00	0.01	0.051	O	|	|	|	|	0.04
175.583	0.00	0.01	0.051	O	|	|	|	|	0.04
175.667	0.00	0.01	0.050	O	|	|	|	|	0.04
175.750	0.00	0.01	0.050	O	|	|	|	|	0.04
175.833	0.00	0.01	0.050	O	|	|	|	|	0.04
175.917	0.00	0.01	0.050	O	|	|	|	|	0.04
176.000	0.00	0.01	0.050	O	|	|	|	|	0.04
176.083	0.00	0.01	0.050	O	|	|	|	|	0.04
176.167	0.00	0.01	0.050	O	|	|	|	|	0.04
176.250	0.00	0.01	0.050	O	|	|	|	|	0.04
176.333	0.00	0.01	0.050	O	|	|	|	|	0.04
176.417	0.00	0.01	0.050	O	|	|	|	|	0.04
176.500	0.00	0.01	0.050	O	|	|	|	|	0.04
176.583	0.00	0.01	0.049	O	|	|	|	|	0.04
176.667	0.00	0.01	0.049	O	|	|	|	|	0.04
176.750	0.00	0.01	0.049	O	|	|	|	|	0.04
176.833	0.00	0.01	0.049	O	|	|	|	|	0.04
176.917	0.00	0.01	0.049	O	|	|	|	|	0.04
177.000	0.00	0.01	0.049	O	|	|	|	|	0.04
177.083	0.00	0.01	0.049	O	|	|	|	|	0.04
177.167	0.00	0.01	0.049	O	|	|	|	|	0.04
177.250	0.00	0.01	0.049	O	|	|	|	|	0.04
177.333	0.00	0.01	0.049	O	|	|	|	|	0.04
177.417	0.00	0.01	0.048	O	|	|	|	|	0.04
177.500	0.00	0.01	0.048	O	|	|	|	|	0.04
177.583	0.00	0.01	0.048	O	|	|	|	|	0.04
177.667	0.00	0.01	0.048	O	|	|	|	|	0.04

177.750	0.00	0.01	0.048	O	|	|	|	|	0.04
177.833	0.00	0.01	0.048	O	|	|	|	|	0.04
177.917	0.00	0.01	0.048	O	|	|	|	|	0.04
178.000	0.00	0.01	0.048	O	|	|	|	|	0.04
178.083	0.00	0.01	0.048	O	|	|	|	|	0.04
178.167	0.00	0.01	0.048	O	|	|	|	|	0.04
178.250	0.00	0.01	0.048	O	|	|	|	|	0.04
178.333	0.00	0.01	0.047	O	|	|	|	|	0.04
178.417	0.00	0.01	0.047	O	|	|	|	|	0.04
178.500	0.00	0.01	0.047	O	|	|	|	|	0.04
178.583	0.00	0.01	0.047	O	|	|	|	|	0.04
178.667	0.00	0.01	0.047	O	|	|	|	|	0.04
178.750	0.00	0.01	0.047	O	|	|	|	|	0.04
178.833	0.00	0.01	0.047	O	|	|	|	|	0.04
178.917	0.00	0.01	0.047	O	|	|	|	|	0.04
179.000	0.00	0.01	0.047	O	|	|	|	|	0.04
179.083	0.00	0.01	0.047	O	|	|	|	|	0.04
179.167	0.00	0.01	0.047	O	|	|	|	|	0.04
179.250	0.00	0.01	0.046	O	|	|	|	|	0.04
179.333	0.00	0.01	0.046	O	|	|	|	|	0.04
179.417	0.00	0.01	0.046	O	|	|	|	|	0.04
179.500	0.00	0.01	0.046	O	|	|	|	|	0.04
179.583	0.00	0.01	0.046	O	|	|	|	|	0.04
179.667	0.00	0.01	0.046	O	|	|	|	|	0.04
179.750	0.00	0.01	0.046	O	|	|	|	|	0.04
179.833	0.00	0.01	0.046	O	|	|	|	|	0.04
179.917	0.00	0.01	0.046	O	|	|	|	|	0.04
180.000	0.00	0.01	0.046	O	|	|	|	|	0.04
180.083	0.00	0.01	0.046	O	|	|	|	|	0.04
180.167	0.00	0.01	0.046	O	|	|	|	|	0.04
180.250	0.00	0.01	0.045	O	|	|	|	|	0.04
180.333	0.00	0.01	0.045	O	|	|	|	|	0.04
180.417	0.00	0.01	0.045	O	|	|	|	|	0.04
180.500	0.00	0.01	0.045	O	|	|	|	|	0.04
180.583	0.00	0.01	0.045	O	|	|	|	|	0.04
180.667	0.00	0.01	0.045	O	|	|	|	|	0.04
180.750	0.00	0.01	0.045	O	|	|	|	|	0.04
180.833	0.00	0.01	0.045	O	|	|	|	|	0.04
180.917	0.00	0.01	0.045	O	|	|	|	|	0.04
181.000	0.00	0.01	0.045	O	|	|	|	|	0.04
181.083	0.00	0.01	0.045	O	|	|	|	|	0.04
181.167	0.00	0.01	0.044	O	|	|	|	|	0.04
181.250	0.00	0.01	0.044	O	|	|	|	|	0.04
181.333	0.00	0.01	0.044	O	|	|	|	|	0.04
181.417	0.00	0.01	0.044	O	|	|	|	|	0.04
181.500	0.00	0.01	0.044	O	|	|	|	|	0.04
181.583	0.00	0.01	0.044	O	|	|	|	|	0.04
181.667	0.00	0.01	0.044	O	|	|	|	|	0.04
181.750	0.00	0.01	0.044	O	|	|	|	|	0.04
181.833	0.00	0.01	0.044	O	|	|	|	|	0.04
181.917	0.00	0.01	0.044	O	|	|	|	|	0.04
182.000	0.00	0.01	0.044	O	|	|	|	|	0.04
182.083	0.00	0.01	0.044	O	|	|	|	|	0.04
182.167	0.00	0.01	0.043	O	|	|	|	|	0.04
182.250	0.00	0.01	0.043	O	|	|	|	|	0.04
182.333	0.00	0.01	0.043	O	|	|	|	|	0.04
182.417	0.00	0.01	0.043	O	|	|	|	|	0.04
182.500	0.00	0.01	0.043	O	|	|	|	|	0.04
182.583	0.00	0.01	0.043	O	|	|	|	|	0.03
182.667	0.00	0.01	0.043	O	|	|	|	|	0.03
182.750	0.00	0.01	0.043	O	|	|	|	|	0.03
182.833	0.00	0.01	0.043	O	|	|	|	|	0.03
182.917	0.00	0.01	0.043	O	|	|	|	|	0.03
183.000	0.00	0.01	0.043	O	|	|	|	|	0.03
183.083	0.00	0.01	0.043	O	|	|	|	|	0.03
183.167	0.00	0.01	0.042	O	|	|	|	|	0.03
183.250	0.00	0.01	0.042	O	|	|	|	|	0.03
183.333	0.00	0.01	0.042	O	|	|	|	|	0.03
183.417	0.00	0.01	0.042	O	|	|	|	|	0.03
183.500	0.00	0.01	0.042	O	|	|	|	|	0.03
183.583	0.00	0.01	0.042	O	|	|	|	|	0.03

183.667	0.00	0.01	0.042	O	|	|	|	|	0.03
183.750	0.00	0.01	0.042	O	|	|	|	|	0.03
183.833	0.00	0.01	0.042	O	|	|	|	|	0.03
183.917	0.00	0.01	0.042	O	|	|	|	|	0.03
184.000	0.00	0.01	0.042	O	|	|	|	|	0.03
184.083	0.00	0.01	0.042	O	|	|	|	|	0.03
184.167	0.00	0.01	0.041	O	|	|	|	|	0.03
184.250	0.00	0.01	0.041	O	|	|	|	|	0.03
184.333	0.00	0.01	0.041	O	|	|	|	|	0.03
184.417	0.00	0.01	0.041	O	|	|	|	|	0.03
184.500	0.00	0.01	0.041	O	|	|	|	|	0.03
184.583	0.00	0.01	0.041	O	|	|	|	|	0.03
184.667	0.00	0.01	0.041	O	|	|	|	|	0.03
184.750	0.00	0.01	0.041	O	|	|	|	|	0.03
184.833	0.00	0.01	0.041	O	|	|	|	|	0.03
184.917	0.00	0.01	0.041	O	|	|	|	|	0.03
185.000	0.00	0.01	0.041	O	|	|	|	|	0.03
185.083	0.00	0.01	0.041	O	|	|	|	|	0.03
185.167	0.00	0.01	0.041	O	|	|	|	|	0.03
185.250	0.00	0.01	0.040	O	|	|	|	|	0.03
185.333	0.00	0.01	0.040	O	|	|	|	|	0.03
185.417	0.00	0.01	0.040	O	|	|	|	|	0.03
185.500	0.00	0.01	0.040	O	|	|	|	|	0.03
185.583	0.00	0.01	0.040	O	|	|	|	|	0.03
185.667	0.00	0.01	0.040	O	|	|	|	|	0.03
185.750	0.00	0.01	0.040	O	|	|	|	|	0.03
185.833	0.00	0.01	0.040	O	|	|	|	|	0.03
185.917	0.00	0.01	0.040	O	|	|	|	|	0.03
186.000	0.00	0.01	0.040	O	|	|	|	|	0.03
186.083	0.00	0.01	0.040	O	|	|	|	|	0.03
186.167	0.00	0.01	0.040	O	|	|	|	|	0.03
186.250	0.00	0.01	0.040	O	|	|	|	|	0.03
186.333	0.00	0.01	0.039	O	|	|	|	|	0.03
186.417	0.00	0.01	0.039	O	|	|	|	|	0.03
186.500	0.00	0.01	0.039	O	|	|	|	|	0.03
186.583	0.00	0.01	0.039	O	|	|	|	|	0.03
186.667	0.00	0.01	0.039	O	|	|	|	|	0.03
186.750	0.00	0.01	0.039	O	|	|	|	|	0.03
186.833	0.00	0.01	0.039	O	|	|	|	|	0.03
186.917	0.00	0.01	0.039	O	|	|	|	|	0.03
187.000	0.00	0.01	0.039	O	|	|	|	|	0.03
187.083	0.00	0.01	0.039	O	|	|	|	|	0.03
187.167	0.00	0.01	0.039	O	|	|	|	|	0.03
187.250	0.00	0.01	0.039	O	|	|	|	|	0.03
187.333	0.00	0.01	0.039	O	|	|	|	|	0.03
187.417	0.00	0.01	0.038	O	|	|	|	|	0.03
187.500	0.00	0.01	0.038	O	|	|	|	|	0.03
187.583	0.00	0.01	0.038	O	|	|	|	|	0.03
187.667	0.00	0.01	0.038	O	|	|	|	|	0.03
187.750	0.00	0.01	0.038	O	|	|	|	|	0.03
187.833	0.00	0.01	0.038	O	|	|	|	|	0.03
187.917	0.00	0.01	0.038	O	|	|	|	|	0.03
188.000	0.00	0.01	0.038	O	|	|	|	|	0.03
188.083	0.00	0.01	0.038	O	|	|	|	|	0.03
188.167	0.00	0.01	0.038	O	|	|	|	|	0.03
188.250	0.00	0.01	0.038	O	|	|	|	|	0.03
188.333	0.00	0.01	0.038	O	|	|	|	|	0.03
188.417	0.00	0.01	0.038	O	|	|	|	|	0.03
188.500	0.00	0.01	0.038	O	|	|	|	|	0.03
188.583	0.00	0.01	0.037	O	|	|	|	|	0.03
188.667	0.00	0.01	0.037	O	|	|	|	|	0.03
188.750	0.00	0.01	0.037	O	|	|	|	|	0.03
188.833	0.00	0.01	0.037	O	|	|	|	|	0.03
188.917	0.00	0.01	0.037	O	|	|	|	|	0.03
189.000	0.00	0.01	0.037	O	|	|	|	|	0.03
189.083	0.00	0.01	0.037	O	|	|	|	|	0.03
189.167	0.00	0.01	0.037	O	|	|	|	|	0.03
189.250	0.00	0.01	0.037	O	|	|	|	|	0.03
189.333	0.00	0.01	0.037	O	|	|	|	|	0.03
189.417	0.00	0.01	0.037	O	|	|	|	|	0.03
189.500	0.00	0.01	0.037	O	|	|	|	|	0.03

189.583	0.00	0.01	0.037	O	|	|	|	|	0.03
189.667	0.00	0.01	0.037	O	|	|	|	|	0.03
189.750	0.00	0.01	0.036	O	|	|	|	|	0.03
189.833	0.00	0.01	0.036	O	|	|	|	|	0.03
189.917	0.00	0.01	0.036	O	|	|	|	|	0.03
190.000	0.00	0.01	0.036	O	|	|	|	|	0.03
190.083	0.00	0.01	0.036	O	|	|	|	|	0.03
190.167	0.00	0.01	0.036	O	|	|	|	|	0.03
190.250	0.00	0.01	0.036	O	|	|	|	|	0.03
190.333	0.00	0.01	0.036	O	|	|	|	|	0.03
190.417	0.00	0.01	0.036	O	|	|	|	|	0.03
190.500	0.00	0.01	0.036	O	|	|	|	|	0.03
190.583	0.00	0.01	0.036	O	|	|	|	|	0.03
190.667	0.00	0.01	0.036	O	|	|	|	|	0.03
190.750	0.00	0.01	0.036	O	|	|	|	|	0.03
190.833	0.00	0.01	0.036	O	|	|	|	|	0.03
190.917	0.00	0.01	0.036	O	|	|	|	|	0.03
191.000	0.00	0.01	0.035	O	|	|	|	|	0.03
191.083	0.00	0.01	0.035	O	|	|	|	|	0.03
191.167	0.00	0.01	0.035	O	|	|	|	|	0.03
191.250	0.00	0.01	0.035	O	|	|	|	|	0.03
191.333	0.00	0.01	0.035	O	|	|	|	|	0.03
191.417	0.00	0.01	0.035	O	|	|	|	|	0.03
191.500	0.00	0.01	0.035	O	|	|	|	|	0.03
191.583	0.00	0.01	0.035	O	|	|	|	|	0.03
191.667	0.00	0.01	0.035	O	|	|	|	|	0.03
191.750	0.00	0.01	0.035	O	|	|	|	|	0.03
191.833	0.00	0.01	0.035	O	|	|	|	|	0.03
191.917	0.00	0.01	0.035	O	|	|	|	|	0.03
192.000	0.00	0.01	0.035	O	|	|	|	|	0.03
192.083	0.00	0.01	0.035	O	|	|	|	|	0.03
192.167	0.00	0.01	0.034	O	|	|	|	|	0.03
192.250	0.00	0.01	0.034	O	|	|	|	|	0.03
192.333	0.00	0.01	0.034	O	|	|	|	|	0.03
192.417	0.00	0.01	0.034	O	|	|	|	|	0.03
192.500	0.00	0.01	0.034	O	|	|	|	|	0.03
192.583	0.00	0.01	0.034	O	|	|	|	|	0.03
192.667	0.00	0.01	0.034	O	|	|	|	|	0.03
192.750	0.00	0.01	0.034	O	|	|	|	|	0.03
192.833	0.00	0.01	0.034	O	|	|	|	|	0.03
192.917	0.00	0.01	0.034	O	|	|	|	|	0.03
193.000	0.00	0.01	0.034	O	|	|	|	|	0.03
193.083	0.00	0.01	0.034	O	|	|	|	|	0.03
193.167	0.00	0.01	0.034	O	|	|	|	|	0.03
193.250	0.00	0.01	0.034	O	|	|	|	|	0.03
193.333	0.00	0.01	0.034	O	|	|	|	|	0.03
193.417	0.00	0.01	0.034	O	|	|	|	|	0.03
193.500	0.00	0.01	0.033	O	|	|	|	|	0.03
193.583	0.00	0.01	0.033	O	|	|	|	|	0.03
193.667	0.00	0.01	0.033	O	|	|	|	|	0.03
193.750	0.00	0.01	0.033	O	|	|	|	|	0.03
193.833	0.00	0.01	0.033	O	|	|	|	|	0.03
193.917	0.00	0.01	0.033	O	|	|	|	|	0.03
194.000	0.00	0.01	0.033	O	|	|	|	|	0.03
194.083	0.00	0.01	0.033	O	|	|	|	|	0.03
194.167	0.00	0.01	0.033	O	|	|	|	|	0.03
194.250	0.00	0.01	0.033	O	|	|	|	|	0.03
194.333	0.00	0.01	0.033	O	|	|	|	|	0.03
194.417	0.00	0.01	0.033	O	|	|	|	|	0.03
194.500	0.00	0.01	0.033	O	|	|	|	|	0.03
194.583	0.00	0.01	0.033	O	|	|	|	|	0.03
194.667	0.00	0.01	0.033	O	|	|	|	|	0.03
194.750	0.00	0.01	0.033	O	|	|	|	|	0.03
194.833	0.00	0.01	0.032	O	|	|	|	|	0.03
194.917	0.00	0.01	0.032	O	|	|	|	|	0.03
195.000	0.00	0.01	0.032	O	|	|	|	|	0.03
195.083	0.00	0.01	0.032	O	|	|	|	|	0.03
195.167	0.00	0.01	0.032	O	|	|	|	|	0.03
195.250	0.00	0.01	0.032	O	|	|	|	|	0.03
195.333	0.00	0.01	0.032	O	|	|	|	|	0.03
195.417	0.00	0.01	0.032	O	|	|	|	|	0.03

195.500	0.00	0.01	0.032	O	|	|	|	|	0.03
195.583	0.00	0.01	0.032	O	|	|	|	|	0.03
195.667	0.00	0.01	0.032	O	|	|	|	|	0.03
195.750	0.00	0.01	0.032	O	|	|	|	|	0.03
195.833	0.00	0.01	0.032	O	|	|	|	|	0.03
195.917	0.00	0.01	0.032	O	|	|	|	|	0.03
196.000	0.00	0.01	0.032	O	|	|	|	|	0.03
196.083	0.00	0.01	0.032	O	|	|	|	|	0.03
196.167	0.00	0.01	0.031	O	|	|	|	|	0.03
196.250	0.00	0.01	0.031	O	|	|	|	|	0.03
196.333	0.00	0.01	0.031	O	|	|	|	|	0.03
196.417	0.00	0.01	0.031	O	|	|	|	|	0.03
196.500	0.00	0.01	0.031	O	|	|	|	|	0.03
196.583	0.00	0.01	0.031	O	|	|	|	|	0.03
196.667	0.00	0.01	0.031	O	|	|	|	|	0.03
196.750	0.00	0.01	0.031	O	|	|	|	|	0.03
196.833	0.00	0.01	0.031	O	|	|	|	|	0.03
196.917	0.00	0.01	0.031	O	|	|	|	|	0.03
197.000	0.00	0.01	0.031	O	|	|	|	|	0.03
197.083	0.00	0.01	0.031	O	|	|	|	|	0.02
197.167	0.00	0.01	0.031	O	|	|	|	|	0.02
197.250	0.00	0.01	0.031	O	|	|	|	|	0.02
197.333	0.00	0.01	0.031	O	|	|	|	|	0.02
197.417	0.00	0.01	0.031	O	|	|	|	|	0.02
197.500	0.00	0.01	0.031	O	|	|	|	|	0.02
197.583	0.00	0.01	0.030	O	|	|	|	|	0.02
197.667	0.00	0.01	0.030	O	|	|	|	|	0.02
197.750	0.00	0.01	0.030	O	|	|	|	|	0.02
197.833	0.00	0.01	0.030	O	|	|	|	|	0.02
197.917	0.00	0.01	0.030	O	|	|	|	|	0.02
198.000	0.00	0.01	0.030	O	|	|	|	|	0.02
198.083	0.00	0.01	0.030	O	|	|	|	|	0.02
198.167	0.00	0.01	0.030	O	|	|	|	|	0.02
198.250	0.00	0.01	0.030	O	|	|	|	|	0.02
198.333	0.00	0.01	0.030	O	|	|	|	|	0.02
198.417	0.00	0.01	0.030	O	|	|	|	|	0.02
198.500	0.00	0.01	0.030	O	|	|	|	|	0.02
198.583	0.00	0.01	0.030	O	|	|	|	|	0.02
198.667	0.00	0.01	0.030	O	|	|	|	|	0.02
198.750	0.00	0.01	0.030	O	|	|	|	|	0.02
198.833	0.00	0.01	0.030	O	|	|	|	|	0.02
198.917	0.00	0.01	0.030	O	|	|	|	|	0.02
199.000	0.00	0.01	0.029	O	|	|	|	|	0.02
199.083	0.00	0.01	0.029	O	|	|	|	|	0.02
199.167	0.00	0.01	0.029	O	|	|	|	|	0.02
199.250	0.00	0.01	0.029	O	|	|	|	|	0.02
199.333	0.00	0.01	0.029	O	|	|	|	|	0.02
199.417	0.00	0.01	0.029	O	|	|	|	|	0.02
199.500	0.00	0.01	0.029	O	|	|	|	|	0.02
199.583	0.00	0.01	0.029	O	|	|	|	|	0.02
199.667	0.00	0.01	0.029	O	|	|	|	|	0.02
199.750	0.00	0.01	0.029	O	|	|	|	|	0.02
199.833	0.00	0.01	0.029	O	|	|	|	|	0.02
199.917	0.00	0.01	0.029	O	|	|	|	|	0.02
200.000	0.00	0.01	0.029	O	|	|	|	|	0.02
200.083	0.00	0.01	0.029	O	|	|	|	|	0.02
200.167	0.00	0.01	0.029	O	|	|	|	|	0.02
200.250	0.00	0.01	0.029	O	|	|	|	|	0.02
200.333	0.00	0.01	0.029	O	|	|	|	|	0.02
200.417	0.00	0.01	0.029	O	|	|	|	|	0.02
200.500	0.00	0.01	0.028	O	|	|	|	|	0.02
200.583	0.00	0.01	0.028	O	|	|	|	|	0.02
200.667	0.00	0.01	0.028	O	|	|	|	|	0.02
200.750	0.00	0.01	0.028	O	|	|	|	|	0.02
200.833	0.00	0.01	0.028	O	|	|	|	|	0.02
200.917	0.00	0.01	0.028	O	|	|	|	|	0.02
201.000	0.00	0.01	0.028	O	|	|	|	|	0.02
201.083	0.00	0.01	0.028	O	|	|	|	|	0.02
201.167	0.00	0.01	0.028	O	|	|	|	|	0.02
201.250	0.00	0.01	0.028	O	|	|	|	|	0.02
201.333	0.00	0.01	0.028	O	|	|	|	|	0.02

201.417	0.00	0.01	0.028	O	|	|	|	|	0.02
201.500	0.00	0.01	0.028	O	|	|	|	|	0.02
201.583	0.00	0.01	0.028	O	|	|	|	|	0.02
201.667	0.00	0.01	0.028	O	|	|	|	|	0.02
201.750	0.00	0.01	0.028	O	|	|	|	|	0.02
201.833	0.00	0.01	0.028	O	|	|	|	|	0.02
201.917	0.00	0.01	0.028	O	|	|	|	|	0.02
202.000	0.00	0.01	0.027	O	|	|	|	|	0.02
202.083	0.00	0.01	0.027	O	|	|	|	|	0.02
202.167	0.00	0.01	0.027	O	|	|	|	|	0.02
202.250	0.00	0.01	0.027	O	|	|	|	|	0.02
202.333	0.00	0.01	0.027	O	|	|	|	|	0.02
202.417	0.00	0.01	0.027	O	|	|	|	|	0.02
202.500	0.00	0.01	0.027	O	|	|	|	|	0.02
202.583	0.00	0.01	0.027	O	|	|	|	|	0.02
202.667	0.00	0.01	0.027	O	|	|	|	|	0.02
202.750	0.00	0.01	0.027	O	|	|	|	|	0.02
202.833	0.00	0.01	0.027	O	|	|	|	|	0.02
202.917	0.00	0.01	0.027	O	|	|	|	|	0.02
203.000	0.00	0.01	0.027	O	|	|	|	|	0.02
203.083	0.00	0.01	0.027	O	|	|	|	|	0.02
203.167	0.00	0.01	0.027	O	|	|	|	|	0.02
203.250	0.00	0.01	0.027	O	|	|	|	|	0.02
203.333	0.00	0.01	0.027	O	|	|	|	|	0.02
203.417	0.00	0.01	0.027	O	|	|	|	|	0.02
203.500	0.00	0.01	0.027	O	|	|	|	|	0.02
203.583	0.00	0.01	0.027	O	|	|	|	|	0.02
203.667	0.00	0.01	0.026	O	|	|	|	|	0.02
203.750	0.00	0.01	0.026	O	|	|	|	|	0.02
203.833	0.00	0.01	0.026	O	|	|	|	|	0.02
203.917	0.00	0.01	0.026	O	|	|	|	|	0.02
204.000	0.00	0.01	0.026	O	|	|	|	|	0.02
204.083	0.00	0.01	0.026	O	|	|	|	|	0.02
204.167	0.00	0.01	0.026	O	|	|	|	|	0.02
204.250	0.00	0.01	0.026	O	|	|	|	|	0.02
204.333	0.00	0.01	0.026	O	|	|	|	|	0.02
204.417	0.00	0.01	0.026	O	|	|	|	|	0.02
204.500	0.00	0.01	0.026	O	|	|	|	|	0.02
204.583	0.00	0.01	0.026	O	|	|	|	|	0.02
204.667	0.00	0.01	0.026	O	|	|	|	|	0.02
204.750	0.00	0.01	0.026	O	|	|	|	|	0.02
204.833	0.00	0.01	0.026	O	|	|	|	|	0.02
204.917	0.00	0.01	0.026	O	|	|	|	|	0.02
205.000	0.00	0.01	0.026	O	|	|	|	|	0.02
205.083	0.00	0.01	0.026	O	|	|	|	|	0.02
205.167	0.00	0.01	0.026	O	|	|	|	|	0.02
205.250	0.00	0.01	0.026	O	|	|	|	|	0.02
205.333	0.00	0.01	0.025	O	|	|	|	|	0.02
205.417	0.00	0.01	0.025	O	|	|	|	|	0.02
205.500	0.00	0.01	0.025	O	|	|	|	|	0.02
205.583	0.00	0.01	0.025	O	|	|	|	|	0.02
205.667	0.00	0.01	0.025	O	|	|	|	|	0.02
205.750	0.00	0.01	0.025	O	|	|	|	|	0.02
205.833	0.00	0.01	0.025	O	|	|	|	|	0.02
205.917	0.00	0.01	0.025	O	|	|	|	|	0.02
206.000	0.00	0.01	0.025	O	|	|	|	|	0.02
206.083	0.00	0.01	0.025	O	|	|	|	|	0.02
206.167	0.00	0.01	0.025	O	|	|	|	|	0.02
206.250	0.00	0.01	0.025	O	|	|	|	|	0.02
206.333	0.00	0.01	0.025	O	|	|	|	|	0.02
206.417	0.00	0.01	0.025	O	|	|	|	|	0.02
206.500	0.00	0.01	0.025	O	|	|	|	|	0.02
206.583	0.00	0.01	0.025	O	|	|	|	|	0.02
206.667	0.00	0.01	0.025	O	|	|	|	|	0.02
206.750	0.00	0.01	0.025	O	|	|	|	|	0.02
206.833	0.00	0.01	0.025	O	|	|	|	|	0.02
206.917	0.00	0.01	0.025	O	|	|	|	|	0.02
207.000	0.00	0.01	0.024	O	|	|	|	|	0.02
207.083	0.00	0.01	0.024	O	|	|	|	|	0.02
207.167	0.00	0.01	0.024	O	|	|	|	|	0.02
207.250	0.00	0.01	0.024	O	|	|	|	|	0.02

207.333	0.00	0.01	0.024	O	|	|	|	|	0.02
207.417	0.00	0.01	0.024	O	|	|	|	|	0.02
207.500	0.00	0.01	0.024	O	|	|	|	|	0.02
207.583	0.00	0.01	0.024	O	|	|	|	|	0.02
207.667	0.00	0.01	0.024	O	|	|	|	|	0.02
207.750	0.00	0.01	0.024	O	|	|	|	|	0.02
207.833	0.00	0.01	0.024	O	|	|	|	|	0.02
207.917	0.00	0.01	0.024	O	|	|	|	|	0.02
208.000	0.00	0.01	0.024	O	|	|	|	|	0.02
208.083	0.00	0.01	0.024	O	|	|	|	|	0.02
208.167	0.00	0.01	0.024	O	|	|	|	|	0.02
208.250	0.00	0.01	0.024	O	|	|	|	|	0.02
208.333	0.00	0.01	0.024	O	|	|	|	|	0.02
208.417	0.00	0.01	0.024	O	|	|	|	|	0.02
208.500	0.00	0.01	0.024	O	|	|	|	|	0.02
208.583	0.00	0.01	0.024	O	|	|	|	|	0.02
208.667	0.00	0.01	0.024	O	|	|	|	|	0.02
208.750	0.00	0.01	0.024	O	|	|	|	|	0.02
208.833	0.00	0.01	0.023	O	|	|	|	|	0.02
208.917	0.00	0.01	0.023	O	|	|	|	|	0.02
209.000	0.00	0.01	0.023	O	|	|	|	|	0.02
209.083	0.00	0.01	0.023	O	|	|	|	|	0.02
209.167	0.00	0.01	0.023	O	|	|	|	|	0.02
209.250	0.00	0.01	0.023	O	|	|	|	|	0.02
209.333	0.00	0.01	0.023	O	|	|	|	|	0.02
209.417	0.00	0.01	0.023	O	|	|	|	|	0.02
209.500	0.00	0.01	0.023	O	|	|	|	|	0.02
209.583	0.00	0.01	0.023	O	|	|	|	|	0.02
209.667	0.00	0.01	0.023	O	|	|	|	|	0.02
209.750	0.00	0.01	0.023	O	|	|	|	|	0.02
209.833	0.00	0.01	0.023	O	|	|	|	|	0.02
209.917	0.00	0.01	0.023	O	|	|	|	|	0.02
210.000	0.00	0.01	0.023	O	|	|	|	|	0.02
210.083	0.00	0.01	0.023	O	|	|	|	|	0.02
210.167	0.00	0.01	0.023	O	|	|	|	|	0.02
210.250	0.00	0.01	0.023	O	|	|	|	|	0.02
210.333	0.00	0.01	0.023	O	|	|	|	|	0.02
210.417	0.00	0.01	0.023	O	|	|	|	|	0.02
210.500	0.00	0.01	0.023	O	|	|	|	|	0.02
210.583	0.00	0.01	0.023	O	|	|	|	|	0.02
210.667	0.00	0.01	0.023	O	|	|	|	|	0.02
210.750	0.00	0.01	0.022	O	|	|	|	|	0.02
210.833	0.00	0.01	0.022	O	|	|	|	|	0.02
210.917	0.00	0.01	0.022	O	|	|	|	|	0.02
211.000	0.00	0.01	0.022	O	|	|	|	|	0.02
211.083	0.00	0.01	0.022	O	|	|	|	|	0.02
211.167	0.00	0.01	0.022	O	|	|	|	|	0.02
211.250	0.00	0.01	0.022	O	|	|	|	|	0.02
211.333	0.00	0.01	0.022	O	|	|	|	|	0.02
211.417	0.00	0.01	0.022	O	|	|	|	|	0.02
211.500	0.00	0.01	0.022	O	|	|	|	|	0.02
211.583	0.00	0.01	0.022	O	|	|	|	|	0.02
211.667	0.00	0.01	0.022	O	|	|	|	|	0.02
211.750	0.00	0.01	0.022	O	|	|	|	|	0.02
211.833	0.00	0.01	0.022	O	|	|	|	|	0.02
211.917	0.00	0.01	0.022	O	|	|	|	|	0.02
212.000	0.00	0.01	0.022	O	|	|	|	|	0.02
212.083	0.00	0.01	0.022	O	|	|	|	|	0.02
212.167	0.00	0.01	0.022	O	|	|	|	|	0.02
212.250	0.00	0.01	0.022	O	|	|	|	|	0.02
212.333	0.00	0.01	0.022	O	|	|	|	|	0.02
212.417	0.00	0.01	0.022	O	|	|	|	|	0.02
212.500	0.00	0.01	0.022	O	|	|	|	|	0.02
212.583	0.00	0.01	0.022	O	|	|	|	|	0.02
212.667	0.00	0.01	0.021	O	|	|	|	|	0.02
212.750	0.00	0.01	0.021	O	|	|	|	|	0.02
212.833	0.00	0.01	0.021	O	|	|	|	|	0.02
212.917	0.00	0.01	0.021	O	|	|	|	|	0.02
213.000	0.00	0.01	0.021	O	|	|	|	|	0.02
213.083	0.00	0.01	0.021	O	|	|	|	|	0.02
213.167	0.00	0.01	0.021	O	|	|	|	|	0.02

213.250	0.00	0.01	0.021	O	|	|	|	|	0.02
213.333	0.00	0.01	0.021	O	|	|	|	|	0.02
213.417	0.00	0.01	0.021	O	|	|	|	|	0.02
213.500	0.00	0.01	0.021	O	|	|	|	|	0.02
213.583	0.00	0.01	0.021	O	|	|	|	|	0.02
213.667	0.00	0.01	0.021	O	|	|	|	|	0.02
213.750	0.00	0.01	0.021	O	|	|	|	|	0.02
213.833	0.00	0.01	0.021	O	|	|	|	|	0.02
213.917	0.00	0.01	0.021	O	|	|	|	|	0.02
214.000	0.00	0.01	0.021	O	|	|	|	|	0.02
214.083	0.00	0.01	0.021	O	|	|	|	|	0.02
214.167	0.00	0.01	0.021	O	|	|	|	|	0.02
214.250	0.00	0.01	0.021	O	|	|	|	|	0.02
214.333	0.00	0.01	0.021	O	|	|	|	|	0.02
214.417	0.00	0.01	0.021	O	|	|	|	|	0.02
214.500	0.00	0.01	0.021	O	|	|	|	|	0.02
214.583	0.00	0.01	0.021	O	|	|	|	|	0.02
214.667	0.00	0.01	0.021	O	|	|	|	|	0.02
214.750	0.00	0.01	0.020	O	|	|	|	|	0.02
214.833	0.00	0.01	0.020	O	|	|	|	|	0.02
214.917	0.00	0.01	0.020	O	|	|	|	|	0.02
215.000	0.00	0.01	0.020	O	|	|	|	|	0.02
215.083	0.00	0.01	0.020	O	|	|	|	|	0.02
215.167	0.00	0.01	0.020	O	|	|	|	|	0.02
215.250	0.00	0.01	0.020	O	|	|	|	|	0.02
215.333	0.00	0.01	0.020	O	|	|	|	|	0.02
215.417	0.00	0.01	0.020	O	|	|	|	|	0.02
215.500	0.00	0.01	0.020	O	|	|	|	|	0.02
215.583	0.00	0.01	0.020	O	|	|	|	|	0.02
215.667	0.00	0.01	0.020	O	|	|	|	|	0.02
215.750	0.00	0.01	0.020	O	|	|	|	|	0.02
215.833	0.00	0.01	0.020	O	|	|	|	|	0.02
215.917	0.00	0.01	0.020	O	|	|	|	|	0.02
216.000	0.00	0.01	0.020	O	|	|	|	|	0.02
216.083	0.00	0.01	0.020	O	|	|	|	|	0.02
216.167	0.00	0.01	0.020	O	|	|	|	|	0.02
216.250	0.00	0.01	0.020	O	|	|	|	|	0.02
216.333	0.00	0.01	0.020	O	|	|	|	|	0.02
216.417	0.00	0.01	0.020	O	|	|	|	|	0.02
216.500	0.00	0.01	0.020	O	|	|	|	|	0.02
216.583	0.00	0.01	0.020	O	|	|	|	|	0.02
216.667	0.00	0.01	0.020	O	|	|	|	|	0.02
216.750	0.00	0.01	0.020	O	|	|	|	|	0.02
216.833	0.00	0.01	0.020	O	|	|	|	|	0.02
216.917	0.00	0.01	0.019	O	|	|	|	|	0.02
217.000	0.00	0.01	0.019	O	|	|	|	|	0.02
217.083	0.00	0.01	0.019	O	|	|	|	|	0.02
217.167	0.00	0.01	0.019	O	|	|	|	|	0.02
217.250	0.00	0.01	0.019	O	|	|	|	|	0.02
217.333	0.00	0.01	0.019	O	|	|	|	|	0.02
217.417	0.00	0.01	0.019	O	|	|	|	|	0.02
217.500	0.00	0.01	0.019	O	|	|	|	|	0.02
217.583	0.00	0.01	0.019	O	|	|	|	|	0.02
217.667	0.00	0.01	0.019	O	|	|	|	|	0.02
217.750	0.00	0.01	0.019	O	|	|	|	|	0.02
217.833	0.00	0.01	0.019	O	|	|	|	|	0.02
217.917	0.00	0.01	0.019	O	|	|	|	|	0.02
218.000	0.00	0.01	0.019	O	|	|	|	|	0.02
218.083	0.00	0.01	0.019	O	|	|	|	|	0.02
218.167	0.00	0.01	0.019	O	|	|	|	|	0.02
218.250	0.00	0.01	0.019	O	|	|	|	|	0.02
218.333	0.00	0.01	0.019	O	|	|	|	|	0.02
218.417	0.00	0.01	0.019	O	|	|	|	|	0.02
218.500	0.00	0.01	0.019	O	|	|	|	|	0.02
218.583	0.00	0.01	0.019	O	|	|	|	|	0.02
218.667	0.00	0.01	0.019	O	|	|	|	|	0.02
218.750	0.00	0.01	0.019	O	|	|	|	|	0.02
218.833	0.00	0.01	0.019	O	|	|	|	|	0.02
218.917	0.00	0.01	0.019	O	|	|	|	|	0.02
219.000	0.00	0.01	0.019	O	|	|	|	|	0.02
219.083	0.00	0.01	0.019	O	|	|	|	|	0.02

219.167	0.00	0.01	0.019	O	|	|	|	|	0.02
219.250	0.00	0.01	0.018	O	|	|	|	|	0.01
219.333	0.00	0.01	0.018	O	|	|	|	|	0.01
219.417	0.00	0.01	0.018	O	|	|	|	|	0.01
219.500	0.00	0.01	0.018	O	|	|	|	|	0.01
219.583	0.00	0.01	0.018	O	|	|	|	|	0.01
219.667	0.00	0.01	0.018	O	|	|	|	|	0.01
219.750	0.00	0.01	0.018	O	|	|	|	|	0.01
219.833	0.00	0.01	0.018	O	|	|	|	|	0.01
219.917	0.00	0.01	0.018	O	|	|	|	|	0.01
220.000	0.00	0.01	0.018	O	|	|	|	|	0.01
220.083	0.00	0.01	0.018	O	|	|	|	|	0.01
220.167	0.00	0.01	0.018	O	|	|	|	|	0.01
220.250	0.00	0.01	0.018	O	|	|	|	|	0.01
220.333	0.00	0.01	0.018	O	|	|	|	|	0.01
220.417	0.00	0.01	0.018	O	|	|	|	|	0.01
220.500	0.00	0.01	0.018	O	|	|	|	|	0.01
220.583	0.00	0.01	0.018	O	|	|	|	|	0.01
220.667	0.00	0.00	0.018	O	|	|	|	|	0.01
220.750	0.00	0.00	0.018	O	|	|	|	|	0.01
220.833	0.00	0.00	0.018	O	|	|	|	|	0.01
220.917	0.00	0.00	0.018	O	|	|	|	|	0.01
221.000	0.00	0.00	0.018	O	|	|	|	|	0.01
221.083	0.00	0.00	0.018	O	|	|	|	|	0.01
221.167	0.00	0.00	0.018	O	|	|	|	|	0.01
221.250	0.00	0.00	0.018	O	|	|	|	|	0.01
221.333	0.00	0.00	0.018	O	|	|	|	|	0.01
221.417	0.00	0.00	0.018	O	|	|	|	|	0.01
221.500	0.00	0.00	0.018	O	|	|	|	|	0.01
221.583	0.00	0.00	0.017	O	|	|	|	|	0.01
221.667	0.00	0.00	0.017	O	|	|	|	|	0.01
221.750	0.00	0.00	0.017	O	|	|	|	|	0.01
221.833	0.00	0.00	0.017	O	|	|	|	|	0.01
221.917	0.00	0.00	0.017	O	|	|	|	|	0.01
222.000	0.00	0.00	0.017	O	|	|	|	|	0.01
222.083	0.00	0.00	0.017	O	|	|	|	|	0.01
222.167	0.00	0.00	0.017	O	|	|	|	|	0.01
222.250	0.00	0.00	0.017	O	|	|	|	|	0.01
222.333	0.00	0.00	0.017	O	|	|	|	|	0.01
222.417	0.00	0.00	0.017	O	|	|	|	|	0.01
222.500	0.00	0.00	0.017	O	|	|	|	|	0.01
222.583	0.00	0.00	0.017	O	|	|	|	|	0.01
222.667	0.00	0.00	0.017	O	|	|	|	|	0.01
222.750	0.00	0.00	0.017	O	|	|	|	|	0.01
222.833	0.00	0.00	0.017	O	|	|	|	|	0.01
222.917	0.00	0.00	0.017	O	|	|	|	|	0.01
223.000	0.00	0.00	0.017	O	|	|	|	|	0.01
223.083	0.00	0.00	0.017	O	|	|	|	|	0.01
223.167	0.00	0.00	0.017	O	|	|	|	|	0.01
223.250	0.00	0.00	0.017	O	|	|	|	|	0.01
223.333	0.00	0.00	0.017	O	|	|	|	|	0.01
223.417	0.00	0.00	0.017	O	|	|	|	|	0.01
223.500	0.00	0.00	0.017	O	|	|	|	|	0.01
223.583	0.00	0.00	0.017	O	|	|	|	|	0.01
223.667	0.00	0.00	0.017	O	|	|	|	|	0.01
223.750	0.00	0.00	0.017	O	|	|	|	|	0.01
223.833	0.00	0.00	0.017	O	|	|	|	|	0.01
223.917	0.00	0.00	0.017	O	|	|	|	|	0.01
224.000	0.00	0.00	0.017	O	|	|	|	|	0.01
224.083	0.00	0.00	0.017	O	|	|	|	|	0.01
224.167	0.00	0.00	0.016	O	|	|	|	|	0.01
224.250	0.00	0.00	0.016	O	|	|	|	|	0.01
224.333	0.00	0.00	0.016	O	|	|	|	|	0.01
224.417	0.00	0.00	0.016	O	|	|	|	|	0.01
224.500	0.00	0.00	0.016	O	|	|	|	|	0.01
224.583	0.00	0.00	0.016	O	|	|	|	|	0.01
224.667	0.00	0.00	0.016	O	|	|	|	|	0.01
224.750	0.00	0.00	0.016	O	|	|	|	|	0.01
224.833	0.00	0.00	0.016	O	|	|	|	|	0.01
224.917	0.00	0.00	0.016	O	|	|	|	|	0.01
225.000	0.00	0.00	0.016	O	|	|	|	|	0.01

225.083	0.00	0.00	0.016	O	|	|	|	|	0.01
225.167	0.00	0.00	0.016	O	|	|	|	|	0.01
225.250	0.00	0.00	0.016	O	|	|	|	|	0.01
225.333	0.00	0.00	0.016	O	|	|	|	|	0.01
225.417	0.00	0.00	0.016	O	|	|	|	|	0.01
225.500	0.00	0.00	0.016	O	|	|	|	|	0.01
225.583	0.00	0.00	0.016	O	|	|	|	|	0.01
225.667	0.00	0.00	0.016	O	|	|	|	|	0.01
225.750	0.00	0.00	0.016	O	|	|	|	|	0.01
225.833	0.00	0.00	0.016	O	|	|	|	|	0.01
225.917	0.00	0.00	0.016	O	|	|	|	|	0.01
226.000	0.00	0.00	0.016	O	|	|	|	|	0.01
226.083	0.00	0.00	0.016	O	|	|	|	|	0.01
226.167	0.00	0.00	0.016	O	|	|	|	|	0.01
226.250	0.00	0.00	0.016	O	|	|	|	|	0.01
226.333	0.00	0.00	0.016	O	|	|	|	|	0.01
226.417	0.00	0.00	0.016	O	|	|	|	|	0.01
226.500	0.00	0.00	0.016	O	|	|	|	|	0.01
226.583	0.00	0.00	0.016	O	|	|	|	|	0.01
226.667	0.00	0.00	0.016	O	|	|	|	|	0.01
226.750	0.00	0.00	0.016	O	|	|	|	|	0.01
226.833	0.00	0.00	0.016	O	|	|	|	|	0.01
226.917	0.00	0.00	0.015	O	|	|	|	|	0.01
227.000	0.00	0.00	0.015	O	|	|	|	|	0.01
227.083	0.00	0.00	0.015	O	|	|	|	|	0.01
227.167	0.00	0.00	0.015	O	|	|	|	|	0.01
227.250	0.00	0.00	0.015	O	|	|	|	|	0.01
227.333	0.00	0.00	0.015	O	|	|	|	|	0.01
227.417	0.00	0.00	0.015	O	|	|	|	|	0.01
227.500	0.00	0.00	0.015	O	|	|	|	|	0.01
227.583	0.00	0.00	0.015	O	|	|	|	|	0.01
227.667	0.00	0.00	0.015	O	|	|	|	|	0.01
227.750	0.00	0.00	0.015	O	|	|	|	|	0.01
227.833	0.00	0.00	0.015	O	|	|	|	|	0.01
227.917	0.00	0.00	0.015	O	|	|	|	|	0.01
228.000	0.00	0.00	0.015	O	|	|	|	|	0.01
228.083	0.00	0.00	0.015	O	|	|	|	|	0.01
228.167	0.00	0.00	0.015	O	|	|	|	|	0.01
228.250	0.00	0.00	0.015	O	|	|	|	|	0.01
228.333	0.00	0.00	0.015	O	|	|	|	|	0.01
228.417	0.00	0.00	0.015	O	|	|	|	|	0.01
228.500	0.00	0.00	0.015	O	|	|	|	|	0.01
228.583	0.00	0.00	0.015	O	|	|	|	|	0.01
228.667	0.00	0.00	0.015	O	|	|	|	|	0.01
228.750	0.00	0.00	0.015	O	|	|	|	|	0.01
228.833	0.00	0.00	0.015	O	|	|	|	|	0.01
228.917	0.00	0.00	0.015	O	|	|	|	|	0.01
229.000	0.00	0.00	0.015	O	|	|	|	|	0.01
229.083	0.00	0.00	0.015	O	|	|	|	|	0.01
229.167	0.00	0.00	0.015	O	|	|	|	|	0.01
229.250	0.00	0.00	0.015	O	|	|	|	|	0.01
229.333	0.00	0.00	0.015	O	|	|	|	|	0.01
229.417	0.00	0.00	0.015	O	|	|	|	|	0.01
229.500	0.00	0.00	0.015	O	|	|	|	|	0.01
229.583	0.00	0.00	0.015	O	|	|	|	|	0.01
229.667	0.00	0.00	0.015	O	|	|	|	|	0.01
229.750	0.00	0.00	0.014	O	|	|	|	|	0.01
229.833	0.00	0.00	0.014	O	|	|	|	|	0.01
229.917	0.00	0.00	0.014	O	|	|	|	|	0.01
230.000	0.00	0.00	0.014	O	|	|	|	|	0.01
230.083	0.00	0.00	0.014	O	|	|	|	|	0.01
230.167	0.00	0.00	0.014	O	|	|	|	|	0.01
230.250	0.00	0.00	0.014	O	|	|	|	|	0.01
230.333	0.00	0.00	0.014	O	|	|	|	|	0.01
230.417	0.00	0.00	0.014	O	|	|	|	|	0.01
230.500	0.00	0.00	0.014	O	|	|	|	|	0.01
230.583	0.00	0.00	0.014	O	|	|	|	|	0.01
230.667	0.00	0.00	0.014	O	|	|	|	|	0.01
230.750	0.00	0.00	0.014	O	|	|	|	|	0.01
230.833	0.00	0.00	0.014	O	|	|	|	|	0.01
230.917	0.00	0.00	0.014	O	|	|	|	|	0.01

231.000	0.00	0.00	0.014	O	|	|	|	| 0.01
231.083	0.00	0.00	0.014	O	|	|	|	| 0.01
231.167	0.00	0.00	0.014	O	|	|	|	| 0.01
231.250	0.00	0.00	0.014	O	|	|	|	| 0.01
231.333	0.00	0.00	0.014	O	|	|	|	| 0.01
231.417	0.00	0.00	0.014	O	|	|	|	| 0.01
231.500	0.00	0.00	0.014	O	|	|	|	| 0.01
231.583	0.00	0.00	0.014	O	|	|	|	| 0.01
231.667	0.00	0.00	0.014	O	|	|	|	| 0.01
231.750	0.00	0.00	0.014	O	|	|	|	| 0.01
231.833	0.00	0.00	0.014	O	|	|	|	| 0.01
231.917	0.00	0.00	0.014	O	|	|	|	| 0.01
232.000	0.00	0.00	0.014	O	|	|	|	| 0.01
232.083	0.00	0.00	0.014	O	|	|	|	| 0.01
232.167	0.00	0.00	0.014	O	|	|	|	| 0.01
232.250	0.00	0.00	0.014	O	|	|	|	| 0.01
232.333	0.00	0.00	0.014	O	|	|	|	| 0.01
232.417	0.00	0.00	0.014	O	|	|	|	| 0.01
232.500	0.00	0.00	0.014	O	|	|	|	| 0.01
232.583	0.00	0.00	0.014	O	|	|	|	| 0.01
232.667	0.00	0.00	0.014	O	|	|	|	| 0.01
232.750	0.00	0.00	0.014	O	|	|	|	| 0.01
232.833	0.00	0.00	0.013	O	|	|	|	| 0.01
232.917	0.00	0.00	0.013	O	|	|	|	| 0.01
233.000	0.00	0.00	0.013	O	|	|	|	| 0.01
233.083	0.00	0.00	0.013	O	|	|	|	| 0.01
233.167	0.00	0.00	0.013	O	|	|	|	| 0.01
233.250	0.00	0.00	0.013	O	|	|	|	| 0.01
233.333	0.00	0.00	0.013	O	|	|	|	| 0.01
233.417	0.00	0.00	0.013	O	|	|	|	| 0.01
233.500	0.00	0.00	0.013	O	|	|	|	| 0.01
233.583	0.00	0.00	0.013	O	|	|	|	| 0.01
233.667	0.00	0.00	0.013	O	|	|	|	| 0.01
233.750	0.00	0.00	0.013	O	|	|	|	| 0.01
233.833	0.00	0.00	0.013	O	|	|	|	| 0.01
233.917	0.00	0.00	0.013	O	|	|	|	| 0.01
234.000	0.00	0.00	0.013	O	|	|	|	| 0.01
234.083	0.00	0.00	0.013	O	|	|	|	| 0.01
234.167	0.00	0.00	0.013	O	|	|	|	| 0.01
234.250	0.00	0.00	0.013	O	|	|	|	| 0.01
234.333	0.00	0.00	0.013	O	|	|	|	| 0.01
234.417	0.00	0.00	0.013	O	|	|	|	| 0.01
234.500	0.00	0.00	0.013	O	|	|	|	| 0.01
234.583	0.00	0.00	0.013	O	|	|	|	| 0.01
234.667	0.00	0.00	0.013	O	|	|	|	| 0.01
234.750	0.00	0.00	0.013	O	|	|	|	| 0.01
234.833	0.00	0.00	0.013	O	|	|	|	| 0.01
234.917	0.00	0.00	0.013	O	|	|	|	| 0.01
235.000	0.00	0.00	0.013	O	|	|	|	| 0.01
235.083	0.00	0.00	0.013	O	|	|	|	| 0.01
235.167	0.00	0.00	0.013	O	|	|	|	| 0.01
235.250	0.00	0.00	0.013	O	|	|	|	| 0.01
235.333	0.00	0.00	0.013	O	|	|	|	| 0.01
235.417	0.00	0.00	0.013	O	|	|	|	| 0.01
235.500	0.00	0.00	0.013	O	|	|	|	| 0.01
235.583	0.00	0.00	0.013	O	|	|	|	| 0.01
235.667	0.00	0.00	0.013	O	|	|	|	| 0.01
235.750	0.00	0.00	0.013	O	|	|	|	| 0.01
235.833	0.00	0.00	0.013	O	|	|	|	| 0.01
235.917	0.00	0.00	0.013	O	|	|	|	| 0.01
236.000	0.00	0.00	0.013	O	|	|	|	| 0.01
236.083	0.00	0.00	0.013	O	|	|	|	| 0.01
236.167	0.00	0.00	0.012	O	|	|	|	| 0.01
236.250	0.00	0.00	0.012	O	|	|	|	| 0.01
236.333	0.00	0.00	0.012	O	|	|	|	| 0.01
236.417	0.00	0.00	0.012	O	|	|	|	| 0.01
236.500	0.00	0.00	0.012	O	|	|	|	| 0.01
236.583	0.00	0.00	0.012	O	|	|	|	| 0.01
236.667	0.00	0.00	0.012	O	|	|	|	| 0.01
236.750	0.00	0.00	0.012	O	|	|	|	| 0.01
236.833	0.00	0.00	0.012	O	|	|	|	| 0.01

236.917	0.00	0.00	0.012	O	|	|	|	|	0.01
237.000	0.00	0.00	0.012	O	|	|	|	|	0.01
237.083	0.00	0.00	0.012	O	|	|	|	|	0.01
237.167	0.00	0.00	0.012	O	|	|	|	|	0.01
237.250	0.00	0.00	0.012	O	|	|	|	|	0.01
237.333	0.00	0.00	0.012	O	|	|	|	|	0.01
237.417	0.00	0.00	0.012	O	|	|	|	|	0.01
237.500	0.00	0.00	0.012	O	|	|	|	|	0.01
237.583	0.00	0.00	0.012	O	|	|	|	|	0.01
237.667	0.00	0.00	0.012	O	|	|	|	|	0.01
237.750	0.00	0.00	0.012	O	|	|	|	|	0.01
237.833	0.00	0.00	0.012	O	|	|	|	|	0.01
237.917	0.00	0.00	0.012	O	|	|	|	|	0.01
238.000	0.00	0.00	0.012	O	|	|	|	|	0.01
238.083	0.00	0.00	0.012	O	|	|	|	|	0.01
238.167	0.00	0.00	0.012	O	|	|	|	|	0.01
238.250	0.00	0.00	0.012	O	|	|	|	|	0.01
238.333	0.00	0.00	0.012	O	|	|	|	|	0.01
238.417	0.00	0.00	0.012	O	|	|	|	|	0.01
238.500	0.00	0.00	0.012	O	|	|	|	|	0.01
238.583	0.00	0.00	0.012	O	|	|	|	|	0.01
238.667	0.00	0.00	0.012	O	|	|	|	|	0.01
238.750	0.00	0.00	0.012	O	|	|	|	|	0.01
238.833	0.00	0.00	0.012	O	|	|	|	|	0.01
238.917	0.00	0.00	0.012	O	|	|	|	|	0.01
239.000	0.00	0.00	0.012	O	|	|	|	|	0.01
239.083	0.00	0.00	0.012	O	|	|	|	|	0.01
239.167	0.00	0.00	0.012	O	|	|	|	|	0.01
239.250	0.00	0.00	0.012	O	|	|	|	|	0.01
239.333	0.00	0.00	0.012	O	|	|	|	|	0.01
239.417	0.00	0.00	0.012	O	|	|	|	|	0.01
239.500	0.00	0.00	0.012	O	|	|	|	|	0.01
239.583	0.00	0.00	0.012	O	|	|	|	|	0.01
239.667	0.00	0.00	0.012	O	|	|	|	|	0.01
239.750	0.00	0.00	0.012	O	|	|	|	|	0.01
239.833	0.00	0.00	0.011	O	|	|	|	|	0.01
239.917	0.00	0.00	0.011	O	|	|	|	|	0.01
240.000	0.00	0.00	0.011	O	|	|	|	|	0.01
240.083	0.00	0.00	0.011	O	|	|	|	|	0.01
240.167	0.00	0.00	0.011	O	|	|	|	|	0.01
240.250	0.00	0.00	0.011	O	|	|	|	|	0.01
240.333	0.00	0.00	0.011	O	|	|	|	|	0.01
240.417	0.00	0.00	0.011	O	|	|	|	|	0.01
240.500	0.00	0.00	0.011	O	|	|	|	|	0.01
240.583	0.00	0.00	0.011	O	|	|	|	|	0.01
240.667	0.00	0.00	0.011	O	|	|	|	|	0.01
240.750	0.00	0.00	0.011	O	|	|	|	|	0.01
240.833	0.00	0.00	0.011	O	|	|	|	|	0.01
240.917	0.00	0.00	0.011	O	|	|	|	|	0.01
241.000	0.00	0.00	0.011	O	|	|	|	|	0.01
241.083	0.00	0.00	0.011	O	|	|	|	|	0.01
241.167	0.00	0.00	0.011	O	|	|	|	|	0.01
241.250	0.00	0.00	0.011	O	|	|	|	|	0.01
241.333	0.00	0.00	0.011	O	|	|	|	|	0.01
241.417	0.00	0.00	0.011	O	|	|	|	|	0.01
241.500	0.00	0.00	0.011	O	|	|	|	|	0.01
241.583	0.00	0.00	0.011	O	|	|	|	|	0.01
241.667	0.00	0.00	0.011	O	|	|	|	|	0.01
241.750	0.00	0.00	0.011	O	|	|	|	|	0.01
241.833	0.00	0.00	0.011	O	|	|	|	|	0.01
241.917	0.00	0.00	0.011	O	|	|	|	|	0.01
242.000	0.00	0.00	0.011	O	|	|	|	|	0.01
242.083	0.00	0.00	0.011	O	|	|	|	|	0.01
242.167	0.00	0.00	0.011	O	|	|	|	|	0.01
242.250	0.00	0.00	0.011	O	|	|	|	|	0.01
242.333	0.00	0.00	0.011	O	|	|	|	|	0.01
242.417	0.00	0.00	0.011	O	|	|	|	|	0.01
242.500	0.00	0.00	0.011	O	|	|	|	|	0.01
242.583	0.00	0.00	0.011	O	|	|	|	|	0.01
242.667	0.00	0.00	0.011	O	|	|	|	|	0.01
242.750	0.00	0.00	0.011	O	|	|	|	|	0.01

242.833	0.00	0.00	0.011	O	|	|	|	|	0.01
242.917	0.00	0.00	0.011	O	|	|	|	|	0.01
243.000	0.00	0.00	0.011	O	|	|	|	|	0.01
243.083	0.00	0.00	0.011	O	|	|	|	|	0.01
243.167	0.00	0.00	0.011	O	|	|	|	|	0.01
243.250	0.00	0.00	0.011	O	|	|	|	|	0.01
243.333	0.00	0.00	0.011	O	|	|	|	|	0.01
243.417	0.00	0.00	0.011	O	|	|	|	|	0.01
243.500	0.00	0.00	0.011	O	|	|	|	|	0.01
243.583	0.00	0.00	0.011	O	|	|	|	|	0.01
243.667	0.00	0.00	0.011	O	|	|	|	|	0.01
243.750	0.00	0.00	0.010	O	|	|	|	|	0.01
243.833	0.00	0.00	0.010	O	|	|	|	|	0.01
243.917	0.00	0.00	0.010	O	|	|	|	|	0.01
244.000	0.00	0.00	0.010	O	|	|	|	|	0.01
244.083	0.00	0.00	0.010	O	|	|	|	|	0.01
244.167	0.00	0.00	0.010	O	|	|	|	|	0.01
244.250	0.00	0.00	0.010	O	|	|	|	|	0.01
244.333	0.00	0.00	0.010	O	|	|	|	|	0.01
244.417	0.00	0.00	0.010	O	|	|	|	|	0.01
244.500	0.00	0.00	0.010	O	|	|	|	|	0.01
244.583	0.00	0.00	0.010	O	|	|	|	|	0.01
244.667	0.00	0.00	0.010	O	|	|	|	|	0.01
244.750	0.00	0.00	0.010	O	|	|	|	|	0.01
244.833	0.00	0.00	0.010	O	|	|	|	|	0.01
244.917	0.00	0.00	0.010	O	|	|	|	|	0.01
245.000	0.00	0.00	0.010	O	|	|	|	|	0.01
245.083	0.00	0.00	0.010	O	|	|	|	|	0.01
245.167	0.00	0.00	0.010	O	|	|	|	|	0.01
245.250	0.00	0.00	0.010	O	|	|	|	|	0.01
245.333	0.00	0.00	0.010	O	|	|	|	|	0.01
245.417	0.00	0.00	0.010	O	|	|	|	|	0.01
245.500	0.00	0.00	0.010	O	|	|	|	|	0.01
245.583	0.00	0.00	0.010	O	|	|	|	|	0.01
245.667	0.00	0.00	0.010	O	|	|	|	|	0.01
245.750	0.00	0.00	0.010	O	|	|	|	|	0.01
245.833	0.00	0.00	0.010	O	|	|	|	|	0.01
245.917	0.00	0.00	0.010	O	|	|	|	|	0.01
246.000	0.00	0.00	0.010	O	|	|	|	|	0.01
246.083	0.00	0.00	0.010	O	|	|	|	|	0.01
246.167	0.00	0.00	0.010	O	|	|	|	|	0.01
246.250	0.00	0.00	0.010	O	|	|	|	|	0.01
246.333	0.00	0.00	0.010	O	|	|	|	|	0.01
246.417	0.00	0.00	0.010	O	|	|	|	|	0.01
246.500	0.00	0.00	0.010	O	|	|	|	|	0.01
246.583	0.00	0.00	0.010	O	|	|	|	|	0.01
246.667	0.00	0.00	0.010	O	|	|	|	|	0.01
246.750	0.00	0.00	0.010	O	|	|	|	|	0.01
246.833	0.00	0.00	0.010	O	|	|	|	|	0.01
246.917	0.00	0.00	0.010	O	|	|	|	|	0.01
247.000	0.00	0.00	0.010	O	|	|	|	|	0.01
247.083	0.00	0.00	0.010	O	|	|	|	|	0.01
247.167	0.00	0.00	0.010	O	|	|	|	|	0.01
247.250	0.00	0.00	0.010	O	|	|	|	|	0.01
247.333	0.00	0.00	0.010	O	|	|	|	|	0.01
247.417	0.00	0.00	0.010	O	|	|	|	|	0.01
247.500	0.00	0.00	0.010	O	|	|	|	|	0.01
247.583	0.00	0.00	0.010	O	|	|	|	|	0.01
247.667	0.00	0.00	0.010	O	|	|	|	|	0.01
247.750	0.00	0.00	0.010	O	|	|	|	|	0.01
247.833	0.00	0.00	0.010	O	|	|	|	|	0.01
247.917	0.00	0.00	0.010	O	|	|	|	|	0.01
248.000	0.00	0.00	0.010	O	|	|	|	|	0.01
248.083	0.00	0.00	0.009	O	|	|	|	|	0.01
248.167	0.00	0.00	0.009	O	|	|	|	|	0.01
248.250	0.00	0.00	0.009	O	|	|	|	|	0.01
248.333	0.00	0.00	0.009	O	|	|	|	|	0.01
248.417	0.00	0.00	0.009	O	|	|	|	|	0.01
248.500	0.00	0.00	0.009	O	|	|	|	|	0.01
248.583	0.00	0.00	0.009	O	|	|	|	|	0.01
248.667	0.00	0.00	0.009	O	|	|	|	|	0.01

248.750	0.00	0.00	0.009	O	|	|	|	|	0.01
248.833	0.00	0.00	0.009	O	|	|	|	|	0.01
248.917	0.00	0.00	0.009	O	|	|	|	|	0.01
249.000	0.00	0.00	0.009	O	|	|	|	|	0.01
249.083	0.00	0.00	0.009	O	|	|	|	|	0.01
249.167	0.00	0.00	0.009	O	|	|	|	|	0.01
249.250	0.00	0.00	0.009	O	|	|	|	|	0.01
249.333	0.00	0.00	0.009	O	|	|	|	|	0.01
249.417	0.00	0.00	0.009	O	|	|	|	|	0.01
249.500	0.00	0.00	0.009	O	|	|	|	|	0.01
249.583	0.00	0.00	0.009	O	|	|	|	|	0.01
249.667	0.00	0.00	0.009	O	|	|	|	|	0.01
249.750	0.00	0.00	0.009	O	|	|	|	|	0.01
249.833	0.00	0.00	0.009	O	|	|	|	|	0.01
249.917	0.00	0.00	0.009	O	|	|	|	|	0.01
250.000	0.00	0.00	0.009	O	|	|	|	|	0.01
250.083	0.00	0.00	0.009	O	|	|	|	|	0.01
250.167	0.00	0.00	0.009	O	|	|	|	|	0.01
250.250	0.00	0.00	0.009	O	|	|	|	|	0.01
250.333	0.00	0.00	0.009	O	|	|	|	|	0.01
250.417	0.00	0.00	0.009	O	|	|	|	|	0.01
250.500	0.00	0.00	0.009	O	|	|	|	|	0.01
250.583	0.00	0.00	0.009	O	|	|	|	|	0.01
250.667	0.00	0.00	0.009	O	|	|	|	|	0.01
250.750	0.00	0.00	0.009	O	|	|	|	|	0.01
250.833	0.00	0.00	0.009	O	|	|	|	|	0.01
250.917	0.00	0.00	0.009	O	|	|	|	|	0.01
251.000	0.00	0.00	0.009	O	|	|	|	|	0.01
251.083	0.00	0.00	0.009	O	|	|	|	|	0.01
251.167	0.00	0.00	0.009	O	|	|	|	|	0.01
251.250	0.00	0.00	0.009	O	|	|	|	|	0.01
251.333	0.00	0.00	0.009	O	|	|	|	|	0.01
251.417	0.00	0.00	0.009	O	|	|	|	|	0.01
251.500	0.00	0.00	0.009	O	|	|	|	|	0.01
251.583	0.00	0.00	0.009	O	|	|	|	|	0.01
251.667	0.00	0.00	0.009	O	|	|	|	|	0.01
251.750	0.00	0.00	0.009	O	|	|	|	|	0.01
251.833	0.00	0.00	0.009	O	|	|	|	|	0.01
251.917	0.00	0.00	0.009	O	|	|	|	|	0.01
252.000	0.00	0.00	0.009	O	|	|	|	|	0.01
252.083	0.00	0.00	0.009	O	|	|	|	|	0.01
252.167	0.00	0.00	0.009	O	|	|	|	|	0.01
252.250	0.00	0.00	0.009	O	|	|	|	|	0.01
252.333	0.00	0.00	0.009	O	|	|	|	|	0.01
252.417	0.00	0.00	0.009	O	|	|	|	|	0.01
252.500	0.00	0.00	0.009	O	|	|	|	|	0.01
252.583	0.00	0.00	0.009	O	|	|	|	|	0.01
252.667	0.00	0.00	0.009	O	|	|	|	|	0.01
252.750	0.00	0.00	0.009	O	|	|	|	|	0.01
252.833	0.00	0.00	0.009	O	|	|	|	|	0.01
252.917	0.00	0.00	0.008	O	|	|	|	|	0.01
253.000	0.00	0.00	0.008	O	|	|	|	|	0.01
253.083	0.00	0.00	0.008	O	|	|	|	|	0.01
253.167	0.00	0.00	0.008	O	|	|	|	|	0.01
253.250	0.00	0.00	0.008	O	|	|	|	|	0.01
253.333	0.00	0.00	0.008	O	|	|	|	|	0.01
253.417	0.00	0.00	0.008	O	|	|	|	|	0.01
253.500	0.00	0.00	0.008	O	|	|	|	|	0.01
253.583	0.00	0.00	0.008	O	|	|	|	|	0.01
253.667	0.00	0.00	0.008	O	|	|	|	|	0.01
253.750	0.00	0.00	0.008	O	|	|	|	|	0.01
253.833	0.00	0.00	0.008	O	|	|	|	|	0.01
253.917	0.00	0.00	0.008	O	|	|	|	|	0.01
254.000	0.00	0.00	0.008	O	|	|	|	|	0.01
254.083	0.00	0.00	0.008	O	|	|	|	|	0.01
254.167	0.00	0.00	0.008	O	|	|	|	|	0.01
254.250	0.00	0.00	0.008	O	|	|	|	|	0.01
254.333	0.00	0.00	0.008	O	|	|	|	|	0.01
254.417	0.00	0.00	0.008	O	|	|	|	|	0.01
254.500	0.00	0.00	0.008	O	|	|	|	|	0.01
254.583	0.00	0.00	0.008	O	|	|	|	|	0.01

254.667	0.00	0.00	0.008	O	|	|	|	|	0.01
254.750	0.00	0.00	0.008	O	|	|	|	|	0.01
254.833	0.00	0.00	0.008	O	|	|	|	|	0.01
254.917	0.00	0.00	0.008	O	|	|	|	|	0.01
255.000	0.00	0.00	0.008	O	|	|	|	|	0.01
255.083	0.00	0.00	0.008	O	|	|	|	|	0.01
255.167	0.00	0.00	0.008	O	|	|	|	|	0.01
255.250	0.00	0.00	0.008	O	|	|	|	|	0.01
255.333	0.00	0.00	0.008	O	|	|	|	|	0.01
255.417	0.00	0.00	0.008	O	|	|	|	|	0.01
255.500	0.00	0.00	0.008	O	|	|	|	|	0.01
255.583	0.00	0.00	0.008	O	|	|	|	|	0.01
255.667	0.00	0.00	0.008	O	|	|	|	|	0.01
255.750	0.00	0.00	0.008	O	|	|	|	|	0.01
255.833	0.00	0.00	0.008	O	|	|	|	|	0.01
255.917	0.00	0.00	0.008	O	|	|	|	|	0.01
256.000	0.00	0.00	0.008	O	|	|	|	|	0.01
256.083	0.00	0.00	0.008	O	|	|	|	|	0.01
256.167	0.00	0.00	0.008	O	|	|	|	|	0.01
256.250	0.00	0.00	0.008	O	|	|	|	|	0.01
256.333	0.00	0.00	0.008	O	|	|	|	|	0.01
256.417	0.00	0.00	0.008	O	|	|	|	|	0.01
256.500	0.00	0.00	0.008	O	|	|	|	|	0.01
256.583	0.00	0.00	0.008	O	|	|	|	|	0.01
256.667	0.00	0.00	0.008	O	|	|	|	|	0.01
256.750	0.00	0.00	0.008	O	|	|	|	|	0.01
256.833	0.00	0.00	0.008	O	|	|	|	|	0.01
256.917	0.00	0.00	0.008	O	|	|	|	|	0.01
257.000	0.00	0.00	0.008	O	|	|	|	|	0.01
257.083	0.00	0.00	0.008	O	|	|	|	|	0.01
257.167	0.00	0.00	0.008	O	|	|	|	|	0.01
257.250	0.00	0.00	0.008	O	|	|	|	|	0.01
257.333	0.00	0.00	0.008	O	|	|	|	|	0.01
257.417	0.00	0.00	0.008	O	|	|	|	|	0.01
257.500	0.00	0.00	0.008	O	|	|	|	|	0.01
257.583	0.00	0.00	0.008	O	|	|	|	|	0.01
257.667	0.00	0.00	0.008	O	|	|	|	|	0.01
257.750	0.00	0.00	0.008	O	|	|	|	|	0.01
257.833	0.00	0.00	0.008	O	|	|	|	|	0.01
257.917	0.00	0.00	0.008	O	|	|	|	|	0.01
258.000	0.00	0.00	0.008	O	|	|	|	|	0.01
258.083	0.00	0.00	0.008	O	|	|	|	|	0.01
258.167	0.00	0.00	0.008	O	|	|	|	|	0.01
258.250	0.00	0.00	0.008	O	|	|	|	|	0.01
258.333	0.00	0.00	0.007	O	|	|	|	|	0.01
258.417	0.00	0.00	0.007	O	|	|	|	|	0.01
258.500	0.00	0.00	0.007	O	|	|	|	|	0.01
258.583	0.00	0.00	0.007	O	|	|	|	|	0.01
258.667	0.00	0.00	0.007	O	|	|	|	|	0.01
258.750	0.00	0.00	0.007	O	|	|	|	|	0.01
258.833	0.00	0.00	0.007	O	|	|	|	|	0.01
258.917	0.00	0.00	0.007	O	|	|	|	|	0.01
259.000	0.00	0.00	0.007	O	|	|	|	|	0.01
259.083	0.00	0.00	0.007	O	|	|	|	|	0.01
259.167	0.00	0.00	0.007	O	|	|	|	|	0.01
259.250	0.00	0.00	0.007	O	|	|	|	|	0.01
259.333	0.00	0.00	0.007	O	|	|	|	|	0.01
259.417	0.00	0.00	0.007	O	|	|	|	|	0.01
259.500	0.00	0.00	0.007	O	|	|	|	|	0.01
259.583	0.00	0.00	0.007	O	|	|	|	|	0.01
259.667	0.00	0.00	0.007	O	|	|	|	|	0.01
259.750	0.00	0.00	0.007	O	|	|	|	|	0.01
259.833	0.00	0.00	0.007	O	|	|	|	|	0.01
259.917	0.00	0.00	0.007	O	|	|	|	|	0.01
260.000	0.00	0.00	0.007	O	|	|	|	|	0.01
260.083	0.00	0.00	0.007	O	|	|	|	|	0.01
260.167	0.00	0.00	0.007	O	|	|	|	|	0.01
260.250	0.00	0.00	0.007	O	|	|	|	|	0.01
260.333	0.00	0.00	0.007	O	|	|	|	|	0.01
260.417	0.00	0.00	0.007	O	|	|	|	|	0.01
260.500	0.00	0.00	0.007	O	|	|	|	|	0.01

260.583	0.00	0.00	0.007	O	|	|	|	|	0.01
260.667	0.00	0.00	0.007	O	|	|	|	|	0.01
260.750	0.00	0.00	0.007	O	|	|	|	|	0.01
260.833	0.00	0.00	0.007	O	|	|	|	|	0.01
260.917	0.00	0.00	0.007	O	|	|	|	|	0.01
261.000	0.00	0.00	0.007	O	|	|	|	|	0.01
261.083	0.00	0.00	0.007	O	|	|	|	|	0.01
261.167	0.00	0.00	0.007	O	|	|	|	|	0.01
261.250	0.00	0.00	0.007	O	|	|	|	|	0.01
261.333	0.00	0.00	0.007	O	|	|	|	|	0.01
261.417	0.00	0.00	0.007	O	|	|	|	|	0.01
261.500	0.00	0.00	0.007	O	|	|	|	|	0.01
261.583	0.00	0.00	0.007	O	|	|	|	|	0.01
261.667	0.00	0.00	0.007	O	|	|	|	|	0.01
261.750	0.00	0.00	0.007	O	|	|	|	|	0.01
261.833	0.00	0.00	0.007	O	|	|	|	|	0.01
261.917	0.00	0.00	0.007	O	|	|	|	|	0.01
262.000	0.00	0.00	0.007	O	|	|	|	|	0.01
262.083	0.00	0.00	0.007	O	|	|	|	|	0.01
262.167	0.00	0.00	0.007	O	|	|	|	|	0.01
262.250	0.00	0.00	0.007	O	|	|	|	|	0.01
262.333	0.00	0.00	0.007	O	|	|	|	|	0.01
262.417	0.00	0.00	0.007	O	|	|	|	|	0.01
262.500	0.00	0.00	0.007	O	|	|	|	|	0.01
262.583	0.00	0.00	0.007	O	|	|	|	|	0.01
262.667	0.00	0.00	0.007	O	|	|	|	|	0.01
262.750	0.00	0.00	0.007	O	|	|	|	|	0.01
262.833	0.00	0.00	0.007	O	|	|	|	|	0.01
262.917	0.00	0.00	0.007	O	|	|	|	|	0.01
263.000	0.00	0.00	0.007	O	|	|	|	|	0.01
263.083	0.00	0.00	0.007	O	|	|	|	|	0.01
263.167	0.00	0.00	0.007	O	|	|	|	|	0.01
263.250	0.00	0.00	0.007	O	|	|	|	|	0.01
263.333	0.00	0.00	0.007	O	|	|	|	|	0.01
263.417	0.00	0.00	0.007	O	|	|	|	|	0.01
263.500	0.00	0.00	0.007	O	|	|	|	|	0.01
263.583	0.00	0.00	0.007	O	|	|	|	|	0.01
263.667	0.00	0.00	0.007	O	|	|	|	|	0.01
263.750	0.00	0.00	0.007	O	|	|	|	|	0.01
263.833	0.00	0.00	0.007	O	|	|	|	|	0.01
263.917	0.00	0.00	0.007	O	|	|	|	|	0.01
264.000	0.00	0.00	0.007	O	|	|	|	|	0.01
264.083	0.00	0.00	0.007	O	|	|	|	|	0.01
264.167	0.00	0.00	0.007	O	|	|	|	|	0.01
264.250	0.00	0.00	0.007	O	|	|	|	|	0.01
264.333	0.00	0.00	0.007	O	|	|	|	|	0.01
264.417	0.00	0.00	0.007	O	|	|	|	|	0.01
264.500	0.00	0.00	0.006	O	|	|	|	|	0.01
264.583	0.00	0.00	0.006	O	|	|	|	|	0.01
264.667	0.00	0.00	0.006	O	|	|	|	|	0.01
264.750	0.00	0.00	0.006	O	|	|	|	|	0.01
264.833	0.00	0.00	0.006	O	|	|	|	|	0.01
264.917	0.00	0.00	0.006	O	|	|	|	|	0.01
265.000	0.00	0.00	0.006	O	|	|	|	|	0.01
265.083	0.00	0.00	0.006	O	|	|	|	|	0.01
265.167	0.00	0.00	0.006	O	|	|	|	|	0.01
265.250	0.00	0.00	0.006	O	|	|	|	|	0.01
265.333	0.00	0.00	0.006	O	|	|	|	|	0.01
265.417	0.00	0.00	0.006	O	|	|	|	|	0.01
265.500	0.00	0.00	0.006	O	|	|	|	|	0.01
265.583	0.00	0.00	0.006	O	|	|	|	|	0.01
265.667	0.00	0.00	0.006	O	|	|	|	|	0.01
265.750	0.00	0.00	0.006	O	|	|	|	|	0.01
265.833	0.00	0.00	0.006	O	|	|	|	|	0.01
265.917	0.00	0.00	0.006	O	|	|	|	|	0.01
266.000	0.00	0.00	0.006	O	|	|	|	|	0.01
266.083	0.00	0.00	0.006	O	|	|	|	|	0.01
266.167	0.00	0.00	0.006	O	|	|	|	|	0.01
266.250	0.00	0.00	0.006	O	|	|	|	|	0.01
266.333	0.00	0.00	0.006	O	|	|	|	|	0.01
266.417	0.00	0.00	0.006	O	|	|	|	|	0.01

266.500	0.00	0.00	0.006	O	|	|	|	|	0.01
266.583	0.00	0.00	0.006	O	|	|	|	|	0.01
266.667	0.00	0.00	0.006	O	|	|	|	|	0.01
266.750	0.00	0.00	0.006	O	|	|	|	|	0.01
266.833	0.00	0.00	0.006	O	|	|	|	|	0.00
266.917	0.00	0.00	0.006	O	|	|	|	|	0.00
267.000	0.00	0.00	0.006	O	|	|	|	|	0.00
267.083	0.00	0.00	0.006	O	|	|	|	|	0.00
267.167	0.00	0.00	0.006	O	|	|	|	|	0.00
267.250	0.00	0.00	0.006	O	|	|	|	|	0.00
267.333	0.00	0.00	0.006	O	|	|	|	|	0.00
267.417	0.00	0.00	0.006	O	|	|	|	|	0.00
267.500	0.00	0.00	0.006	O	|	|	|	|	0.00
267.583	0.00	0.00	0.006	O	|	|	|	|	0.00
267.667	0.00	0.00	0.006	O	|	|	|	|	0.00
267.750	0.00	0.00	0.006	O	|	|	|	|	0.00
267.833	0.00	0.00	0.006	O	|	|	|	|	0.00
267.917	0.00	0.00	0.006	O	|	|	|	|	0.00
268.000	0.00	0.00	0.006	O	|	|	|	|	0.00
268.083	0.00	0.00	0.006	O	|	|	|	|	0.00
268.167	0.00	0.00	0.006	O	|	|	|	|	0.00
268.250	0.00	0.00	0.006	O	|	|	|	|	0.00
268.333	0.00	0.00	0.006	O	|	|	|	|	0.00
268.417	0.00	0.00	0.006	O	|	|	|	|	0.00
268.500	0.00	0.00	0.006	O	|	|	|	|	0.00
268.583	0.00	0.00	0.006	O	|	|	|	|	0.00
268.667	0.00	0.00	0.006	O	|	|	|	|	0.00
268.750	0.00	0.00	0.006	O	|	|	|	|	0.00
268.833	0.00	0.00	0.006	O	|	|	|	|	0.00
268.917	0.00	0.00	0.006	O	|	|	|	|	0.00
269.000	0.00	0.00	0.006	O	|	|	|	|	0.00
269.083	0.00	0.00	0.006	O	|	|	|	|	0.00
269.167	0.00	0.00	0.006	O	|	|	|	|	0.00
269.250	0.00	0.00	0.006	O	|	|	|	|	0.00
269.333	0.00	0.00	0.006	O	|	|	|	|	0.00
269.417	0.00	0.00	0.006	O	|	|	|	|	0.00
269.500	0.00	0.00	0.006	O	|	|	|	|	0.00
269.583	0.00	0.00	0.006	O	|	|	|	|	0.00
269.667	0.00	0.00	0.006	O	|	|	|	|	0.00
269.750	0.00	0.00	0.006	O	|	|	|	|	0.00
269.833	0.00	0.00	0.006	O	|	|	|	|	0.00
269.917	0.00	0.00	0.006	O	|	|	|	|	0.00
270.000	0.00	0.00	0.006	O	|	|	|	|	0.00
270.083	0.00	0.00	0.006	O	|	|	|	|	0.00
270.167	0.00	0.00	0.006	O	|	|	|	|	0.00
270.250	0.00	0.00	0.006	O	|	|	|	|	0.00
270.333	0.00	0.00	0.006	O	|	|	|	|	0.00
270.417	0.00	0.00	0.006	O	|	|	|	|	0.00
270.500	0.00	0.00	0.006	O	|	|	|	|	0.00
270.583	0.00	0.00	0.006	O	|	|	|	|	0.00
270.667	0.00	0.00	0.006	O	|	|	|	|	0.00
270.750	0.00	0.00	0.006	O	|	|	|	|	0.00
270.833	0.00	0.00	0.006	O	|	|	|	|	0.00
270.917	0.00	0.00	0.006	O	|	|	|	|	0.00
271.000	0.00	0.00	0.006	O	|	|	|	|	0.00
271.083	0.00	0.00	0.006	O	|	|	|	|	0.00
271.167	0.00	0.00	0.006	O	|	|	|	|	0.00
271.250	0.00	0.00	0.006	O	|	|	|	|	0.00
271.333	0.00	0.00	0.006	O	|	|	|	|	0.00
271.417	0.00	0.00	0.006	O	|	|	|	|	0.00
271.500	0.00	0.00	0.006	O	|	|	|	|	0.00
271.583	0.00	0.00	0.006	O	|	|	|	|	0.00
271.667	0.00	0.00	0.006	O	|	|	|	|	0.00
271.750	0.00	0.00	0.005	O	|	|	|	|	0.00
271.833	0.00	0.00	0.005	O	|	|	|	|	0.00
271.917	0.00	0.00	0.005	O	|	|	|	|	0.00
272.000	0.00	0.00	0.005	O	|	|	|	|	0.00
272.083	0.00	0.00	0.005	O	|	|	|	|	0.00
272.167	0.00	0.00	0.005	O	|	|	|	|	0.00
272.250	0.00	0.00	0.005	O	|	|	|	|	0.00
272.333	0.00	0.00	0.005	O	|	|	|	|	0.00

272.417	0.00	0.00	0.005	O	|	|	|	|	0.00
272.500	0.00	0.00	0.005	O	|	|	|	|	0.00
272.583	0.00	0.00	0.005	O	|	|	|	|	0.00
272.667	0.00	0.00	0.005	O	|	|	|	|	0.00
272.750	0.00	0.00	0.005	O	|	|	|	|	0.00
272.833	0.00	0.00	0.005	O	|	|	|	|	0.00
272.917	0.00	0.00	0.005	O	|	|	|	|	0.00
273.000	0.00	0.00	0.005	O	|	|	|	|	0.00
273.083	0.00	0.00	0.005	O	|	|	|	|	0.00
273.167	0.00	0.00	0.005	O	|	|	|	|	0.00
273.250	0.00	0.00	0.005	O	|	|	|	|	0.00
273.333	0.00	0.00	0.005	O	|	|	|	|	0.00
273.417	0.00	0.00	0.005	O	|	|	|	|	0.00
273.500	0.00	0.00	0.005	O	|	|	|	|	0.00
273.583	0.00	0.00	0.005	O	|	|	|	|	0.00
273.667	0.00	0.00	0.005	O	|	|	|	|	0.00
273.750	0.00	0.00	0.005	O	|	|	|	|	0.00
273.833	0.00	0.00	0.005	O	|	|	|	|	0.00
273.917	0.00	0.00	0.005	O	|	|	|	|	0.00
274.000	0.00	0.00	0.005	O	|	|	|	|	0.00
274.083	0.00	0.00	0.005	O	|	|	|	|	0.00
274.167	0.00	0.00	0.005	O	|	|	|	|	0.00
274.250	0.00	0.00	0.005	O	|	|	|	|	0.00
274.333	0.00	0.00	0.005	O	|	|	|	|	0.00
274.417	0.00	0.00	0.005	O	|	|	|	|	0.00
274.500	0.00	0.00	0.005	O	|	|	|	|	0.00
274.583	0.00	0.00	0.005	O	|	|	|	|	0.00
274.667	0.00	0.00	0.005	O	|	|	|	|	0.00
274.750	0.00	0.00	0.005	O	|	|	|	|	0.00
274.833	0.00	0.00	0.005	O	|	|	|	|	0.00
274.917	0.00	0.00	0.005	O	|	|	|	|	0.00
275.000	0.00	0.00	0.005	O	|	|	|	|	0.00
275.083	0.00	0.00	0.005	O	|	|	|	|	0.00
275.167	0.00	0.00	0.005	O	|	|	|	|	0.00
275.250	0.00	0.00	0.005	O	|	|	|	|	0.00
275.333	0.00	0.00	0.005	O	|	|	|	|	0.00
275.417	0.00	0.00	0.005	O	|	|	|	|	0.00
275.500	0.00	0.00	0.005	O	|	|	|	|	0.00
275.583	0.00	0.00	0.005	O	|	|	|	|	0.00
275.667	0.00	0.00	0.005	O	|	|	|	|	0.00
275.750	0.00	0.00	0.005	O	|	|	|	|	0.00
275.833	0.00	0.00	0.005	O	|	|	|	|	0.00
275.917	0.00	0.00	0.005	O	|	|	|	|	0.00
276.000	0.00	0.00	0.005	O	|	|	|	|	0.00
276.083	0.00	0.00	0.005	O	|	|	|	|	0.00
276.167	0.00	0.00	0.005	O	|	|	|	|	0.00
276.250	0.00	0.00	0.005	O	|	|	|	|	0.00
276.333	0.00	0.00	0.005	O	|	|	|	|	0.00
276.417	0.00	0.00	0.005	O	|	|	|	|	0.00
276.500	0.00	0.00	0.005	O	|	|	|	|	0.00
276.583	0.00	0.00	0.005	O	|	|	|	|	0.00
276.667	0.00	0.00	0.005	O	|	|	|	|	0.00
276.750	0.00	0.00	0.005	O	|	|	|	|	0.00
276.833	0.00	0.00	0.005	O	|	|	|	|	0.00
276.917	0.00	0.00	0.005	O	|	|	|	|	0.00
277.000	0.00	0.00	0.005	O	|	|	|	|	0.00
277.083	0.00	0.00	0.005	O	|	|	|	|	0.00
277.167	0.00	0.00	0.005	O	|	|	|	|	0.00
277.250	0.00	0.00	0.005	O	|	|	|	|	0.00
277.333	0.00	0.00	0.005	O	|	|	|	|	0.00
277.417	0.00	0.00	0.005	O	|	|	|	|	0.00
277.500	0.00	0.00	0.005	O	|	|	|	|	0.00
277.583	0.00	0.00	0.005	O	|	|	|	|	0.00
277.667	0.00	0.00	0.005	O	|	|	|	|	0.00
277.750	0.00	0.00	0.005	O	|	|	|	|	0.00
277.833	0.00	0.00	0.005	O	|	|	|	|	0.00
277.917	0.00	0.00	0.005	O	|	|	|	|	0.00
278.000	0.00	0.00	0.005	O	|	|	|	|	0.00
278.083	0.00	0.00	0.005	O	|	|	|	|	0.00
278.167	0.00	0.00	0.005	O	|	|	|	|	0.00
278.250	0.00	0.00	0.005	O	|	|	|	|	0.00

278.333	0.00	0.00	0.005	O	|	|	|	|	0.00
278.417	0.00	0.00	0.005	O	|	|	|	|	0.00
278.500	0.00	0.00	0.005	O	|	|	|	|	0.00
278.583	0.00	0.00	0.005	O	|	|	|	|	0.00
278.667	0.00	0.00	0.005	O	|	|	|	|	0.00
278.750	0.00	0.00	0.005	O	|	|	|	|	0.00
278.833	0.00	0.00	0.005	O	|	|	|	|	0.00
278.917	0.00	0.00	0.005	O	|	|	|	|	0.00
279.000	0.00	0.00	0.005	O	|	|	|	|	0.00
279.083	0.00	0.00	0.005	O	|	|	|	|	0.00
279.167	0.00	0.00	0.005	O	|	|	|	|	0.00
279.250	0.00	0.00	0.005	O	|	|	|	|	0.00
279.333	0.00	0.00	0.005	O	|	|	|	|	0.00
279.417	0.00	0.00	0.005	O	|	|	|	|	0.00
279.500	0.00	0.00	0.005	O	|	|	|	|	0.00
279.583	0.00	0.00	0.005	O	|	|	|	|	0.00
279.667	0.00	0.00	0.005	O	|	|	|	|	0.00
279.750	0.00	0.00	0.005	O	|	|	|	|	0.00
279.833	0.00	0.00	0.005	O	|	|	|	|	0.00
279.917	0.00	0.00	0.005	O	|	|	|	|	0.00
280.000	0.00	0.00	0.005	O	|	|	|	|	0.00
280.083	0.00	0.00	0.005	O	|	|	|	|	0.00
280.167	0.00	0.00	0.005	O	|	|	|	|	0.00
280.250	0.00	0.00	0.005	O	|	|	|	|	0.00
280.333	0.00	0.00	0.005	O	|	|	|	|	0.00
280.417	0.00	0.00	0.005	O	|	|	|	|	0.00
280.500	0.00	0.00	0.004	O	|	|	|	|	0.00
280.583	0.00	0.00	0.004	O	|	|	|	|	0.00
280.667	0.00	0.00	0.004	O	|	|	|	|	0.00
280.750	0.00	0.00	0.004	O	|	|	|	|	0.00
280.833	0.00	0.00	0.004	O	|	|	|	|	0.00
280.917	0.00	0.00	0.004	O	|	|	|	|	0.00
281.000	0.00	0.00	0.004	O	|	|	|	|	0.00
281.083	0.00	0.00	0.004	O	|	|	|	|	0.00
281.167	0.00	0.00	0.004	O	|	|	|	|	0.00
281.250	0.00	0.00	0.004	O	|	|	|	|	0.00
281.333	0.00	0.00	0.004	O	|	|	|	|	0.00
281.417	0.00	0.00	0.004	O	|	|	|	|	0.00
281.500	0.00	0.00	0.004	O	|	|	|	|	0.00
281.583	0.00	0.00	0.004	O	|	|	|	|	0.00
281.667	0.00	0.00	0.004	O	|	|	|	|	0.00
281.750	0.00	0.00	0.004	O	|	|	|	|	0.00
281.833	0.00	0.00	0.004	O	|	|	|	|	0.00
281.917	0.00	0.00	0.004	O	|	|	|	|	0.00
282.000	0.00	0.00	0.004	O	|	|	|	|	0.00
282.083	0.00	0.00	0.004	O	|	|	|	|	0.00
282.167	0.00	0.00	0.004	O	|	|	|	|	0.00
282.250	0.00	0.00	0.004	O	|	|	|	|	0.00
282.333	0.00	0.00	0.004	O	|	|	|	|	0.00
282.417	0.00	0.00	0.004	O	|	|	|	|	0.00
282.500	0.00	0.00	0.004	O	|	|	|	|	0.00
282.583	0.00	0.00	0.004	O	|	|	|	|	0.00
282.667	0.00	0.00	0.004	O	|	|	|	|	0.00
282.750	0.00	0.00	0.004	O	|	|	|	|	0.00
282.833	0.00	0.00	0.004	O	|	|	|	|	0.00
282.917	0.00	0.00	0.004	O	|	|	|	|	0.00
283.000	0.00	0.00	0.004	O	|	|	|	|	0.00
283.083	0.00	0.00	0.004	O	|	|	|	|	0.00
283.167	0.00	0.00	0.004	O	|	|	|	|	0.00
283.250	0.00	0.00	0.004	O	|	|	|	|	0.00
283.333	0.00	0.00	0.004	O	|	|	|	|	0.00
283.417	0.00	0.00	0.004	O	|	|	|	|	0.00
283.500	0.00	0.00	0.004	O	|	|	|	|	0.00
283.583	0.00	0.00	0.004	O	|	|	|	|	0.00
283.667	0.00	0.00	0.004	O	|	|	|	|	0.00
283.750	0.00	0.00	0.004	O	|	|	|	|	0.00
283.833	0.00	0.00	0.004	O	|	|	|	|	0.00
283.917	0.00	0.00	0.004	O	|	|	|	|	0.00
284.000	0.00	0.00	0.004	O	|	|	|	|	0.00
284.083	0.00	0.00	0.004	O	|	|	|	|	0.00
284.167	0.00	0.00	0.004	O	|	|	|	|	0.00

284.250	0.00	0.00	0.004	O	|	|	|	|	0.00
284.333	0.00	0.00	0.004	O	|	|	|	|	0.00
284.417	0.00	0.00	0.004	O	|	|	|	|	0.00
284.500	0.00	0.00	0.004	O	|	|	|	|	0.00
284.583	0.00	0.00	0.004	O	|	|	|	|	0.00
284.667	0.00	0.00	0.004	O	|	|	|	|	0.00
284.750	0.00	0.00	0.004	O	|	|	|	|	0.00
284.833	0.00	0.00	0.004	O	|	|	|	|	0.00
284.917	0.00	0.00	0.004	O	|	|	|	|	0.00
285.000	0.00	0.00	0.004	O	|	|	|	|	0.00
285.083	0.00	0.00	0.004	O	|	|	|	|	0.00
285.167	0.00	0.00	0.004	O	|	|	|	|	0.00
285.250	0.00	0.00	0.004	O	|	|	|	|	0.00
285.333	0.00	0.00	0.004	O	|	|	|	|	0.00
285.417	0.00	0.00	0.004	O	|	|	|	|	0.00
285.500	0.00	0.00	0.004	O	|	|	|	|	0.00
285.583	0.00	0.00	0.004	O	|	|	|	|	0.00
285.667	0.00	0.00	0.004	O	|	|	|	|	0.00
285.750	0.00	0.00	0.004	O	|	|	|	|	0.00
285.833	0.00	0.00	0.004	O	|	|	|	|	0.00
285.917	0.00	0.00	0.004	O	|	|	|	|	0.00
286.000	0.00	0.00	0.004	O	|	|	|	|	0.00
286.083	0.00	0.00	0.004	O	|	|	|	|	0.00
286.167	0.00	0.00	0.004	O	|	|	|	|	0.00
286.250	0.00	0.00	0.004	O	|	|	|	|	0.00
286.333	0.00	0.00	0.004	O	|	|	|	|	0.00
286.417	0.00	0.00	0.004	O	|	|	|	|	0.00
286.500	0.00	0.00	0.004	O	|	|	|	|	0.00
286.583	0.00	0.00	0.004	O	|	|	|	|	0.00
286.667	0.00	0.00	0.004	O	|	|	|	|	0.00
286.750	0.00	0.00	0.004	O	|	|	|	|	0.00
286.833	0.00	0.00	0.004	O	|	|	|	|	0.00
286.917	0.00	0.00	0.004	O	|	|	|	|	0.00
287.000	0.00	0.00	0.004	O	|	|	|	|	0.00
287.083	0.00	0.00	0.004	O	|	|	|	|	0.00
287.167	0.00	0.00	0.004	O	|	|	|	|	0.00
287.250	0.00	0.00	0.004	O	|	|	|	|	0.00
287.333	0.00	0.00	0.004	O	|	|	|	|	0.00
287.417	0.00	0.00	0.004	O	|	|	|	|	0.00
287.500	0.00	0.00	0.004	O	|	|	|	|	0.00
287.583	0.00	0.00	0.004	O	|	|	|	|	0.00
287.667	0.00	0.00	0.004	O	|	|	|	|	0.00
287.750	0.00	0.00	0.004	O	|	|	|	|	0.00
287.833	0.00	0.00	0.004	O	|	|	|	|	0.00
287.917	0.00	0.00	0.004	O	|	|	|	|	0.00
288.000	0.00	0.00	0.004	O	|	|	|	|	0.00
288.083	0.00	0.00	0.004	O	|	|	|	|	0.00
288.167	0.00	0.00	0.004	O	|	|	|	|	0.00
288.250	0.00	0.00	0.004	O	|	|	|	|	0.00
288.333	0.00	0.00	0.004	O	|	|	|	|	0.00
288.417	0.00	0.00	0.004	O	|	|	|	|	0.00
288.500	0.00	0.00	0.004	O	|	|	|	|	0.00
288.583	0.00	0.00	0.004	O	|	|	|	|	0.00
288.667	0.00	0.00	0.004	O	|	|	|	|	0.00
288.750	0.00	0.00	0.004	O	|	|	|	|	0.00
288.833	0.00	0.00	0.004	O	|	|	|	|	0.00
288.917	0.00	0.00	0.004	O	|	|	|	|	0.00
289.000	0.00	0.00	0.004	O	|	|	|	|	0.00
289.083	0.00	0.00	0.004	O	|	|	|	|	0.00
289.167	0.00	0.00	0.004	O	|	|	|	|	0.00
289.250	0.00	0.00	0.004	O	|	|	|	|	0.00
289.333	0.00	0.00	0.004	O	|	|	|	|	0.00
289.417	0.00	0.00	0.004	O	|	|	|	|	0.00
289.500	0.00	0.00	0.004	O	|	|	|	|	0.00
289.583	0.00	0.00	0.004	O	|	|	|	|	0.00
289.667	0.00	0.00	0.004	O	|	|	|	|	0.00
289.750	0.00	0.00	0.004	O	|	|	|	|	0.00
289.833	0.00	0.00	0.004	O	|	|	|	|	0.00
289.917	0.00	0.00	0.004	O	|	|	|	|	0.00
290.000	0.00	0.00	0.004	O	|	|	|	|	0.00
290.083	0.00	0.00	0.004	O	|	|	|	|	0.00

```
290.167    0.00    0.00      0.004  O       |       |       |       |     0.00
290.250    0.00    0.00      0.004  O       |       |       |       |     0.00
290.333    0.00    0.00      0.004  O       |       |       |       |     0.00

        Remaining water in basin =    0.00 (Ac.Ft)


        ****************************HYDROGRAPH DATA****************************
                      Number of intervals =  3484
                      Time interval =    5.0 (Min.)
                      Maximum/Peak flow rate =        0.303 (CFS)
                      Total volume =       1.891 (Ac.Ft)
               Status of hydrographs being held in storage
                           Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
               Peak (CFS)      0.000     0.000     0.000     0.000     0.000
               Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
        ************************************************************************

        ------------------------------------------------------------------
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APPENDIX H: OFFSITE INTERIM CHANNEL ANALYSIS

APPENDIX H.1: COMBINED OFFSITE HYDROGRAPH AND ONSITE BASIN ROUTING CALCULATIONS – 100-YEAR, 1-HOUR STORM DURATION

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014
Study date: 11/01/21

HEMET 30 ONSITE BASIN ROUTING AND OFFSITE UNIT HYDROGRAPH
COMBINED ROUTING
100-YEAR, 1-HOUR ROUTING ANALYSIS
FILENAME: ONOFFTOTAL1100

Program License Serial Number 6279

********** HYDROGRAPH INFORMATION **********

From study/file name: ARA1POST1100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 15
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 61.227 (CFS)
Total volume = 1.894 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****
_____

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 15
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.500	0.616	0.172	0.615	0.617
1.500	1.965	0.312	1.964	1.966
2.500	3.433	15.406	3.380	3.486
3.500	5.020	37.934	4.889	5.151

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 15.3 30.61 45.92 61.23	Depth (Ft.)
0.083	4.33	0.00	0.015	O I	0.01
0.167	8.29	0.02	0.058	O I	0.05

0.250	10.26	0.03	0.122	O	I	|	|	|	0.10
0.333	11.54	0.05	0.197	O	I	|	|	|	0.16
0.417	13.00	0.08	0.281	O	I	|	|	|	0.23
0.500	15.29	0.11	0.378	O	I	|	|	|	0.31
0.583	17.89	0.14	0.491	O	I	|	|	|	0.40
0.667	21.30	0.17	0.625	O	I	|	|	|	0.51
0.750	29.13	0.19	0.797	O	I	|	|	|	0.63
0.833	61.23	0.22	1.107	O	I	|	|	|	0.86
0.917	50.42	0.26	1.490	O	I	|	|	|	1.15
1.000	21.37	0.29	1.735	O	I	|	|	|	1.33
1.083	9.15	0.30	1.838	O	I	|	|	|	1.41
1.167	1.47	0.30	1.873	O	I	|	|	|	1.43
1.250	0.36	0.30	1.877	O	I	|	|	|	1.43
1.333	0.00	0.30	1.876	O	I	|	|	|	1.43
1.417	0.00	0.30	1.874	O	I	|	|	|	1.43
1.500	0.00	0.30	1.872	O	I	|	|	|	1.43
1.583	0.00	0.30	1.870	O	I	|	|	|	1.43
1.667	0.00	0.30	1.868	O	I	|	|	|	1.43
1.750	0.00	0.30	1.866	O	I	|	|	|	1.43
1.833	0.00	0.30	1.864	O	I	|	|	|	1.42
1.917	0.00	0.30	1.861	O	I	|	|	|	1.42
2.000	0.00	0.30	1.859	O	I	|	|	|	1.42
2.083	0.00	0.30	1.857	O	I	|	|	|	1.42
2.167	0.00	0.30	1.855	O	I	|	|	|	1.42
2.250	0.00	0.30	1.853	O	I	|	|	|	1.42
2.333	0.00	0.30	1.851	O	I	|	|	|	1.42
2.417	0.00	0.30	1.849	O	I	|	|	|	1.41
2.500	0.00	0.30	1.847	O	I	|	|	|	1.41
2.583	0.00	0.30	1.845	O	I	|	|	|	1.41
2.667	0.00	0.30	1.843	O	I	|	|	|	1.41
2.750	0.00	0.30	1.841	O	I	|	|	|	1.41
2.833	0.00	0.30	1.839	O	I	|	|	|	1.41
2.917	0.00	0.30	1.837	O	I	|	|	|	1.40
3.000	0.00	0.30	1.835	O	I	|	|	|	1.40
3.083	0.00	0.30	1.833	O	I	|	|	|	1.40
3.167	0.00	0.30	1.831	O	I	|	|	|	1.40
3.250	0.00	0.30	1.828	O	I	|	|	|	1.40
3.333	0.00	0.30	1.826	O	I	|	|	|	1.40
3.417	0.00	0.30	1.824	O	I	|	|	|	1.40
3.500	0.00	0.30	1.822	O	I	|	|	|	1.39
3.583	0.00	0.30	1.820	O	I	|	|	|	1.39
3.667	0.00	0.30	1.818	O	I	|	|	|	1.39
3.750	0.00	0.30	1.816	O	I	|	|	|	1.39
3.833	0.00	0.30	1.814	O	I	|	|	|	1.39
3.917	0.00	0.30	1.812	O	I	|	|	|	1.39
4.000	0.00	0.30	1.810	O	I	|	|	|	1.39
4.083	0.00	0.30	1.808	O	I	|	|	|	1.38
4.167	0.00	0.30	1.806	O	I	|	|	|	1.38
4.250	0.00	0.30	1.804	O	I	|	|	|	1.38
4.333	0.00	0.30	1.802	O	I	|	|	|	1.38
4.417	0.00	0.29	1.800	O	I	|	|	|	1.38
4.500	0.00	0.29	1.798	O	I	|	|	|	1.38
4.583	0.00	0.29	1.796	O	I	|	|	|	1.37
4.667	0.00	0.29	1.794	O	I	|	|	|	1.37
4.750	0.00	0.29	1.792	O	I	|	|	|	1.37
4.833	0.00	0.29	1.790	O	I	|	|	|	1.37
4.917	0.00	0.29	1.788	O	I	|	|	|	1.37
5.000	0.00	0.29	1.786	O	I	|	|	|	1.37
5.083	0.00	0.29	1.784	O	I	|	|	|	1.37
5.167	0.00	0.29	1.782	O	I	|	|	|	1.36
5.250	0.00	0.29	1.780	O	I	|	|	|	1.36
5.333	0.00	0.29	1.778	O	I	|	|	|	1.36
5.417	0.00	0.29	1.776	O	I	|	|	|	1.36
5.500	0.00	0.29	1.774	O	I	|	|	|	1.36
5.583	0.00	0.29	1.772	O	I	|	|	|	1.36
5.667	0.00	0.29	1.770	O	I	|	|	|	1.36
5.750	0.00	0.29	1.768	O	I	|	|	|	1.35
5.833	0.00	0.29	1.766	O	I	|	|	|	1.35
5.917	0.00	0.29	1.764	O	I	|	|	|	1.35
6.000	0.00	0.29	1.762	O	I	|	|	|	1.35
6.083	0.00	0.29	1.760	O	I	|	|	|	1.35

6.167	0.00	0.29	1.758	O					1.35
6.250	0.00	0.29	1.756	O					1.34
6.333	0.00	0.29	1.754	O					1.34
6.417	0.00	0.29	1.752	O					1.34
6.500	0.00	0.29	1.750	O					1.34
6.583	0.00	0.29	1.748	O					1.34
6.667	0.00	0.29	1.746	O					1.34
6.750	0.00	0.29	1.744	O					1.34
6.833	0.00	0.29	1.742	O					1.33
6.917	0.00	0.29	1.740	O					1.33
7.000	0.00	0.29	1.738	O					1.33
7.083	0.00	0.29	1.736	O					1.33
7.167	0.00	0.29	1.734	O					1.33
7.250	0.00	0.29	1.732	O					1.33
7.333	0.00	0.29	1.730	O					1.33
7.417	0.00	0.29	1.728	O					1.32
7.500	0.00	0.29	1.726	O					1.32
7.583	0.00	0.29	1.724	O					1.32
7.667	0.00	0.29	1.722	O					1.32
7.750	0.00	0.29	1.720	O					1.32
7.833	0.00	0.29	1.718	O					1.32
7.917	0.00	0.29	1.716	O					1.32
8.000	0.00	0.29	1.714	O					1.31
8.083	0.00	0.29	1.712	O					1.31
8.167	0.00	0.29	1.710	O					1.31
8.250	0.00	0.29	1.708	O					1.31
8.333	0.00	0.29	1.706	O					1.31
8.417	0.00	0.28	1.704	O					1.31
8.500	0.00	0.28	1.702	O					1.31
8.583	0.00	0.28	1.700	O					1.30
8.667	0.00	0.28	1.698	O					1.30
8.750	0.00	0.28	1.696	O					1.30
8.833	0.00	0.28	1.694	O					1.30
8.917	0.00	0.28	1.692	O					1.30
9.000	0.00	0.28	1.690	O					1.30
9.083	0.00	0.28	1.688	O					1.29
9.167	0.00	0.28	1.686	O					1.29
9.250	0.00	0.28	1.685	O					1.29
9.333	0.00	0.28	1.683	O					1.29
9.417	0.00	0.28	1.681	O					1.29
9.500	0.00	0.28	1.679	O					1.29
9.583	0.00	0.28	1.677	O					1.29
9.667	0.00	0.28	1.675	O					1.28
9.750	0.00	0.28	1.673	O					1.28
9.833	0.00	0.28	1.671	O					1.28
9.917	0.00	0.28	1.669	O					1.28
10.000	0.00	0.28	1.667	O					1.28
10.083	0.00	0.28	1.665	O					1.28
10.167	0.00	0.28	1.663	O					1.28
10.250	0.00	0.28	1.661	O					1.27
10.333	0.00	0.28	1.659	O					1.27
10.417	0.00	0.28	1.657	O					1.27
10.500	0.00	0.28	1.655	O					1.27
10.583	0.00	0.28	1.654	O					1.27
10.667	0.00	0.28	1.652	O					1.27
10.750	0.00	0.28	1.650	O					1.27
10.833	0.00	0.28	1.648	O					1.26
10.917	0.00	0.28	1.646	O					1.26
11.000	0.00	0.28	1.644	O					1.26
11.083	0.00	0.28	1.642	O					1.26
11.167	0.00	0.28	1.640	O					1.26
11.250	0.00	0.28	1.638	O					1.26
11.333	0.00	0.28	1.636	O					1.26
11.417	0.00	0.28	1.634	O					1.25
11.500	0.00	0.28	1.632	O					1.25
11.583	0.00	0.28	1.631	O					1.25
11.667	0.00	0.28	1.629	O					1.25
11.750	0.00	0.28	1.627	O					1.25
11.833	0.00	0.28	1.625	O					1.25
11.917	0.00	0.28	1.623	O					1.25
12.000	0.00	0.28	1.621	O					1.24

12.083	0.00	0.28	1.619	O				1.24
12.167	0.00	0.28	1.617	O				1.24
12.250	0.00	0.28	1.615	O				1.24
12.333	0.00	0.28	1.613	O				1.24
12.417	0.00	0.28	1.611	O				1.24
12.500	0.00	0.28	1.610	O				1.24
12.583	0.00	0.27	1.608	O				1.24
12.667	0.00	0.27	1.606	O				1.23
12.750	0.00	0.27	1.604	O				1.23
12.833	0.00	0.27	1.602	O				1.23
12.917	0.00	0.27	1.600	O				1.23
13.000	0.00	0.27	1.598	O				1.23
13.083	0.00	0.27	1.596	O				1.23
13.167	0.00	0.27	1.594	O				1.23
13.250	0.00	0.27	1.593	O				1.22
13.333	0.00	0.27	1.591	O				1.22
13.417	0.00	0.27	1.589	O				1.22
13.500	0.00	0.27	1.587	O				1.22
13.583	0.00	0.27	1.585	O				1.22
13.667	0.00	0.27	1.583	O				1.22
13.750	0.00	0.27	1.581	O				1.22
13.833	0.00	0.27	1.579	O				1.21
13.917	0.00	0.27	1.578	O				1.21
14.000	0.00	0.27	1.576	O				1.21
14.083	0.00	0.27	1.574	O				1.21
14.167	0.00	0.27	1.572	O				1.21
14.250	0.00	0.27	1.570	O				1.21
14.333	0.00	0.27	1.568	O				1.21
14.417	0.00	0.27	1.566	O				1.20
14.500	0.00	0.27	1.565	O				1.20
14.583	0.00	0.27	1.563	O				1.20
14.667	0.00	0.27	1.561	O				1.20
14.750	0.00	0.27	1.559	O				1.20
14.833	0.00	0.27	1.557	O				1.20
14.917	0.00	0.27	1.555	O				1.20
15.000	0.00	0.27	1.553	O				1.19
15.083	0.00	0.27	1.552	O				1.19
15.167	0.00	0.27	1.550	O				1.19
15.250	0.00	0.27	1.548	O				1.19
15.333	0.00	0.27	1.546	O				1.19
15.417	0.00	0.27	1.544	O				1.19
15.500	0.00	0.27	1.542	O				1.19
15.583	0.00	0.27	1.540	O				1.19
15.667	0.00	0.27	1.539	O				1.18
15.750	0.00	0.27	1.537	O				1.18
15.833	0.00	0.27	1.535	O				1.18
15.917	0.00	0.27	1.533	O				1.18
16.000	0.00	0.27	1.531	O				1.18
16.083	0.00	0.27	1.529	O				1.18
16.167	0.00	0.27	1.528	O				1.18
16.250	0.00	0.27	1.526	O				1.17
16.333	0.00	0.27	1.524	O				1.17
16.417	0.00	0.27	1.522	O				1.17
16.500	0.00	0.27	1.520	O				1.17
16.583	0.00	0.27	1.518	O				1.17
16.667	0.00	0.27	1.517	O				1.17
16.750	0.00	0.27	1.515	O				1.17
16.833	0.00	0.27	1.513	O				1.16
16.917	0.00	0.26	1.511	O				1.16
17.000	0.00	0.26	1.509	O				1.16
17.083	0.00	0.26	1.507	O				1.16
17.167	0.00	0.26	1.506	O				1.16
17.250	0.00	0.26	1.504	O				1.16
17.333	0.00	0.26	1.502	O				1.16
17.417	0.00	0.26	1.500	O				1.16
17.500	0.00	0.26	1.498	O				1.15
17.583	0.00	0.26	1.496	O				1.15
17.667	0.00	0.26	1.495	O				1.15
17.750	0.00	0.26	1.493	O				1.15
17.833	0.00	0.26	1.491	O				1.15
17.917	0.00	0.26	1.489	O				1.15

18.000	0.00	0.26	1.487	O					1.15
18.083	0.00	0.26	1.486	O					1.14
18.167	0.00	0.26	1.484	O					1.14
18.250	0.00	0.26	1.482	O					1.14
18.333	0.00	0.26	1.480	O					1.14
18.417	0.00	0.26	1.478	O					1.14
18.500	0.00	0.26	1.477	O					1.14
18.583	0.00	0.26	1.475	O					1.14
18.667	0.00	0.26	1.473	O					1.14
18.750	0.00	0.26	1.471	O					1.13
18.833	0.00	0.26	1.469	O					1.13
18.917	0.00	0.26	1.468	O					1.13
19.000	0.00	0.26	1.466	O					1.13
19.083	0.00	0.26	1.464	O					1.13
19.167	0.00	0.26	1.462	O					1.13
19.250	0.00	0.26	1.460	O					1.13
19.333	0.00	0.26	1.459	O					1.12
19.417	0.00	0.26	1.457	O					1.12
19.500	0.00	0.26	1.455	O					1.12
19.583	0.00	0.26	1.453	O					1.12
19.667	0.00	0.26	1.452	O					1.12
19.750	0.00	0.26	1.450	O					1.12
19.833	0.00	0.26	1.448	O					1.12
19.917	0.00	0.26	1.446	O					1.12
20.000	0.00	0.26	1.444	O					1.11
20.083	0.00	0.26	1.443	O					1.11
20.167	0.00	0.26	1.441	O					1.11
20.250	0.00	0.26	1.439	O					1.11
20.333	0.00	0.26	1.437	O					1.11
20.417	0.00	0.26	1.436	O					1.11
20.500	0.00	0.26	1.434	O					1.11
20.583	0.00	0.26	1.432	O					1.10
20.667	0.00	0.26	1.430	O					1.10
20.750	0.00	0.26	1.428	O					1.10
20.833	0.00	0.26	1.427	O					1.10
20.917	0.00	0.26	1.425	O					1.10
21.000	0.00	0.26	1.423	O					1.10
21.083	0.00	0.26	1.421	O					1.10
21.167	0.00	0.26	1.420	O					1.10
21.250	0.00	0.26	1.418	O					1.09
21.333	0.00	0.26	1.416	O					1.09
21.417	0.00	0.25	1.414	O					1.09
21.500	0.00	0.25	1.413	O					1.09
21.583	0.00	0.25	1.411	O					1.09
21.667	0.00	0.25	1.409	O					1.09
21.750	0.00	0.25	1.407	O					1.09
21.833	0.00	0.25	1.406	O					1.09
21.917	0.00	0.25	1.404	O					1.08
22.000	0.00	0.25	1.402	O					1.08
22.083	0.00	0.25	1.400	O					1.08
22.167	0.00	0.25	1.399	O					1.08
22.250	0.00	0.25	1.397	O					1.08
22.333	0.00	0.25	1.395	O					1.08
22.417	0.00	0.25	1.393	O					1.08
22.500	0.00	0.25	1.392	O					1.08
22.583	0.00	0.25	1.390	O					1.07
22.667	0.00	0.25	1.388	O					1.07
22.750	0.00	0.25	1.386	O					1.07
22.833	0.00	0.25	1.385	O					1.07
22.917	0.00	0.25	1.383	O					1.07
23.000	0.00	0.25	1.381	O					1.07
23.083	0.00	0.25	1.380	O					1.07
23.167	0.00	0.25	1.378	O					1.06
23.250	0.00	0.25	1.376	O					1.06
23.333	0.00	0.25	1.374	O					1.06
23.417	0.00	0.25	1.373	O					1.06
23.500	0.00	0.25	1.371	O					1.06
23.583	0.00	0.25	1.369	O					1.06
23.667	0.00	0.25	1.367	O					1.06
23.750	0.00	0.25	1.366	O					1.06
23.833	0.00	0.25	1.364	O					1.05

23.917	0.00	0.25	1.362	O					1.05
24.000	0.00	0.25	1.361	O					1.05
24.083	0.00	0.25	1.359	O					1.05
24.167	0.00	0.25	1.357	O					1.05
24.250	0.00	0.25	1.355	O					1.05
24.333	0.00	0.25	1.354	O					1.05
24.417	0.00	0.25	1.352	O					1.05
24.500	0.00	0.25	1.350	O					1.04
24.583	0.00	0.25	1.349	O					1.04
24.667	0.00	0.25	1.347	O					1.04
24.750	0.00	0.25	1.345	O					1.04
24.833	0.00	0.25	1.343	O					1.04
24.917	0.00	0.25	1.342	O					1.04
25.000	0.00	0.25	1.340	O					1.04
25.083	0.00	0.25	1.338	O					1.04
25.167	0.00	0.25	1.337	O					1.03
25.250	0.00	0.25	1.335	O					1.03
25.333	0.00	0.25	1.333	O					1.03
25.417	0.00	0.25	1.332	O					1.03
25.500	0.00	0.25	1.330	O					1.03
25.583	0.00	0.25	1.328	O					1.03
25.667	0.00	0.25	1.327	O					1.03
25.750	0.00	0.25	1.325	O					1.03
25.833	0.00	0.25	1.323	O					1.02
25.917	0.00	0.25	1.321	O					1.02
26.000	0.00	0.25	1.320	O					1.02
26.083	0.00	0.24	1.318	O					1.02
26.167	0.00	0.24	1.316	O					1.02
26.250	0.00	0.24	1.315	O					1.02
26.333	0.00	0.24	1.313	O					1.02
26.417	0.00	0.24	1.311	O					1.02
26.500	0.00	0.24	1.310	O					1.01
26.583	0.00	0.24	1.308	O					1.01
26.667	0.00	0.24	1.306	O					1.01
26.750	0.00	0.24	1.305	O					1.01
26.833	0.00	0.24	1.303	O					1.01
26.917	0.00	0.24	1.301	O					1.01
27.000	0.00	0.24	1.300	O					1.01
27.083	0.00	0.24	1.298	O					1.01
27.167	0.00	0.24	1.296	O					1.00
27.250	0.00	0.24	1.295	O					1.00
27.333	0.00	0.24	1.293	O					1.00
27.417	0.00	0.24	1.291	O					1.00
27.500	0.00	0.24	1.290	O					1.00
27.583	0.00	0.24	1.288	O					1.00
27.667	0.00	0.24	1.286	O					1.00
27.750	0.00	0.24	1.285	O					1.00
27.833	0.00	0.24	1.283	O					0.99
27.917	0.00	0.24	1.281	O					0.99
28.000	0.00	0.24	1.280	O					0.99
28.083	0.00	0.24	1.278	O					0.99
28.167	0.00	0.24	1.276	O					0.99
28.250	0.00	0.24	1.275	O					0.99
28.333	0.00	0.24	1.273	O					0.99
28.417	0.00	0.24	1.271	O					0.99
28.500	0.00	0.24	1.270	O					0.98
28.583	0.00	0.24	1.268	O					0.98
28.667	0.00	0.24	1.266	O					0.98
28.750	0.00	0.24	1.265	O					0.98
28.833	0.00	0.24	1.263	O					0.98
28.917	0.00	0.24	1.261	O					0.98
29.000	0.00	0.24	1.260	O					0.98
29.083	0.00	0.24	1.258	O					0.98
29.167	0.00	0.24	1.256	O					0.97
29.250	0.00	0.24	1.255	O					0.97
29.333	0.00	0.24	1.253	O					0.97
29.417	0.00	0.24	1.252	O					0.97
29.500	0.00	0.24	1.250	O					0.97
29.583	0.00	0.24	1.248	O					0.97
29.667	0.00	0.24	1.247	O					0.97
29.750	0.00	0.24	1.245	O					0.97

29.833	0.00	0.24	1.243	O				0.97
29.917	0.00	0.24	1.242	O				0.96
30.000	0.00	0.24	1.240	O				0.96
30.083	0.00	0.24	1.238	O				0.96
30.167	0.00	0.24	1.237	O				0.96
30.250	0.00	0.24	1.235	O				0.96
30.333	0.00	0.24	1.234	O				0.96
30.417	0.00	0.24	1.232	O				0.96
30.500	0.00	0.24	1.230	O				0.96
30.583	0.00	0.24	1.229	O				0.95
30.667	0.00	0.24	1.227	O				0.95
30.750	0.00	0.24	1.225	O				0.95
30.833	0.00	0.24	1.224	O				0.95
30.917	0.00	0.23	1.222	O				0.95
31.000	0.00	0.23	1.221	O				0.95
31.083	0.00	0.23	1.219	O				0.95
31.167	0.00	0.23	1.217	O				0.95
31.250	0.00	0.23	1.216	O				0.94
31.333	0.00	0.23	1.214	O				0.94
31.417	0.00	0.23	1.213	O				0.94
31.500	0.00	0.23	1.211	O				0.94
31.583	0.00	0.23	1.209	O				0.94
31.667	0.00	0.23	1.208	O				0.94
31.750	0.00	0.23	1.206	O				0.94
31.833	0.00	0.23	1.205	O				0.94
31.917	0.00	0.23	1.203	O				0.94
32.000	0.00	0.23	1.201	O				0.93
32.083	0.00	0.23	1.200	O				0.93
32.167	0.00	0.23	1.198	O				0.93
32.250	0.00	0.23	1.197	O				0.93
32.333	0.00	0.23	1.195	O				0.93
32.417	0.00	0.23	1.193	O				0.93
32.500	0.00	0.23	1.192	O				0.93
32.583	0.00	0.23	1.190	O				0.93
32.667	0.00	0.23	1.189	O				0.92
32.750	0.00	0.23	1.187	O				0.92
32.833	0.00	0.23	1.185	O				0.92
32.917	0.00	0.23	1.184	O				0.92
33.000	0.00	0.23	1.182	O				0.92
33.083	0.00	0.23	1.181	O				0.92
33.167	0.00	0.23	1.179	O				0.92
33.250	0.00	0.23	1.177	O				0.92
33.333	0.00	0.23	1.176	O				0.91
33.417	0.00	0.23	1.174	O				0.91
33.500	0.00	0.23	1.173	O				0.91
33.583	0.00	0.23	1.171	O				0.91
33.667	0.00	0.23	1.169	O				0.91
33.750	0.00	0.23	1.168	O				0.91
33.833	0.00	0.23	1.166	O				0.91
33.917	0.00	0.23	1.165	O				0.91
34.000	0.00	0.23	1.163	O				0.91
34.083	0.00	0.23	1.162	O				0.90
34.167	0.00	0.23	1.160	O				0.90
34.250	0.00	0.23	1.158	O				0.90
34.333	0.00	0.23	1.157	O				0.90
34.417	0.00	0.23	1.155	O				0.90
34.500	0.00	0.23	1.154	O				0.90
34.583	0.00	0.23	1.152	O				0.90
34.667	0.00	0.23	1.151	O				0.90
34.750	0.00	0.23	1.149	O				0.90
34.833	0.00	0.23	1.147	O				0.89
34.917	0.00	0.23	1.146	O				0.89
35.000	0.00	0.23	1.144	O				0.89
35.083	0.00	0.23	1.143	O				0.89
35.167	0.00	0.23	1.141	O				0.89
35.250	0.00	0.23	1.140	O				0.89
35.333	0.00	0.23	1.138	O				0.89
35.417	0.00	0.23	1.137	O				0.89
35.500	0.00	0.23	1.135	O				0.88
35.583	0.00	0.23	1.133	O				0.88
35.667	0.00	0.23	1.132	O				0.88

35.750	0.00	0.23	1.130	O				0.88
35.833	0.00	0.23	1.129	O				0.88
35.917	0.00	0.23	1.127	O				0.88
36.000	0.00	0.22	1.126	O				0.88
36.083	0.00	0.22	1.124	O				0.88
36.167	0.00	0.22	1.123	O				0.88
36.250	0.00	0.22	1.121	O				0.87
36.333	0.00	0.22	1.119	O				0.87
36.417	0.00	0.22	1.118	O				0.87
36.500	0.00	0.22	1.116	O				0.87
36.583	0.00	0.22	1.115	O				0.87
36.667	0.00	0.22	1.113	O				0.87
36.750	0.00	0.22	1.112	O				0.87
36.833	0.00	0.22	1.110	O				0.87
36.917	0.00	0.22	1.109	O				0.87
37.000	0.00	0.22	1.107	O				0.86
37.083	0.00	0.22	1.106	O				0.86
37.167	0.00	0.22	1.104	O				0.86
37.250	0.00	0.22	1.103	O				0.86
37.333	0.00	0.22	1.101	O				0.86
37.417	0.00	0.22	1.100	O				0.86
37.500	0.00	0.22	1.098	O				0.86
37.583	0.00	0.22	1.096	O				0.86
37.667	0.00	0.22	1.095	O				0.86
37.750	0.00	0.22	1.093	O				0.85
37.833	0.00	0.22	1.092	O				0.85
37.917	0.00	0.22	1.090	O				0.85
38.000	0.00	0.22	1.089	O				0.85
38.083	0.00	0.22	1.087	O				0.85
38.167	0.00	0.22	1.086	O				0.85
38.250	0.00	0.22	1.084	O				0.85
38.333	0.00	0.22	1.083	O				0.85
38.417	0.00	0.22	1.081	O				0.84
38.500	0.00	0.22	1.080	O				0.84
38.583	0.00	0.22	1.078	O				0.84
38.667	0.00	0.22	1.077	O				0.84
38.750	0.00	0.22	1.075	O				0.84
38.833	0.00	0.22	1.074	O				0.84
38.917	0.00	0.22	1.072	O				0.84
39.000	0.00	0.22	1.071	O				0.84
39.083	0.00	0.22	1.069	O				0.84
39.167	0.00	0.22	1.068	O				0.83
39.250	0.00	0.22	1.066	O				0.83
39.333	0.00	0.22	1.065	O				0.83
39.417	0.00	0.22	1.063	O				0.83
39.500	0.00	0.22	1.062	O				0.83
39.583	0.00	0.22	1.060	O				0.83
39.667	0.00	0.22	1.059	O				0.83
39.750	0.00	0.22	1.057	O				0.83
39.833	0.00	0.22	1.056	O				0.83
39.917	0.00	0.22	1.054	O				0.82
40.000	0.00	0.22	1.053	O				0.82
40.083	0.00	0.22	1.051	O				0.82
40.167	0.00	0.22	1.050	O				0.82
40.250	0.00	0.22	1.048	O				0.82
40.333	0.00	0.22	1.047	O				0.82
40.417	0.00	0.22	1.045	O				0.82
40.500	0.00	0.22	1.044	O				0.82
40.583	0.00	0.22	1.042	O				0.82
40.667	0.00	0.22	1.041	O				0.81
40.750	0.00	0.22	1.039	O				0.81
40.833	0.00	0.22	1.038	O				0.81
40.917	0.00	0.22	1.036	O				0.81
41.000	0.00	0.22	1.035	O				0.81
41.083	0.00	0.22	1.033	O				0.81
41.167	0.00	0.22	1.032	O				0.81
41.250	0.00	0.21	1.030	O				0.81
41.333	0.00	0.21	1.029	O				0.81
41.417	0.00	0.21	1.027	O				0.80
41.500	0.00	0.21	1.026	O				0.80
41.583	0.00	0.21	1.024	O				0.80

41.667	0.00	0.21	1.023	O	|	|	|	|	0.80
41.750	0.00	0.21	1.021	O	|	|	|	|	0.80
41.833	0.00	0.21	1.020	O	|	|	|	|	0.80
41.917	0.00	0.21	1.018	O	|	|	|	|	0.80
42.000	0.00	0.21	1.017	O	|	|	|	|	0.80
42.083	0.00	0.21	1.016	O	|	|	|	|	0.80
42.167	0.00	0.21	1.014	O	|	|	|	|	0.80
42.250	0.00	0.21	1.013	O	|	|	|	|	0.79
42.333	0.00	0.21	1.011	O	|	|	|	|	0.79
42.417	0.00	0.21	1.010	O	|	|	|	|	0.79
42.500	0.00	0.21	1.008	O	|	|	|	|	0.79
42.583	0.00	0.21	1.007	O	|	|	|	|	0.79
42.667	0.00	0.21	1.005	O	|	|	|	|	0.79
42.750	0.00	0.21	1.004	O	|	|	|	|	0.79
42.833	0.00	0.21	1.002	O	|	|	|	|	0.79
42.917	0.00	0.21	1.001	O	|	|	|	|	0.79
43.000	0.00	0.21	0.999	O	|	|	|	|	0.78
43.083	0.00	0.21	0.998	O	|	|	|	|	0.78
43.167	0.00	0.21	0.996	O	|	|	|	|	0.78
43.250	0.00	0.21	0.995	O	|	|	|	|	0.78
43.333	0.00	0.21	0.994	O	|	|	|	|	0.78
43.417	0.00	0.21	0.992	O	|	|	|	|	0.78
43.500	0.00	0.21	0.991	O	|	|	|	|	0.78
43.583	0.00	0.21	0.989	O	|	|	|	|	0.78
43.667	0.00	0.21	0.988	O	|	|	|	|	0.78
43.750	0.00	0.21	0.986	O	|	|	|	|	0.77
43.833	0.00	0.21	0.985	O	|	|	|	|	0.77
43.917	0.00	0.21	0.983	O	|	|	|	|	0.77
44.000	0.00	0.21	0.982	O	|	|	|	|	0.77
44.083	0.00	0.21	0.981	O	|	|	|	|	0.77
44.167	0.00	0.21	0.979	O	|	|	|	|	0.77
44.250	0.00	0.21	0.978	O	|	|	|	|	0.77
44.333	0.00	0.21	0.976	O	|	|	|	|	0.77
44.417	0.00	0.21	0.975	O	|	|	|	|	0.77
44.500	0.00	0.21	0.973	O	|	|	|	|	0.76
44.583	0.00	0.21	0.972	O	|	|	|	|	0.76
44.667	0.00	0.21	0.970	O	|	|	|	|	0.76
44.750	0.00	0.21	0.969	O	|	|	|	|	0.76
44.833	0.00	0.21	0.968	O	|	|	|	|	0.76
44.917	0.00	0.21	0.966	O	|	|	|	|	0.76
45.000	0.00	0.21	0.965	O	|	|	|	|	0.76
45.083	0.00	0.21	0.963	O	|	|	|	|	0.76
45.167	0.00	0.21	0.962	O	|	|	|	|	0.76
45.250	0.00	0.21	0.960	O	|	|	|	|	0.76
45.333	0.00	0.21	0.959	O	|	|	|	|	0.75
45.417	0.00	0.21	0.958	O	|	|	|	|	0.75
45.500	0.00	0.21	0.956	O	|	|	|	|	0.75
45.583	0.00	0.21	0.955	O	|	|	|	|	0.75
45.667	0.00	0.21	0.953	O	|	|	|	|	0.75
45.750	0.00	0.21	0.952	O	|	|	|	|	0.75
45.833	0.00	0.21	0.950	O	|	|	|	|	0.75
45.917	0.00	0.21	0.949	O	|	|	|	|	0.75
46.000	0.00	0.21	0.948	O	|	|	|	|	0.75
46.083	0.00	0.21	0.946	O	|	|	|	|	0.74
46.167	0.00	0.21	0.945	O	|	|	|	|	0.74
46.250	0.00	0.21	0.943	O	|	|	|	|	0.74
46.333	0.00	0.21	0.942	O	|	|	|	|	0.74
46.417	0.00	0.21	0.940	O	|	|	|	|	0.74
46.500	0.00	0.21	0.939	O	|	|	|	|	0.74
46.583	0.00	0.21	0.938	O	|	|	|	|	0.74
46.667	0.00	0.21	0.936	O	|	|	|	|	0.74
46.750	0.00	0.21	0.935	O	|	|	|	|	0.74
46.833	0.00	0.20	0.933	O	|	|	|	|	0.74
46.917	0.00	0.20	0.932	O	|	|	|	|	0.73
47.000	0.00	0.20	0.931	O	|	|	|	|	0.73
47.083	0.00	0.20	0.929	O	|	|	|	|	0.73
47.167	0.00	0.20	0.928	O	|	|	|	|	0.73
47.250	0.00	0.20	0.926	O	|	|	|	|	0.73
47.333	0.00	0.20	0.925	O	|	|	|	|	0.73
47.417	0.00	0.20	0.924	O	|	|	|	|	0.73
47.500	0.00	0.20	0.922	O	|	|	|	|	0.73

47.583	0.00	0.20	0.921	O	|	|	|	|	0.73
47.667	0.00	0.20	0.919	O	|	|	|	|	0.72
47.750	0.00	0.20	0.918	O	|	|	|	|	0.72
47.833	0.00	0.20	0.917	O	|	|	|	|	0.72
47.917	0.00	0.20	0.915	O	|	|	|	|	0.72
48.000	0.00	0.20	0.914	O	|	|	|	|	0.72
48.083	0.00	0.20	0.912	O	|	|	|	|	0.72
48.167	0.00	0.20	0.911	O	|	|	|	|	0.72
48.250	0.00	0.20	0.910	O	|	|	|	|	0.72
48.333	0.00	0.20	0.908	O	|	|	|	|	0.72
48.417	0.00	0.20	0.907	O	|	|	|	|	0.72
48.500	0.00	0.20	0.905	O	|	|	|	|	0.71
48.583	0.00	0.20	0.904	O	|	|	|	|	0.71
48.667	0.00	0.20	0.903	O	|	|	|	|	0.71
48.750	0.00	0.20	0.901	O	|	|	|	|	0.71
48.833	0.00	0.20	0.900	O	|	|	|	|	0.71
48.917	0.00	0.20	0.898	O	|	|	|	|	0.71
49.000	0.00	0.20	0.897	O	|	|	|	|	0.71
49.083	0.00	0.20	0.896	O	|	|	|	|	0.71
49.167	0.00	0.20	0.894	O	|	|	|	|	0.71
49.250	0.00	0.20	0.893	O	|	|	|	|	0.71
49.333	0.00	0.20	0.892	O	|	|	|	|	0.70
49.417	0.00	0.20	0.890	O	|	|	|	|	0.70
49.500	0.00	0.20	0.889	O	|	|	|	|	0.70
49.583	0.00	0.20	0.887	O	|	|	|	|	0.70
49.667	0.00	0.20	0.886	O	|	|	|	|	0.70
49.750	0.00	0.20	0.885	O	|	|	|	|	0.70
49.833	0.00	0.20	0.883	O	|	|	|	|	0.70
49.917	0.00	0.20	0.882	O	|	|	|	|	0.70
50.000	0.00	0.20	0.880	O	|	|	|	|	0.70
50.083	0.00	0.20	0.879	O	|	|	|	|	0.70
50.167	0.00	0.20	0.878	O	|	|	|	|	0.69
50.250	0.00	0.20	0.876	O	|	|	|	|	0.69
50.333	0.00	0.20	0.875	O	|	|	|	|	0.69
50.417	0.00	0.20	0.874	O	|	|	|	|	0.69
50.500	0.00	0.20	0.872	O	|	|	|	|	0.69
50.583	0.00	0.20	0.871	O	|	|	|	|	0.69
50.667	0.00	0.20	0.870	O	|	|	|	|	0.69
50.750	0.00	0.20	0.868	O	|	|	|	|	0.69
50.833	0.00	0.20	0.867	O	|	|	|	|	0.69
50.917	0.00	0.20	0.865	O	|	|	|	|	0.68
51.000	0.00	0.20	0.864	O	|	|	|	|	0.68
51.083	0.00	0.20	0.863	O	|	|	|	|	0.68
51.167	0.00	0.20	0.861	O	|	|	|	|	0.68
51.250	0.00	0.20	0.860	O	|	|	|	|	0.68
51.333	0.00	0.20	0.859	O	|	|	|	|	0.68
51.417	0.00	0.20	0.857	O	|	|	|	|	0.68
51.500	0.00	0.20	0.856	O	|	|	|	|	0.68
51.583	0.00	0.20	0.855	O	|	|	|	|	0.68
51.667	0.00	0.20	0.853	O	|	|	|	|	0.68
51.750	0.00	0.20	0.852	O	|	|	|	|	0.67
51.833	0.00	0.20	0.851	O	|	|	|	|	0.67
51.917	0.00	0.20	0.849	O	|	|	|	|	0.67
52.000	0.00	0.20	0.848	O	|	|	|	|	0.67
52.083	0.00	0.20	0.846	O	|	|	|	|	0.67
52.167	0.00	0.20	0.845	O	|	|	|	|	0.67
52.250	0.00	0.20	0.844	O	|	|	|	|	0.67
52.333	0.00	0.20	0.842	O	|	|	|	|	0.67
52.417	0.00	0.20	0.841	O	|	|	|	|	0.67
52.500	0.00	0.20	0.840	O	|	|	|	|	0.67
52.583	0.00	0.20	0.838	O	|	|	|	|	0.66
52.667	0.00	0.19	0.837	O	|	|	|	|	0.66
52.750	0.00	0.19	0.836	O	|	|	|	|	0.66
52.833	0.00	0.19	0.834	O	|	|	|	|	0.66
52.917	0.00	0.19	0.833	O	|	|	|	|	0.66
53.000	0.00	0.19	0.832	O	|	|	|	|	0.66
53.083	0.00	0.19	0.830	O	|	|	|	|	0.66
53.167	0.00	0.19	0.829	O	|	|	|	|	0.66
53.250	0.00	0.19	0.828	O	|	|	|	|	0.66
53.333	0.00	0.19	0.826	O	|	|	|	|	0.66
53.417	0.00	0.19	0.825	O	|	|	|	|	0.65

53.500	0.00	0.19	0.824	O	|	|	|	|	0.65
53.583	0.00	0.19	0.822	O	|	|	|	|	0.65
53.667	0.00	0.19	0.821	O	|	|	|	|	0.65
53.750	0.00	0.19	0.820	O	|	|	|	|	0.65
53.833	0.00	0.19	0.818	O	|	|	|	|	0.65
53.917	0.00	0.19	0.817	O	|	|	|	|	0.65
54.000	0.00	0.19	0.816	O	|	|	|	|	0.65
54.083	0.00	0.19	0.814	O	|	|	|	|	0.65
54.167	0.00	0.19	0.813	O	|	|	|	|	0.65
54.250	0.00	0.19	0.812	O	|	|	|	|	0.65
54.333	0.00	0.19	0.810	O	|	|	|	|	0.64
54.417	0.00	0.19	0.809	O	|	|	|	|	0.64
54.500	0.00	0.19	0.808	O	|	|	|	|	0.64
54.583	0.00	0.19	0.806	O	|	|	|	|	0.64
54.667	0.00	0.19	0.805	O	|	|	|	|	0.64
54.750	0.00	0.19	0.804	O	|	|	|	|	0.64
54.833	0.00	0.19	0.802	O	|	|	|	|	0.64
54.917	0.00	0.19	0.801	O	|	|	|	|	0.64
55.000	0.00	0.19	0.800	O	|	|	|	|	0.64
55.083	0.00	0.19	0.798	O	|	|	|	|	0.64
55.167	0.00	0.19	0.797	O	|	|	|	|	0.63
55.250	0.00	0.19	0.796	O	|	|	|	|	0.63
55.333	0.00	0.19	0.795	O	|	|	|	|	0.63
55.417	0.00	0.19	0.793	O	|	|	|	|	0.63
55.500	0.00	0.19	0.792	O	|	|	|	|	0.63
55.583	0.00	0.19	0.791	O	|	|	|	|	0.63
55.667	0.00	0.19	0.789	O	|	|	|	|	0.63
55.750	0.00	0.19	0.788	O	|	|	|	|	0.63
55.833	0.00	0.19	0.787	O	|	|	|	|	0.63
55.917	0.00	0.19	0.785	O	|	|	|	|	0.63
56.000	0.00	0.19	0.784	O	|	|	|	|	0.62
56.083	0.00	0.19	0.783	O	|	|	|	|	0.62
56.167	0.00	0.19	0.781	O	|	|	|	|	0.62
56.250	0.00	0.19	0.780	O	|	|	|	|	0.62
56.333	0.00	0.19	0.779	O	|	|	|	|	0.62
56.417	0.00	0.19	0.778	O	|	|	|	|	0.62
56.500	0.00	0.19	0.776	O	|	|	|	|	0.62
56.583	0.00	0.19	0.775	O	|	|	|	|	0.62
56.667	0.00	0.19	0.774	O	|	|	|	|	0.62
56.750	0.00	0.19	0.772	O	|	|	|	|	0.62
56.833	0.00	0.19	0.771	O	|	|	|	|	0.61
56.917	0.00	0.19	0.770	O	|	|	|	|	0.61
57.000	0.00	0.19	0.769	O	|	|	|	|	0.61
57.083	0.00	0.19	0.767	O	|	|	|	|	0.61
57.167	0.00	0.19	0.766	O	|	|	|	|	0.61
57.250	0.00	0.19	0.765	O	|	|	|	|	0.61
57.333	0.00	0.19	0.763	O	|	|	|	|	0.61
57.417	0.00	0.19	0.762	O	|	|	|	|	0.61
57.500	0.00	0.19	0.761	O	|	|	|	|	0.61
57.583	0.00	0.19	0.759	O	|	|	|	|	0.61
57.667	0.00	0.19	0.758	O	|	|	|	|	0.61
57.750	0.00	0.19	0.757	O	|	|	|	|	0.60
57.833	0.00	0.19	0.756	O	|	|	|	|	0.60
57.917	0.00	0.19	0.754	O	|	|	|	|	0.60
58.000	0.00	0.19	0.753	O	|	|	|	|	0.60
58.083	0.00	0.19	0.752	O	|	|	|	|	0.60
58.167	0.00	0.19	0.750	O	|	|	|	|	0.60
58.250	0.00	0.19	0.749	O	|	|	|	|	0.60
58.333	0.00	0.19	0.748	O	|	|	|	|	0.60
58.417	0.00	0.19	0.747	O	|	|	|	|	0.60
58.500	0.00	0.19	0.745	O	|	|	|	|	0.60
58.583	0.00	0.19	0.744	O	|	|	|	|	0.59
58.667	0.00	0.19	0.743	O	|	|	|	|	0.59
58.750	0.00	0.19	0.742	O	|	|	|	|	0.59
58.833	0.00	0.18	0.740	O	|	|	|	|	0.59
58.917	0.00	0.18	0.739	O	|	|	|	|	0.59
59.000	0.00	0.18	0.738	O	|	|	|	|	0.59
59.083	0.00	0.18	0.736	O	|	|	|	|	0.59
59.167	0.00	0.18	0.735	O	|	|	|	|	0.59
59.250	0.00	0.18	0.734	O	|	|	|	|	0.59
59.333	0.00	0.18	0.733	O	|	|	|	|	0.59

59.417	0.00	0.18	0.731	O	|	|	|	|	0.59
59.500	0.00	0.18	0.730	O	|	|	|	|	0.58
59.583	0.00	0.18	0.729	O	|	|	|	|	0.58
59.667	0.00	0.18	0.728	O	|	|	|	|	0.58
59.750	0.00	0.18	0.726	O	|	|	|	|	0.58
59.833	0.00	0.18	0.725	O	|	|	|	|	0.58
59.917	0.00	0.18	0.724	O	|	|	|	|	0.58
60.000	0.00	0.18	0.723	O	|	|	|	|	0.58
60.083	0.00	0.18	0.721	O	|	|	|	|	0.58
60.167	0.00	0.18	0.720	O	|	|	|	|	0.58
60.250	0.00	0.18	0.719	O	|	|	|	|	0.58
60.333	0.00	0.18	0.717	O	|	|	|	|	0.58
60.417	0.00	0.18	0.716	O	|	|	|	|	0.57
60.500	0.00	0.18	0.715	O	|	|	|	|	0.57
60.583	0.00	0.18	0.714	O	|	|	|	|	0.57
60.667	0.00	0.18	0.712	O	|	|	|	|	0.57
60.750	0.00	0.18	0.711	O	|	|	|	|	0.57
60.833	0.00	0.18	0.710	O	|	|	|	|	0.57
60.917	0.00	0.18	0.709	O	|	|	|	|	0.57
61.000	0.00	0.18	0.707	O	|	|	|	|	0.57
61.083	0.00	0.18	0.706	O	|	|	|	|	0.57
61.167	0.00	0.18	0.705	O	|	|	|	|	0.57
61.250	0.00	0.18	0.704	O	|	|	|	|	0.57
61.333	0.00	0.18	0.702	O	|	|	|	|	0.56
61.417	0.00	0.18	0.701	O	|	|	|	|	0.56
61.500	0.00	0.18	0.700	O	|	|	|	|	0.56
61.583	0.00	0.18	0.699	O	|	|	|	|	0.56
61.667	0.00	0.18	0.697	O	|	|	|	|	0.56
61.750	0.00	0.18	0.696	O	|	|	|	|	0.56
61.833	0.00	0.18	0.695	O	|	|	|	|	0.56
61.917	0.00	0.18	0.694	O	|	|	|	|	0.56
62.000	0.00	0.18	0.693	O	|	|	|	|	0.56
62.083	0.00	0.18	0.691	O	|	|	|	|	0.56
62.167	0.00	0.18	0.690	O	|	|	|	|	0.55
62.250	0.00	0.18	0.689	O	|	|	|	|	0.55
62.333	0.00	0.18	0.688	O	|	|	|	|	0.55
62.417	0.00	0.18	0.686	O	|	|	|	|	0.55
62.500	0.00	0.18	0.685	O	|	|	|	|	0.55
62.583	0.00	0.18	0.684	O	|	|	|	|	0.55
62.667	0.00	0.18	0.683	O	|	|	|	|	0.55
62.750	0.00	0.18	0.681	O	|	|	|	|	0.55
62.833	0.00	0.18	0.680	O	|	|	|	|	0.55
62.917	0.00	0.18	0.679	O	|	|	|	|	0.55
63.000	0.00	0.18	0.678	O	|	|	|	|	0.55
63.083	0.00	0.18	0.676	O	|	|	|	|	0.54
63.167	0.00	0.18	0.675	O	|	|	|	|	0.54
63.250	0.00	0.18	0.674	O	|	|	|	|	0.54
63.333	0.00	0.18	0.673	O	|	|	|	|	0.54
63.417	0.00	0.18	0.672	O	|	|	|	|	0.54
63.500	0.00	0.18	0.670	O	|	|	|	|	0.54
63.583	0.00	0.18	0.669	O	|	|	|	|	0.54
63.667	0.00	0.18	0.668	O	|	|	|	|	0.54
63.750	0.00	0.18	0.667	O	|	|	|	|	0.54
63.833	0.00	0.18	0.665	O	|	|	|	|	0.54
63.917	0.00	0.18	0.664	O	|	|	|	|	0.54
64.000	0.00	0.18	0.663	O	|	|	|	|	0.53
64.083	0.00	0.18	0.662	O	|	|	|	|	0.53
64.167	0.00	0.18	0.661	O	|	|	|	|	0.53
64.250	0.00	0.18	0.659	O	|	|	|	|	0.53
64.333	0.00	0.18	0.658	O	|	|	|	|	0.53
64.417	0.00	0.18	0.657	O	|	|	|	|	0.53
64.500	0.00	0.18	0.656	O	|	|	|	|	0.53
64.583	0.00	0.18	0.655	O	|	|	|	|	0.53
64.667	0.00	0.18	0.653	O	|	|	|	|	0.53
64.750	0.00	0.18	0.652	O	|	|	|	|	0.53
64.833	0.00	0.18	0.651	O	|	|	|	|	0.53
64.917	0.00	0.18	0.650	O	|	|	|	|	0.52
65.000	0.00	0.18	0.648	O	|	|	|	|	0.52
65.083	0.00	0.18	0.647	O	|	|	|	|	0.52
65.167	0.00	0.18	0.646	O	|	|	|	|	0.52
65.250	0.00	0.17	0.645	O	|	|	|	|	0.52

65.333	0.00	0.17	0.644	O				0.52
65.417	0.00	0.17	0.642	O				0.52
65.500	0.00	0.17	0.641	O				0.52
65.583	0.00	0.17	0.640	O				0.52
65.667	0.00	0.17	0.639	O				0.52
65.750	0.00	0.17	0.638	O				0.52
65.833	0.00	0.17	0.636	O				0.52
65.917	0.00	0.17	0.635	O				0.51
66.000	0.00	0.17	0.634	O				0.51
66.083	0.00	0.17	0.633	O				0.51
66.167	0.00	0.17	0.632	O				0.51
66.250	0.00	0.17	0.630	O				0.51
66.333	0.00	0.17	0.629	O				0.51
66.417	0.00	0.17	0.628	O				0.51
66.500	0.00	0.17	0.627	O				0.51
66.583	0.00	0.17	0.626	O				0.51
66.667	0.00	0.17	0.624	O				0.51
66.750	0.00	0.17	0.623	O				0.51
66.833	0.00	0.17	0.622	O				0.50
66.917	0.00	0.17	0.621	O				0.50
67.000	0.00	0.17	0.620	O				0.50
67.083	0.00	0.17	0.619	O				0.50
67.167	0.00	0.17	0.617	O				0.50
67.250	0.00	0.17	0.616	O				0.50
67.333	0.00	0.17	0.615	O				0.50
67.417	0.00	0.17	0.614	O				0.50
67.500	0.00	0.17	0.613	O				0.50
67.583	0.00	0.17	0.611	O				0.50
67.667	0.00	0.17	0.610	O				0.50
67.750	0.00	0.17	0.609	O				0.49
67.833	0.00	0.17	0.608	O				0.49
67.917	0.00	0.17	0.607	O				0.49
68.000	0.00	0.17	0.606	O				0.49
68.083	0.00	0.17	0.604	O				0.49
68.167	0.00	0.17	0.603	O				0.49
68.250	0.00	0.17	0.602	O				0.49
68.333	0.00	0.17	0.601	O				0.49
68.417	0.00	0.17	0.600	O				0.49
68.500	0.00	0.17	0.599	O				0.49
68.583	0.00	0.17	0.598	O				0.48
68.667	0.00	0.17	0.596	O				0.48
68.750	0.00	0.17	0.595	O				0.48
68.833	0.00	0.17	0.594	O				0.48
68.917	0.00	0.17	0.593	O				0.48
69.000	0.00	0.17	0.592	O				0.48
69.083	0.00	0.16	0.591	O				0.48
69.167	0.00	0.16	0.590	O				0.48
69.250	0.00	0.16	0.588	O				0.48
69.333	0.00	0.16	0.587	O				0.48
69.417	0.00	0.16	0.586	O				0.48
69.500	0.00	0.16	0.585	O				0.47
69.583	0.00	0.16	0.584	O				0.47
69.667	0.00	0.16	0.583	O				0.47
69.750	0.00	0.16	0.582	O				0.47
69.833	0.00	0.16	0.581	O				0.47
69.917	0.00	0.16	0.579	O				0.47
70.000	0.00	0.16	0.578	O				0.47
70.083	0.00	0.16	0.577	O				0.47
70.167	0.00	0.16	0.576	O				0.47
70.250	0.00	0.16	0.575	O				0.47
70.333	0.00	0.16	0.574	O				0.47
70.417	0.00	0.16	0.573	O				0.46
70.500	0.00	0.16	0.572	O				0.46
70.583	0.00	0.16	0.571	O				0.46
70.667	0.00	0.16	0.569	O				0.46
70.750	0.00	0.16	0.568	O				0.46
70.833	0.00	0.16	0.567	O				0.46
70.917	0.00	0.16	0.566	O				0.46
71.000	0.00	0.16	0.565	O				0.46
71.083	0.00	0.16	0.564	O				0.46
71.167	0.00	0.16	0.563	O				0.46

71.250	0.00	0.16	0.562	O	|	|	|	|	0.46
71.333	0.00	0.16	0.561	O	|	|	|	|	0.46
71.417	0.00	0.16	0.560	O	|	|	|	|	0.45
71.500	0.00	0.16	0.559	O	|	|	|	|	0.45
71.583	0.00	0.16	0.558	O	|	|	|	|	0.45
71.667	0.00	0.16	0.556	O	|	|	|	|	0.45
71.750	0.00	0.16	0.555	O	|	|	|	|	0.45
71.833	0.00	0.15	0.554	O	|	|	|	|	0.45
71.917	0.00	0.15	0.553	O	|	|	|	|	0.45
72.000	0.00	0.15	0.552	O	|	|	|	|	0.45
72.083	0.00	0.15	0.551	O	|	|	|	|	0.45
72.167	0.00	0.15	0.550	O	|	|	|	|	0.45
72.250	0.00	0.15	0.549	O	|	|	|	|	0.45
72.333	0.00	0.15	0.548	O	|	|	|	|	0.44
72.417	0.00	0.15	0.547	O	|	|	|	|	0.44
72.500	0.00	0.15	0.546	O	|	|	|	|	0.44
72.583	0.00	0.15	0.545	O	|	|	|	|	0.44
72.667	0.00	0.15	0.544	O	|	|	|	|	0.44
72.750	0.00	0.15	0.543	O	|	|	|	|	0.44
72.833	0.00	0.15	0.542	O	|	|	|	|	0.44
72.917	0.00	0.15	0.541	O	|	|	|	|	0.44
73.000	0.00	0.15	0.540	O	|	|	|	|	0.44
73.083	0.00	0.15	0.539	O	|	|	|	|	0.44
73.167	0.00	0.15	0.538	O	|	|	|	|	0.44
73.250	0.00	0.15	0.537	O	|	|	|	|	0.44
73.333	0.00	0.15	0.535	O	|	|	|	|	0.43
73.417	0.00	0.15	0.534	O	|	|	|	|	0.43
73.500	0.00	0.15	0.533	O	|	|	|	|	0.43
73.583	0.00	0.15	0.532	O	|	|	|	|	0.43
73.667	0.00	0.15	0.531	O	|	|	|	|	0.43
73.750	0.00	0.15	0.530	O	|	|	|	|	0.43
73.833	0.00	0.15	0.529	O	|	|	|	|	0.43
73.917	0.00	0.15	0.528	O	|	|	|	|	0.43
74.000	0.00	0.15	0.527	O	|	|	|	|	0.43
74.083	0.00	0.15	0.526	O	|	|	|	|	0.43
74.167	0.00	0.15	0.525	O	|	|	|	|	0.43
74.250	0.00	0.15	0.524	O	|	|	|	|	0.43
74.333	0.00	0.15	0.523	O	|	|	|	|	0.42
74.417	0.00	0.15	0.522	O	|	|	|	|	0.42
74.500	0.00	0.15	0.521	O	|	|	|	|	0.42
74.583	0.00	0.15	0.520	O	|	|	|	|	0.42
74.667	0.00	0.14	0.519	O	|	|	|	|	0.42
74.750	0.00	0.14	0.518	O	|	|	|	|	0.42
74.833	0.00	0.14	0.517	O	|	|	|	|	0.42
74.917	0.00	0.14	0.516	O	|	|	|	|	0.42
75.000	0.00	0.14	0.515	O	|	|	|	|	0.42
75.083	0.00	0.14	0.514	O	|	|	|	|	0.42
75.167	0.00	0.14	0.513	O	|	|	|	|	0.42
75.250	0.00	0.14	0.512	O	|	|	|	|	0.42
75.333	0.00	0.14	0.511	O	|	|	|	|	0.42
75.417	0.00	0.14	0.510	O	|	|	|	|	0.41
75.500	0.00	0.14	0.509	O	|	|	|	|	0.41
75.583	0.00	0.14	0.508	O	|	|	|	|	0.41
75.667	0.00	0.14	0.507	O	|	|	|	|	0.41
75.750	0.00	0.14	0.506	O	|	|	|	|	0.41
75.833	0.00	0.14	0.505	O	|	|	|	|	0.41
75.917	0.00	0.14	0.504	O	|	|	|	|	0.41
76.000	0.00	0.14	0.504	O	|	|	|	|	0.41
76.083	0.00	0.14	0.503	O	|	|	|	|	0.41
76.167	0.00	0.14	0.502	O	|	|	|	|	0.41
76.250	0.00	0.14	0.501	O	|	|	|	|	0.41
76.333	0.00	0.14	0.500	O	|	|	|	|	0.41
76.417	0.00	0.14	0.499	O	|	|	|	|	0.40
76.500	0.00	0.14	0.498	O	|	|	|	|	0.40
76.583	0.00	0.14	0.497	O	|	|	|	|	0.40
76.667	0.00	0.14	0.496	O	|	|	|	|	0.40
76.750	0.00	0.14	0.495	O	|	|	|	|	0.40
76.833	0.00	0.14	0.494	O	|	|	|	|	0.40
76.917	0.00	0.14	0.493	O	|	|	|	|	0.40
77.000	0.00	0.14	0.492	O	|	|	|	|	0.40
77.083	0.00	0.14	0.491	O	|	|	|	|	0.40

77.167	0.00	0.14	0.490	O	|	|	|	|	0.40
77.250	0.00	0.14	0.489	O	|	|	|	|	0.40
77.333	0.00	0.14	0.488	O	|	|	|	|	0.40
77.417	0.00	0.14	0.487	O	|	|	|	|	0.40
77.500	0.00	0.14	0.486	O	|	|	|	|	0.39
77.583	0.00	0.14	0.485	O	|	|	|	|	0.39
77.667	0.00	0.14	0.485	O	|	|	|	|	0.39
77.750	0.00	0.14	0.484	O	|	|	|	|	0.39
77.833	0.00	0.13	0.483	O	|	|	|	|	0.39
77.917	0.00	0.13	0.482	O	|	|	|	|	0.39
78.000	0.00	0.13	0.481	O	|	|	|	|	0.39
78.083	0.00	0.13	0.480	O	|	|	|	|	0.39
78.167	0.00	0.13	0.479	O	|	|	|	|	0.39
78.250	0.00	0.13	0.478	O	|	|	|	|	0.39
78.333	0.00	0.13	0.477	O	|	|	|	|	0.39
78.417	0.00	0.13	0.476	O	|	|	|	|	0.39
78.500	0.00	0.13	0.475	O	|	|	|	|	0.39
78.583	0.00	0.13	0.474	O	|	|	|	|	0.39
78.667	0.00	0.13	0.473	O	|	|	|	|	0.38
78.750	0.00	0.13	0.473	O	|	|	|	|	0.38
78.833	0.00	0.13	0.472	O	|	|	|	|	0.38
78.917	0.00	0.13	0.471	O	|	|	|	|	0.38
79.000	0.00	0.13	0.470	O	|	|	|	|	0.38
79.083	0.00	0.13	0.469	O	|	|	|	|	0.38
79.167	0.00	0.13	0.468	O	|	|	|	|	0.38
79.250	0.00	0.13	0.467	O	|	|	|	|	0.38
79.333	0.00	0.13	0.466	O	|	|	|	|	0.38
79.417	0.00	0.13	0.465	O	|	|	|	|	0.38
79.500	0.00	0.13	0.464	O	|	|	|	|	0.38
79.583	0.00	0.13	0.464	O	|	|	|	|	0.38
79.667	0.00	0.13	0.463	O	|	|	|	|	0.38
79.750	0.00	0.13	0.462	O	|	|	|	|	0.37
79.833	0.00	0.13	0.461	O	|	|	|	|	0.37
79.917	0.00	0.13	0.460	O	|	|	|	|	0.37
80.000	0.00	0.13	0.459	O	|	|	|	|	0.37
80.083	0.00	0.13	0.458	O	|	|	|	|	0.37
80.167	0.00	0.13	0.457	O	|	|	|	|	0.37
80.250	0.00	0.13	0.456	O	|	|	|	|	0.37
80.333	0.00	0.13	0.456	O	|	|	|	|	0.37
80.417	0.00	0.13	0.455	O	|	|	|	|	0.37
80.500	0.00	0.13	0.454	O	|	|	|	|	0.37
80.583	0.00	0.13	0.453	O	|	|	|	|	0.37
80.667	0.00	0.13	0.452	O	|	|	|	|	0.37
80.750	0.00	0.13	0.451	O	|	|	|	|	0.37
80.833	0.00	0.13	0.450	O	|	|	|	|	0.37
80.917	0.00	0.13	0.450	O	|	|	|	|	0.36
81.000	0.00	0.13	0.449	O	|	|	|	|	0.36
81.083	0.00	0.13	0.448	O	|	|	|	|	0.36
81.167	0.00	0.12	0.447	O	|	|	|	|	0.36
81.250	0.00	0.12	0.446	O	|	|	|	|	0.36
81.333	0.00	0.12	0.445	O	|	|	|	|	0.36
81.417	0.00	0.12	0.444	O	|	|	|	|	0.36
81.500	0.00	0.12	0.444	O	|	|	|	|	0.36
81.583	0.00	0.12	0.443	O	|	|	|	|	0.36
81.667	0.00	0.12	0.442	O	|	|	|	|	0.36
81.750	0.00	0.12	0.441	O	|	|	|	|	0.36
81.833	0.00	0.12	0.440	O	|	|	|	|	0.36
81.917	0.00	0.12	0.439	O	|	|	|	|	0.36
82.000	0.00	0.12	0.438	O	|	|	|	|	0.36
82.083	0.00	0.12	0.438	O	|	|	|	|	0.36
82.167	0.00	0.12	0.437	O	|	|	|	|	0.35
82.250	0.00	0.12	0.436	O	|	|	|	|	0.35
82.333	0.00	0.12	0.435	O	|	|	|	|	0.35
82.417	0.00	0.12	0.434	O	|	|	|	|	0.35
82.500	0.00	0.12	0.433	O	|	|	|	|	0.35
82.583	0.00	0.12	0.433	O	|	|	|	|	0.35
82.667	0.00	0.12	0.432	O	|	|	|	|	0.35
82.750	0.00	0.12	0.431	O	|	|	|	|	0.35
82.833	0.00	0.12	0.430	O	|	|	|	|	0.35
82.917	0.00	0.12	0.429	O	|	|	|	|	0.35
83.000	0.00	0.12	0.428	O	|	|	|	|	0.35

83.083	0.00	0.12	0.428	O	|	|	|	|	0.35
83.167	0.00	0.12	0.427	O	|	|	|	|	0.35
83.250	0.00	0.12	0.426	O	|	|	|	|	0.35
83.333	0.00	0.12	0.425	O	|	|	|	|	0.35
83.417	0.00	0.12	0.424	O	|	|	|	|	0.34
83.500	0.00	0.12	0.424	O	|	|	|	|	0.34
83.583	0.00	0.12	0.423	O	|	|	|	|	0.34
83.667	0.00	0.12	0.422	O	|	|	|	|	0.34
83.750	0.00	0.12	0.421	O	|	|	|	|	0.34
83.833	0.00	0.12	0.420	O	|	|	|	|	0.34
83.917	0.00	0.12	0.419	O	|	|	|	|	0.34
84.000	0.00	0.12	0.419	O	|	|	|	|	0.34
84.083	0.00	0.12	0.418	O	|	|	|	|	0.34
84.167	0.00	0.12	0.417	O	|	|	|	|	0.34
84.250	0.00	0.12	0.416	O	|	|	|	|	0.34
84.333	0.00	0.12	0.415	O	|	|	|	|	0.34
84.417	0.00	0.12	0.415	O	|	|	|	|	0.34
84.500	0.00	0.12	0.414	O	|	|	|	|	0.34
84.583	0.00	0.12	0.413	O	|	|	|	|	0.34
84.667	0.00	0.12	0.412	O	|	|	|	|	0.33
84.750	0.00	0.11	0.411	O	|	|	|	|	0.33
84.833	0.00	0.11	0.411	O	|	|	|	|	0.33
84.917	0.00	0.11	0.410	O	|	|	|	|	0.33
85.000	0.00	0.11	0.409	O	|	|	|	|	0.33
85.083	0.00	0.11	0.408	O	|	|	|	|	0.33
85.167	0.00	0.11	0.408	O	|	|	|	|	0.33
85.250	0.00	0.11	0.407	O	|	|	|	|	0.33
85.333	0.00	0.11	0.406	O	|	|	|	|	0.33
85.417	0.00	0.11	0.405	O	|	|	|	|	0.33
85.500	0.00	0.11	0.404	O	|	|	|	|	0.33
85.583	0.00	0.11	0.404	O	|	|	|	|	0.33
85.667	0.00	0.11	0.403	O	|	|	|	|	0.33
85.750	0.00	0.11	0.402	O	|	|	|	|	0.33
85.833	0.00	0.11	0.401	O	|	|	|	|	0.33
85.917	0.00	0.11	0.401	O	|	|	|	|	0.33
86.000	0.00	0.11	0.400	O	|	|	|	|	0.32
86.083	0.00	0.11	0.399	O	|	|	|	|	0.32
86.167	0.00	0.11	0.398	O	|	|	|	|	0.32
86.250	0.00	0.11	0.397	O	|	|	|	|	0.32
86.333	0.00	0.11	0.397	O	|	|	|	|	0.32
86.417	0.00	0.11	0.396	O	|	|	|	|	0.32
86.500	0.00	0.11	0.395	O	|	|	|	|	0.32
86.583	0.00	0.11	0.394	O	|	|	|	|	0.32
86.667	0.00	0.11	0.394	O	|	|	|	|	0.32
86.750	0.00	0.11	0.393	O	|	|	|	|	0.32
86.833	0.00	0.11	0.392	O	|	|	|	|	0.32
86.917	0.00	0.11	0.391	O	|	|	|	|	0.32
87.000	0.00	0.11	0.391	O	|	|	|	|	0.32
87.083	0.00	0.11	0.390	O	|	|	|	|	0.32
87.167	0.00	0.11	0.389	O	|	|	|	|	0.32
87.250	0.00	0.11	0.388	O	|	|	|	|	0.32
87.333	0.00	0.11	0.388	O	|	|	|	|	0.31
87.417	0.00	0.11	0.387	O	|	|	|	|	0.31
87.500	0.00	0.11	0.386	O	|	|	|	|	0.31
87.583	0.00	0.11	0.385	O	|	|	|	|	0.31
87.667	0.00	0.11	0.385	O	|	|	|	|	0.31
87.750	0.00	0.11	0.384	O	|	|	|	|	0.31
87.833	0.00	0.11	0.383	O	|	|	|	|	0.31
87.917	0.00	0.11	0.382	O	|	|	|	|	0.31
88.000	0.00	0.11	0.382	O	|	|	|	|	0.31
88.083	0.00	0.11	0.381	O	|	|	|	|	0.31
88.167	0.00	0.11	0.380	O	|	|	|	|	0.31
88.250	0.00	0.11	0.380	O	|	|	|	|	0.31
88.333	0.00	0.11	0.379	O	|	|	|	|	0.31
88.417	0.00	0.11	0.378	O	|	|	|	|	0.31
88.500	0.00	0.11	0.377	O	|	|	|	|	0.31
88.583	0.00	0.11	0.377	O	|	|	|	|	0.31
88.667	0.00	0.10	0.376	O	|	|	|	|	0.31
88.750	0.00	0.10	0.375	O	|	|	|	|	0.30
88.833	0.00	0.10	0.374	O	|	|	|	|	0.30
88.917	0.00	0.10	0.374	O	|	|	|	|	0.30

89.000	0.00	0.10	0.373	O	|	|	|	|	0.30
89.083	0.00	0.10	0.372	O	|	|	|	|	0.30
89.167	0.00	0.10	0.372	O	|	|	|	|	0.30
89.250	0.00	0.10	0.371	O	|	|	|	|	0.30
89.333	0.00	0.10	0.370	O	|	|	|	|	0.30
89.417	0.00	0.10	0.369	O	|	|	|	|	0.30
89.500	0.00	0.10	0.369	O	|	|	|	|	0.30
89.583	0.00	0.10	0.368	O	|	|	|	|	0.30
89.667	0.00	0.10	0.367	O	|	|	|	|	0.30
89.750	0.00	0.10	0.367	O	|	|	|	|	0.30
89.833	0.00	0.10	0.366	O	|	|	|	|	0.30
89.917	0.00	0.10	0.365	O	|	|	|	|	0.30
90.000	0.00	0.10	0.365	O	|	|	|	|	0.30
90.083	0.00	0.10	0.364	O	|	|	|	|	0.30
90.167	0.00	0.10	0.363	O	|	|	|	|	0.29
90.250	0.00	0.10	0.362	O	|	|	|	|	0.29
90.333	0.00	0.10	0.362	O	|	|	|	|	0.29
90.417	0.00	0.10	0.361	O	|	|	|	|	0.29
90.500	0.00	0.10	0.360	O	|	|	|	|	0.29
90.583	0.00	0.10	0.360	O	|	|	|	|	0.29
90.667	0.00	0.10	0.359	O	|	|	|	|	0.29
90.750	0.00	0.10	0.358	O	|	|	|	|	0.29
90.833	0.00	0.10	0.358	O	|	|	|	|	0.29
90.917	0.00	0.10	0.357	O	|	|	|	|	0.29
91.000	0.00	0.10	0.356	O	|	|	|	|	0.29
91.083	0.00	0.10	0.356	O	|	|	|	|	0.29
91.167	0.00	0.10	0.355	O	|	|	|	|	0.29
91.250	0.00	0.10	0.354	O	|	|	|	|	0.29
91.333	0.00	0.10	0.353	O	|	|	|	|	0.29
91.417	0.00	0.10	0.353	O	|	|	|	|	0.29
91.500	0.00	0.10	0.352	O	|	|	|	|	0.29
91.583	0.00	0.10	0.351	O	|	|	|	|	0.29
91.667	0.00	0.10	0.351	O	|	|	|	|	0.28
91.750	0.00	0.10	0.350	O	|	|	|	|	0.28
91.833	0.00	0.10	0.349	O	|	|	|	|	0.28
91.917	0.00	0.10	0.349	O	|	|	|	|	0.28
92.000	0.00	0.10	0.348	O	|	|	|	|	0.28
92.083	0.00	0.10	0.347	O	|	|	|	|	0.28
92.167	0.00	0.10	0.347	O	|	|	|	|	0.28
92.250	0.00	0.10	0.346	O	|	|	|	|	0.28
92.333	0.00	0.10	0.345	O	|	|	|	|	0.28
92.417	0.00	0.10	0.345	O	|	|	|	|	0.28
92.500	0.00	0.10	0.344	O	|	|	|	|	0.28
92.583	0.00	0.10	0.343	O	|	|	|	|	0.28
92.667	0.00	0.10	0.343	O	|	|	|	|	0.28
92.750	0.00	0.10	0.342	O	|	|	|	|	0.28
92.833	0.00	0.10	0.341	O	|	|	|	|	0.28
92.917	0.00	0.10	0.341	O	|	|	|	|	0.28
93.000	0.00	0.09	0.340	O	|	|	|	|	0.28
93.083	0.00	0.09	0.339	O	|	|	|	|	0.28
93.167	0.00	0.09	0.339	O	|	|	|	|	0.28
93.250	0.00	0.09	0.338	O	|	|	|	|	0.27
93.333	0.00	0.09	0.338	O	|	|	|	|	0.27
93.417	0.00	0.09	0.337	O	|	|	|	|	0.27
93.500	0.00	0.09	0.336	O	|	|	|	|	0.27
93.583	0.00	0.09	0.336	O	|	|	|	|	0.27
93.667	0.00	0.09	0.335	O	|	|	|	|	0.27
93.750	0.00	0.09	0.334	O	|	|	|	|	0.27
93.833	0.00	0.09	0.334	O	|	|	|	|	0.27
93.917	0.00	0.09	0.333	O	|	|	|	|	0.27
94.000	0.00	0.09	0.332	O	|	|	|	|	0.27
94.083	0.00	0.09	0.332	O	|	|	|	|	0.27
94.167	0.00	0.09	0.331	O	|	|	|	|	0.27
94.250	0.00	0.09	0.330	O	|	|	|	|	0.27
94.333	0.00	0.09	0.330	O	|	|	|	|	0.27
94.417	0.00	0.09	0.329	O	|	|	|	|	0.27
94.500	0.00	0.09	0.329	O	|	|	|	|	0.27
94.583	0.00	0.09	0.328	O	|	|	|	|	0.27
94.667	0.00	0.09	0.327	O	|	|	|	|	0.27
94.750	0.00	0.09	0.327	O	|	|	|	|	0.27
94.833	0.00	0.09	0.326	O	|	|	|	|	0.26

94.917	0.00	0.09	0.325	O					0.26
95.000	0.00	0.09	0.325	O					0.26
95.083	0.00	0.09	0.324	O					0.26
95.167	0.00	0.09	0.324	O					0.26
95.250	0.00	0.09	0.323	O					0.26
95.333	0.00	0.09	0.322	O					0.26
95.417	0.00	0.09	0.322	O					0.26
95.500	0.00	0.09	0.321	O					0.26
95.583	0.00	0.09	0.320	O					0.26
95.667	0.00	0.09	0.320	O					0.26
95.750	0.00	0.09	0.319	O					0.26
95.833	0.00	0.09	0.319	O					0.26
95.917	0.00	0.09	0.318	O					0.26
96.000	0.00	0.09	0.317	O					0.26
96.083	0.00	0.09	0.317	O					0.26
96.167	0.00	0.09	0.316	O					0.26
96.250	0.00	0.09	0.316	O					0.26
96.333	0.00	0.09	0.315	O					0.26
96.417	0.00	0.09	0.314	O					0.26
96.500	0.00	0.09	0.314	O					0.25
96.583	0.00	0.09	0.313	O					0.25
96.667	0.00	0.09	0.313	O					0.25
96.750	0.00	0.09	0.312	O					0.25
96.833	0.00	0.09	0.311	O					0.25
96.917	0.00	0.09	0.311	O					0.25
97.000	0.00	0.09	0.310	O					0.25
97.083	0.00	0.09	0.310	O					0.25
97.167	0.00	0.09	0.309	O					0.25
97.250	0.00	0.09	0.308	O					0.25
97.333	0.00	0.09	0.308	O					0.25
97.417	0.00	0.09	0.307	O					0.25
97.500	0.00	0.09	0.307	O					0.25
97.583	0.00	0.09	0.306	O					0.25
97.667	0.00	0.09	0.305	O					0.25
97.750	0.00	0.09	0.305	O					0.25
97.833	0.00	0.08	0.304	O					0.25
97.917	0.00	0.08	0.304	O					0.25
98.000	0.00	0.08	0.303	O					0.25
98.083	0.00	0.08	0.302	O					0.25
98.167	0.00	0.08	0.302	O					0.25
98.250	0.00	0.08	0.301	O					0.24
98.333	0.00	0.08	0.301	O					0.24
98.417	0.00	0.08	0.300	O					0.24
98.500	0.00	0.08	0.300	O					0.24
98.583	0.00	0.08	0.299	O					0.24
98.667	0.00	0.08	0.298	O					0.24
98.750	0.00	0.08	0.298	O					0.24
98.833	0.00	0.08	0.297	O					0.24
98.917	0.00	0.08	0.297	O					0.24
99.000	0.00	0.08	0.296	O					0.24
99.083	0.00	0.08	0.296	O					0.24
99.167	0.00	0.08	0.295	O					0.24
99.250	0.00	0.08	0.294	O					0.24
99.333	0.00	0.08	0.294	O					0.24
99.417	0.00	0.08	0.293	O					0.24
99.500	0.00	0.08	0.293	O					0.24
99.583	0.00	0.08	0.292	O					0.24
99.667	0.00	0.08	0.292	O					0.24
99.750	0.00	0.08	0.291	O					0.24
99.833	0.00	0.08	0.291	O					0.24
99.917	0.00	0.08	0.290	O					0.24
100.000	0.00	0.08	0.289	O					0.23
100.083	0.00	0.08	0.289	O					0.23
100.167	0.00	0.08	0.288	O					0.23
100.250	0.00	0.08	0.288	O					0.23
100.333	0.00	0.08	0.287	O					0.23
100.417	0.00	0.08	0.287	O					0.23
100.500	0.00	0.08	0.286	O					0.23
100.583	0.00	0.08	0.286	O					0.23
100.667	0.00	0.08	0.285	O					0.23
100.750	0.00	0.08	0.284	O					0.23

100.833	0.00	0.08	0.284	O	|	|	|	|	0.23
100.917	0.00	0.08	0.283	O	|	|	|	|	0.23
101.000	0.00	0.08	0.283	O	|	|	|	|	0.23
101.083	0.00	0.08	0.282	O	|	|	|	|	0.23
101.167	0.00	0.08	0.282	O	|	|	|	|	0.23
101.250	0.00	0.08	0.281	O	|	|	|	|	0.23
101.333	0.00	0.08	0.281	O	|	|	|	|	0.23
101.417	0.00	0.08	0.280	O	|	|	|	|	0.23
101.500	0.00	0.08	0.280	O	|	|	|	|	0.23
101.583	0.00	0.08	0.279	O	|	|	|	|	0.23
101.667	0.00	0.08	0.278	O	|	|	|	|	0.23
101.750	0.00	0.08	0.278	O	|	|	|	|	0.23
101.833	0.00	0.08	0.277	O	|	|	|	|	0.23
101.917	0.00	0.08	0.277	O	|	|	|	|	0.22
102.000	0.00	0.08	0.276	O	|	|	|	|	0.22
102.083	0.00	0.08	0.276	O	|	|	|	|	0.22
102.167	0.00	0.08	0.275	O	|	|	|	|	0.22
102.250	0.00	0.08	0.275	O	|	|	|	|	0.22
102.333	0.00	0.08	0.274	O	|	|	|	|	0.22
102.417	0.00	0.08	0.274	O	|	|	|	|	0.22
102.500	0.00	0.08	0.273	O	|	|	|	|	0.22
102.583	0.00	0.08	0.273	O	|	|	|	|	0.22
102.667	0.00	0.08	0.272	O	|	|	|	|	0.22
102.750	0.00	0.08	0.272	O	|	|	|	|	0.22
102.833	0.00	0.08	0.271	O	|	|	|	|	0.22
102.917	0.00	0.08	0.271	O	|	|	|	|	0.22
103.000	0.00	0.08	0.270	O	|	|	|	|	0.22
103.083	0.00	0.08	0.270	O	|	|	|	|	0.22
103.167	0.00	0.08	0.269	O	|	|	|	|	0.22
103.250	0.00	0.07	0.268	O	|	|	|	|	0.22
103.333	0.00	0.07	0.268	O	|	|	|	|	0.22
103.417	0.00	0.07	0.267	O	|	|	|	|	0.22
103.500	0.00	0.07	0.267	O	|	|	|	|	0.22
103.583	0.00	0.07	0.266	O	|	|	|	|	0.22
103.667	0.00	0.07	0.266	O	|	|	|	|	0.22
103.750	0.00	0.07	0.265	O	|	|	|	|	0.22
103.833	0.00	0.07	0.265	O	|	|	|	|	0.22
103.917	0.00	0.07	0.264	O	|	|	|	|	0.21
104.000	0.00	0.07	0.264	O	|	|	|	|	0.21
104.083	0.00	0.07	0.263	O	|	|	|	|	0.21
104.167	0.00	0.07	0.263	O	|	|	|	|	0.21
104.250	0.00	0.07	0.262	O	|	|	|	|	0.21
104.333	0.00	0.07	0.262	O	|	|	|	|	0.21
104.417	0.00	0.07	0.261	O	|	|	|	|	0.21
104.500	0.00	0.07	0.261	O	|	|	|	|	0.21
104.583	0.00	0.07	0.260	O	|	|	|	|	0.21
104.667	0.00	0.07	0.260	O	|	|	|	|	0.21
104.750	0.00	0.07	0.259	O	|	|	|	|	0.21
104.833	0.00	0.07	0.259	O	|	|	|	|	0.21
104.917	0.00	0.07	0.258	O	|	|	|	|	0.21
105.000	0.00	0.07	0.258	O	|	|	|	|	0.21
105.083	0.00	0.07	0.257	O	|	|	|	|	0.21
105.167	0.00	0.07	0.257	O	|	|	|	|	0.21
105.250	0.00	0.07	0.256	O	|	|	|	|	0.21
105.333	0.00	0.07	0.256	O	|	|	|	|	0.21
105.417	0.00	0.07	0.255	O	|	|	|	|	0.21
105.500	0.00	0.07	0.255	O	|	|	|	|	0.21
105.583	0.00	0.07	0.254	O	|	|	|	|	0.21
105.667	0.00	0.07	0.254	O	|	|	|	|	0.21
105.750	0.00	0.07	0.253	O	|	|	|	|	0.21
105.833	0.00	0.07	0.253	O	|	|	|	|	0.21
105.917	0.00	0.07	0.252	O	|	|	|	|	0.20
106.000	0.00	0.07	0.252	O	|	|	|	|	0.20
106.083	0.00	0.07	0.251	O	|	|	|	|	0.20
106.167	0.00	0.07	0.251	O	|	|	|	|	0.20
106.250	0.00	0.07	0.251	O	|	|	|	|	0.20
106.333	0.00	0.07	0.250	O	|	|	|	|	0.20
106.417	0.00	0.07	0.250	O	|	|	|	|	0.20
106.500	0.00	0.07	0.249	O	|	|	|	|	0.20
106.583	0.00	0.07	0.249	O	|	|	|	|	0.20
106.667	0.00	0.07	0.248	O	|	|	|	|	0.20

106.750	0.00	0.07	0.248	O	|	|	|	|	0.20
106.833	0.00	0.07	0.247	O	|	|	|	|	0.20
106.917	0.00	0.07	0.247	O	|	|	|	|	0.20
107.000	0.00	0.07	0.246	O	|	|	|	|	0.20
107.083	0.00	0.07	0.246	O	|	|	|	|	0.20
107.167	0.00	0.07	0.245	O	|	|	|	|	0.20
107.250	0.00	0.07	0.245	O	|	|	|	|	0.20
107.333	0.00	0.07	0.244	O	|	|	|	|	0.20
107.417	0.00	0.07	0.244	O	|	|	|	|	0.20
107.500	0.00	0.07	0.243	O	|	|	|	|	0.20
107.583	0.00	0.07	0.243	O	|	|	|	|	0.20
107.667	0.00	0.07	0.242	O	|	|	|	|	0.20
107.750	0.00	0.07	0.242	O	|	|	|	|	0.20
107.833	0.00	0.07	0.242	O	|	|	|	|	0.20
107.917	0.00	0.07	0.241	O	|	|	|	|	0.20
108.000	0.00	0.07	0.241	O	|	|	|	|	0.20
108.083	0.00	0.07	0.240	O	|	|	|	|	0.19
108.167	0.00	0.07	0.240	O	|	|	|	|	0.19
108.250	0.00	0.07	0.239	O	|	|	|	|	0.19
108.333	0.00	0.07	0.239	O	|	|	|	|	0.19
108.417	0.00	0.07	0.238	O	|	|	|	|	0.19
108.500	0.00	0.07	0.238	O	|	|	|	|	0.19
108.583	0.00	0.07	0.237	O	|	|	|	|	0.19
108.667	0.00	0.07	0.237	O	|	|	|	|	0.19
108.750	0.00	0.07	0.236	O	|	|	|	|	0.19
108.833	0.00	0.07	0.236	O	|	|	|	|	0.19
108.917	0.00	0.07	0.236	O	|	|	|	|	0.19
109.000	0.00	0.07	0.235	O	|	|	|	|	0.19
109.083	0.00	0.07	0.235	O	|	|	|	|	0.19
109.167	0.00	0.07	0.234	O	|	|	|	|	0.19
109.250	0.00	0.07	0.234	O	|	|	|	|	0.19
109.333	0.00	0.07	0.233	O	|	|	|	|	0.19
109.417	0.00	0.07	0.233	O	|	|	|	|	0.19
109.500	0.00	0.06	0.232	O	|	|	|	|	0.19
109.583	0.00	0.06	0.232	O	|	|	|	|	0.19
109.667	0.00	0.06	0.232	O	|	|	|	|	0.19
109.750	0.00	0.06	0.231	O	|	|	|	|	0.19
109.833	0.00	0.06	0.231	O	|	|	|	|	0.19
109.917	0.00	0.06	0.230	O	|	|	|	|	0.19
110.000	0.00	0.06	0.230	O	|	|	|	|	0.19
110.083	0.00	0.06	0.229	O	|	|	|	|	0.19
110.167	0.00	0.06	0.229	O	|	|	|	|	0.19
110.250	0.00	0.06	0.228	O	|	|	|	|	0.19
110.333	0.00	0.06	0.228	O	|	|	|	|	0.19
110.417	0.00	0.06	0.228	O	|	|	|	|	0.18
110.500	0.00	0.06	0.227	O	|	|	|	|	0.18
110.583	0.00	0.06	0.227	O	|	|	|	|	0.18
110.667	0.00	0.06	0.226	O	|	|	|	|	0.18
110.750	0.00	0.06	0.226	O	|	|	|	|	0.18
110.833	0.00	0.06	0.225	O	|	|	|	|	0.18
110.917	0.00	0.06	0.225	O	|	|	|	|	0.18
111.000	0.00	0.06	0.225	O	|	|	|	|	0.18
111.083	0.00	0.06	0.224	O	|	|	|	|	0.18
111.167	0.00	0.06	0.224	O	|	|	|	|	0.18
111.250	0.00	0.06	0.223	O	|	|	|	|	0.18
111.333	0.00	0.06	0.223	O	|	|	|	|	0.18
111.417	0.00	0.06	0.222	O	|	|	|	|	0.18
111.500	0.00	0.06	0.222	O	|	|	|	|	0.18
111.583	0.00	0.06	0.222	O	|	|	|	|	0.18
111.667	0.00	0.06	0.221	O	|	|	|	|	0.18
111.750	0.00	0.06	0.221	O	|	|	|	|	0.18
111.833	0.00	0.06	0.220	O	|	|	|	|	0.18
111.917	0.00	0.06	0.220	O	|	|	|	|	0.18
112.000	0.00	0.06	0.219	O	|	|	|	|	0.18
112.083	0.00	0.06	0.219	O	|	|	|	|	0.18
112.167	0.00	0.06	0.219	O	|	|	|	|	0.18
112.250	0.00	0.06	0.218	O	|	|	|	|	0.18
112.333	0.00	0.06	0.218	O	|	|	|	|	0.18
112.417	0.00	0.06	0.217	O	|	|	|	|	0.18
112.500	0.00	0.06	0.217	O	|	|	|	|	0.18
112.583	0.00	0.06	0.216	O	|	|	|	|	0.18

112.667	0.00	0.06	0.216	O	|	|	|	|	0.18
112.750	0.00	0.06	0.216	O	|	|	|	|	0.18
112.833	0.00	0.06	0.215	O	|	|	|	|	0.17
112.917	0.00	0.06	0.215	O	|	|	|	|	0.17
113.000	0.00	0.06	0.214	O	|	|	|	|	0.17
113.083	0.00	0.06	0.214	O	|	|	|	|	0.17
113.167	0.00	0.06	0.214	O	|	|	|	|	0.17
113.250	0.00	0.06	0.213	O	|	|	|	|	0.17
113.333	0.00	0.06	0.213	O	|	|	|	|	0.17
113.417	0.00	0.06	0.212	O	|	|	|	|	0.17
113.500	0.00	0.06	0.212	O	|	|	|	|	0.17
113.583	0.00	0.06	0.212	O	|	|	|	|	0.17
113.667	0.00	0.06	0.211	O	|	|	|	|	0.17
113.750	0.00	0.06	0.211	O	|	|	|	|	0.17
113.833	0.00	0.06	0.210	O	|	|	|	|	0.17
113.917	0.00	0.06	0.210	O	|	|	|	|	0.17
114.000	0.00	0.06	0.210	O	|	|	|	|	0.17
114.083	0.00	0.06	0.209	O	|	|	|	|	0.17
114.167	0.00	0.06	0.209	O	|	|	|	|	0.17
114.250	0.00	0.06	0.208	O	|	|	|	|	0.17
114.333	0.00	0.06	0.208	O	|	|	|	|	0.17
114.417	0.00	0.06	0.207	O	|	|	|	|	0.17
114.500	0.00	0.06	0.207	O	|	|	|	|	0.17
114.583	0.00	0.06	0.207	O	|	|	|	|	0.17
114.667	0.00	0.06	0.206	O	|	|	|	|	0.17
114.750	0.00	0.06	0.206	O	|	|	|	|	0.17
114.833	0.00	0.06	0.206	O	|	|	|	|	0.17
114.917	0.00	0.06	0.205	O	|	|	|	|	0.17
115.000	0.00	0.06	0.205	O	|	|	|	|	0.17
115.083	0.00	0.06	0.204	O	|	|	|	|	0.17
115.167	0.00	0.06	0.204	O	|	|	|	|	0.17
115.250	0.00	0.06	0.204	O	|	|	|	|	0.17
115.333	0.00	0.06	0.203	O	|	|	|	|	0.16
115.417	0.00	0.06	0.203	O	|	|	|	|	0.16
115.500	0.00	0.06	0.202	O	|	|	|	|	0.16
115.583	0.00	0.06	0.202	O	|	|	|	|	0.16
115.667	0.00	0.06	0.202	O	|	|	|	|	0.16
115.750	0.00	0.06	0.201	O	|	|	|	|	0.16
115.833	0.00	0.06	0.201	O	|	|	|	|	0.16
115.917	0.00	0.06	0.200	O	|	|	|	|	0.16
116.000	0.00	0.06	0.200	O	|	|	|	|	0.16
116.083	0.00	0.06	0.200	O	|	|	|	|	0.16
116.167	0.00	0.06	0.199	O	|	|	|	|	0.16
116.250	0.00	0.06	0.199	O	|	|	|	|	0.16
116.333	0.00	0.06	0.199	O	|	|	|	|	0.16
116.417	0.00	0.06	0.198	O	|	|	|	|	0.16
116.500	0.00	0.06	0.198	O	|	|	|	|	0.16
116.583	0.00	0.06	0.197	O	|	|	|	|	0.16
116.667	0.00	0.06	0.197	O	|	|	|	|	0.16
116.750	0.00	0.05	0.197	O	|	|	|	|	0.16
116.833	0.00	0.05	0.196	O	|	|	|	|	0.16
116.917	0.00	0.05	0.196	O	|	|	|	|	0.16
117.000	0.00	0.05	0.195	O	|	|	|	|	0.16
117.083	0.00	0.05	0.195	O	|	|	|	|	0.16
117.167	0.00	0.05	0.195	O	|	|	|	|	0.16
117.250	0.00	0.05	0.194	O	|	|	|	|	0.16
117.333	0.00	0.05	0.194	O	|	|	|	|	0.16
117.417	0.00	0.05	0.194	O	|	|	|	|	0.16
117.500	0.00	0.05	0.193	O	|	|	|	|	0.16
117.583	0.00	0.05	0.193	O	|	|	|	|	0.16
117.667	0.00	0.05	0.193	O	|	|	|	|	0.16
117.750	0.00	0.05	0.192	O	|	|	|	|	0.16
117.833	0.00	0.05	0.192	O	|	|	|	|	0.16
117.917	0.00	0.05	0.191	O	|	|	|	|	0.16
118.000	0.00	0.05	0.191	O	|	|	|	|	0.16
118.083	0.00	0.05	0.191	O	|	|	|	|	0.15
118.167	0.00	0.05	0.190	O	|	|	|	|	0.15
118.250	0.00	0.05	0.190	O	|	|	|	|	0.15
118.333	0.00	0.05	0.190	O	|	|	|	|	0.15
118.417	0.00	0.05	0.189	O	|	|	|	|	0.15
118.500	0.00	0.05	0.189	O	|	|	|	|	0.15

118.583	0.00	0.05	0.188	O	|	|	|	|	0.15
118.667	0.00	0.05	0.188	O	|	|	|	|	0.15
118.750	0.00	0.05	0.188	O	|	|	|	|	0.15
118.833	0.00	0.05	0.187	O	|	|	|	|	0.15
118.917	0.00	0.05	0.187	O	|	|	|	|	0.15
119.000	0.00	0.05	0.187	O	|	|	|	|	0.15
119.083	0.00	0.05	0.186	O	|	|	|	|	0.15
119.167	0.00	0.05	0.186	O	|	|	|	|	0.15
119.250	0.00	0.05	0.186	O	|	|	|	|	0.15
119.333	0.00	0.05	0.185	O	|	|	|	|	0.15
119.417	0.00	0.05	0.185	O	|	|	|	|	0.15
119.500	0.00	0.05	0.185	O	|	|	|	|	0.15
119.583	0.00	0.05	0.184	O	|	|	|	|	0.15
119.667	0.00	0.05	0.184	O	|	|	|	|	0.15
119.750	0.00	0.05	0.183	O	|	|	|	|	0.15
119.833	0.00	0.05	0.183	O	|	|	|	|	0.15
119.917	0.00	0.05	0.183	O	|	|	|	|	0.15
120.000	0.00	0.05	0.182	O	|	|	|	|	0.15
120.083	0.00	0.05	0.182	O	|	|	|	|	0.15
120.167	0.00	0.05	0.182	O	|	|	|	|	0.15
120.250	0.00	0.05	0.181	O	|	|	|	|	0.15
120.333	0.00	0.05	0.181	O	|	|	|	|	0.15
120.417	0.00	0.05	0.181	O	|	|	|	|	0.15
120.500	0.00	0.05	0.180	O	|	|	|	|	0.15
120.583	0.00	0.05	0.180	O	|	|	|	|	0.15
120.667	0.00	0.05	0.180	O	|	|	|	|	0.15
120.750	0.00	0.05	0.179	O	|	|	|	|	0.15
120.833	0.00	0.05	0.179	O	|	|	|	|	0.15
120.917	0.00	0.05	0.179	O	|	|	|	|	0.14
121.000	0.00	0.05	0.178	O	|	|	|	|	0.14
121.083	0.00	0.05	0.178	O	|	|	|	|	0.14
121.167	0.00	0.05	0.178	O	|	|	|	|	0.14
121.250	0.00	0.05	0.177	O	|	|	|	|	0.14
121.333	0.00	0.05	0.177	O	|	|	|	|	0.14
121.417	0.00	0.05	0.177	O	|	|	|	|	0.14
121.500	0.00	0.05	0.176	O	|	|	|	|	0.14
121.583	0.00	0.05	0.176	O	|	|	|	|	0.14
121.667	0.00	0.05	0.176	O	|	|	|	|	0.14
121.750	0.00	0.05	0.175	O	|	|	|	|	0.14
121.833	0.00	0.05	0.175	O	|	|	|	|	0.14
121.917	0.00	0.05	0.175	O	|	|	|	|	0.14
122.000	0.00	0.05	0.174	O	|	|	|	|	0.14
122.083	0.00	0.05	0.174	O	|	|	|	|	0.14
122.167	0.00	0.05	0.174	O	|	|	|	|	0.14
122.250	0.00	0.05	0.173	O	|	|	|	|	0.14
122.333	0.00	0.05	0.173	O	|	|	|	|	0.14
122.417	0.00	0.05	0.173	O	|	|	|	|	0.14
122.500	0.00	0.05	0.172	O	|	|	|	|	0.14
122.583	0.00	0.05	0.172	O	|	|	|	|	0.14
122.667	0.00	0.05	0.172	O	|	|	|	|	0.14
122.750	0.00	0.05	0.171	O	|	|	|	|	0.14
122.833	0.00	0.05	0.171	O	|	|	|	|	0.14
122.917	0.00	0.05	0.171	O	|	|	|	|	0.14
123.000	0.00	0.05	0.170	O	|	|	|	|	0.14
123.083	0.00	0.05	0.170	O	|	|	|	|	0.14
123.167	0.00	0.05	0.170	O	|	|	|	|	0.14
123.250	0.00	0.05	0.169	O	|	|	|	|	0.14
123.333	0.00	0.05	0.169	O	|	|	|	|	0.14
123.417	0.00	0.05	0.169	O	|	|	|	|	0.14
123.500	0.00	0.05	0.168	O	|	|	|	|	0.14
123.583	0.00	0.05	0.168	O	|	|	|	|	0.14
123.667	0.00	0.05	0.168	O	|	|	|	|	0.14
123.750	0.00	0.05	0.167	O	|	|	|	|	0.14
123.833	0.00	0.05	0.167	O	|	|	|	|	0.14
123.917	0.00	0.05	0.167	O	|	|	|	|	0.14
124.000	0.00	0.05	0.166	O	|	|	|	|	0.14
124.083	0.00	0.05	0.166	O	|	|	|	|	0.13
124.167	0.00	0.05	0.166	O	|	|	|	|	0.13
124.250	0.00	0.05	0.165	O	|	|	|	|	0.13
124.333	0.00	0.05	0.165	O	|	|	|	|	0.13
124.417	0.00	0.05	0.165	O	|	|	|	|	0.13

124.500	0.00	0.05	0.164	O					0.13
124.583	0.00	0.05	0.164	O					0.13
124.667	0.00	0.05	0.164	O					0.13
124.750	0.00	0.05	0.163	O					0.13
124.833	0.00	0.05	0.163	O					0.13
124.917	0.00	0.05	0.163	O					0.13
125.000	0.00	0.05	0.163	O					0.13
125.083	0.00	0.05	0.162	O					0.13
125.167	0.00	0.05	0.162	O					0.13
125.250	0.00	0.05	0.162	O					0.13
125.333	0.00	0.05	0.161	O					0.13
125.417	0.00	0.04	0.161	O					0.13
125.500	0.00	0.04	0.161	O					0.13
125.583	0.00	0.04	0.160	O					0.13
125.667	0.00	0.04	0.160	O					0.13
125.750	0.00	0.04	0.160	O					0.13
125.833	0.00	0.04	0.159	O					0.13
125.917	0.00	0.04	0.159	O					0.13
126.000	0.00	0.04	0.159	O					0.13
126.083	0.00	0.04	0.159	O					0.13
126.167	0.00	0.04	0.158	O					0.13
126.250	0.00	0.04	0.158	O					0.13
126.333	0.00	0.04	0.158	O					0.13
126.417	0.00	0.04	0.157	O					0.13
126.500	0.00	0.04	0.157	O					0.13
126.583	0.00	0.04	0.157	O					0.13
126.667	0.00	0.04	0.156	O					0.13
126.750	0.00	0.04	0.156	O					0.13
126.833	0.00	0.04	0.156	O					0.13
126.917	0.00	0.04	0.156	O					0.13
127.000	0.00	0.04	0.155	O					0.13
127.083	0.00	0.04	0.155	O					0.13
127.167	0.00	0.04	0.155	O					0.13
127.250	0.00	0.04	0.154	O					0.13
127.333	0.00	0.04	0.154	O					0.13
127.417	0.00	0.04	0.154	O					0.12
127.500	0.00	0.04	0.153	O					0.12
127.583	0.00	0.04	0.153	O					0.12
127.667	0.00	0.04	0.153	O					0.12
127.750	0.00	0.04	0.153	O					0.12
127.833	0.00	0.04	0.152	O					0.12
127.917	0.00	0.04	0.152	O					0.12
128.000	0.00	0.04	0.152	O					0.12
128.083	0.00	0.04	0.151	O					0.12
128.167	0.00	0.04	0.151	O					0.12
128.250	0.00	0.04	0.151	O					0.12
128.333	0.00	0.04	0.151	O					0.12
128.417	0.00	0.04	0.150	O					0.12
128.500	0.00	0.04	0.150	O					0.12
128.583	0.00	0.04	0.150	O					0.12
128.667	0.00	0.04	0.149	O					0.12
128.750	0.00	0.04	0.149	O					0.12
128.833	0.00	0.04	0.149	O					0.12
128.917	0.00	0.04	0.148	O					0.12
129.000	0.00	0.04	0.148	O					0.12
129.083	0.00	0.04	0.148	O					0.12
129.167	0.00	0.04	0.148	O					0.12
129.250	0.00	0.04	0.147	O					0.12
129.333	0.00	0.04	0.147	O					0.12
129.417	0.00	0.04	0.147	O					0.12
129.500	0.00	0.04	0.147	O					0.12
129.583	0.00	0.04	0.146	O					0.12
129.667	0.00	0.04	0.146	O					0.12
129.750	0.00	0.04	0.146	O					0.12
129.833	0.00	0.04	0.145	O					0.12
129.917	0.00	0.04	0.145	O					0.12
130.000	0.00	0.04	0.145	O					0.12
130.083	0.00	0.04	0.145	O					0.12
130.167	0.00	0.04	0.144	O					0.12
130.250	0.00	0.04	0.144	O					0.12
130.333	0.00	0.04	0.144	O					0.12

130.417	0.00	0.04	0.143	O	|	|	|	|	0.12
130.500	0.00	0.04	0.143	O	|	|	|	|	0.12
130.583	0.00	0.04	0.143	O	|	|	|	|	0.12
130.667	0.00	0.04	0.143	O	|	|	|	|	0.12
130.750	0.00	0.04	0.142	O	|	|	|	|	0.12
130.833	0.00	0.04	0.142	O	|	|	|	|	0.12
130.917	0.00	0.04	0.142	O	|	|	|	|	0.12
131.000	0.00	0.04	0.142	O	|	|	|	|	0.11
131.083	0.00	0.04	0.141	O	|	|	|	|	0.11
131.167	0.00	0.04	0.141	O	|	|	|	|	0.11
131.250	0.00	0.04	0.141	O	|	|	|	|	0.11
131.333	0.00	0.04	0.140	O	|	|	|	|	0.11
131.417	0.00	0.04	0.140	O	|	|	|	|	0.11
131.500	0.00	0.04	0.140	O	|	|	|	|	0.11
131.583	0.00	0.04	0.140	O	|	|	|	|	0.11
131.667	0.00	0.04	0.139	O	|	|	|	|	0.11
131.750	0.00	0.04	0.139	O	|	|	|	|	0.11
131.833	0.00	0.04	0.139	O	|	|	|	|	0.11
131.917	0.00	0.04	0.139	O	|	|	|	|	0.11
132.000	0.00	0.04	0.138	O	|	|	|	|	0.11
132.083	0.00	0.04	0.138	O	|	|	|	|	0.11
132.167	0.00	0.04	0.138	O	|	|	|	|	0.11
132.250	0.00	0.04	0.137	O	|	|	|	|	0.11
132.333	0.00	0.04	0.137	O	|	|	|	|	0.11
132.417	0.00	0.04	0.137	O	|	|	|	|	0.11
132.500	0.00	0.04	0.137	O	|	|	|	|	0.11
132.583	0.00	0.04	0.136	O	|	|	|	|	0.11
132.667	0.00	0.04	0.136	O	|	|	|	|	0.11
132.750	0.00	0.04	0.136	O	|	|	|	|	0.11
132.833	0.00	0.04	0.136	O	|	|	|	|	0.11
132.917	0.00	0.04	0.135	O	|	|	|	|	0.11
133.000	0.00	0.04	0.135	O	|	|	|	|	0.11
133.083	0.00	0.04	0.135	O	|	|	|	|	0.11
133.167	0.00	0.04	0.135	O	|	|	|	|	0.11
133.250	0.00	0.04	0.134	O	|	|	|	|	0.11
133.333	0.00	0.04	0.134	O	|	|	|	|	0.11
133.417	0.00	0.04	0.134	O	|	|	|	|	0.11
133.500	0.00	0.04	0.134	O	|	|	|	|	0.11
133.583	0.00	0.04	0.133	O	|	|	|	|	0.11
133.667	0.00	0.04	0.133	O	|	|	|	|	0.11
133.750	0.00	0.04	0.133	O	|	|	|	|	0.11
133.833	0.00	0.04	0.133	O	|	|	|	|	0.11
133.917	0.00	0.04	0.132	O	|	|	|	|	0.11
134.000	0.00	0.04	0.132	O	|	|	|	|	0.11
134.083	0.00	0.04	0.132	O	|	|	|	|	0.11
134.167	0.00	0.04	0.132	O	|	|	|	|	0.11
134.250	0.00	0.04	0.131	O	|	|	|	|	0.11
134.333	0.00	0.04	0.131	O	|	|	|	|	0.11
134.417	0.00	0.04	0.131	O	|	|	|	|	0.11
134.500	0.00	0.04	0.131	O	|	|	|	|	0.11
134.583	0.00	0.04	0.130	O	|	|	|	|	0.11
134.667	0.00	0.04	0.130	O	|	|	|	|	0.11
134.750	0.00	0.04	0.130	O	|	|	|	|	0.11
134.833	0.00	0.04	0.130	O	|	|	|	|	0.11
134.917	0.00	0.04	0.129	O	|	|	|	|	0.10
135.000	0.00	0.04	0.129	O	|	|	|	|	0.10
135.083	0.00	0.04	0.129	O	|	|	|	|	0.10
135.167	0.00	0.04	0.129	O	|	|	|	|	0.10
135.250	0.00	0.04	0.128	O	|	|	|	|	0.10
135.333	0.00	0.04	0.128	O	|	|	|	|	0.10
135.417	0.00	0.04	0.128	O	|	|	|	|	0.10
135.500	0.00	0.04	0.128	O	|	|	|	|	0.10
135.583	0.00	0.04	0.127	O	|	|	|	|	0.10
135.667	0.00	0.04	0.127	O	|	|	|	|	0.10
135.750	0.00	0.04	0.127	O	|	|	|	|	0.10
135.833	0.00	0.04	0.127	O	|	|	|	|	0.10
135.917	0.00	0.04	0.126	O	|	|	|	|	0.10
136.000	0.00	0.04	0.126	O	|	|	|	|	0.10
136.083	0.00	0.04	0.126	O	|	|	|	|	0.10
136.167	0.00	0.04	0.126	O	|	|	|	|	0.10
136.250	0.00	0.04	0.125	O	|	|	|	|	0.10

136.333	0.00	0.03	0.125	O					0.10
136.417	0.00	0.03	0.125	O					0.10
136.500	0.00	0.03	0.125	O					0.10
136.583	0.00	0.03	0.124	O					0.10
136.667	0.00	0.03	0.124	O					0.10
136.750	0.00	0.03	0.124	O					0.10
136.833	0.00	0.03	0.124	O					0.10
136.917	0.00	0.03	0.123	O					0.10
137.000	0.00	0.03	0.123	O					0.10
137.083	0.00	0.03	0.123	O					0.10
137.167	0.00	0.03	0.123	O					0.10
137.250	0.00	0.03	0.123	O					0.10
137.333	0.00	0.03	0.122	O					0.10
137.417	0.00	0.03	0.122	O					0.10
137.500	0.00	0.03	0.122	O					0.10
137.583	0.00	0.03	0.122	O					0.10
137.667	0.00	0.03	0.121	O					0.10
137.750	0.00	0.03	0.121	O					0.10
137.833	0.00	0.03	0.121	O					0.10
137.917	0.00	0.03	0.121	O					0.10
138.000	0.00	0.03	0.120	O					0.10
138.083	0.00	0.03	0.120	O					0.10
138.167	0.00	0.03	0.120	O					0.10
138.250	0.00	0.03	0.120	O					0.10
138.333	0.00	0.03	0.119	O					0.10
138.417	0.00	0.03	0.119	O					0.10
138.500	0.00	0.03	0.119	O					0.10
138.583	0.00	0.03	0.119	O					0.10
138.667	0.00	0.03	0.119	O					0.10
138.750	0.00	0.03	0.118	O					0.10
138.833	0.00	0.03	0.118	O					0.10
138.917	0.00	0.03	0.118	O					0.10
139.000	0.00	0.03	0.118	O					0.10
139.083	0.00	0.03	0.117	O					0.10
139.167	0.00	0.03	0.117	O					0.10
139.250	0.00	0.03	0.117	O					0.09
139.333	0.00	0.03	0.117	O					0.09
139.417	0.00	0.03	0.117	O					0.09
139.500	0.00	0.03	0.116	O					0.09
139.583	0.00	0.03	0.116	O					0.09
139.667	0.00	0.03	0.116	O					0.09
139.750	0.00	0.03	0.116	O					0.09
139.833	0.00	0.03	0.115	O					0.09
139.917	0.00	0.03	0.115	O					0.09
140.000	0.00	0.03	0.115	O					0.09
140.083	0.00	0.03	0.115	O					0.09
140.167	0.00	0.03	0.115	O					0.09
140.250	0.00	0.03	0.114	O					0.09
140.333	0.00	0.03	0.114	O					0.09
140.417	0.00	0.03	0.114	O					0.09
140.500	0.00	0.03	0.114	O					0.09
140.583	0.00	0.03	0.113	O					0.09
140.667	0.00	0.03	0.113	O					0.09
140.750	0.00	0.03	0.113	O					0.09
140.833	0.00	0.03	0.113	O					0.09
140.917	0.00	0.03	0.113	O					0.09
141.000	0.00	0.03	0.112	O					0.09
141.083	0.00	0.03	0.112	O					0.09
141.167	0.00	0.03	0.112	O					0.09
141.250	0.00	0.03	0.112	O					0.09
141.333	0.00	0.03	0.111	O					0.09
141.417	0.00	0.03	0.111	O					0.09
141.500	0.00	0.03	0.111	O					0.09
141.583	0.00	0.03	0.111	O					0.09
141.667	0.00	0.03	0.111	O					0.09
141.750	0.00	0.03	0.110	O					0.09
141.833	0.00	0.03	0.110	O					0.09
141.917	0.00	0.03	0.110	O					0.09
142.000	0.00	0.03	0.110	O					0.09
142.083	0.00	0.03	0.110	O					0.09
142.167	0.00	0.03	0.109	O					0.09

142.250	0.00	0.03	0.109	O	|	|	|	|	0.09
142.333	0.00	0.03	0.109	O	|	|	|	|	0.09
142.417	0.00	0.03	0.109	O	|	|	|	|	0.09
142.500	0.00	0.03	0.109	O	|	|	|	|	0.09
142.583	0.00	0.03	0.108	O	|	|	|	|	0.09
142.667	0.00	0.03	0.108	O	|	|	|	|	0.09
142.750	0.00	0.03	0.108	O	|	|	|	|	0.09
142.833	0.00	0.03	0.108	O	|	|	|	|	0.09
142.917	0.00	0.03	0.107	O	|	|	|	|	0.09
143.000	0.00	0.03	0.107	O	|	|	|	|	0.09
143.083	0.00	0.03	0.107	O	|	|	|	|	0.09
143.167	0.00	0.03	0.107	O	|	|	|	|	0.09
143.250	0.00	0.03	0.107	O	|	|	|	|	0.09
143.333	0.00	0.03	0.106	O	|	|	|	|	0.09
143.417	0.00	0.03	0.106	O	|	|	|	|	0.09
143.500	0.00	0.03	0.106	O	|	|	|	|	0.09
143.583	0.00	0.03	0.106	O	|	|	|	|	0.09
143.667	0.00	0.03	0.106	O	|	|	|	|	0.09
143.750	0.00	0.03	0.105	O	|	|	|	|	0.09
143.833	0.00	0.03	0.105	O	|	|	|	|	0.09
143.917	0.00	0.03	0.105	O	|	|	|	|	0.09
144.000	0.00	0.03	0.105	O	|	|	|	|	0.09
144.083	0.00	0.03	0.105	O	|	|	|	|	0.08
144.167	0.00	0.03	0.104	O	|	|	|	|	0.08
144.250	0.00	0.03	0.104	O	|	|	|	|	0.08
144.333	0.00	0.03	0.104	O	|	|	|	|	0.08
144.417	0.00	0.03	0.104	O	|	|	|	|	0.08
144.500	0.00	0.03	0.104	O	|	|	|	|	0.08
144.583	0.00	0.03	0.103	O	|	|	|	|	0.08
144.667	0.00	0.03	0.103	O	|	|	|	|	0.08
144.750	0.00	0.03	0.103	O	|	|	|	|	0.08
144.833	0.00	0.03	0.103	O	|	|	|	|	0.08
144.917	0.00	0.03	0.103	O	|	|	|	|	0.08
145.000	0.00	0.03	0.102	O	|	|	|	|	0.08
145.083	0.00	0.03	0.102	O	|	|	|	|	0.08
145.167	0.00	0.03	0.102	O	|	|	|	|	0.08
145.250	0.00	0.03	0.102	O	|	|	|	|	0.08
145.333	0.00	0.03	0.102	O	|	|	|	|	0.08
145.417	0.00	0.03	0.101	O	|	|	|	|	0.08
145.500	0.00	0.03	0.101	O	|	|	|	|	0.08
145.583	0.00	0.03	0.101	O	|	|	|	|	0.08
145.667	0.00	0.03	0.101	O	|	|	|	|	0.08
145.750	0.00	0.03	0.101	O	|	|	|	|	0.08
145.833	0.00	0.03	0.100	O	|	|	|	|	0.08
145.917	0.00	0.03	0.100	O	|	|	|	|	0.08
146.000	0.00	0.03	0.100	O	|	|	|	|	0.08
146.083	0.00	0.03	0.100	O	|	|	|	|	0.08
146.167	0.00	0.03	0.100	O	|	|	|	|	0.08
146.250	0.00	0.03	0.100	O	|	|	|	|	0.08
146.333	0.00	0.03	0.099	O	|	|	|	|	0.08
146.417	0.00	0.03	0.099	O	|	|	|	|	0.08
146.500	0.00	0.03	0.099	O	|	|	|	|	0.08
146.583	0.00	0.03	0.099	O	|	|	|	|	0.08
146.667	0.00	0.03	0.099	O	|	|	|	|	0.08
146.750	0.00	0.03	0.098	O	|	|	|	|	0.08
146.833	0.00	0.03	0.098	O	|	|	|	|	0.08
146.917	0.00	0.03	0.098	O	|	|	|	|	0.08
147.000	0.00	0.03	0.098	O	|	|	|	|	0.08
147.083	0.00	0.03	0.098	O	|	|	|	|	0.08
147.167	0.00	0.03	0.097	O	|	|	|	|	0.08
147.250	0.00	0.03	0.097	O	|	|	|	|	0.08
147.333	0.00	0.03	0.097	O	|	|	|	|	0.08
147.417	0.00	0.03	0.097	O	|	|	|	|	0.08
147.500	0.00	0.03	0.097	O	|	|	|	|	0.08
147.583	0.00	0.03	0.097	O	|	|	|	|	0.08
147.667	0.00	0.03	0.096	O	|	|	|	|	0.08
147.750	0.00	0.03	0.096	O	|	|	|	|	0.08
147.833	0.00	0.03	0.096	O	|	|	|	|	0.08
147.917	0.00	0.03	0.096	O	|	|	|	|	0.08
148.000	0.00	0.03	0.096	O	|	|	|	|	0.08
148.083	0.00	0.03	0.095	O	|	|	|	|	0.08

148.167	0.00	0.03	0.095	O	|	|	|	|	0.08
148.250	0.00	0.03	0.095	O	|	|	|	|	0.08
148.333	0.00	0.03	0.095	O	|	|	|	|	0.08
148.417	0.00	0.03	0.095	O	|	|	|	|	0.08
148.500	0.00	0.03	0.095	O	|	|	|	|	0.08
148.583	0.00	0.03	0.094	O	|	|	|	|	0.08
148.667	0.00	0.03	0.094	O	|	|	|	|	0.08
148.750	0.00	0.03	0.094	O	|	|	|	|	0.08
148.833	0.00	0.03	0.094	O	|	|	|	|	0.08
148.917	0.00	0.03	0.094	O	|	|	|	|	0.08
149.000	0.00	0.03	0.093	O	|	|	|	|	0.08
149.083	0.00	0.03	0.093	O	|	|	|	|	0.08
149.167	0.00	0.03	0.093	O	|	|	|	|	0.08
149.250	0.00	0.03	0.093	O	|	|	|	|	0.08
149.333	0.00	0.03	0.093	O	|	|	|	|	0.08
149.417	0.00	0.03	0.093	O	|	|	|	|	0.08
149.500	0.00	0.03	0.092	O	|	|	|	|	0.07
149.583	0.00	0.03	0.092	O	|	|	|	|	0.07
149.667	0.00	0.03	0.092	O	|	|	|	|	0.07
149.750	0.00	0.03	0.092	O	|	|	|	|	0.07
149.833	0.00	0.03	0.092	O	|	|	|	|	0.07
149.917	0.00	0.03	0.091	O	|	|	|	|	0.07
150.000	0.00	0.03	0.091	O	|	|	|	|	0.07
150.083	0.00	0.03	0.091	O	|	|	|	|	0.07
150.167	0.00	0.03	0.091	O	|	|	|	|	0.07
150.250	0.00	0.03	0.091	O	|	|	|	|	0.07
150.333	0.00	0.03	0.091	O	|	|	|	|	0.07
150.417	0.00	0.03	0.090	O	|	|	|	|	0.07
150.500	0.00	0.03	0.090	O	|	|	|	|	0.07
150.583	0.00	0.03	0.090	O	|	|	|	|	0.07
150.667	0.00	0.03	0.090	O	|	|	|	|	0.07
150.750	0.00	0.03	0.090	O	|	|	|	|	0.07
150.833	0.00	0.03	0.090	O	|	|	|	|	0.07
150.917	0.00	0.02	0.089	O	|	|	|	|	0.07
151.000	0.00	0.02	0.089	O	|	|	|	|	0.07
151.083	0.00	0.02	0.089	O	|	|	|	|	0.07
151.167	0.00	0.02	0.089	O	|	|	|	|	0.07
151.250	0.00	0.02	0.089	O	|	|	|	|	0.07
151.333	0.00	0.02	0.089	O	|	|	|	|	0.07
151.417	0.00	0.02	0.088	O	|	|	|	|	0.07
151.500	0.00	0.02	0.088	O	|	|	|	|	0.07
151.583	0.00	0.02	0.088	O	|	|	|	|	0.07
151.667	0.00	0.02	0.088	O	|	|	|	|	0.07
151.750	0.00	0.02	0.088	O	|	|	|	|	0.07
151.833	0.00	0.02	0.088	O	|	|	|	|	0.07
151.917	0.00	0.02	0.087	O	|	|	|	|	0.07
152.000	0.00	0.02	0.087	O	|	|	|	|	0.07
152.083	0.00	0.02	0.087	O	|	|	|	|	0.07
152.167	0.00	0.02	0.087	O	|	|	|	|	0.07
152.250	0.00	0.02	0.087	O	|	|	|	|	0.07
152.333	0.00	0.02	0.087	O	|	|	|	|	0.07
152.417	0.00	0.02	0.086	O	|	|	|	|	0.07
152.500	0.00	0.02	0.086	O	|	|	|	|	0.07
152.583	0.00	0.02	0.086	O	|	|	|	|	0.07
152.667	0.00	0.02	0.086	O	|	|	|	|	0.07
152.750	0.00	0.02	0.086	O	|	|	|	|	0.07
152.833	0.00	0.02	0.086	O	|	|	|	|	0.07
152.917	0.00	0.02	0.085	O	|	|	|	|	0.07
153.000	0.00	0.02	0.085	O	|	|	|	|	0.07
153.083	0.00	0.02	0.085	O	|	|	|	|	0.07
153.167	0.00	0.02	0.085	O	|	|	|	|	0.07
153.250	0.00	0.02	0.085	O	|	|	|	|	0.07
153.333	0.00	0.02	0.085	O	|	|	|	|	0.07
153.417	0.00	0.02	0.084	O	|	|	|	|	0.07
153.500	0.00	0.02	0.084	O	|	|	|	|	0.07
153.583	0.00	0.02	0.084	O	|	|	|	|	0.07
153.667	0.00	0.02	0.084	O	|	|	|	|	0.07
153.750	0.00	0.02	0.084	O	|	|	|	|	0.07
153.833	0.00	0.02	0.084	O	|	|	|	|	0.07
153.917	0.00	0.02	0.083	O	|	|	|	|	0.07
154.000	0.00	0.02	0.083	O	|	|	|	|	0.07

154.083	0.00	0.02	0.083	O	|	|	|	|	0.07
154.167	0.00	0.02	0.083	O	|	|	|	|	0.07
154.250	0.00	0.02	0.083	O	|	|	|	|	0.07
154.333	0.00	0.02	0.083	O	|	|	|	|	0.07
154.417	0.00	0.02	0.082	O	|	|	|	|	0.07
154.500	0.00	0.02	0.082	O	|	|	|	|	0.07
154.583	0.00	0.02	0.082	O	|	|	|	|	0.07
154.667	0.00	0.02	0.082	O	|	|	|	|	0.07
154.750	0.00	0.02	0.082	O	|	|	|	|	0.07
154.833	0.00	0.02	0.082	O	|	|	|	|	0.07
154.917	0.00	0.02	0.081	O	|	|	|	|	0.07
155.000	0.00	0.02	0.081	O	|	|	|	|	0.07
155.083	0.00	0.02	0.081	O	|	|	|	|	0.07
155.167	0.00	0.02	0.081	O	|	|	|	|	0.07
155.250	0.00	0.02	0.081	O	|	|	|	|	0.07
155.333	0.00	0.02	0.081	O	|	|	|	|	0.07
155.417	0.00	0.02	0.081	O	|	|	|	|	0.07
155.500	0.00	0.02	0.080	O	|	|	|	|	0.07
155.583	0.00	0.02	0.080	O	|	|	|	|	0.07
155.667	0.00	0.02	0.080	O	|	|	|	|	0.07
155.750	0.00	0.02	0.080	O	|	|	|	|	0.06
155.833	0.00	0.02	0.080	O	|	|	|	|	0.06
155.917	0.00	0.02	0.080	O	|	|	|	|	0.06
156.000	0.00	0.02	0.079	O	|	|	|	|	0.06
156.083	0.00	0.02	0.079	O	|	|	|	|	0.06
156.167	0.00	0.02	0.079	O	|	|	|	|	0.06
156.250	0.00	0.02	0.079	O	|	|	|	|	0.06
156.333	0.00	0.02	0.079	O	|	|	|	|	0.06
156.417	0.00	0.02	0.079	O	|	|	|	|	0.06
156.500	0.00	0.02	0.079	O	|	|	|	|	0.06
156.583	0.00	0.02	0.078	O	|	|	|	|	0.06
156.667	0.00	0.02	0.078	O	|	|	|	|	0.06
156.750	0.00	0.02	0.078	O	|	|	|	|	0.06
156.833	0.00	0.02	0.078	O	|	|	|	|	0.06
156.917	0.00	0.02	0.078	O	|	|	|	|	0.06
157.000	0.00	0.02	0.078	O	|	|	|	|	0.06
157.083	0.00	0.02	0.078	O	|	|	|	|	0.06
157.167	0.00	0.02	0.077	O	|	|	|	|	0.06
157.250	0.00	0.02	0.077	O	|	|	|	|	0.06
157.333	0.00	0.02	0.077	O	|	|	|	|	0.06
157.417	0.00	0.02	0.077	O	|	|	|	|	0.06
157.500	0.00	0.02	0.077	O	|	|	|	|	0.06
157.583	0.00	0.02	0.077	O	|	|	|	|	0.06
157.667	0.00	0.02	0.076	O	|	|	|	|	0.06
157.750	0.00	0.02	0.076	O	|	|	|	|	0.06
157.833	0.00	0.02	0.076	O	|	|	|	|	0.06
157.917	0.00	0.02	0.076	O	|	|	|	|	0.06
158.000	0.00	0.02	0.076	O	|	|	|	|	0.06
158.083	0.00	0.02	0.076	O	|	|	|	|	0.06
158.167	0.00	0.02	0.076	O	|	|	|	|	0.06
158.250	0.00	0.02	0.075	O	|	|	|	|	0.06
158.333	0.00	0.02	0.075	O	|	|	|	|	0.06
158.417	0.00	0.02	0.075	O	|	|	|	|	0.06
158.500	0.00	0.02	0.075	O	|	|	|	|	0.06
158.583	0.00	0.02	0.075	O	|	|	|	|	0.06
158.667	0.00	0.02	0.075	O	|	|	|	|	0.06
158.750	0.00	0.02	0.075	O	|	|	|	|	0.06
158.833	0.00	0.02	0.074	O	|	|	|	|	0.06
158.917	0.00	0.02	0.074	O	|	|	|	|	0.06
159.000	0.00	0.02	0.074	O	|	|	|	|	0.06
159.083	0.00	0.02	0.074	O	|	|	|	|	0.06
159.167	0.00	0.02	0.074	O	|	|	|	|	0.06
159.250	0.00	0.02	0.074	O	|	|	|	|	0.06
159.333	0.00	0.02	0.074	O	|	|	|	|	0.06
159.417	0.00	0.02	0.073	O	|	|	|	|	0.06
159.500	0.00	0.02	0.073	O	|	|	|	|	0.06
159.583	0.00	0.02	0.073	O	|	|	|	|	0.06
159.667	0.00	0.02	0.073	O	|	|	|	|	0.06
159.750	0.00	0.02	0.073	O	|	|	|	|	0.06
159.833	0.00	0.02	0.073	O	|	|	|	|	0.06
159.917	0.00	0.02	0.073	O	|	|	|	|	0.06

160.000	0.00	0.02	0.072	O	|	|	|	0.06
160.083	0.00	0.02	0.072	O	|	|	|	0.06
160.167	0.00	0.02	0.072	O	|	|	|	0.06
160.250	0.00	0.02	0.072	O	|	|	|	0.06
160.333	0.00	0.02	0.072	O	|	|	|	0.06
160.417	0.00	0.02	0.072	O	|	|	|	0.06
160.500	0.00	0.02	0.072	O	|	|	|	0.06
160.583	0.00	0.02	0.072	O	|	|	|	0.06
160.667	0.00	0.02	0.071	O	|	|	|	0.06
160.750	0.00	0.02	0.071	O	|	|	|	0.06
160.833	0.00	0.02	0.071	O	|	|	|	0.06
160.917	0.00	0.02	0.071	O	|	|	|	0.06
161.000	0.00	0.02	0.071	O	|	|	|	0.06
161.083	0.00	0.02	0.071	O	|	|	|	0.06
161.167	0.00	0.02	0.071	O	|	|	|	0.06
161.250	0.00	0.02	0.070	O	|	|	|	0.06
161.333	0.00	0.02	0.070	O	|	|	|	0.06
161.417	0.00	0.02	0.070	O	|	|	|	0.06
161.500	0.00	0.02	0.070	O	|	|	|	0.06
161.583	0.00	0.02	0.070	O	|	|	|	0.06
161.667	0.00	0.02	0.070	O	|	|	|	0.06
161.750	0.00	0.02	0.070	O	|	|	|	0.06
161.833	0.00	0.02	0.069	O	|	|	|	0.06
161.917	0.00	0.02	0.069	O	|	|	|	0.06
162.000	0.00	0.02	0.069	O	|	|	|	0.06
162.083	0.00	0.02	0.069	O	|	|	|	0.06
162.167	0.00	0.02	0.069	O	|	|	|	0.06
162.250	0.00	0.02	0.069	O	|	|	|	0.06
162.333	0.00	0.02	0.069	O	|	|	|	0.06
162.417	0.00	0.02	0.069	O	|	|	|	0.06
162.500	0.00	0.02	0.068	O	|	|	|	0.06
162.583	0.00	0.02	0.068	O	|	|	|	0.06
162.667	0.00	0.02	0.068	O	|	|	|	0.06
162.750	0.00	0.02	0.068	O	|	|	|	0.06
162.833	0.00	0.02	0.068	O	|	|	|	0.06
162.917	0.00	0.02	0.068	O	|	|	|	0.05
163.000	0.00	0.02	0.068	O	|	|	|	0.05
163.083	0.00	0.02	0.067	O	|	|	|	0.05
163.167	0.00	0.02	0.067	O	|	|	|	0.05
163.250	0.00	0.02	0.067	O	|	|	|	0.05
163.333	0.00	0.02	0.067	O	|	|	|	0.05
163.417	0.00	0.02	0.067	O	|	|	|	0.05
163.500	0.00	0.02	0.067	O	|	|	|	0.05
163.583	0.00	0.02	0.067	O	|	|	|	0.05
163.667	0.00	0.02	0.067	O	|	|	|	0.05
163.750	0.00	0.02	0.066	O	|	|	|	0.05
163.833	0.00	0.02	0.066	O	|	|	|	0.05
163.917	0.00	0.02	0.066	O	|	|	|	0.05
164.000	0.00	0.02	0.066	O	|	|	|	0.05
164.083	0.00	0.02	0.066	O	|	|	|	0.05
164.167	0.00	0.02	0.066	O	|	|	|	0.05
164.250	0.00	0.02	0.066	O	|	|	|	0.05
164.333	0.00	0.02	0.066	O	|	|	|	0.05
164.417	0.00	0.02	0.065	O	|	|	|	0.05
164.500	0.00	0.02	0.065	O	|	|	|	0.05
164.583	0.00	0.02	0.065	O	|	|	|	0.05
164.667	0.00	0.02	0.065	O	|	|	|	0.05
164.750	0.00	0.02	0.065	O	|	|	|	0.05
164.833	0.00	0.02	0.065	O	|	|	|	0.05
164.917	0.00	0.02	0.065	O	|	|	|	0.05
165.000	0.00	0.02	0.065	O	|	|	|	0.05
165.083	0.00	0.02	0.064	O	|	|	|	0.05
165.167	0.00	0.02	0.064	O	|	|	|	0.05
165.250	0.00	0.02	0.064	O	|	|	|	0.05
165.333	0.00	0.02	0.064	O	|	|	|	0.05
165.417	0.00	0.02	0.064	O	|	|	|	0.05
165.500	0.00	0.02	0.064	O	|	|	|	0.05
165.583	0.00	0.02	0.064	O	|	|	|	0.05
165.667	0.00	0.02	0.064	O	|	|	|	0.05
165.750	0.00	0.02	0.063	O	|	|	|	0.05
165.833	0.00	0.02	0.063	O	|	|	|	0.05

165.917	0.00	0.02	0.063	O	|	|	|	|	0.05
166.000	0.00	0.02	0.063	O	|	|	|	|	0.05
166.083	0.00	0.02	0.063	O	|	|	|	|	0.05
166.167	0.00	0.02	0.063	O	|	|	|	|	0.05
166.250	0.00	0.02	0.063	O	|	|	|	|	0.05
166.333	0.00	0.02	0.063	O	|	|	|	|	0.05
166.417	0.00	0.02	0.062	O	|	|	|	|	0.05
166.500	0.00	0.02	0.062	O	|	|	|	|	0.05
166.583	0.00	0.02	0.062	O	|	|	|	|	0.05
166.667	0.00	0.02	0.062	O	|	|	|	|	0.05
166.750	0.00	0.02	0.062	O	|	|	|	|	0.05
166.833	0.00	0.02	0.062	O	|	|	|	|	0.05
166.917	0.00	0.02	0.062	O	|	|	|	|	0.05
167.000	0.00	0.02	0.062	O	|	|	|	|	0.05
167.083	0.00	0.02	0.062	O	|	|	|	|	0.05
167.167	0.00	0.02	0.061	O	|	|	|	|	0.05
167.250	0.00	0.02	0.061	O	|	|	|	|	0.05
167.333	0.00	0.02	0.061	O	|	|	|	|	0.05
167.417	0.00	0.02	0.061	O	|	|	|	|	0.05
167.500	0.00	0.02	0.061	O	|	|	|	|	0.05
167.583	0.00	0.02	0.061	O	|	|	|	|	0.05
167.667	0.00	0.02	0.061	O	|	|	|	|	0.05
167.750	0.00	0.02	0.061	O	|	|	|	|	0.05
167.833	0.00	0.02	0.060	O	|	|	|	|	0.05
167.917	0.00	0.02	0.060	O	|	|	|	|	0.05
168.000	0.00	0.02	0.060	O	|	|	|	|	0.05
168.083	0.00	0.02	0.060	O	|	|	|	|	0.05
168.167	0.00	0.02	0.060	O	|	|	|	|	0.05
168.250	0.00	0.02	0.060	O	|	|	|	|	0.05
168.333	0.00	0.02	0.060	O	|	|	|	|	0.05
168.417	0.00	0.02	0.060	O	|	|	|	|	0.05
168.500	0.00	0.02	0.060	O	|	|	|	|	0.05
168.583	0.00	0.02	0.059	O	|	|	|	|	0.05
168.667	0.00	0.02	0.059	O	|	|	|	|	0.05
168.750	0.00	0.02	0.059	O	|	|	|	|	0.05
168.833	0.00	0.02	0.059	O	|	|	|	|	0.05
168.917	0.00	0.02	0.059	O	|	|	|	|	0.05
169.000	0.00	0.02	0.059	O	|	|	|	|	0.05
169.083	0.00	0.02	0.059	O	|	|	|	|	0.05
169.167	0.00	0.02	0.059	O	|	|	|	|	0.05
169.250	0.00	0.02	0.059	O	|	|	|	|	0.05
169.333	0.00	0.02	0.058	O	|	|	|	|	0.05
169.417	0.00	0.02	0.058	O	|	|	|	|	0.05
169.500	0.00	0.02	0.058	O	|	|	|	|	0.05
169.583	0.00	0.02	0.058	O	|	|	|	|	0.05
169.667	0.00	0.02	0.058	O	|	|	|	|	0.05
169.750	0.00	0.02	0.058	O	|	|	|	|	0.05
169.833	0.00	0.02	0.058	O	|	|	|	|	0.05
169.917	0.00	0.02	0.058	O	|	|	|	|	0.05
170.000	0.00	0.02	0.058	O	|	|	|	|	0.05
170.083	0.00	0.02	0.057	O	|	|	|	|	0.05
170.167	0.00	0.02	0.057	O	|	|	|	|	0.05
170.250	0.00	0.02	0.057	O	|	|	|	|	0.05
170.333	0.00	0.02	0.057	O	|	|	|	|	0.05
170.417	0.00	0.02	0.057	O	|	|	|	|	0.05
170.500	0.00	0.02	0.057	O	|	|	|	|	0.05
170.583	0.00	0.02	0.057	O	|	|	|	|	0.05
170.667	0.00	0.02	0.057	O	|	|	|	|	0.05
170.750	0.00	0.02	0.057	O	|	|	|	|	0.05
170.833	0.00	0.02	0.056	O	|	|	|	|	0.05
170.917	0.00	0.02	0.056	O	|	|	|	|	0.05
171.000	0.00	0.02	0.056	O	|	|	|	|	0.05
171.083	0.00	0.02	0.056	O	|	|	|	|	0.05
171.167	0.00	0.02	0.056	O	|	|	|	|	0.05
171.250	0.00	0.02	0.056	O	|	|	|	|	0.05
171.333	0.00	0.02	0.056	O	|	|	|	|	0.05
171.417	0.00	0.02	0.056	O	|	|	|	|	0.05
171.500	0.00	0.02	0.056	O	|	|	|	|	0.05
171.583	0.00	0.02	0.055	O	|	|	|	|	0.05
171.667	0.00	0.02	0.055	O	|	|	|	|	0.04
171.750	0.00	0.02	0.055	O	|	|	|	|	0.04

171.833	0.00	0.02	0.055	O	|	|	|	|	0.04
171.917	0.00	0.02	0.055	O	|	|	|	|	0.04
172.000	0.00	0.02	0.055	O	|	|	|	|	0.04
172.083	0.00	0.02	0.055	O	|	|	|	|	0.04
172.167	0.00	0.02	0.055	O	|	|	|	|	0.04
172.250	0.00	0.02	0.055	O	|	|	|	|	0.04
172.333	0.00	0.02	0.055	O	|	|	|	|	0.04
172.417	0.00	0.02	0.054	O	|	|	|	|	0.04
172.500	0.00	0.02	0.054	O	|	|	|	|	0.04
172.583	0.00	0.02	0.054	O	|	|	|	|	0.04
172.667	0.00	0.02	0.054	O	|	|	|	|	0.04
172.750	0.00	0.02	0.054	O	|	|	|	|	0.04
172.833	0.00	0.02	0.054	O	|	|	|	|	0.04
172.917	0.00	0.02	0.054	O	|	|	|	|	0.04
173.000	0.00	0.01	0.054	O	|	|	|	|	0.04
173.083	0.00	0.01	0.054	O	|	|	|	|	0.04
173.167	0.00	0.01	0.053	O	|	|	|	|	0.04
173.250	0.00	0.01	0.053	O	|	|	|	|	0.04
173.333	0.00	0.01	0.053	O	|	|	|	|	0.04
173.417	0.00	0.01	0.053	O	|	|	|	|	0.04
173.500	0.00	0.01	0.053	O	|	|	|	|	0.04
173.583	0.00	0.01	0.053	O	|	|	|	|	0.04
173.667	0.00	0.01	0.053	O	|	|	|	|	0.04
173.750	0.00	0.01	0.053	O	|	|	|	|	0.04
173.833	0.00	0.01	0.053	O	|	|	|	|	0.04
173.917	0.00	0.01	0.053	O	|	|	|	|	0.04
174.000	0.00	0.01	0.052	O	|	|	|	|	0.04
174.083	0.00	0.01	0.052	O	|	|	|	|	0.04
174.167	0.00	0.01	0.052	O	|	|	|	|	0.04
174.250	0.00	0.01	0.052	O	|	|	|	|	0.04
174.333	0.00	0.01	0.052	O	|	|	|	|	0.04
174.417	0.00	0.01	0.052	O	|	|	|	|	0.04
174.500	0.00	0.01	0.052	O	|	|	|	|	0.04
174.583	0.00	0.01	0.052	O	|	|	|	|	0.04
174.667	0.00	0.01	0.052	O	|	|	|	|	0.04
174.750	0.00	0.01	0.052	O	|	|	|	|	0.04
174.833	0.00	0.01	0.051	O	|	|	|	|	0.04
174.917	0.00	0.01	0.051	O	|	|	|	|	0.04
175.000	0.00	0.01	0.051	O	|	|	|	|	0.04
175.083	0.00	0.01	0.051	O	|	|	|	|	0.04
175.167	0.00	0.01	0.051	O	|	|	|	|	0.04
175.250	0.00	0.01	0.051	O	|	|	|	|	0.04
175.333	0.00	0.01	0.051	O	|	|	|	|	0.04
175.417	0.00	0.01	0.051	O	|	|	|	|	0.04
175.500	0.00	0.01	0.051	O	|	|	|	|	0.04
175.583	0.00	0.01	0.051	O	|	|	|	|	0.04
175.667	0.00	0.01	0.050	O	|	|	|	|	0.04
175.750	0.00	0.01	0.050	O	|	|	|	|	0.04
175.833	0.00	0.01	0.050	O	|	|	|	|	0.04
175.917	0.00	0.01	0.050	O	|	|	|	|	0.04
176.000	0.00	0.01	0.050	O	|	|	|	|	0.04
176.083	0.00	0.01	0.050	O	|	|	|	|	0.04
176.167	0.00	0.01	0.050	O	|	|	|	|	0.04
176.250	0.00	0.01	0.050	O	|	|	|	|	0.04
176.333	0.00	0.01	0.050	O	|	|	|	|	0.04
176.417	0.00	0.01	0.050	O	|	|	|	|	0.04
176.500	0.00	0.01	0.050	O	|	|	|	|	0.04
176.583	0.00	0.01	0.049	O	|	|	|	|	0.04
176.667	0.00	0.01	0.049	O	|	|	|	|	0.04
176.750	0.00	0.01	0.049	O	|	|	|	|	0.04
176.833	0.00	0.01	0.049	O	|	|	|	|	0.04
176.917	0.00	0.01	0.049	O	|	|	|	|	0.04
177.000	0.00	0.01	0.049	O	|	|	|	|	0.04
177.083	0.00	0.01	0.049	O	|	|	|	|	0.04
177.167	0.00	0.01	0.049	O	|	|	|	|	0.04
177.250	0.00	0.01	0.049	O	|	|	|	|	0.04
177.333	0.00	0.01	0.049	O	|	|	|	|	0.04
177.417	0.00	0.01	0.048	O	|	|	|	|	0.04
177.500	0.00	0.01	0.048	O	|	|	|	|	0.04
177.583	0.00	0.01	0.048	O	|	|	|	|	0.04
177.667	0.00	0.01	0.048	O	|	|	|	|	0.04

177.750	0.00	0.01	0.048	O	|	|	|	|	0.04
177.833	0.00	0.01	0.048	O	|	|	|	|	0.04
177.917	0.00	0.01	0.048	O	|	|	|	|	0.04
178.000	0.00	0.01	0.048	O	|	|	|	|	0.04
178.083	0.00	0.01	0.048	O	|	|	|	|	0.04
178.167	0.00	0.01	0.048	O	|	|	|	|	0.04
178.250	0.00	0.01	0.048	O	|	|	|	|	0.04
178.333	0.00	0.01	0.047	O	|	|	|	|	0.04
178.417	0.00	0.01	0.047	O	|	|	|	|	0.04
178.500	0.00	0.01	0.047	O	|	|	|	|	0.04
178.583	0.00	0.01	0.047	O	|	|	|	|	0.04
178.667	0.00	0.01	0.047	O	|	|	|	|	0.04
178.750	0.00	0.01	0.047	O	|	|	|	|	0.04
178.833	0.00	0.01	0.047	O	|	|	|	|	0.04
178.917	0.00	0.01	0.047	O	|	|	|	|	0.04
179.000	0.00	0.01	0.047	O	|	|	|	|	0.04
179.083	0.00	0.01	0.047	O	|	|	|	|	0.04
179.167	0.00	0.01	0.047	O	|	|	|	|	0.04
179.250	0.00	0.01	0.046	O	|	|	|	|	0.04
179.333	0.00	0.01	0.046	O	|	|	|	|	0.04
179.417	0.00	0.01	0.046	O	|	|	|	|	0.04
179.500	0.00	0.01	0.046	O	|	|	|	|	0.04
179.583	0.00	0.01	0.046	O	|	|	|	|	0.04
179.667	0.00	0.01	0.046	O	|	|	|	|	0.04
179.750	0.00	0.01	0.046	O	|	|	|	|	0.04
179.833	0.00	0.01	0.046	O	|	|	|	|	0.04
179.917	0.00	0.01	0.046	O	|	|	|	|	0.04
180.000	0.00	0.01	0.046	O	|	|	|	|	0.04
180.083	0.00	0.01	0.046	O	|	|	|	|	0.04
180.167	0.00	0.01	0.046	O	|	|	|	|	0.04
180.250	0.00	0.01	0.045	O	|	|	|	|	0.04
180.333	0.00	0.01	0.045	O	|	|	|	|	0.04
180.417	0.00	0.01	0.045	O	|	|	|	|	0.04
180.500	0.00	0.01	0.045	O	|	|	|	|	0.04
180.583	0.00	0.01	0.045	O	|	|	|	|	0.04
180.667	0.00	0.01	0.045	O	|	|	|	|	0.04
180.750	0.00	0.01	0.045	O	|	|	|	|	0.04
180.833	0.00	0.01	0.045	O	|	|	|	|	0.04
180.917	0.00	0.01	0.045	O	|	|	|	|	0.04
181.000	0.00	0.01	0.045	O	|	|	|	|	0.04
181.083	0.00	0.01	0.045	O	|	|	|	|	0.04
181.167	0.00	0.01	0.044	O	|	|	|	|	0.04
181.250	0.00	0.01	0.044	O	|	|	|	|	0.04
181.333	0.00	0.01	0.044	O	|	|	|	|	0.04
181.417	0.00	0.01	0.044	O	|	|	|	|	0.04
181.500	0.00	0.01	0.044	O	|	|	|	|	0.04
181.583	0.00	0.01	0.044	O	|	|	|	|	0.04
181.667	0.00	0.01	0.044	O	|	|	|	|	0.04
181.750	0.00	0.01	0.044	O	|	|	|	|	0.04
181.833	0.00	0.01	0.044	O	|	|	|	|	0.04
181.917	0.00	0.01	0.044	O	|	|	|	|	0.04
182.000	0.00	0.01	0.044	O	|	|	|	|	0.04
182.083	0.00	0.01	0.044	O	|	|	|	|	0.04
182.167	0.00	0.01	0.043	O	|	|	|	|	0.04
182.250	0.00	0.01	0.043	O	|	|	|	|	0.04
182.333	0.00	0.01	0.043	O	|	|	|	|	0.04
182.417	0.00	0.01	0.043	O	|	|	|	|	0.04
182.500	0.00	0.01	0.043	O	|	|	|	|	0.04
182.583	0.00	0.01	0.043	O	|	|	|	|	0.03
182.667	0.00	0.01	0.043	O	|	|	|	|	0.03
182.750	0.00	0.01	0.043	O	|	|	|	|	0.03
182.833	0.00	0.01	0.043	O	|	|	|	|	0.03
182.917	0.00	0.01	0.043	O	|	|	|	|	0.03
183.000	0.00	0.01	0.043	O	|	|	|	|	0.03
183.083	0.00	0.01	0.043	O	|	|	|	|	0.03
183.167	0.00	0.01	0.042	O	|	|	|	|	0.03
183.250	0.00	0.01	0.042	O	|	|	|	|	0.03
183.333	0.00	0.01	0.042	O	|	|	|	|	0.03
183.417	0.00	0.01	0.042	O	|	|	|	|	0.03
183.500	0.00	0.01	0.042	O	|	|	|	|	0.03
183.583	0.00	0.01	0.042	O	|	|	|	|	0.03

183.667	0.00	0.01	0.042	O	|	|	|	|	0.03
183.750	0.00	0.01	0.042	O	|	|	|	|	0.03
183.833	0.00	0.01	0.042	O	|	|	|	|	0.03
183.917	0.00	0.01	0.042	O	|	|	|	|	0.03
184.000	0.00	0.01	0.042	O	|	|	|	|	0.03
184.083	0.00	0.01	0.042	O	|	|	|	|	0.03
184.167	0.00	0.01	0.041	O	|	|	|	|	0.03
184.250	0.00	0.01	0.041	O	|	|	|	|	0.03
184.333	0.00	0.01	0.041	O	|	|	|	|	0.03
184.417	0.00	0.01	0.041	O	|	|	|	|	0.03
184.500	0.00	0.01	0.041	O	|	|	|	|	0.03
184.583	0.00	0.01	0.041	O	|	|	|	|	0.03
184.667	0.00	0.01	0.041	O	|	|	|	|	0.03
184.750	0.00	0.01	0.041	O	|	|	|	|	0.03
184.833	0.00	0.01	0.041	O	|	|	|	|	0.03
184.917	0.00	0.01	0.041	O	|	|	|	|	0.03
185.000	0.00	0.01	0.041	O	|	|	|	|	0.03
185.083	0.00	0.01	0.041	O	|	|	|	|	0.03
185.167	0.00	0.01	0.041	O	|	|	|	|	0.03
185.250	0.00	0.01	0.040	O	|	|	|	|	0.03
185.333	0.00	0.01	0.040	O	|	|	|	|	0.03
185.417	0.00	0.01	0.040	O	|	|	|	|	0.03
185.500	0.00	0.01	0.040	O	|	|	|	|	0.03
185.583	0.00	0.01	0.040	O	|	|	|	|	0.03
185.667	0.00	0.01	0.040	O	|	|	|	|	0.03
185.750	0.00	0.01	0.040	O	|	|	|	|	0.03
185.833	0.00	0.01	0.040	O	|	|	|	|	0.03
185.917	0.00	0.01	0.040	O	|	|	|	|	0.03
186.000	0.00	0.01	0.040	O	|	|	|	|	0.03
186.083	0.00	0.01	0.040	O	|	|	|	|	0.03
186.167	0.00	0.01	0.040	O	|	|	|	|	0.03
186.250	0.00	0.01	0.040	O	|	|	|	|	0.03
186.333	0.00	0.01	0.039	O	|	|	|	|	0.03
186.417	0.00	0.01	0.039	O	|	|	|	|	0.03
186.500	0.00	0.01	0.039	O	|	|	|	|	0.03
186.583	0.00	0.01	0.039	O	|	|	|	|	0.03
186.667	0.00	0.01	0.039	O	|	|	|	|	0.03
186.750	0.00	0.01	0.039	O	|	|	|	|	0.03
186.833	0.00	0.01	0.039	O	|	|	|	|	0.03
186.917	0.00	0.01	0.039	O	|	|	|	|	0.03
187.000	0.00	0.01	0.039	O	|	|	|	|	0.03
187.083	0.00	0.01	0.039	O	|	|	|	|	0.03
187.167	0.00	0.01	0.039	O	|	|	|	|	0.03
187.250	0.00	0.01	0.039	O	|	|	|	|	0.03
187.333	0.00	0.01	0.039	O	|	|	|	|	0.03
187.417	0.00	0.01	0.038	O	|	|	|	|	0.03
187.500	0.00	0.01	0.038	O	|	|	|	|	0.03
187.583	0.00	0.01	0.038	O	|	|	|	|	0.03
187.667	0.00	0.01	0.038	O	|	|	|	|	0.03
187.750	0.00	0.01	0.038	O	|	|	|	|	0.03
187.833	0.00	0.01	0.038	O	|	|	|	|	0.03
187.917	0.00	0.01	0.038	O	|	|	|	|	0.03
188.000	0.00	0.01	0.038	O	|	|	|	|	0.03
188.083	0.00	0.01	0.038	O	|	|	|	|	0.03
188.167	0.00	0.01	0.038	O	|	|	|	|	0.03
188.250	0.00	0.01	0.038	O	|	|	|	|	0.03
188.333	0.00	0.01	0.038	O	|	|	|	|	0.03
188.417	0.00	0.01	0.038	O	|	|	|	|	0.03
188.500	0.00	0.01	0.038	O	|	|	|	|	0.03
188.583	0.00	0.01	0.037	O	|	|	|	|	0.03
188.667	0.00	0.01	0.037	O	|	|	|	|	0.03
188.750	0.00	0.01	0.037	O	|	|	|	|	0.03
188.833	0.00	0.01	0.037	O	|	|	|	|	0.03
188.917	0.00	0.01	0.037	O	|	|	|	|	0.03
189.000	0.00	0.01	0.037	O	|	|	|	|	0.03
189.083	0.00	0.01	0.037	O	|	|	|	|	0.03
189.167	0.00	0.01	0.037	O	|	|	|	|	0.03
189.250	0.00	0.01	0.037	O	|	|	|	|	0.03
189.333	0.00	0.01	0.037	O	|	|	|	|	0.03
189.417	0.00	0.01	0.037	O	|	|	|	|	0.03
189.500	0.00	0.01	0.037	O	|	|	|	|	0.03

189.583	0.00	0.01	0.037	O	|	|	|	|	0.03
189.667	0.00	0.01	0.037	O	|	|	|	|	0.03
189.750	0.00	0.01	0.036	O	|	|	|	|	0.03
189.833	0.00	0.01	0.036	O	|	|	|	|	0.03
189.917	0.00	0.01	0.036	O	|	|	|	|	0.03
190.000	0.00	0.01	0.036	O	|	|	|	|	0.03
190.083	0.00	0.01	0.036	O	|	|	|	|	0.03
190.167	0.00	0.01	0.036	O	|	|	|	|	0.03
190.250	0.00	0.01	0.036	O	|	|	|	|	0.03
190.333	0.00	0.01	0.036	O	|	|	|	|	0.03
190.417	0.00	0.01	0.036	O	|	|	|	|	0.03
190.500	0.00	0.01	0.036	O	|	|	|	|	0.03
190.583	0.00	0.01	0.036	O	|	|	|	|	0.03
190.667	0.00	0.01	0.036	O	|	|	|	|	0.03
190.750	0.00	0.01	0.036	O	|	|	|	|	0.03
190.833	0.00	0.01	0.036	O	|	|	|	|	0.03
190.917	0.00	0.01	0.036	O	|	|	|	|	0.03
191.000	0.00	0.01	0.035	O	|	|	|	|	0.03
191.083	0.00	0.01	0.035	O	|	|	|	|	0.03
191.167	0.00	0.01	0.035	O	|	|	|	|	0.03
191.250	0.00	0.01	0.035	O	|	|	|	|	0.03
191.333	0.00	0.01	0.035	O	|	|	|	|	0.03
191.417	0.00	0.01	0.035	O	|	|	|	|	0.03
191.500	0.00	0.01	0.035	O	|	|	|	|	0.03
191.583	0.00	0.01	0.035	O	|	|	|	|	0.03
191.667	0.00	0.01	0.035	O	|	|	|	|	0.03
191.750	0.00	0.01	0.035	O	|	|	|	|	0.03
191.833	0.00	0.01	0.035	O	|	|	|	|	0.03
191.917	0.00	0.01	0.035	O	|	|	|	|	0.03
192.000	0.00	0.01	0.035	O	|	|	|	|	0.03
192.083	0.00	0.01	0.035	O	|	|	|	|	0.03
192.167	0.00	0.01	0.034	O	|	|	|	|	0.03
192.250	0.00	0.01	0.034	O	|	|	|	|	0.03
192.333	0.00	0.01	0.034	O	|	|	|	|	0.03
192.417	0.00	0.01	0.034	O	|	|	|	|	0.03
192.500	0.00	0.01	0.034	O	|	|	|	|	0.03
192.583	0.00	0.01	0.034	O	|	|	|	|	0.03
192.667	0.00	0.01	0.034	O	|	|	|	|	0.03
192.750	0.00	0.01	0.034	O	|	|	|	|	0.03
192.833	0.00	0.01	0.034	O	|	|	|	|	0.03
192.917	0.00	0.01	0.034	O	|	|	|	|	0.03
193.000	0.00	0.01	0.034	O	|	|	|	|	0.03
193.083	0.00	0.01	0.034	O	|	|	|	|	0.03
193.167	0.00	0.01	0.034	O	|	|	|	|	0.03
193.250	0.00	0.01	0.034	O	|	|	|	|	0.03
193.333	0.00	0.01	0.034	O	|	|	|	|	0.03
193.417	0.00	0.01	0.034	O	|	|	|	|	0.03
193.500	0.00	0.01	0.033	O	|	|	|	|	0.03
193.583	0.00	0.01	0.033	O	|	|	|	|	0.03
193.667	0.00	0.01	0.033	O	|	|	|	|	0.03
193.750	0.00	0.01	0.033	O	|	|	|	|	0.03
193.833	0.00	0.01	0.033	O	|	|	|	|	0.03
193.917	0.00	0.01	0.033	O	|	|	|	|	0.03
194.000	0.00	0.01	0.033	O	|	|	|	|	0.03
194.083	0.00	0.01	0.033	O	|	|	|	|	0.03
194.167	0.00	0.01	0.033	O	|	|	|	|	0.03
194.250	0.00	0.01	0.033	O	|	|	|	|	0.03
194.333	0.00	0.01	0.033	O	|	|	|	|	0.03
194.417	0.00	0.01	0.033	O	|	|	|	|	0.03
194.500	0.00	0.01	0.033	O	|	|	|	|	0.03
194.583	0.00	0.01	0.033	O	|	|	|	|	0.03
194.667	0.00	0.01	0.033	O	|	|	|	|	0.03
194.750	0.00	0.01	0.033	O	|	|	|	|	0.03
194.833	0.00	0.01	0.032	O	|	|	|	|	0.03
194.917	0.00	0.01	0.032	O	|	|	|	|	0.03
195.000	0.00	0.01	0.032	O	|	|	|	|	0.03
195.083	0.00	0.01	0.032	O	|	|	|	|	0.03
195.167	0.00	0.01	0.032	O	|	|	|	|	0.03
195.250	0.00	0.01	0.032	O	|	|	|	|	0.03
195.333	0.00	0.01	0.032	O	|	|	|	|	0.03
195.417	0.00	0.01	0.032	O	|	|	|	|	0.03

195.500	0.00	0.01	0.032	O	|	|	|	|	0.03
195.583	0.00	0.01	0.032	O	|	|	|	|	0.03
195.667	0.00	0.01	0.032	O	|	|	|	|	0.03
195.750	0.00	0.01	0.032	O	|	|	|	|	0.03
195.833	0.00	0.01	0.032	O	|	|	|	|	0.03
195.917	0.00	0.01	0.032	O	|	|	|	|	0.03
196.000	0.00	0.01	0.032	O	|	|	|	|	0.03
196.083	0.00	0.01	0.032	O	|	|	|	|	0.03
196.167	0.00	0.01	0.031	O	|	|	|	|	0.03
196.250	0.00	0.01	0.031	O	|	|	|	|	0.03
196.333	0.00	0.01	0.031	O	|	|	|	|	0.03
196.417	0.00	0.01	0.031	O	|	|	|	|	0.03
196.500	0.00	0.01	0.031	O	|	|	|	|	0.03
196.583	0.00	0.01	0.031	O	|	|	|	|	0.03
196.667	0.00	0.01	0.031	O	|	|	|	|	0.03
196.750	0.00	0.01	0.031	O	|	|	|	|	0.03
196.833	0.00	0.01	0.031	O	|	|	|	|	0.03
196.917	0.00	0.01	0.031	O	|	|	|	|	0.03
197.000	0.00	0.01	0.031	O	|	|	|	|	0.03
197.083	0.00	0.01	0.031	O	|	|	|	|	0.02
197.167	0.00	0.01	0.031	O	|	|	|	|	0.02
197.250	0.00	0.01	0.031	O	|	|	|	|	0.02
197.333	0.00	0.01	0.031	O	|	|	|	|	0.02
197.417	0.00	0.01	0.031	O	|	|	|	|	0.02
197.500	0.00	0.01	0.031	O	|	|	|	|	0.02
197.583	0.00	0.01	0.030	O	|	|	|	|	0.02
197.667	0.00	0.01	0.030	O	|	|	|	|	0.02
197.750	0.00	0.01	0.030	O	|	|	|	|	0.02
197.833	0.00	0.01	0.030	O	|	|	|	|	0.02
197.917	0.00	0.01	0.030	O	|	|	|	|	0.02
198.000	0.00	0.01	0.030	O	|	|	|	|	0.02
198.083	0.00	0.01	0.030	O	|	|	|	|	0.02
198.167	0.00	0.01	0.030	O	|	|	|	|	0.02
198.250	0.00	0.01	0.030	O	|	|	|	|	0.02
198.333	0.00	0.01	0.030	O	|	|	|	|	0.02
198.417	0.00	0.01	0.030	O	|	|	|	|	0.02
198.500	0.00	0.01	0.030	O	|	|	|	|	0.02
198.583	0.00	0.01	0.030	O	|	|	|	|	0.02
198.667	0.00	0.01	0.030	O	|	|	|	|	0.02
198.750	0.00	0.01	0.030	O	|	|	|	|	0.02
198.833	0.00	0.01	0.030	O	|	|	|	|	0.02
198.917	0.00	0.01	0.030	O	|	|	|	|	0.02
199.000	0.00	0.01	0.029	O	|	|	|	|	0.02
199.083	0.00	0.01	0.029	O	|	|	|	|	0.02
199.167	0.00	0.01	0.029	O	|	|	|	|	0.02
199.250	0.00	0.01	0.029	O	|	|	|	|	0.02
199.333	0.00	0.01	0.029	O	|	|	|	|	0.02
199.417	0.00	0.01	0.029	O	|	|	|	|	0.02
199.500	0.00	0.01	0.029	O	|	|	|	|	0.02
199.583	0.00	0.01	0.029	O	|	|	|	|	0.02
199.667	0.00	0.01	0.029	O	|	|	|	|	0.02
199.750	0.00	0.01	0.029	O	|	|	|	|	0.02
199.833	0.00	0.01	0.029	O	|	|	|	|	0.02
199.917	0.00	0.01	0.029	O	|	|	|	|	0.02
200.000	0.00	0.01	0.029	O	|	|	|	|	0.02
200.083	0.00	0.01	0.029	O	|	|	|	|	0.02
200.167	0.00	0.01	0.029	O	|	|	|	|	0.02
200.250	0.00	0.01	0.029	O	|	|	|	|	0.02
200.333	0.00	0.01	0.029	O	|	|	|	|	0.02
200.417	0.00	0.01	0.029	O	|	|	|	|	0.02
200.500	0.00	0.01	0.028	O	|	|	|	|	0.02
200.583	0.00	0.01	0.028	O	|	|	|	|	0.02
200.667	0.00	0.01	0.028	O	|	|	|	|	0.02
200.750	0.00	0.01	0.028	O	|	|	|	|	0.02
200.833	0.00	0.01	0.028	O	|	|	|	|	0.02
200.917	0.00	0.01	0.028	O	|	|	|	|	0.02
201.000	0.00	0.01	0.028	O	|	|	|	|	0.02
201.083	0.00	0.01	0.028	O	|	|	|	|	0.02
201.167	0.00	0.01	0.028	O	|	|	|	|	0.02
201.250	0.00	0.01	0.028	O	|	|	|	|	0.02
201.333	0.00	0.01	0.028	O	|	|	|	|	0.02

201.417	0.00	0.01	0.028	O	|	|	|	|	0.02
201.500	0.00	0.01	0.028	O	|	|	|	|	0.02
201.583	0.00	0.01	0.028	O	|	|	|	|	0.02
201.667	0.00	0.01	0.028	O	|	|	|	|	0.02
201.750	0.00	0.01	0.028	O	|	|	|	|	0.02
201.833	0.00	0.01	0.028	O	|	|	|	|	0.02
201.917	0.00	0.01	0.028	O	|	|	|	|	0.02
202.000	0.00	0.01	0.027	O	|	|	|	|	0.02
202.083	0.00	0.01	0.027	O	|	|	|	|	0.02
202.167	0.00	0.01	0.027	O	|	|	|	|	0.02
202.250	0.00	0.01	0.027	O	|	|	|	|	0.02
202.333	0.00	0.01	0.027	O	|	|	|	|	0.02
202.417	0.00	0.01	0.027	O	|	|	|	|	0.02
202.500	0.00	0.01	0.027	O	|	|	|	|	0.02
202.583	0.00	0.01	0.027	O	|	|	|	|	0.02
202.667	0.00	0.01	0.027	O	|	|	|	|	0.02
202.750	0.00	0.01	0.027	O	|	|	|	|	0.02
202.833	0.00	0.01	0.027	O	|	|	|	|	0.02
202.917	0.00	0.01	0.027	O	|	|	|	|	0.02
203.000	0.00	0.01	0.027	O	|	|	|	|	0.02
203.083	0.00	0.01	0.027	O	|	|	|	|	0.02
203.167	0.00	0.01	0.027	O	|	|	|	|	0.02
203.250	0.00	0.01	0.027	O	|	|	|	|	0.02
203.333	0.00	0.01	0.027	O	|	|	|	|	0.02
203.417	0.00	0.01	0.027	O	|	|	|	|	0.02
203.500	0.00	0.01	0.027	O	|	|	|	|	0.02
203.583	0.00	0.01	0.027	O	|	|	|	|	0.02
203.667	0.00	0.01	0.026	O	|	|	|	|	0.02
203.750	0.00	0.01	0.026	O	|	|	|	|	0.02
203.833	0.00	0.01	0.026	O	|	|	|	|	0.02
203.917	0.00	0.01	0.026	O	|	|	|	|	0.02
204.000	0.00	0.01	0.026	O	|	|	|	|	0.02
204.083	0.00	0.01	0.026	O	|	|	|	|	0.02
204.167	0.00	0.01	0.026	O	|	|	|	|	0.02
204.250	0.00	0.01	0.026	O	|	|	|	|	0.02
204.333	0.00	0.01	0.026	O	|	|	|	|	0.02
204.417	0.00	0.01	0.026	O	|	|	|	|	0.02
204.500	0.00	0.01	0.026	O	|	|	|	|	0.02
204.583	0.00	0.01	0.026	O	|	|	|	|	0.02
204.667	0.00	0.01	0.026	O	|	|	|	|	0.02
204.750	0.00	0.01	0.026	O	|	|	|	|	0.02
204.833	0.00	0.01	0.026	O	|	|	|	|	0.02
204.917	0.00	0.01	0.026	O	|	|	|	|	0.02
205.000	0.00	0.01	0.026	O	|	|	|	|	0.02
205.083	0.00	0.01	0.026	O	|	|	|	|	0.02
205.167	0.00	0.01	0.026	O	|	|	|	|	0.02
205.250	0.00	0.01	0.026	O	|	|	|	|	0.02
205.333	0.00	0.01	0.025	O	|	|	|	|	0.02
205.417	0.00	0.01	0.025	O	|	|	|	|	0.02
205.500	0.00	0.01	0.025	O	|	|	|	|	0.02
205.583	0.00	0.01	0.025	O	|	|	|	|	0.02
205.667	0.00	0.01	0.025	O	|	|	|	|	0.02
205.750	0.00	0.01	0.025	O	|	|	|	|	0.02
205.833	0.00	0.01	0.025	O	|	|	|	|	0.02
205.917	0.00	0.01	0.025	O	|	|	|	|	0.02
206.000	0.00	0.01	0.025	O	|	|	|	|	0.02
206.083	0.00	0.01	0.025	O	|	|	|	|	0.02
206.167	0.00	0.01	0.025	O	|	|	|	|	0.02
206.250	0.00	0.01	0.025	O	|	|	|	|	0.02
206.333	0.00	0.01	0.025	O	|	|	|	|	0.02
206.417	0.00	0.01	0.025	O	|	|	|	|	0.02
206.500	0.00	0.01	0.025	O	|	|	|	|	0.02
206.583	0.00	0.01	0.025	O	|	|	|	|	0.02
206.667	0.00	0.01	0.025	O	|	|	|	|	0.02
206.750	0.00	0.01	0.025	O	|	|	|	|	0.02
206.833	0.00	0.01	0.025	O	|	|	|	|	0.02
206.917	0.00	0.01	0.025	O	|	|	|	|	0.02
207.000	0.00	0.01	0.024	O	|	|	|	|	0.02
207.083	0.00	0.01	0.024	O	|	|	|	|	0.02
207.167	0.00	0.01	0.024	O	|	|	|	|	0.02
207.250	0.00	0.01	0.024	O	|	|	|	|	0.02

207.333	0.00	0.01	0.024	O	|	|	|	|	0.02
207.417	0.00	0.01	0.024	O	|	|	|	|	0.02
207.500	0.00	0.01	0.024	O	|	|	|	|	0.02
207.583	0.00	0.01	0.024	O	|	|	|	|	0.02
207.667	0.00	0.01	0.024	O	|	|	|	|	0.02
207.750	0.00	0.01	0.024	O	|	|	|	|	0.02
207.833	0.00	0.01	0.024	O	|	|	|	|	0.02
207.917	0.00	0.01	0.024	O	|	|	|	|	0.02
208.000	0.00	0.01	0.024	O	|	|	|	|	0.02
208.083	0.00	0.01	0.024	O	|	|	|	|	0.02
208.167	0.00	0.01	0.024	O	|	|	|	|	0.02
208.250	0.00	0.01	0.024	O	|	|	|	|	0.02
208.333	0.00	0.01	0.024	O	|	|	|	|	0.02
208.417	0.00	0.01	0.024	O	|	|	|	|	0.02
208.500	0.00	0.01	0.024	O	|	|	|	|	0.02
208.583	0.00	0.01	0.024	O	|	|	|	|	0.02
208.667	0.00	0.01	0.024	O	|	|	|	|	0.02
208.750	0.00	0.01	0.024	O	|	|	|	|	0.02
208.833	0.00	0.01	0.023	O	|	|	|	|	0.02
208.917	0.00	0.01	0.023	O	|	|	|	|	0.02
209.000	0.00	0.01	0.023	O	|	|	|	|	0.02
209.083	0.00	0.01	0.023	O	|	|	|	|	0.02
209.167	0.00	0.01	0.023	O	|	|	|	|	0.02
209.250	0.00	0.01	0.023	O	|	|	|	|	0.02
209.333	0.00	0.01	0.023	O	|	|	|	|	0.02
209.417	0.00	0.01	0.023	O	|	|	|	|	0.02
209.500	0.00	0.01	0.023	O	|	|	|	|	0.02
209.583	0.00	0.01	0.023	O	|	|	|	|	0.02
209.667	0.00	0.01	0.023	O	|	|	|	|	0.02
209.750	0.00	0.01	0.023	O	|	|	|	|	0.02
209.833	0.00	0.01	0.023	O	|	|	|	|	0.02
209.917	0.00	0.01	0.023	O	|	|	|	|	0.02
210.000	0.00	0.01	0.023	O	|	|	|	|	0.02
210.083	0.00	0.01	0.023	O	|	|	|	|	0.02
210.167	0.00	0.01	0.023	O	|	|	|	|	0.02
210.250	0.00	0.01	0.023	O	|	|	|	|	0.02
210.333	0.00	0.01	0.023	O	|	|	|	|	0.02
210.417	0.00	0.01	0.023	O	|	|	|	|	0.02
210.500	0.00	0.01	0.023	O	|	|	|	|	0.02
210.583	0.00	0.01	0.023	O	|	|	|	|	0.02
210.667	0.00	0.01	0.023	O	|	|	|	|	0.02
210.750	0.00	0.01	0.022	O	|	|	|	|	0.02
210.833	0.00	0.01	0.022	O	|	|	|	|	0.02
210.917	0.00	0.01	0.022	O	|	|	|	|	0.02
211.000	0.00	0.01	0.022	O	|	|	|	|	0.02
211.083	0.00	0.01	0.022	O	|	|	|	|	0.02
211.167	0.00	0.01	0.022	O	|	|	|	|	0.02
211.250	0.00	0.01	0.022	O	|	|	|	|	0.02
211.333	0.00	0.01	0.022	O	|	|	|	|	0.02
211.417	0.00	0.01	0.022	O	|	|	|	|	0.02
211.500	0.00	0.01	0.022	O	|	|	|	|	0.02
211.583	0.00	0.01	0.022	O	|	|	|	|	0.02
211.667	0.00	0.01	0.022	O	|	|	|	|	0.02
211.750	0.00	0.01	0.022	O	|	|	|	|	0.02
211.833	0.00	0.01	0.022	O	|	|	|	|	0.02
211.917	0.00	0.01	0.022	O	|	|	|	|	0.02
212.000	0.00	0.01	0.022	O	|	|	|	|	0.02
212.083	0.00	0.01	0.022	O	|	|	|	|	0.02
212.167	0.00	0.01	0.022	O	|	|	|	|	0.02
212.250	0.00	0.01	0.022	O	|	|	|	|	0.02
212.333	0.00	0.01	0.022	O	|	|	|	|	0.02
212.417	0.00	0.01	0.022	O	|	|	|	|	0.02
212.500	0.00	0.01	0.022	O	|	|	|	|	0.02
212.583	0.00	0.01	0.022	O	|	|	|	|	0.02
212.667	0.00	0.01	0.021	O	|	|	|	|	0.02
212.750	0.00	0.01	0.021	O	|	|	|	|	0.02
212.833	0.00	0.01	0.021	O	|	|	|	|	0.02
212.917	0.00	0.01	0.021	O	|	|	|	|	0.02
213.000	0.00	0.01	0.021	O	|	|	|	|	0.02
213.083	0.00	0.01	0.021	O	|	|	|	|	0.02
213.167	0.00	0.01	0.021	O	|	|	|	|	0.02

213.250	0.00	0.01	0.021	O	|	|	|	|	0.02
213.333	0.00	0.01	0.021	O	|	|	|	|	0.02
213.417	0.00	0.01	0.021	O	|	|	|	|	0.02
213.500	0.00	0.01	0.021	O	|	|	|	|	0.02
213.583	0.00	0.01	0.021	O	|	|	|	|	0.02
213.667	0.00	0.01	0.021	O	|	|	|	|	0.02
213.750	0.00	0.01	0.021	O	|	|	|	|	0.02
213.833	0.00	0.01	0.021	O	|	|	|	|	0.02
213.917	0.00	0.01	0.021	O	|	|	|	|	0.02
214.000	0.00	0.01	0.021	O	|	|	|	|	0.02
214.083	0.00	0.01	0.021	O	|	|	|	|	0.02
214.167	0.00	0.01	0.021	O	|	|	|	|	0.02
214.250	0.00	0.01	0.021	O	|	|	|	|	0.02
214.333	0.00	0.01	0.021	O	|	|	|	|	0.02
214.417	0.00	0.01	0.021	O	|	|	|	|	0.02
214.500	0.00	0.01	0.021	O	|	|	|	|	0.02
214.583	0.00	0.01	0.021	O	|	|	|	|	0.02
214.667	0.00	0.01	0.021	O	|	|	|	|	0.02
214.750	0.00	0.01	0.020	O	|	|	|	|	0.02
214.833	0.00	0.01	0.020	O	|	|	|	|	0.02
214.917	0.00	0.01	0.020	O	|	|	|	|	0.02
215.000	0.00	0.01	0.020	O	|	|	|	|	0.02
215.083	0.00	0.01	0.020	O	|	|	|	|	0.02
215.167	0.00	0.01	0.020	O	|	|	|	|	0.02
215.250	0.00	0.01	0.020	O	|	|	|	|	0.02
215.333	0.00	0.01	0.020	O	|	|	|	|	0.02
215.417	0.00	0.01	0.020	O	|	|	|	|	0.02
215.500	0.00	0.01	0.020	O	|	|	|	|	0.02
215.583	0.00	0.01	0.020	O	|	|	|	|	0.02
215.667	0.00	0.01	0.020	O	|	|	|	|	0.02
215.750	0.00	0.01	0.020	O	|	|	|	|	0.02
215.833	0.00	0.01	0.020	O	|	|	|	|	0.02
215.917	0.00	0.01	0.020	O	|	|	|	|	0.02
216.000	0.00	0.01	0.020	O	|	|	|	|	0.02
216.083	0.00	0.01	0.020	O	|	|	|	|	0.02
216.167	0.00	0.01	0.020	O	|	|	|	|	0.02
216.250	0.00	0.01	0.020	O	|	|	|	|	0.02
216.333	0.00	0.01	0.020	O	|	|	|	|	0.02
216.417	0.00	0.01	0.020	O	|	|	|	|	0.02
216.500	0.00	0.01	0.020	O	|	|	|	|	0.02
216.583	0.00	0.01	0.020	O	|	|	|	|	0.02
216.667	0.00	0.01	0.020	O	|	|	|	|	0.02
216.750	0.00	0.01	0.020	O	|	|	|	|	0.02
216.833	0.00	0.01	0.020	O	|	|	|	|	0.02
216.917	0.00	0.01	0.019	O	|	|	|	|	0.02
217.000	0.00	0.01	0.019	O	|	|	|	|	0.02
217.083	0.00	0.01	0.019	O	|	|	|	|	0.02
217.167	0.00	0.01	0.019	O	|	|	|	|	0.02
217.250	0.00	0.01	0.019	O	|	|	|	|	0.02
217.333	0.00	0.01	0.019	O	|	|	|	|	0.02
217.417	0.00	0.01	0.019	O	|	|	|	|	0.02
217.500	0.00	0.01	0.019	O	|	|	|	|	0.02
217.583	0.00	0.01	0.019	O	|	|	|	|	0.02
217.667	0.00	0.01	0.019	O	|	|	|	|	0.02
217.750	0.00	0.01	0.019	O	|	|	|	|	0.02
217.833	0.00	0.01	0.019	O	|	|	|	|	0.02
217.917	0.00	0.01	0.019	O	|	|	|	|	0.02
218.000	0.00	0.01	0.019	O	|	|	|	|	0.02
218.083	0.00	0.01	0.019	O	|	|	|	|	0.02
218.167	0.00	0.01	0.019	O	|	|	|	|	0.02
218.250	0.00	0.01	0.019	O	|	|	|	|	0.02
218.333	0.00	0.01	0.019	O	|	|	|	|	0.02
218.417	0.00	0.01	0.019	O	|	|	|	|	0.02
218.500	0.00	0.01	0.019	O	|	|	|	|	0.02
218.583	0.00	0.01	0.019	O	|	|	|	|	0.02
218.667	0.00	0.01	0.019	O	|	|	|	|	0.02
218.750	0.00	0.01	0.019	O	|	|	|	|	0.02
218.833	0.00	0.01	0.019	O	|	|	|	|	0.02
218.917	0.00	0.01	0.019	O	|	|	|	|	0.02
219.000	0.00	0.01	0.019	O	|	|	|	|	0.02
219.083	0.00	0.01	0.019	O	|	|	|	|	0.02

219.167	0.00	0.01	0.019	O	|	|	|	|	0.02
219.250	0.00	0.01	0.018	O	|	|	|	|	0.01
219.333	0.00	0.01	0.018	O	|	|	|	|	0.01
219.417	0.00	0.01	0.018	O	|	|	|	|	0.01
219.500	0.00	0.01	0.018	O	|	|	|	|	0.01
219.583	0.00	0.01	0.018	O	|	|	|	|	0.01
219.667	0.00	0.01	0.018	O	|	|	|	|	0.01
219.750	0.00	0.01	0.018	O	|	|	|	|	0.01
219.833	0.00	0.01	0.018	O	|	|	|	|	0.01
219.917	0.00	0.01	0.018	O	|	|	|	|	0.01
220.000	0.00	0.01	0.018	O	|	|	|	|	0.01
220.083	0.00	0.01	0.018	O	|	|	|	|	0.01
220.167	0.00	0.01	0.018	O	|	|	|	|	0.01
220.250	0.00	0.01	0.018	O	|	|	|	|	0.01
220.333	0.00	0.01	0.018	O	|	|	|	|	0.01
220.417	0.00	0.01	0.018	O	|	|	|	|	0.01
220.500	0.00	0.01	0.018	O	|	|	|	|	0.01
220.583	0.00	0.01	0.018	O	|	|	|	|	0.01
220.667	0.00	0.00	0.018	O	|	|	|	|	0.01
220.750	0.00	0.00	0.018	O	|	|	|	|	0.01
220.833	0.00	0.00	0.018	O	|	|	|	|	0.01
220.917	0.00	0.00	0.018	O	|	|	|	|	0.01
221.000	0.00	0.00	0.018	O	|	|	|	|	0.01
221.083	0.00	0.00	0.018	O	|	|	|	|	0.01
221.167	0.00	0.00	0.018	O	|	|	|	|	0.01
221.250	0.00	0.00	0.018	O	|	|	|	|	0.01
221.333	0.00	0.00	0.018	O	|	|	|	|	0.01
221.417	0.00	0.00	0.018	O	|	|	|	|	0.01
221.500	0.00	0.00	0.018	O	|	|	|	|	0.01
221.583	0.00	0.00	0.017	O	|	|	|	|	0.01
221.667	0.00	0.00	0.017	O	|	|	|	|	0.01
221.750	0.00	0.00	0.017	O	|	|	|	|	0.01
221.833	0.00	0.00	0.017	O	|	|	|	|	0.01
221.917	0.00	0.00	0.017	O	|	|	|	|	0.01
222.000	0.00	0.00	0.017	O	|	|	|	|	0.01
222.083	0.00	0.00	0.017	O	|	|	|	|	0.01
222.167	0.00	0.00	0.017	O	|	|	|	|	0.01
222.250	0.00	0.00	0.017	O	|	|	|	|	0.01
222.333	0.00	0.00	0.017	O	|	|	|	|	0.01
222.417	0.00	0.00	0.017	O	|	|	|	|	0.01
222.500	0.00	0.00	0.017	O	|	|	|	|	0.01
222.583	0.00	0.00	0.017	O	|	|	|	|	0.01
222.667	0.00	0.00	0.017	O	|	|	|	|	0.01
222.750	0.00	0.00	0.017	O	|	|	|	|	0.01
222.833	0.00	0.00	0.017	O	|	|	|	|	0.01
222.917	0.00	0.00	0.017	O	|	|	|	|	0.01
223.000	0.00	0.00	0.017	O	|	|	|	|	0.01
223.083	0.00	0.00	0.017	O	|	|	|	|	0.01
223.167	0.00	0.00	0.017	O	|	|	|	|	0.01
223.250	0.00	0.00	0.017	O	|	|	|	|	0.01
223.333	0.00	0.00	0.017	O	|	|	|	|	0.01
223.417	0.00	0.00	0.017	O	|	|	|	|	0.01
223.500	0.00	0.00	0.017	O	|	|	|	|	0.01
223.583	0.00	0.00	0.017	O	|	|	|	|	0.01
223.667	0.00	0.00	0.017	O	|	|	|	|	0.01
223.750	0.00	0.00	0.017	O	|	|	|	|	0.01
223.833	0.00	0.00	0.017	O	|	|	|	|	0.01
223.917	0.00	0.00	0.017	O	|	|	|	|	0.01
224.000	0.00	0.00	0.017	O	|	|	|	|	0.01
224.083	0.00	0.00	0.017	O	|	|	|	|	0.01
224.167	0.00	0.00	0.016	O	|	|	|	|	0.01
224.250	0.00	0.00	0.016	O	|	|	|	|	0.01
224.333	0.00	0.00	0.016	O	|	|	|	|	0.01
224.417	0.00	0.00	0.016	O	|	|	|	|	0.01
224.500	0.00	0.00	0.016	O	|	|	|	|	0.01
224.583	0.00	0.00	0.016	O	|	|	|	|	0.01
224.667	0.00	0.00	0.016	O	|	|	|	|	0.01
224.750	0.00	0.00	0.016	O	|	|	|	|	0.01
224.833	0.00	0.00	0.016	O	|	|	|	|	0.01
224.917	0.00	0.00	0.016	O	|	|	|	|	0.01
225.000	0.00	0.00	0.016	O	|	|	|	|	0.01

225.083	0.00	0.00	0.016	O	|	|	|	|	0.01
225.167	0.00	0.00	0.016	O	|	|	|	|	0.01
225.250	0.00	0.00	0.016	O	|	|	|	|	0.01
225.333	0.00	0.00	0.016	O	|	|	|	|	0.01
225.417	0.00	0.00	0.016	O	|	|	|	|	0.01
225.500	0.00	0.00	0.016	O	|	|	|	|	0.01
225.583	0.00	0.00	0.016	O	|	|	|	|	0.01
225.667	0.00	0.00	0.016	O	|	|	|	|	0.01
225.750	0.00	0.00	0.016	O	|	|	|	|	0.01
225.833	0.00	0.00	0.016	O	|	|	|	|	0.01
225.917	0.00	0.00	0.016	O	|	|	|	|	0.01
226.000	0.00	0.00	0.016	O	|	|	|	|	0.01
226.083	0.00	0.00	0.016	O	|	|	|	|	0.01
226.167	0.00	0.00	0.016	O	|	|	|	|	0.01
226.250	0.00	0.00	0.016	O	|	|	|	|	0.01
226.333	0.00	0.00	0.016	O	|	|	|	|	0.01
226.417	0.00	0.00	0.016	O	|	|	|	|	0.01
226.500	0.00	0.00	0.016	O	|	|	|	|	0.01
226.583	0.00	0.00	0.016	O	|	|	|	|	0.01
226.667	0.00	0.00	0.016	O	|	|	|	|	0.01
226.750	0.00	0.00	0.016	O	|	|	|	|	0.01
226.833	0.00	0.00	0.016	O	|	|	|	|	0.01
226.917	0.00	0.00	0.015	O	|	|	|	|	0.01
227.000	0.00	0.00	0.015	O	|	|	|	|	0.01
227.083	0.00	0.00	0.015	O	|	|	|	|	0.01
227.167	0.00	0.00	0.015	O	|	|	|	|	0.01
227.250	0.00	0.00	0.015	O	|	|	|	|	0.01
227.333	0.00	0.00	0.015	O	|	|	|	|	0.01
227.417	0.00	0.00	0.015	O	|	|	|	|	0.01
227.500	0.00	0.00	0.015	O	|	|	|	|	0.01
227.583	0.00	0.00	0.015	O	|	|	|	|	0.01
227.667	0.00	0.00	0.015	O	|	|	|	|	0.01
227.750	0.00	0.00	0.015	O	|	|	|	|	0.01
227.833	0.00	0.00	0.015	O	|	|	|	|	0.01
227.917	0.00	0.00	0.015	O	|	|	|	|	0.01
228.000	0.00	0.00	0.015	O	|	|	|	|	0.01
228.083	0.00	0.00	0.015	O	|	|	|	|	0.01
228.167	0.00	0.00	0.015	O	|	|	|	|	0.01
228.250	0.00	0.00	0.015	O	|	|	|	|	0.01
228.333	0.00	0.00	0.015	O	|	|	|	|	0.01
228.417	0.00	0.00	0.015	O	|	|	|	|	0.01
228.500	0.00	0.00	0.015	O	|	|	|	|	0.01
228.583	0.00	0.00	0.015	O	|	|	|	|	0.01
228.667	0.00	0.00	0.015	O	|	|	|	|	0.01
228.750	0.00	0.00	0.015	O	|	|	|	|	0.01
228.833	0.00	0.00	0.015	O	|	|	|	|	0.01
228.917	0.00	0.00	0.015	O	|	|	|	|	0.01
229.000	0.00	0.00	0.015	O	|	|	|	|	0.01
229.083	0.00	0.00	0.015	O	|	|	|	|	0.01
229.167	0.00	0.00	0.015	O	|	|	|	|	0.01
229.250	0.00	0.00	0.015	O	|	|	|	|	0.01
229.333	0.00	0.00	0.015	O	|	|	|	|	0.01
229.417	0.00	0.00	0.015	O	|	|	|	|	0.01
229.500	0.00	0.00	0.015	O	|	|	|	|	0.01
229.583	0.00	0.00	0.015	O	|	|	|	|	0.01
229.667	0.00	0.00	0.015	O	|	|	|	|	0.01
229.750	0.00	0.00	0.014	O	|	|	|	|	0.01
229.833	0.00	0.00	0.014	O	|	|	|	|	0.01
229.917	0.00	0.00	0.014	O	|	|	|	|	0.01
230.000	0.00	0.00	0.014	O	|	|	|	|	0.01
230.083	0.00	0.00	0.014	O	|	|	|	|	0.01
230.167	0.00	0.00	0.014	O	|	|	|	|	0.01
230.250	0.00	0.00	0.014	O	|	|	|	|	0.01
230.333	0.00	0.00	0.014	O	|	|	|	|	0.01
230.417	0.00	0.00	0.014	O	|	|	|	|	0.01
230.500	0.00	0.00	0.014	O	|	|	|	|	0.01
230.583	0.00	0.00	0.014	O	|	|	|	|	0.01
230.667	0.00	0.00	0.014	O	|	|	|	|	0.01
230.750	0.00	0.00	0.014	O	|	|	|	|	0.01
230.833	0.00	0.00	0.014	O	|	|	|	|	0.01
230.917	0.00	0.00	0.014	O	|	|	|	|	0.01

231.000	0.00	0.00	0.014	O	|	|	|	| 0.01
231.083	0.00	0.00	0.014	O	|	|	|	| 0.01
231.167	0.00	0.00	0.014	O	|	|	|	| 0.01
231.250	0.00	0.00	0.014	O	|	|	|	| 0.01
231.333	0.00	0.00	0.014	O	|	|	|	| 0.01
231.417	0.00	0.00	0.014	O	|	|	|	| 0.01
231.500	0.00	0.00	0.014	O	|	|	|	| 0.01
231.583	0.00	0.00	0.014	O	|	|	|	| 0.01
231.667	0.00	0.00	0.014	O	|	|	|	| 0.01
231.750	0.00	0.00	0.014	O	|	|	|	| 0.01
231.833	0.00	0.00	0.014	O	|	|	|	| 0.01
231.917	0.00	0.00	0.014	O	|	|	|	| 0.01
232.000	0.00	0.00	0.014	O	|	|	|	| 0.01
232.083	0.00	0.00	0.014	O	|	|	|	| 0.01
232.167	0.00	0.00	0.014	O	|	|	|	| 0.01
232.250	0.00	0.00	0.014	O	|	|	|	| 0.01
232.333	0.00	0.00	0.014	O	|	|	|	| 0.01
232.417	0.00	0.00	0.014	O	|	|	|	| 0.01
232.500	0.00	0.00	0.014	O	|	|	|	| 0.01
232.583	0.00	0.00	0.014	O	|	|	|	| 0.01
232.667	0.00	0.00	0.014	O	|	|	|	| 0.01
232.750	0.00	0.00	0.014	O	|	|	|	| 0.01
232.833	0.00	0.00	0.013	O	|	|	|	| 0.01
232.917	0.00	0.00	0.013	O	|	|	|	| 0.01
233.000	0.00	0.00	0.013	O	|	|	|	| 0.01
233.083	0.00	0.00	0.013	O	|	|	|	| 0.01
233.167	0.00	0.00	0.013	O	|	|	|	| 0.01
233.250	0.00	0.00	0.013	O	|	|	|	| 0.01
233.333	0.00	0.00	0.013	O	|	|	|	| 0.01
233.417	0.00	0.00	0.013	O	|	|	|	| 0.01
233.500	0.00	0.00	0.013	O	|	|	|	| 0.01
233.583	0.00	0.00	0.013	O	|	|	|	| 0.01
233.667	0.00	0.00	0.013	O	|	|	|	| 0.01
233.750	0.00	0.00	0.013	O	|	|	|	| 0.01
233.833	0.00	0.00	0.013	O	|	|	|	| 0.01
233.917	0.00	0.00	0.013	O	|	|	|	| 0.01
234.000	0.00	0.00	0.013	O	|	|	|	| 0.01
234.083	0.00	0.00	0.013	O	|	|	|	| 0.01
234.167	0.00	0.00	0.013	O	|	|	|	| 0.01
234.250	0.00	0.00	0.013	O	|	|	|	| 0.01
234.333	0.00	0.00	0.013	O	|	|	|	| 0.01
234.417	0.00	0.00	0.013	O	|	|	|	| 0.01
234.500	0.00	0.00	0.013	O	|	|	|	| 0.01
234.583	0.00	0.00	0.013	O	|	|	|	| 0.01
234.667	0.00	0.00	0.013	O	|	|	|	| 0.01
234.750	0.00	0.00	0.013	O	|	|	|	| 0.01
234.833	0.00	0.00	0.013	O	|	|	|	| 0.01
234.917	0.00	0.00	0.013	O	|	|	|	| 0.01
235.000	0.00	0.00	0.013	O	|	|	|	| 0.01
235.083	0.00	0.00	0.013	O	|	|	|	| 0.01
235.167	0.00	0.00	0.013	O	|	|	|	| 0.01
235.250	0.00	0.00	0.013	O	|	|	|	| 0.01
235.333	0.00	0.00	0.013	O	|	|	|	| 0.01
235.417	0.00	0.00	0.013	O	|	|	|	| 0.01
235.500	0.00	0.00	0.013	O	|	|	|	| 0.01
235.583	0.00	0.00	0.013	O	|	|	|	| 0.01
235.667	0.00	0.00	0.013	O	|	|	|	| 0.01
235.750	0.00	0.00	0.013	O	|	|	|	| 0.01
235.833	0.00	0.00	0.013	O	|	|	|	| 0.01
235.917	0.00	0.00	0.013	O	|	|	|	| 0.01
236.000	0.00	0.00	0.013	O	|	|	|	| 0.01
236.083	0.00	0.00	0.013	O	|	|	|	| 0.01
236.167	0.00	0.00	0.012	O	|	|	|	| 0.01
236.250	0.00	0.00	0.012	O	|	|	|	| 0.01
236.333	0.00	0.00	0.012	O	|	|	|	| 0.01
236.417	0.00	0.00	0.012	O	|	|	|	| 0.01
236.500	0.00	0.00	0.012	O	|	|	|	| 0.01
236.583	0.00	0.00	0.012	O	|	|	|	| 0.01
236.667	0.00	0.00	0.012	O	|	|	|	| 0.01
236.750	0.00	0.00	0.012	O	|	|	|	| 0.01
236.833	0.00	0.00	0.012	O	|	|	|	| 0.01

236.917	0.00	0.00	0.012	O	|	|	|	|	0.01
237.000	0.00	0.00	0.012	O	|	|	|	|	0.01
237.083	0.00	0.00	0.012	O	|	|	|	|	0.01
237.167	0.00	0.00	0.012	O	|	|	|	|	0.01
237.250	0.00	0.00	0.012	O	|	|	|	|	0.01
237.333	0.00	0.00	0.012	O	|	|	|	|	0.01
237.417	0.00	0.00	0.012	O	|	|	|	|	0.01
237.500	0.00	0.00	0.012	O	|	|	|	|	0.01
237.583	0.00	0.00	0.012	O	|	|	|	|	0.01
237.667	0.00	0.00	0.012	O	|	|	|	|	0.01
237.750	0.00	0.00	0.012	O	|	|	|	|	0.01
237.833	0.00	0.00	0.012	O	|	|	|	|	0.01
237.917	0.00	0.00	0.012	O	|	|	|	|	0.01
238.000	0.00	0.00	0.012	O	|	|	|	|	0.01
238.083	0.00	0.00	0.012	O	|	|	|	|	0.01
238.167	0.00	0.00	0.012	O	|	|	|	|	0.01
238.250	0.00	0.00	0.012	O	|	|	|	|	0.01
238.333	0.00	0.00	0.012	O	|	|	|	|	0.01
238.417	0.00	0.00	0.012	O	|	|	|	|	0.01
238.500	0.00	0.00	0.012	O	|	|	|	|	0.01
238.583	0.00	0.00	0.012	O	|	|	|	|	0.01
238.667	0.00	0.00	0.012	O	|	|	|	|	0.01
238.750	0.00	0.00	0.012	O	|	|	|	|	0.01
238.833	0.00	0.00	0.012	O	|	|	|	|	0.01
238.917	0.00	0.00	0.012	O	|	|	|	|	0.01
239.000	0.00	0.00	0.012	O	|	|	|	|	0.01
239.083	0.00	0.00	0.012	O	|	|	|	|	0.01
239.167	0.00	0.00	0.012	O	|	|	|	|	0.01
239.250	0.00	0.00	0.012	O	|	|	|	|	0.01
239.333	0.00	0.00	0.012	O	|	|	|	|	0.01
239.417	0.00	0.00	0.012	O	|	|	|	|	0.01
239.500	0.00	0.00	0.012	O	|	|	|	|	0.01
239.583	0.00	0.00	0.012	O	|	|	|	|	0.01
239.667	0.00	0.00	0.012	O	|	|	|	|	0.01
239.750	0.00	0.00	0.012	O	|	|	|	|	0.01
239.833	0.00	0.00	0.011	O	|	|	|	|	0.01
239.917	0.00	0.00	0.011	O	|	|	|	|	0.01
240.000	0.00	0.00	0.011	O	|	|	|	|	0.01
240.083	0.00	0.00	0.011	O	|	|	|	|	0.01
240.167	0.00	0.00	0.011	O	|	|	|	|	0.01
240.250	0.00	0.00	0.011	O	|	|	|	|	0.01
240.333	0.00	0.00	0.011	O	|	|	|	|	0.01
240.417	0.00	0.00	0.011	O	|	|	|	|	0.01
240.500	0.00	0.00	0.011	O	|	|	|	|	0.01
240.583	0.00	0.00	0.011	O	|	|	|	|	0.01
240.667	0.00	0.00	0.011	O	|	|	|	|	0.01
240.750	0.00	0.00	0.011	O	|	|	|	|	0.01
240.833	0.00	0.00	0.011	O	|	|	|	|	0.01
240.917	0.00	0.00	0.011	O	|	|	|	|	0.01
241.000	0.00	0.00	0.011	O	|	|	|	|	0.01
241.083	0.00	0.00	0.011	O	|	|	|	|	0.01
241.167	0.00	0.00	0.011	O	|	|	|	|	0.01
241.250	0.00	0.00	0.011	O	|	|	|	|	0.01
241.333	0.00	0.00	0.011	O	|	|	|	|	0.01
241.417	0.00	0.00	0.011	O	|	|	|	|	0.01
241.500	0.00	0.00	0.011	O	|	|	|	|	0.01
241.583	0.00	0.00	0.011	O	|	|	|	|	0.01
241.667	0.00	0.00	0.011	O	|	|	|	|	0.01
241.750	0.00	0.00	0.011	O	|	|	|	|	0.01
241.833	0.00	0.00	0.011	O	|	|	|	|	0.01
241.917	0.00	0.00	0.011	O	|	|	|	|	0.01
242.000	0.00	0.00	0.011	O	|	|	|	|	0.01
242.083	0.00	0.00	0.011	O	|	|	|	|	0.01
242.167	0.00	0.00	0.011	O	|	|	|	|	0.01
242.250	0.00	0.00	0.011	O	|	|	|	|	0.01
242.333	0.00	0.00	0.011	O	|	|	|	|	0.01
242.417	0.00	0.00	0.011	O	|	|	|	|	0.01
242.500	0.00	0.00	0.011	O	|	|	|	|	0.01
242.583	0.00	0.00	0.011	O	|	|	|	|	0.01
242.667	0.00	0.00	0.011	O	|	|	|	|	0.01
242.750	0.00	0.00	0.011	O	|	|	|	|	0.01

242.833	0.00	0.00	0.011	O	|	|	|	|	0.01
242.917	0.00	0.00	0.011	O	|	|	|	|	0.01
243.000	0.00	0.00	0.011	O	|	|	|	|	0.01
243.083	0.00	0.00	0.011	O	|	|	|	|	0.01
243.167	0.00	0.00	0.011	O	|	|	|	|	0.01
243.250	0.00	0.00	0.011	O	|	|	|	|	0.01
243.333	0.00	0.00	0.011	O	|	|	|	|	0.01
243.417	0.00	0.00	0.011	O	|	|	|	|	0.01
243.500	0.00	0.00	0.011	O	|	|	|	|	0.01
243.583	0.00	0.00	0.011	O	|	|	|	|	0.01
243.667	0.00	0.00	0.011	O	|	|	|	|	0.01
243.750	0.00	0.00	0.010	O	|	|	|	|	0.01
243.833	0.00	0.00	0.010	O	|	|	|	|	0.01
243.917	0.00	0.00	0.010	O	|	|	|	|	0.01
244.000	0.00	0.00	0.010	O	|	|	|	|	0.01
244.083	0.00	0.00	0.010	O	|	|	|	|	0.01
244.167	0.00	0.00	0.010	O	|	|	|	|	0.01
244.250	0.00	0.00	0.010	O	|	|	|	|	0.01
244.333	0.00	0.00	0.010	O	|	|	|	|	0.01
244.417	0.00	0.00	0.010	O	|	|	|	|	0.01
244.500	0.00	0.00	0.010	O	|	|	|	|	0.01
244.583	0.00	0.00	0.010	O	|	|	|	|	0.01
244.667	0.00	0.00	0.010	O	|	|	|	|	0.01
244.750	0.00	0.00	0.010	O	|	|	|	|	0.01
244.833	0.00	0.00	0.010	O	|	|	|	|	0.01
244.917	0.00	0.00	0.010	O	|	|	|	|	0.01
245.000	0.00	0.00	0.010	O	|	|	|	|	0.01
245.083	0.00	0.00	0.010	O	|	|	|	|	0.01
245.167	0.00	0.00	0.010	O	|	|	|	|	0.01
245.250	0.00	0.00	0.010	O	|	|	|	|	0.01
245.333	0.00	0.00	0.010	O	|	|	|	|	0.01
245.417	0.00	0.00	0.010	O	|	|	|	|	0.01
245.500	0.00	0.00	0.010	O	|	|	|	|	0.01
245.583	0.00	0.00	0.010	O	|	|	|	|	0.01
245.667	0.00	0.00	0.010	O	|	|	|	|	0.01
245.750	0.00	0.00	0.010	O	|	|	|	|	0.01
245.833	0.00	0.00	0.010	O	|	|	|	|	0.01
245.917	0.00	0.00	0.010	O	|	|	|	|	0.01
246.000	0.00	0.00	0.010	O	|	|	|	|	0.01
246.083	0.00	0.00	0.010	O	|	|	|	|	0.01
246.167	0.00	0.00	0.010	O	|	|	|	|	0.01
246.250	0.00	0.00	0.010	O	|	|	|	|	0.01
246.333	0.00	0.00	0.010	O	|	|	|	|	0.01
246.417	0.00	0.00	0.010	O	|	|	|	|	0.01
246.500	0.00	0.00	0.010	O	|	|	|	|	0.01
246.583	0.00	0.00	0.010	O	|	|	|	|	0.01
246.667	0.00	0.00	0.010	O	|	|	|	|	0.01
246.750	0.00	0.00	0.010	O	|	|	|	|	0.01
246.833	0.00	0.00	0.010	O	|	|	|	|	0.01
246.917	0.00	0.00	0.010	O	|	|	|	|	0.01
247.000	0.00	0.00	0.010	O	|	|	|	|	0.01
247.083	0.00	0.00	0.010	O	|	|	|	|	0.01
247.167	0.00	0.00	0.010	O	|	|	|	|	0.01
247.250	0.00	0.00	0.010	O	|	|	|	|	0.01
247.333	0.00	0.00	0.010	O	|	|	|	|	0.01
247.417	0.00	0.00	0.010	O	|	|	|	|	0.01
247.500	0.00	0.00	0.010	O	|	|	|	|	0.01
247.583	0.00	0.00	0.010	O	|	|	|	|	0.01
247.667	0.00	0.00	0.010	O	|	|	|	|	0.01
247.750	0.00	0.00	0.010	O	|	|	|	|	0.01
247.833	0.00	0.00	0.010	O	|	|	|	|	0.01
247.917	0.00	0.00	0.010	O	|	|	|	|	0.01
248.000	0.00	0.00	0.010	O	|	|	|	|	0.01
248.083	0.00	0.00	0.009	O	|	|	|	|	0.01
248.167	0.00	0.00	0.009	O	|	|	|	|	0.01
248.250	0.00	0.00	0.009	O	|	|	|	|	0.01
248.333	0.00	0.00	0.009	O	|	|	|	|	0.01
248.417	0.00	0.00	0.009	O	|	|	|	|	0.01
248.500	0.00	0.00	0.009	O	|	|	|	|	0.01
248.583	0.00	0.00	0.009	O	|	|	|	|	0.01
248.667	0.00	0.00	0.009	O	|	|	|	|	0.01

248.750	0.00	0.00	0.009	O	|	|	|	|	0.01
248.833	0.00	0.00	0.009	O	|	|	|	|	0.01
248.917	0.00	0.00	0.009	O	|	|	|	|	0.01
249.000	0.00	0.00	0.009	O	|	|	|	|	0.01
249.083	0.00	0.00	0.009	O	|	|	|	|	0.01
249.167	0.00	0.00	0.009	O	|	|	|	|	0.01
249.250	0.00	0.00	0.009	O	|	|	|	|	0.01
249.333	0.00	0.00	0.009	O	|	|	|	|	0.01
249.417	0.00	0.00	0.009	O	|	|	|	|	0.01
249.500	0.00	0.00	0.009	O	|	|	|	|	0.01
249.583	0.00	0.00	0.009	O	|	|	|	|	0.01
249.667	0.00	0.00	0.009	O	|	|	|	|	0.01
249.750	0.00	0.00	0.009	O	|	|	|	|	0.01
249.833	0.00	0.00	0.009	O	|	|	|	|	0.01
249.917	0.00	0.00	0.009	O	|	|	|	|	0.01
250.000	0.00	0.00	0.009	O	|	|	|	|	0.01
250.083	0.00	0.00	0.009	O	|	|	|	|	0.01
250.167	0.00	0.00	0.009	O	|	|	|	|	0.01
250.250	0.00	0.00	0.009	O	|	|	|	|	0.01
250.333	0.00	0.00	0.009	O	|	|	|	|	0.01
250.417	0.00	0.00	0.009	O	|	|	|	|	0.01
250.500	0.00	0.00	0.009	O	|	|	|	|	0.01
250.583	0.00	0.00	0.009	O	|	|	|	|	0.01
250.667	0.00	0.00	0.009	O	|	|	|	|	0.01
250.750	0.00	0.00	0.009	O	|	|	|	|	0.01
250.833	0.00	0.00	0.009	O	|	|	|	|	0.01
250.917	0.00	0.00	0.009	O	|	|	|	|	0.01
251.000	0.00	0.00	0.009	O	|	|	|	|	0.01
251.083	0.00	0.00	0.009	O	|	|	|	|	0.01
251.167	0.00	0.00	0.009	O	|	|	|	|	0.01
251.250	0.00	0.00	0.009	O	|	|	|	|	0.01
251.333	0.00	0.00	0.009	O	|	|	|	|	0.01
251.417	0.00	0.00	0.009	O	|	|	|	|	0.01
251.500	0.00	0.00	0.009	O	|	|	|	|	0.01
251.583	0.00	0.00	0.009	O	|	|	|	|	0.01
251.667	0.00	0.00	0.009	O	|	|	|	|	0.01
251.750	0.00	0.00	0.009	O	|	|	|	|	0.01
251.833	0.00	0.00	0.009	O	|	|	|	|	0.01
251.917	0.00	0.00	0.009	O	|	|	|	|	0.01
252.000	0.00	0.00	0.009	O	|	|	|	|	0.01
252.083	0.00	0.00	0.009	O	|	|	|	|	0.01
252.167	0.00	0.00	0.009	O	|	|	|	|	0.01
252.250	0.00	0.00	0.009	O	|	|	|	|	0.01
252.333	0.00	0.00	0.009	O	|	|	|	|	0.01
252.417	0.00	0.00	0.009	O	|	|	|	|	0.01
252.500	0.00	0.00	0.009	O	|	|	|	|	0.01
252.583	0.00	0.00	0.009	O	|	|	|	|	0.01
252.667	0.00	0.00	0.009	O	|	|	|	|	0.01
252.750	0.00	0.00	0.009	O	|	|	|	|	0.01
252.833	0.00	0.00	0.009	O	|	|	|	|	0.01
252.917	0.00	0.00	0.008	O	|	|	|	|	0.01
253.000	0.00	0.00	0.008	O	|	|	|	|	0.01
253.083	0.00	0.00	0.008	O	|	|	|	|	0.01
253.167	0.00	0.00	0.008	O	|	|	|	|	0.01
253.250	0.00	0.00	0.008	O	|	|	|	|	0.01
253.333	0.00	0.00	0.008	O	|	|	|	|	0.01
253.417	0.00	0.00	0.008	O	|	|	|	|	0.01
253.500	0.00	0.00	0.008	O	|	|	|	|	0.01
253.583	0.00	0.00	0.008	O	|	|	|	|	0.01
253.667	0.00	0.00	0.008	O	|	|	|	|	0.01
253.750	0.00	0.00	0.008	O	|	|	|	|	0.01
253.833	0.00	0.00	0.008	O	|	|	|	|	0.01
253.917	0.00	0.00	0.008	O	|	|	|	|	0.01
254.000	0.00	0.00	0.008	O	|	|	|	|	0.01
254.083	0.00	0.00	0.008	O	|	|	|	|	0.01
254.167	0.00	0.00	0.008	O	|	|	|	|	0.01
254.250	0.00	0.00	0.008	O	|	|	|	|	0.01
254.333	0.00	0.00	0.008	O	|	|	|	|	0.01
254.417	0.00	0.00	0.008	O	|	|	|	|	0.01
254.500	0.00	0.00	0.008	O	|	|	|	|	0.01
254.583	0.00	0.00	0.008	O	|	|	|	|	0.01

254.667	0.00	0.00	0.008	O	|	|	|	|	0.01
254.750	0.00	0.00	0.008	O	|	|	|	|	0.01
254.833	0.00	0.00	0.008	O	|	|	|	|	0.01
254.917	0.00	0.00	0.008	O	|	|	|	|	0.01
255.000	0.00	0.00	0.008	O	|	|	|	|	0.01
255.083	0.00	0.00	0.008	O	|	|	|	|	0.01
255.167	0.00	0.00	0.008	O	|	|	|	|	0.01
255.250	0.00	0.00	0.008	O	|	|	|	|	0.01
255.333	0.00	0.00	0.008	O	|	|	|	|	0.01
255.417	0.00	0.00	0.008	O	|	|	|	|	0.01
255.500	0.00	0.00	0.008	O	|	|	|	|	0.01
255.583	0.00	0.00	0.008	O	|	|	|	|	0.01
255.667	0.00	0.00	0.008	O	|	|	|	|	0.01
255.750	0.00	0.00	0.008	O	|	|	|	|	0.01
255.833	0.00	0.00	0.008	O	|	|	|	|	0.01
255.917	0.00	0.00	0.008	O	|	|	|	|	0.01
256.000	0.00	0.00	0.008	O	|	|	|	|	0.01
256.083	0.00	0.00	0.008	O	|	|	|	|	0.01
256.167	0.00	0.00	0.008	O	|	|	|	|	0.01
256.250	0.00	0.00	0.008	O	|	|	|	|	0.01
256.333	0.00	0.00	0.008	O	|	|	|	|	0.01
256.417	0.00	0.00	0.008	O	|	|	|	|	0.01
256.500	0.00	0.00	0.008	O	|	|	|	|	0.01
256.583	0.00	0.00	0.008	O	|	|	|	|	0.01
256.667	0.00	0.00	0.008	O	|	|	|	|	0.01
256.750	0.00	0.00	0.008	O	|	|	|	|	0.01
256.833	0.00	0.00	0.008	O	|	|	|	|	0.01
256.917	0.00	0.00	0.008	O	|	|	|	|	0.01
257.000	0.00	0.00	0.008	O	|	|	|	|	0.01
257.083	0.00	0.00	0.008	O	|	|	|	|	0.01
257.167	0.00	0.00	0.008	O	|	|	|	|	0.01
257.250	0.00	0.00	0.008	O	|	|	|	|	0.01
257.333	0.00	0.00	0.008	O	|	|	|	|	0.01
257.417	0.00	0.00	0.008	O	|	|	|	|	0.01
257.500	0.00	0.00	0.008	O	|	|	|	|	0.01
257.583	0.00	0.00	0.008	O	|	|	|	|	0.01
257.667	0.00	0.00	0.008	O	|	|	|	|	0.01
257.750	0.00	0.00	0.008	O	|	|	|	|	0.01
257.833	0.00	0.00	0.008	O	|	|	|	|	0.01
257.917	0.00	0.00	0.008	O	|	|	|	|	0.01
258.000	0.00	0.00	0.008	O	|	|	|	|	0.01
258.083	0.00	0.00	0.008	O	|	|	|	|	0.01
258.167	0.00	0.00	0.008	O	|	|	|	|	0.01
258.250	0.00	0.00	0.008	O	|	|	|	|	0.01
258.333	0.00	0.00	0.007	O	|	|	|	|	0.01
258.417	0.00	0.00	0.007	O	|	|	|	|	0.01
258.500	0.00	0.00	0.007	O	|	|	|	|	0.01
258.583	0.00	0.00	0.007	O	|	|	|	|	0.01
258.667	0.00	0.00	0.007	O	|	|	|	|	0.01
258.750	0.00	0.00	0.007	O	|	|	|	|	0.01
258.833	0.00	0.00	0.007	O	|	|	|	|	0.01
258.917	0.00	0.00	0.007	O	|	|	|	|	0.01
259.000	0.00	0.00	0.007	O	|	|	|	|	0.01
259.083	0.00	0.00	0.007	O	|	|	|	|	0.01
259.167	0.00	0.00	0.007	O	|	|	|	|	0.01
259.250	0.00	0.00	0.007	O	|	|	|	|	0.01
259.333	0.00	0.00	0.007	O	|	|	|	|	0.01
259.417	0.00	0.00	0.007	O	|	|	|	|	0.01
259.500	0.00	0.00	0.007	O	|	|	|	|	0.01
259.583	0.00	0.00	0.007	O	|	|	|	|	0.01
259.667	0.00	0.00	0.007	O	|	|	|	|	0.01
259.750	0.00	0.00	0.007	O	|	|	|	|	0.01
259.833	0.00	0.00	0.007	O	|	|	|	|	0.01
259.917	0.00	0.00	0.007	O	|	|	|	|	0.01
260.000	0.00	0.00	0.007	O	|	|	|	|	0.01
260.083	0.00	0.00	0.007	O	|	|	|	|	0.01
260.167	0.00	0.00	0.007	O	|	|	|	|	0.01
260.250	0.00	0.00	0.007	O	|	|	|	|	0.01
260.333	0.00	0.00	0.007	O	|	|	|	|	0.01
260.417	0.00	0.00	0.007	O	|	|	|	|	0.01
260.500	0.00	0.00	0.007	O	|	|	|	|	0.01

260.583	0.00	0.00	0.007	O	|	|	|	|	0.01
260.667	0.00	0.00	0.007	O	|	|	|	|	0.01
260.750	0.00	0.00	0.007	O	|	|	|	|	0.01
260.833	0.00	0.00	0.007	O	|	|	|	|	0.01
260.917	0.00	0.00	0.007	O	|	|	|	|	0.01
261.000	0.00	0.00	0.007	O	|	|	|	|	0.01
261.083	0.00	0.00	0.007	O	|	|	|	|	0.01
261.167	0.00	0.00	0.007	O	|	|	|	|	0.01
261.250	0.00	0.00	0.007	O	|	|	|	|	0.01
261.333	0.00	0.00	0.007	O	|	|	|	|	0.01
261.417	0.00	0.00	0.007	O	|	|	|	|	0.01
261.500	0.00	0.00	0.007	O	|	|	|	|	0.01
261.583	0.00	0.00	0.007	O	|	|	|	|	0.01
261.667	0.00	0.00	0.007	O	|	|	|	|	0.01
261.750	0.00	0.00	0.007	O	|	|	|	|	0.01
261.833	0.00	0.00	0.007	O	|	|	|	|	0.01
261.917	0.00	0.00	0.007	O	|	|	|	|	0.01
262.000	0.00	0.00	0.007	O	|	|	|	|	0.01
262.083	0.00	0.00	0.007	O	|	|	|	|	0.01
262.167	0.00	0.00	0.007	O	|	|	|	|	0.01
262.250	0.00	0.00	0.007	O	|	|	|	|	0.01
262.333	0.00	0.00	0.007	O	|	|	|	|	0.01
262.417	0.00	0.00	0.007	O	|	|	|	|	0.01
262.500	0.00	0.00	0.007	O	|	|	|	|	0.01
262.583	0.00	0.00	0.007	O	|	|	|	|	0.01
262.667	0.00	0.00	0.007	O	|	|	|	|	0.01
262.750	0.00	0.00	0.007	O	|	|	|	|	0.01
262.833	0.00	0.00	0.007	O	|	|	|	|	0.01
262.917	0.00	0.00	0.007	O	|	|	|	|	0.01
263.000	0.00	0.00	0.007	O	|	|	|	|	0.01
263.083	0.00	0.00	0.007	O	|	|	|	|	0.01
263.167	0.00	0.00	0.007	O	|	|	|	|	0.01
263.250	0.00	0.00	0.007	O	|	|	|	|	0.01
263.333	0.00	0.00	0.007	O	|	|	|	|	0.01
263.417	0.00	0.00	0.007	O	|	|	|	|	0.01
263.500	0.00	0.00	0.007	O	|	|	|	|	0.01
263.583	0.00	0.00	0.007	O	|	|	|	|	0.01
263.667	0.00	0.00	0.007	O	|	|	|	|	0.01
263.750	0.00	0.00	0.007	O	|	|	|	|	0.01
263.833	0.00	0.00	0.007	O	|	|	|	|	0.01
263.917	0.00	0.00	0.007	O	|	|	|	|	0.01
264.000	0.00	0.00	0.007	O	|	|	|	|	0.01
264.083	0.00	0.00	0.007	O	|	|	|	|	0.01
264.167	0.00	0.00	0.007	O	|	|	|	|	0.01
264.250	0.00	0.00	0.007	O	|	|	|	|	0.01
264.333	0.00	0.00	0.007	O	|	|	|	|	0.01
264.417	0.00	0.00	0.007	O	|	|	|	|	0.01
264.500	0.00	0.00	0.006	O	|	|	|	|	0.01
264.583	0.00	0.00	0.006	O	|	|	|	|	0.01
264.667	0.00	0.00	0.006	O	|	|	|	|	0.01
264.750	0.00	0.00	0.006	O	|	|	|	|	0.01
264.833	0.00	0.00	0.006	O	|	|	|	|	0.01
264.917	0.00	0.00	0.006	O	|	|	|	|	0.01
265.000	0.00	0.00	0.006	O	|	|	|	|	0.01
265.083	0.00	0.00	0.006	O	|	|	|	|	0.01
265.167	0.00	0.00	0.006	O	|	|	|	|	0.01
265.250	0.00	0.00	0.006	O	|	|	|	|	0.01
265.333	0.00	0.00	0.006	O	|	|	|	|	0.01
265.417	0.00	0.00	0.006	O	|	|	|	|	0.01
265.500	0.00	0.00	0.006	O	|	|	|	|	0.01
265.583	0.00	0.00	0.006	O	|	|	|	|	0.01
265.667	0.00	0.00	0.006	O	|	|	|	|	0.01
265.750	0.00	0.00	0.006	O	|	|	|	|	0.01
265.833	0.00	0.00	0.006	O	|	|	|	|	0.01
265.917	0.00	0.00	0.006	O	|	|	|	|	0.01
266.000	0.00	0.00	0.006	O	|	|	|	|	0.01
266.083	0.00	0.00	0.006	O	|	|	|	|	0.01
266.167	0.00	0.00	0.006	O	|	|	|	|	0.01
266.250	0.00	0.00	0.006	O	|	|	|	|	0.01
266.333	0.00	0.00	0.006	O	|	|	|	|	0.01
266.417	0.00	0.00	0.006	O	|	|	|	|	0.01

266.500	0.00	0.00	0.006	O	|	|	|	|	0.01
266.583	0.00	0.00	0.006	O	|	|	|	|	0.01
266.667	0.00	0.00	0.006	O	|	|	|	|	0.01
266.750	0.00	0.00	0.006	O	|	|	|	|	0.01
266.833	0.00	0.00	0.006	O	|	|	|	|	0.00
266.917	0.00	0.00	0.006	O	|	|	|	|	0.00
267.000	0.00	0.00	0.006	O	|	|	|	|	0.00
267.083	0.00	0.00	0.006	O	|	|	|	|	0.00
267.167	0.00	0.00	0.006	O	|	|	|	|	0.00
267.250	0.00	0.00	0.006	O	|	|	|	|	0.00
267.333	0.00	0.00	0.006	O	|	|	|	|	0.00
267.417	0.00	0.00	0.006	O	|	|	|	|	0.00
267.500	0.00	0.00	0.006	O	|	|	|	|	0.00
267.583	0.00	0.00	0.006	O	|	|	|	|	0.00
267.667	0.00	0.00	0.006	O	|	|	|	|	0.00
267.750	0.00	0.00	0.006	O	|	|	|	|	0.00
267.833	0.00	0.00	0.006	O	|	|	|	|	0.00
267.917	0.00	0.00	0.006	O	|	|	|	|	0.00
268.000	0.00	0.00	0.006	O	|	|	|	|	0.00
268.083	0.00	0.00	0.006	O	|	|	|	|	0.00
268.167	0.00	0.00	0.006	O	|	|	|	|	0.00
268.250	0.00	0.00	0.006	O	|	|	|	|	0.00
268.333	0.00	0.00	0.006	O	|	|	|	|	0.00
268.417	0.00	0.00	0.006	O	|	|	|	|	0.00
268.500	0.00	0.00	0.006	O	|	|	|	|	0.00
268.583	0.00	0.00	0.006	O	|	|	|	|	0.00
268.667	0.00	0.00	0.006	O	|	|	|	|	0.00
268.750	0.00	0.00	0.006	O	|	|	|	|	0.00
268.833	0.00	0.00	0.006	O	|	|	|	|	0.00
268.917	0.00	0.00	0.006	O	|	|	|	|	0.00
269.000	0.00	0.00	0.006	O	|	|	|	|	0.00
269.083	0.00	0.00	0.006	O	|	|	|	|	0.00
269.167	0.00	0.00	0.006	O	|	|	|	|	0.00
269.250	0.00	0.00	0.006	O	|	|	|	|	0.00
269.333	0.00	0.00	0.006	O	|	|	|	|	0.00
269.417	0.00	0.00	0.006	O	|	|	|	|	0.00
269.500	0.00	0.00	0.006	O	|	|	|	|	0.00
269.583	0.00	0.00	0.006	O	|	|	|	|	0.00
269.667	0.00	0.00	0.006	O	|	|	|	|	0.00
269.750	0.00	0.00	0.006	O	|	|	|	|	0.00
269.833	0.00	0.00	0.006	O	|	|	|	|	0.00
269.917	0.00	0.00	0.006	O	|	|	|	|	0.00
270.000	0.00	0.00	0.006	O	|	|	|	|	0.00
270.083	0.00	0.00	0.006	O	|	|	|	|	0.00
270.167	0.00	0.00	0.006	O	|	|	|	|	0.00
270.250	0.00	0.00	0.006	O	|	|	|	|	0.00
270.333	0.00	0.00	0.006	O	|	|	|	|	0.00
270.417	0.00	0.00	0.006	O	|	|	|	|	0.00
270.500	0.00	0.00	0.006	O	|	|	|	|	0.00
270.583	0.00	0.00	0.006	O	|	|	|	|	0.00
270.667	0.00	0.00	0.006	O	|	|	|	|	0.00
270.750	0.00	0.00	0.006	O	|	|	|	|	0.00
270.833	0.00	0.00	0.006	O	|	|	|	|	0.00
270.917	0.00	0.00	0.006	O	|	|	|	|	0.00
271.000	0.00	0.00	0.006	O	|	|	|	|	0.00
271.083	0.00	0.00	0.006	O	|	|	|	|	0.00
271.167	0.00	0.00	0.006	O	|	|	|	|	0.00
271.250	0.00	0.00	0.006	O	|	|	|	|	0.00
271.333	0.00	0.00	0.006	O	|	|	|	|	0.00
271.417	0.00	0.00	0.006	O	|	|	|	|	0.00
271.500	0.00	0.00	0.006	O	|	|	|	|	0.00
271.583	0.00	0.00	0.006	O	|	|	|	|	0.00
271.667	0.00	0.00	0.006	O	|	|	|	|	0.00
271.750	0.00	0.00	0.005	O	|	|	|	|	0.00
271.833	0.00	0.00	0.005	O	|	|	|	|	0.00
271.917	0.00	0.00	0.005	O	|	|	|	|	0.00
272.000	0.00	0.00	0.005	O	|	|	|	|	0.00
272.083	0.00	0.00	0.005	O	|	|	|	|	0.00
272.167	0.00	0.00	0.005	O	|	|	|	|	0.00
272.250	0.00	0.00	0.005	O	|	|	|	|	0.00
272.333	0.00	0.00	0.005	O	|	|	|	|	0.00

272.417	0.00	0.00	0.005	O	|	|	|	|	0.00
272.500	0.00	0.00	0.005	O	|	|	|	|	0.00
272.583	0.00	0.00	0.005	O	|	|	|	|	0.00
272.667	0.00	0.00	0.005	O	|	|	|	|	0.00
272.750	0.00	0.00	0.005	O	|	|	|	|	0.00
272.833	0.00	0.00	0.005	O	|	|	|	|	0.00
272.917	0.00	0.00	0.005	O	|	|	|	|	0.00
273.000	0.00	0.00	0.005	O	|	|	|	|	0.00
273.083	0.00	0.00	0.005	O	|	|	|	|	0.00
273.167	0.00	0.00	0.005	O	|	|	|	|	0.00
273.250	0.00	0.00	0.005	O	|	|	|	|	0.00
273.333	0.00	0.00	0.005	O	|	|	|	|	0.00
273.417	0.00	0.00	0.005	O	|	|	|	|	0.00
273.500	0.00	0.00	0.005	O	|	|	|	|	0.00
273.583	0.00	0.00	0.005	O	|	|	|	|	0.00
273.667	0.00	0.00	0.005	O	|	|	|	|	0.00
273.750	0.00	0.00	0.005	O	|	|	|	|	0.00
273.833	0.00	0.00	0.005	O	|	|	|	|	0.00
273.917	0.00	0.00	0.005	O	|	|	|	|	0.00
274.000	0.00	0.00	0.005	O	|	|	|	|	0.00
274.083	0.00	0.00	0.005	O	|	|	|	|	0.00
274.167	0.00	0.00	0.005	O	|	|	|	|	0.00
274.250	0.00	0.00	0.005	O	|	|	|	|	0.00
274.333	0.00	0.00	0.005	O	|	|	|	|	0.00
274.417	0.00	0.00	0.005	O	|	|	|	|	0.00
274.500	0.00	0.00	0.005	O	|	|	|	|	0.00
274.583	0.00	0.00	0.005	O	|	|	|	|	0.00
274.667	0.00	0.00	0.005	O	|	|	|	|	0.00
274.750	0.00	0.00	0.005	O	|	|	|	|	0.00
274.833	0.00	0.00	0.005	O	|	|	|	|	0.00
274.917	0.00	0.00	0.005	O	|	|	|	|	0.00
275.000	0.00	0.00	0.005	O	|	|	|	|	0.00
275.083	0.00	0.00	0.005	O	|	|	|	|	0.00
275.167	0.00	0.00	0.005	O	|	|	|	|	0.00
275.250	0.00	0.00	0.005	O	|	|	|	|	0.00
275.333	0.00	0.00	0.005	O	|	|	|	|	0.00
275.417	0.00	0.00	0.005	O	|	|	|	|	0.00
275.500	0.00	0.00	0.005	O	|	|	|	|	0.00
275.583	0.00	0.00	0.005	O	|	|	|	|	0.00
275.667	0.00	0.00	0.005	O	|	|	|	|	0.00
275.750	0.00	0.00	0.005	O	|	|	|	|	0.00
275.833	0.00	0.00	0.005	O	|	|	|	|	0.00
275.917	0.00	0.00	0.005	O	|	|	|	|	0.00
276.000	0.00	0.00	0.005	O	|	|	|	|	0.00
276.083	0.00	0.00	0.005	O	|	|	|	|	0.00
276.167	0.00	0.00	0.005	O	|	|	|	|	0.00
276.250	0.00	0.00	0.005	O	|	|	|	|	0.00
276.333	0.00	0.00	0.005	O	|	|	|	|	0.00
276.417	0.00	0.00	0.005	O	|	|	|	|	0.00
276.500	0.00	0.00	0.005	O	|	|	|	|	0.00
276.583	0.00	0.00	0.005	O	|	|	|	|	0.00
276.667	0.00	0.00	0.005	O	|	|	|	|	0.00
276.750	0.00	0.00	0.005	O	|	|	|	|	0.00
276.833	0.00	0.00	0.005	O	|	|	|	|	0.00
276.917	0.00	0.00	0.005	O	|	|	|	|	0.00
277.000	0.00	0.00	0.005	O	|	|	|	|	0.00
277.083	0.00	0.00	0.005	O	|	|	|	|	0.00
277.167	0.00	0.00	0.005	O	|	|	|	|	0.00
277.250	0.00	0.00	0.005	O	|	|	|	|	0.00
277.333	0.00	0.00	0.005	O	|	|	|	|	0.00
277.417	0.00	0.00	0.005	O	|	|	|	|	0.00
277.500	0.00	0.00	0.005	O	|	|	|	|	0.00
277.583	0.00	0.00	0.005	O	|	|	|	|	0.00
277.667	0.00	0.00	0.005	O	|	|	|	|	0.00
277.750	0.00	0.00	0.005	O	|	|	|	|	0.00
277.833	0.00	0.00	0.005	O	|	|	|	|	0.00
277.917	0.00	0.00	0.005	O	|	|	|	|	0.00
278.000	0.00	0.00	0.005	O	|	|	|	|	0.00
278.083	0.00	0.00	0.005	O	|	|	|	|	0.00
278.167	0.00	0.00	0.005	O	|	|	|	|	0.00
278.250	0.00	0.00	0.005	O	|	|	|	|	0.00

278.333	0.00	0.00	0.005	O	|	|	|	|	0.00
278.417	0.00	0.00	0.005	O	|	|	|	|	0.00
278.500	0.00	0.00	0.005	O	|	|	|	|	0.00
278.583	0.00	0.00	0.005	O	|	|	|	|	0.00
278.667	0.00	0.00	0.005	O	|	|	|	|	0.00
278.750	0.00	0.00	0.005	O	|	|	|	|	0.00
278.833	0.00	0.00	0.005	O	|	|	|	|	0.00
278.917	0.00	0.00	0.005	O	|	|	|	|	0.00
279.000	0.00	0.00	0.005	O	|	|	|	|	0.00
279.083	0.00	0.00	0.005	O	|	|	|	|	0.00
279.167	0.00	0.00	0.005	O	|	|	|	|	0.00
279.250	0.00	0.00	0.005	O	|	|	|	|	0.00
279.333	0.00	0.00	0.005	O	|	|	|	|	0.00
279.417	0.00	0.00	0.005	O	|	|	|	|	0.00
279.500	0.00	0.00	0.005	O	|	|	|	|	0.00
279.583	0.00	0.00	0.005	O	|	|	|	|	0.00
279.667	0.00	0.00	0.005	O	|	|	|	|	0.00
279.750	0.00	0.00	0.005	O	|	|	|	|	0.00
279.833	0.00	0.00	0.005	O	|	|	|	|	0.00
279.917	0.00	0.00	0.005	O	|	|	|	|	0.00
280.000	0.00	0.00	0.005	O	|	|	|	|	0.00
280.083	0.00	0.00	0.005	O	|	|	|	|	0.00
280.167	0.00	0.00	0.005	O	|	|	|	|	0.00
280.250	0.00	0.00	0.005	O	|	|	|	|	0.00
280.333	0.00	0.00	0.005	O	|	|	|	|	0.00
280.417	0.00	0.00	0.005	O	|	|	|	|	0.00
280.500	0.00	0.00	0.004	O	|	|	|	|	0.00
280.583	0.00	0.00	0.004	O	|	|	|	|	0.00
280.667	0.00	0.00	0.004	O	|	|	|	|	0.00
280.750	0.00	0.00	0.004	O	|	|	|	|	0.00
280.833	0.00	0.00	0.004	O	|	|	|	|	0.00
280.917	0.00	0.00	0.004	O	|	|	|	|	0.00
281.000	0.00	0.00	0.004	O	|	|	|	|	0.00
281.083	0.00	0.00	0.004	O	|	|	|	|	0.00
281.167	0.00	0.00	0.004	O	|	|	|	|	0.00
281.250	0.00	0.00	0.004	O	|	|	|	|	0.00
281.333	0.00	0.00	0.004	O	|	|	|	|	0.00
281.417	0.00	0.00	0.004	O	|	|	|	|	0.00
281.500	0.00	0.00	0.004	O	|	|	|	|	0.00
281.583	0.00	0.00	0.004	O	|	|	|	|	0.00
281.667	0.00	0.00	0.004	O	|	|	|	|	0.00
281.750	0.00	0.00	0.004	O	|	|	|	|	0.00
281.833	0.00	0.00	0.004	O	|	|	|	|	0.00
281.917	0.00	0.00	0.004	O	|	|	|	|	0.00
282.000	0.00	0.00	0.004	O	|	|	|	|	0.00
282.083	0.00	0.00	0.004	O	|	|	|	|	0.00
282.167	0.00	0.00	0.004	O	|	|	|	|	0.00
282.250	0.00	0.00	0.004	O	|	|	|	|	0.00
282.333	0.00	0.00	0.004	O	|	|	|	|	0.00
282.417	0.00	0.00	0.004	O	|	|	|	|	0.00
282.500	0.00	0.00	0.004	O	|	|	|	|	0.00
282.583	0.00	0.00	0.004	O	|	|	|	|	0.00
282.667	0.00	0.00	0.004	O	|	|	|	|	0.00
282.750	0.00	0.00	0.004	O	|	|	|	|	0.00
282.833	0.00	0.00	0.004	O	|	|	|	|	0.00
282.917	0.00	0.00	0.004	O	|	|	|	|	0.00
283.000	0.00	0.00	0.004	O	|	|	|	|	0.00
283.083	0.00	0.00	0.004	O	|	|	|	|	0.00
283.167	0.00	0.00	0.004	O	|	|	|	|	0.00
283.250	0.00	0.00	0.004	O	|	|	|	|	0.00
283.333	0.00	0.00	0.004	O	|	|	|	|	0.00
283.417	0.00	0.00	0.004	O	|	|	|	|	0.00
283.500	0.00	0.00	0.004	O	|	|	|	|	0.00
283.583	0.00	0.00	0.004	O	|	|	|	|	0.00
283.667	0.00	0.00	0.004	O	|	|	|	|	0.00
283.750	0.00	0.00	0.004	O	|	|	|	|	0.00
283.833	0.00	0.00	0.004	O	|	|	|	|	0.00
283.917	0.00	0.00	0.004	O	|	|	|	|	0.00
284.000	0.00	0.00	0.004	O	|	|	|	|	0.00
284.083	0.00	0.00	0.004	O	|	|	|	|	0.00
284.167	0.00	0.00	0.004	O	|	|	|	|	0.00

284.250	0.00	0.00	0.004	O	|	|	|	|	0.00
284.333	0.00	0.00	0.004	O	|	|	|	|	0.00
284.417	0.00	0.00	0.004	O	|	|	|	|	0.00
284.500	0.00	0.00	0.004	O	|	|	|	|	0.00
284.583	0.00	0.00	0.004	O	|	|	|	|	0.00
284.667	0.00	0.00	0.004	O	|	|	|	|	0.00
284.750	0.00	0.00	0.004	O	|	|	|	|	0.00
284.833	0.00	0.00	0.004	O	|	|	|	|	0.00
284.917	0.00	0.00	0.004	O	|	|	|	|	0.00
285.000	0.00	0.00	0.004	O	|	|	|	|	0.00
285.083	0.00	0.00	0.004	O	|	|	|	|	0.00
285.167	0.00	0.00	0.004	O	|	|	|	|	0.00
285.250	0.00	0.00	0.004	O	|	|	|	|	0.00
285.333	0.00	0.00	0.004	O	|	|	|	|	0.00
285.417	0.00	0.00	0.004	O	|	|	|	|	0.00
285.500	0.00	0.00	0.004	O	|	|	|	|	0.00
285.583	0.00	0.00	0.004	O	|	|	|	|	0.00
285.667	0.00	0.00	0.004	O	|	|	|	|	0.00
285.750	0.00	0.00	0.004	O	|	|	|	|	0.00
285.833	0.00	0.00	0.004	O	|	|	|	|	0.00
285.917	0.00	0.00	0.004	O	|	|	|	|	0.00
286.000	0.00	0.00	0.004	O	|	|	|	|	0.00
286.083	0.00	0.00	0.004	O	|	|	|	|	0.00
286.167	0.00	0.00	0.004	O	|	|	|	|	0.00
286.250	0.00	0.00	0.004	O	|	|	|	|	0.00
286.333	0.00	0.00	0.004	O	|	|	|	|	0.00
286.417	0.00	0.00	0.004	O	|	|	|	|	0.00
286.500	0.00	0.00	0.004	O	|	|	|	|	0.00
286.583	0.00	0.00	0.004	O	|	|	|	|	0.00
286.667	0.00	0.00	0.004	O	|	|	|	|	0.00
286.750	0.00	0.00	0.004	O	|	|	|	|	0.00
286.833	0.00	0.00	0.004	O	|	|	|	|	0.00
286.917	0.00	0.00	0.004	O	|	|	|	|	0.00
287.000	0.00	0.00	0.004	O	|	|	|	|	0.00
287.083	0.00	0.00	0.004	O	|	|	|	|	0.00
287.167	0.00	0.00	0.004	O	|	|	|	|	0.00
287.250	0.00	0.00	0.004	O	|	|	|	|	0.00
287.333	0.00	0.00	0.004	O	|	|	|	|	0.00
287.417	0.00	0.00	0.004	O	|	|	|	|	0.00
287.500	0.00	0.00	0.004	O	|	|	|	|	0.00
287.583	0.00	0.00	0.004	O	|	|	|	|	0.00
287.667	0.00	0.00	0.004	O	|	|	|	|	0.00
287.750	0.00	0.00	0.004	O	|	|	|	|	0.00
287.833	0.00	0.00	0.004	O	|	|	|	|	0.00
287.917	0.00	0.00	0.004	O	|	|	|	|	0.00
288.000	0.00	0.00	0.004	O	|	|	|	|	0.00
288.083	0.00	0.00	0.004	O	|	|	|	|	0.00
288.167	0.00	0.00	0.004	O	|	|	|	|	0.00
288.250	0.00	0.00	0.004	O	|	|	|	|	0.00
288.333	0.00	0.00	0.004	O	|	|	|	|	0.00
288.417	0.00	0.00	0.004	O	|	|	|	|	0.00
288.500	0.00	0.00	0.004	O	|	|	|	|	0.00
288.583	0.00	0.00	0.004	O	|	|	|	|	0.00
288.667	0.00	0.00	0.004	O	|	|	|	|	0.00
288.750	0.00	0.00	0.004	O	|	|	|	|	0.00
288.833	0.00	0.00	0.004	O	|	|	|	|	0.00
288.917	0.00	0.00	0.004	O	|	|	|	|	0.00
289.000	0.00	0.00	0.004	O	|	|	|	|	0.00
289.083	0.00	0.00	0.004	O	|	|	|	|	0.00
289.167	0.00	0.00	0.004	O	|	|	|	|	0.00
289.250	0.00	0.00	0.004	O	|	|	|	|	0.00
289.333	0.00	0.00	0.004	O	|	|	|	|	0.00
289.417	0.00	0.00	0.004	O	|	|	|	|	0.00
289.500	0.00	0.00	0.004	O	|	|	|	|	0.00
289.583	0.00	0.00	0.004	O	|	|	|	|	0.00
289.667	0.00	0.00	0.004	O	|	|	|	|	0.00
289.750	0.00	0.00	0.004	O	|	|	|	|	0.00
289.833	0.00	0.00	0.004	O	|	|	|	|	0.00
289.917	0.00	0.00	0.004	O	|	|	|	|	0.00
290.000	0.00	0.00	0.004	O	|	|	|	|	0.00
290.083	0.00	0.00	0.004	O	|	|	|	|	0.00

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290.167    0.00    0.00      0.004  O       |       |       |       |     0.00
290.250    0.00    0.00      0.004  O       |       |       |       |     0.00
290.333    0.00    0.00      0.004  O       |       |       |       |     0.00

       Remaining water in basin =    0.00 (Ac.Ft)

       ****************************HYDROGRAPH DATA****************************
                     Number of intervals =  3484
                     Time interval =    5.0 (Min.)
                     Maximum/Peak flow rate =        0.303 (CFS)
                     Total volume =       1.891 (Ac.Ft)
              Status of hydrographs being held in storage
                        Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
              Peak (CFS)      0.000     0.000     0.000     0.000     0.000
              Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
       ************************************************************************

       ------------------------------------------------------------------


       ++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
       Process from Point/Station        1.000 to Point/Station        3.000
       **** STORE OR DELETE CURRENT HYDROGRAPH ****
       ________________________________________________________________________
       Current stream hydrograph of   5.0 minute
       intervals has been stored as stream number 1 with
       a starting time of   0.00 hours and ending time of 333.00 hours
       With a total volume of       1.89(Ac.Ft)
       ****************************HYDROGRAPH DATA****************************
                     Number of intervals =     0
                     Time interval =    0.0 (Min.)
                     Maximum/Peak flow rate =        0.000 (CFS)
                     Total volume =       0.000 (Ac.Ft)
              Status of hydrographs being held in storage
                        Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
              Peak (CFS)      0.303     0.000     0.000     0.000     0.000
              Vol (Ac.Ft)      1.891     0.000     0.000     0.000     0.000
       ************************************************************************

       ------------------------------------------------------------------


       ++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
       Process from Point/Station        1.000 to Point/Station        3.000
       **** ADD/COMBINE/RECOVER HYDROGRAPHS ****
       ________________________________________________________________________
       ********************* HYDROGRAPH INFORMATION **********************

                     From study/file name: ARA1100.rte
       ++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                        P R I N T  O F  S T O R M
                     R u n o f f     H y d r o g r a p h
       ------------------------------------------------------------------------
                   Hydrograph in   5   Minute intervals (CFS)

       ------------------------------------------------------------------------
 Time(h+m) Add q(CFS)  Tot. Q   0       69.7     139.4     209.1     278.7
 ------------------------------------------------------------------------------
   0+ 5       2.9822      2.98  Q         |         |         |         |
   0+10      15.5860     15.59  | Q       |         |         |         |
   0+15      33.8032     33.80  |   Q     |         |         |         |
   0+20      47.1866     47.19  |     Q   |         |         |         |
   0+25      57.6211     57.62  |       Q |         |         |         |
   0+30      68.0633     68.06  |        Q|         |         |         |
   0+35      81.3651     81.37  |         |Q        |         |         |
   0+40      97.2053     97.21  |         |  Q      |         |         |
   0+45     119.1714    119.17  |         |      Q  |         |         |
   0+50     171.3210    171.32  |         |         |   Q     |         |
   0+55     259.7654    259.77  |         |         |         |      Q  |
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   1+ 0     278.7369    278.74  |          |          |          |          Q
   1+ 5     191.2216    191.22  |          |          |       Q  |          |
   1+10     119.4933    119.49  |          |       Q  |          |          |
   1+15      76.9466     76.95  |          |Q         |          |          |
   1+20      54.3094     54.31  |       Q  |          |          |          |
   1+25      41.0897     41.09  |     Q    |          |          |          |
   1+30      32.4470     32.45  |   Q      |          |          |          |
   1+35      25.5408     25.54  |  Q       |          |          |          |
   1+40      20.5862     20.59  | Q        |          |          |          |
   1+45      17.2587     17.26  | Q        |          |          |          |
   1+50      13.7622     13.76  |Q         |          |          |          |
   1+55      11.1727     11.17  |Q         |          |          |          |
   2+ 0       8.8493      8.85  |Q         |          |          |          |
   2+ 5       6.8802      6.88  Q          |          |          |          |
   2+10       5.5472      5.55  Q          |          |          |          |
   2+15       4.5654      4.57  Q          |          |          |          |
   2+20       3.0891      3.09  Q          |          |          |          |
   2+25       0.7615      0.76  Q          |          |          |          |
   2+30       0.2734      0.27  Q          |          |          |          |
------------------------------------------------------------------------
      ****************************HYDROGRAPH DATA****************************
                  Number of intervals =    30
                  Time interval =    5.0 (Min.)
                  Maximum/Peak flow rate =      278.737 (CFS)
                  Total volume =      12.855 (Ac.Ft)
            Status of hydrographs being held in storage
                     Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
            Peak (CFS)      0.303     0.000     0.000     0.000     0.000
            Vol (Ac.Ft)      1.891     0.000     0.000     0.000     0.000
      ************************************************************************

      ------------------------------------------------------------------------


      ++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
      Process from Point/Station        2.000 to Point/Station        3.000
      **** ADD/COMBINE/RECOVER HYDROGRAPHS ****
      ________________________________________________________________________
      From stored stream number 1 the total
      volume of       1.89 (Ac.Ft) is being added to the
      current hydrograph at its original rate from user
      with a delay time to start of addition of    0.00 hours.
      ++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                      P R I N T  O F  S T O R M
                     R u n o f f     H y d r o g r a p h
      ------------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals (CFS)

      ------------------------------------------------------------------------
 Time(h+m) Add q(CFS)  Tot. Q   0       69.8     139.5     209.3     279.0
 ------------------------------------------------------------------------
   0+ 5       0.0042      2.99  Q          |          |          |          |
   0+10       0.0163     15.60  q Q        |          |          |          |
   0+15       0.0341     33.84  q   Q      |          |          |          |
   0+20       0.0549     47.24  q     Q    |          |          |          |
   0+25       0.0784     57.70  q       Q  |          |          |          |
   0+30       0.1054     68.17  q        Q |          |          |          |
   0+35       0.1371     81.50  q         |Q         |          |          |
   0+40       0.1729     97.38  q         |  Q       |          |          |
   0+45       0.1908    119.36  q         |       Q  |          |          |
   0+50       0.2230    171.54  q         |          |    Q     |          |
   0+55       0.2627    260.03  q         |          |          |       Q  |
   1+ 0       0.2881    279.03  q         |          |          |          Q
   1+ 5       0.2988    191.52  q         |          |       Q  |          |
   1+10       0.3024    119.80  q         |          |    Q     |          |
   1+15       0.3029     77.25  q         |Q         |          |          |
   1+20       0.3028     54.61  q       Q  |          |          |          |
   1+25       0.3026     41.39  q     Q    |          |          |          |
   1+30       0.3023     32.75  q    Q     |          |          |          |
   1+35       0.3021     25.84  q  Q       |          |          |          |
   1+40       0.3019     20.89  q Q        |          |          |          |
```

1+45	0.3017	17.56	q Q	|	|	|	|
1+50	0.3015	14.06	q Q	|	|	|	|
1+55	0.3013	11.47	qQ	|	|	|	|
2+ 0	0.3010	9.15	qQ	|	|	|	|
2+ 5	0.3008	7.18	qQ	|	|	|	|
2+10	0.3006	5.85	Q	|	|	|	|
2+15	0.3004	4.87	Q	|	|	|	|
2+20	0.3002	3.39	Q	|	|	|	|
2+25	0.3000	1.06	Q	|	|	|	|
2+30	0.2998	0.57	Q	|	|	|	|
2+35	0.2995	0.30	Q	|	|	|	|
2+40	0.2993	0.30	Q	|	|	|	|
2+45	0.2991	0.30	Q	|	|	|	|
2+50	0.2989	0.30	Q	|	|	|	|
2+55	0.2987	0.30	Q	|	|	|	|
3+ 0	0.2985	0.30	Q	|	|	|	|
3+ 5	0.2983	0.30	Q	|	|	|	|
3+10	0.2980	0.30	Q	|	|	|	|
3+15	0.2978	0.30	Q	|	|	|	|
3+20	0.2976	0.30	Q	|	|	|	|
3+25	0.2974	0.30	Q	|	|	|	|
3+30	0.2972	0.30	Q	|	|	|	|
3+35	0.2970	0.30	Q	|	|	|	|
3+40	0.2968	0.30	Q	|	|	|	|
3+45	0.2966	0.30	Q	|	|	|	|
3+50	0.2963	0.30	Q	|	|	|	|
3+55	0.2961	0.30	Q	|	|	|	|
4+ 0	0.2959	0.30	Q	|	|	|	|
4+ 5	0.2957	0.30	Q	|	|	|	|
4+10	0.2955	0.30	Q	|	|	|	|
4+15	0.2953	0.30	Q	|	|	|	|
4+20	0.2951	0.30	Q	|	|	|	|
4+25	0.2949	0.29	Q	|	|	|	|
4+30	0.2947	0.29	Q	|	|	|	|
4+35	0.2944	0.29	Q	|	|	|	|
4+40	0.2942	0.29	Q	|	|	|	|
4+45	0.2940	0.29	Q	|	|	|	|
4+50	0.2938	0.29	Q	|	|	|	|
4+55	0.2936	0.29	Q	|	|	|	|
5+ 0	0.2934	0.29	Q	|	|	|	|
5+ 5	0.2932	0.29	Q	|	|	|	|
5+10	0.2930	0.29	Q	|	|	|	|
5+15	0.2928	0.29	Q	|	|	|	|
5+20	0.2926	0.29	Q	|	|	|	|
5+25	0.2923	0.29	Q	|	|	|	|
5+30	0.2921	0.29	Q	|	|	|	|
5+35	0.2919	0.29	Q	|	|	|	|
5+40	0.2917	0.29	Q	|	|	|	|
5+45	0.2915	0.29	Q	|	|	|	|
5+50	0.2913	0.29	Q	|	|	|	|
5+55	0.2911	0.29	Q	|	|	|	|
6+ 0	0.2909	0.29	Q	|	|	|	|
6+ 5	0.2907	0.29	Q	|	|	|	|
6+10	0.2905	0.29	Q	|	|	|	|
6+15	0.2903	0.29	Q	|	|	|	|
6+20	0.2901	0.29	Q	|	|	|	|
6+25	0.2899	0.29	Q	|	|	|	|
6+30	0.2896	0.29	Q	|	|	|	|
6+35	0.2894	0.29	Q	|	|	|	|
6+40	0.2892	0.29	Q	|	|	|	|
6+45	0.2890	0.29	Q	|	|	|	|
6+50	0.2888	0.29	Q	|	|	|	|
6+55	0.2886	0.29	Q	|	|	|	|
7+ 0	0.2884	0.29	Q	|	|	|	|
7+ 5	0.2882	0.29	Q	|	|	|	|
7+10	0.2880	0.29	Q	|	|	|	|
7+15	0.2878	0.29	Q	|	|	|	|
7+20	0.2876	0.29	Q	|	|	|	|
7+25	0.2874	0.29	Q	|	|	|	|
7+30	0.2872	0.29	Q	|	|	|	|
7+35	0.2870	0.29	Q	|	|	|	|

7+40	0.2868	0.29	Q				
7+45	0.2866	0.29	Q				
7+50	0.2864	0.29	Q				
7+55	0.2861	0.29	Q				
8+ 0	0.2859	0.29	Q				
8+ 5	0.2857	0.29	Q				
8+10	0.2855	0.29	Q				
8+15	0.2853	0.29	Q				
8+20	0.2851	0.29	Q				
8+25	0.2849	0.28	Q				
8+30	0.2847	0.28	Q				
8+35	0.2845	0.28	Q				
8+40	0.2843	0.28	Q				
8+45	0.2841	0.28	Q				
8+50	0.2839	0.28	Q				
8+55	0.2837	0.28	Q				
9+ 0	0.2835	0.28	Q				
9+ 5	0.2833	0.28	Q				
9+10	0.2831	0.28	Q				
9+15	0.2829	0.28	Q				
9+20	0.2827	0.28	Q				
9+25	0.2825	0.28	Q				
9+30	0.2823	0.28	Q				
9+35	0.2821	0.28	Q				
9+40	0.2819	0.28	Q				
9+45	0.2817	0.28	Q				
9+50	0.2815	0.28	Q				
9+55	0.2813	0.28	Q				
10+ 0	0.2811	0.28	Q				
10+ 5	0.2809	0.28	Q				
10+10	0.2807	0.28	Q				
10+15	0.2805	0.28	Q				
10+20	0.2803	0.28	Q				
10+25	0.2801	0.28	Q				
10+30	0.2799	0.28	Q				
10+35	0.2797	0.28	Q				
10+40	0.2795	0.28	Q				
10+45	0.2793	0.28	Q				
10+50	0.2791	0.28	Q				
10+55	0.2789	0.28	Q				
11+ 0	0.2787	0.28	Q				
11+ 5	0.2785	0.28	Q				
11+10	0.2783	0.28	Q				
11+15	0.2781	0.28	Q				
11+20	0.2779	0.28	Q				
11+25	0.2777	0.28	Q				
11+30	0.2775	0.28	Q				
11+35	0.2773	0.28	Q				
11+40	0.2771	0.28	Q				
11+45	0.2769	0.28	Q				
11+50	0.2767	0.28	Q				
11+55	0.2765	0.28	Q				
12+ 0	0.2763	0.28	Q				
12+ 5	0.2761	0.28	Q				
12+10	0.2759	0.28	Q				
12+15	0.2757	0.28	Q				
12+20	0.2755	0.28	Q				
12+25	0.2753	0.28	Q				
12+30	0.2751	0.28	Q				
12+35	0.2749	0.27	Q				
12+40	0.2747	0.27	Q				
12+45	0.2745	0.27	Q				
12+50	0.2743	0.27	Q				
12+55	0.2741	0.27	Q				
13+ 0	0.2739	0.27	Q				
13+ 5	0.2737	0.27	Q				
13+10	0.2735	0.27	Q				
13+15	0.2734	0.27	Q				
13+20	0.2732	0.27	Q				
13+25	0.2730	0.27	Q				
13+30	0.2728	0.27	Q				

13+35	0.2726	0.27	Q				
13+40	0.2724	0.27	Q				
13+45	0.2722	0.27	Q				
13+50	0.2720	0.27	Q				
13+55	0.2718	0.27	Q				
14+ 0	0.2716	0.27	Q				
14+ 5	0.2714	0.27	Q				
14+10	0.2712	0.27	Q				
14+15	0.2710	0.27	Q				
14+20	0.2708	0.27	Q				
14+25	0.2706	0.27	Q				
14+30	0.2704	0.27	Q				
14+35	0.2702	0.27	Q				
14+40	0.2701	0.27	Q				
14+45	0.2699	0.27	Q				
14+50	0.2697	0.27	Q				
14+55	0.2695	0.27	Q				
15+ 0	0.2693	0.27	Q				
15+ 5	0.2691	0.27	Q				
15+10	0.2689	0.27	Q				
15+15	0.2687	0.27	Q				
15+20	0.2685	0.27	Q				
15+25	0.2683	0.27	Q				
15+30	0.2681	0.27	Q				
15+35	0.2679	0.27	Q				
15+40	0.2677	0.27	Q				
15+45	0.2676	0.27	Q				
15+50	0.2674	0.27	Q				
15+55	0.2672	0.27	Q				
16+ 0	0.2670	0.27	Q				
16+ 5	0.2668	0.27	Q				
16+10	0.2666	0.27	Q				
16+15	0.2664	0.27	Q				
16+20	0.2662	0.27	Q				
16+25	0.2660	0.27	Q				
16+30	0.2658	0.27	Q				
16+35	0.2656	0.27	Q				
16+40	0.2655	0.27	Q				
16+45	0.2653	0.27	Q				
16+50	0.2651	0.27	Q				
16+55	0.2649	0.26	Q				
17+ 0	0.2647	0.26	Q				
17+ 5	0.2645	0.26	Q				
17+10	0.2643	0.26	Q				
17+15	0.2641	0.26	Q				
17+20	0.2639	0.26	Q				
17+25	0.2638	0.26	Q				
17+30	0.2636	0.26	Q				
17+35	0.2634	0.26	Q				
17+40	0.2632	0.26	Q				
17+45	0.2630	0.26	Q				
17+50	0.2628	0.26	Q				
17+55	0.2626	0.26	Q				
18+ 0	0.2624	0.26	Q				
18+ 5	0.2623	0.26	Q				
18+10	0.2621	0.26	Q				
18+15	0.2619	0.26	Q				
18+20	0.2617	0.26	Q				
18+25	0.2615	0.26	Q				
18+30	0.2613	0.26	Q				
18+35	0.2611	0.26	Q				
18+40	0.2609	0.26	Q				
18+45	0.2608	0.26	Q				
18+50	0.2606	0.26	Q				
18+55	0.2604	0.26	Q				
19+ 0	0.2602	0.26	Q				
19+ 5	0.2600	0.26	Q				
19+10	0.2598	0.26	Q				
19+15	0.2596	0.26	Q				
19+20	0.2595	0.26	Q				
19+25	0.2593	0.26	Q				

19+30	0.2591	0.26	Q				
19+35	0.2589	0.26	Q				
19+40	0.2587	0.26	Q				
19+45	0.2585	0.26	Q				
19+50	0.2583	0.26	Q				
19+55	0.2582	0.26	Q				
20+ 0	0.2580	0.26	Q				
20+ 5	0.2578	0.26	Q				
20+10	0.2576	0.26	Q				
20+15	0.2574	0.26	Q				
20+20	0.2572	0.26	Q				
20+25	0.2571	0.26	Q				
20+30	0.2569	0.26	Q				
20+35	0.2567	0.26	Q				
20+40	0.2565	0.26	Q				
20+45	0.2563	0.26	Q				
20+50	0.2561	0.26	Q				
20+55	0.2560	0.26	Q				
21+ 0	0.2558	0.26	Q				
21+ 5	0.2556	0.26	Q				
21+10	0.2554	0.26	Q				
21+15	0.2552	0.26	Q				
21+20	0.2550	0.26	Q				
21+25	0.2549	0.25	Q				
21+30	0.2547	0.25	Q				
21+35	0.2545	0.25	Q				
21+40	0.2543	0.25	Q				
21+45	0.2541	0.25	Q				
21+50	0.2540	0.25	Q				
21+55	0.2538	0.25	Q				
22+ 0	0.2536	0.25	Q				
22+ 5	0.2534	0.25	Q				
22+10	0.2532	0.25	Q				
22+15	0.2530	0.25	Q				
22+20	0.2529	0.25	Q				
22+25	0.2527	0.25	Q				
22+30	0.2525	0.25	Q				
22+35	0.2523	0.25	Q				
22+40	0.2521	0.25	Q				
22+45	0.2520	0.25	Q				
22+50	0.2518	0.25	Q				
22+55	0.2516	0.25	Q				
23+ 0	0.2514	0.25	Q				
23+ 5	0.2512	0.25	Q				
23+10	0.2511	0.25	Q				
23+15	0.2509	0.25	Q				
23+20	0.2507	0.25	Q				
23+25	0.2505	0.25	Q				
23+30	0.2503	0.25	Q				
23+35	0.2502	0.25	Q				
23+40	0.2500	0.25	Q				
23+45	0.2498	0.25	Q				
23+50	0.2496	0.25	Q				
23+55	0.2495	0.25	Q				
24+ 0	0.2493	0.25	Q				
24+ 5	0.2491	0.25	Q				
24+10	0.2489	0.25	Q				
24+15	0.2487	0.25	Q				
24+20	0.2486	0.25	Q				
24+25	0.2484	0.25	Q				
24+30	0.2482	0.25	Q				
24+35	0.2480	0.25	Q				
24+40	0.2479	0.25	Q				
24+45	0.2477	0.25	Q				
24+50	0.2475	0.25	Q				
24+55	0.2473	0.25	Q				
25+ 0	0.2471	0.25	Q				
25+ 5	0.2470	0.25	Q				
25+10	0.2468	0.25	Q				
25+15	0.2466	0.25	Q				
25+20	0.2464	0.25	Q				

25+25	0.2463	0.25	Q	|	|	|	|
25+30	0.2461	0.25	Q	|	|	|	|
25+35	0.2459	0.25	Q	|	|	|	|
25+40	0.2457	0.25	Q	|	|	|	|
25+45	0.2456	0.25	Q	|	|	|	|
25+50	0.2454	0.25	Q	|	|	|	|
25+55	0.2452	0.25	Q	|	|	|	|
26+ 0	0.2450	0.25	Q	|	|	|	|
26+ 5	0.2449	0.24	Q	|	|	|	|
26+10	0.2447	0.24	Q	|	|	|	|
26+15	0.2445	0.24	Q	|	|	|	|
26+20	0.2443	0.24	Q	|	|	|	|
26+25	0.2442	0.24	Q	|	|	|	|
26+30	0.2440	0.24	Q	|	|	|	|
26+35	0.2438	0.24	Q	|	|	|	|
26+40	0.2436	0.24	Q	|	|	|	|
26+45	0.2435	0.24	Q	|	|	|	|
26+50	0.2433	0.24	Q	|	|	|	|
26+55	0.2431	0.24	Q	|	|	|	|
27+ 0	0.2429	0.24	Q	|	|	|	|
27+ 5	0.2428	0.24	Q	|	|	|	|
27+10	0.2426	0.24	Q	|	|	|	|
27+15	0.2424	0.24	Q	|	|	|	|
27+20	0.2422	0.24	Q	|	|	|	|
27+25	0.2421	0.24	Q	|	|	|	|
27+30	0.2419	0.24	Q	|	|	|	|
27+35	0.2417	0.24	Q	|	|	|	|
27+40	0.2416	0.24	Q	|	|	|	|
27+45	0.2414	0.24	Q	|	|	|	|
27+50	0.2412	0.24	Q	|	|	|	|
27+55	0.2410	0.24	Q	|	|	|	|
28+ 0	0.2409	0.24	Q	|	|	|	|
28+ 5	0.2407	0.24	Q	|	|	|	|
28+10	0.2405	0.24	Q	|	|	|	|
28+15	0.2404	0.24	Q	|	|	|	|
28+20	0.2402	0.24	Q	|	|	|	|
28+25	0.2400	0.24	Q	|	|	|	|
28+30	0.2398	0.24	Q	|	|	|	|
28+35	0.2397	0.24	Q	|	|	|	|
28+40	0.2395	0.24	Q	|	|	|	|
28+45	0.2393	0.24	Q	|	|	|	|
28+50	0.2392	0.24	Q	|	|	|	|
28+55	0.2390	0.24	Q	|	|	|	|
29+ 0	0.2388	0.24	Q	|	|	|	|
29+ 5	0.2386	0.24	Q	|	|	|	|
29+10	0.2385	0.24	Q	|	|	|	|
29+15	0.2383	0.24	Q	|	|	|	|
29+20	0.2381	0.24	Q	|	|	|	|
29+25	0.2380	0.24	Q	|	|	|	|
29+30	0.2378	0.24	Q	|	|	|	|
29+35	0.2376	0.24	Q	|	|	|	|
29+40	0.2374	0.24	Q	|	|	|	|
29+45	0.2373	0.24	Q	|	|	|	|
29+50	0.2371	0.24	Q	|	|	|	|
29+55	0.2369	0.24	Q	|	|	|	|
30+ 0	0.2368	0.24	Q	|	|	|	|
30+ 5	0.2366	0.24	Q	|	|	|	|
30+10	0.2364	0.24	Q	|	|	|	|
30+15	0.2363	0.24	Q	|	|	|	|
30+20	0.2361	0.24	Q	|	|	|	|
30+25	0.2359	0.24	Q	|	|	|	|
30+30	0.2358	0.24	Q	|	|	|	|
30+35	0.2356	0.24	Q	|	|	|	|
30+40	0.2354	0.24	Q	|	|	|	|
30+45	0.2353	0.24	Q	|	|	|	|
30+50	0.2351	0.24	Q	|	|	|	|
30+55	0.2349	0.23	Q	|	|	|	|
31+ 0	0.2347	0.23	Q	|	|	|	|
31+ 5	0.2346	0.23	Q	|	|	|	|
31+10	0.2344	0.23	Q	|	|	|	|
31+15	0.2342	0.23	Q	|	|	|	|

31+20	0.2341	0.23	Q			Q	
31+25	0.2339	0.23	Q			Q	
31+30	0.2337	0.23	Q			Q	
31+35	0.2336	0.23	Q			Q	
31+40	0.2334	0.23	Q			Q	
31+45	0.2332	0.23	Q			Q	
31+50	0.2331	0.23	Q			Q	
31+55	0.2329	0.23	Q			Q	
32+ 0	0.2327	0.23	Q			Q	
32+ 5	0.2326	0.23	Q			Q	
32+10	0.2324	0.23	Q			Q	
32+15	0.2322	0.23	Q			Q	
32+20	0.2321	0.23	Q			Q	
32+25	0.2319	0.23	Q			Q	
32+30	0.2317	0.23	Q			Q	
32+35	0.2316	0.23	Q			Q	
32+40	0.2314	0.23	Q			Q	
32+45	0.2313	0.23	Q			Q	
32+50	0.2311	0.23	Q			Q	
32+55	0.2309	0.23	Q			Q	
33+ 0	0.2308	0.23	Q			Q	
33+ 5	0.2306	0.23	Q			Q	
33+10	0.2304	0.23	Q			Q	
33+15	0.2303	0.23	Q			Q	
33+20	0.2301	0.23	Q			Q	
33+25	0.2299	0.23	Q			Q	
33+30	0.2298	0.23	Q			Q	
33+35	0.2296	0.23	Q			Q	
33+40	0.2294	0.23	Q			Q	
33+45	0.2293	0.23	Q			Q	
33+50	0.2291	0.23	Q			Q	
33+55	0.2289	0.23	Q			Q	
34+ 0	0.2288	0.23	Q			Q	
34+ 5	0.2286	0.23	Q			Q	
34+10	0.2285	0.23	Q			Q	
34+15	0.2283	0.23	Q			Q	
34+20	0.2281	0.23	Q			Q	
34+25	0.2280	0.23	Q			Q	
34+30	0.2278	0.23	Q			Q	
34+35	0.2276	0.23	Q			Q	
34+40	0.2275	0.23	Q			Q	
34+45	0.2273	0.23	Q			Q	
34+50	0.2272	0.23	Q			Q	
34+55	0.2270	0.23	Q			Q	
35+ 0	0.2268	0.23	Q			Q	
35+ 5	0.2267	0.23	Q			Q	
35+10	0.2265	0.23	Q			Q	
35+15	0.2263	0.23	Q			Q	
35+20	0.2262	0.23	Q			Q	
35+25	0.2260	0.23	Q			Q	
35+30	0.2259	0.23	Q			Q	
35+35	0.2257	0.23	Q			Q	
35+40	0.2255	0.23	Q			Q	
35+45	0.2254	0.23	Q			Q	
35+50	0.2252	0.23	Q			Q	
35+55	0.2251	0.23	Q			Q	
36+ 0	0.2249	0.22	Q			Q	
36+ 5	0.2247	0.22	Q			Q	
36+10	0.2246	0.22	Q			Q	
36+15	0.2244	0.22	Q			Q	
36+20	0.2243	0.22	Q			Q	
36+25	0.2241	0.22	Q			Q	
36+30	0.2239	0.22	Q			Q	
36+35	0.2238	0.22	Q			Q	
36+40	0.2236	0.22	Q			Q	
36+45	0.2235	0.22	Q			Q	
36+50	0.2233	0.22	Q			Q	
36+55	0.2231	0.22	Q			Q	
37+ 0	0.2230	0.22	Q			Q	
37+ 5	0.2228	0.22	Q			Q	
37+10	0.2227	0.22	Q			Q	

37+15	0.2225	0.22	Q				
37+20	0.2223	0.22	Q				
37+25	0.2222	0.22	Q				
37+30	0.2220	0.22	Q				
37+35	0.2219	0.22	Q				
37+40	0.2217	0.22	Q				
37+45	0.2215	0.22	Q				
37+50	0.2214	0.22	Q				
37+55	0.2212	0.22	Q				
38+ 0	0.2211	0.22	Q				
38+ 5	0.2209	0.22	Q				
38+10	0.2208	0.22	Q				
38+15	0.2206	0.22	Q				
38+20	0.2204	0.22	Q				
38+25	0.2203	0.22	Q				
38+30	0.2201	0.22	Q				
38+35	0.2200	0.22	Q				
38+40	0.2198	0.22	Q				
38+45	0.2197	0.22	Q				
38+50	0.2195	0.22	Q				
38+55	0.2193	0.22	Q				
39+ 0	0.2192	0.22	Q				
39+ 5	0.2190	0.22	Q				
39+10	0.2189	0.22	Q				
39+15	0.2187	0.22	Q				
39+20	0.2186	0.22	Q				
39+25	0.2184	0.22	Q				
39+30	0.2182	0.22	Q				
39+35	0.2181	0.22	Q				
39+40	0.2179	0.22	Q				
39+45	0.2178	0.22	Q				
39+50	0.2176	0.22	Q				
39+55	0.2175	0.22	Q				
40+ 0	0.2173	0.22	Q				
40+ 5	0.2172	0.22	Q				
40+10	0.2170	0.22	Q				
40+15	0.2168	0.22	Q				
40+20	0.2167	0.22	Q				
40+25	0.2165	0.22	Q				
40+30	0.2164	0.22	Q				
40+35	0.2162	0.22	Q				
40+40	0.2161	0.22	Q				
40+45	0.2159	0.22	Q				
40+50	0.2158	0.22	Q				
40+55	0.2156	0.22	Q				
41+ 0	0.2155	0.22	Q				
41+ 5	0.2153	0.22	Q				
41+10	0.2151	0.22	Q				
41+15	0.2150	0.21	Q				
41+20	0.2148	0.21	Q				
41+25	0.2147	0.21	Q				
41+30	0.2145	0.21	Q				
41+35	0.2144	0.21	Q				
41+40	0.2142	0.21	Q				
41+45	0.2141	0.21	Q				
41+50	0.2139	0.21	Q				
41+55	0.2138	0.21	Q				
42+ 0	0.2136	0.21	Q				
42+ 5	0.2135	0.21	Q				
42+10	0.2133	0.21	Q				
42+15	0.2132	0.21	Q				
42+20	0.2130	0.21	Q				
42+25	0.2129	0.21	Q				
42+30	0.2127	0.21	Q				
42+35	0.2125	0.21	Q				
42+40	0.2124	0.21	Q				
42+45	0.2122	0.21	Q				
42+50	0.2121	0.21	Q				
42+55	0.2119	0.21	Q				
43+ 0	0.2118	0.21	Q				
43+ 5	0.2116	0.21	Q				

43+10	0.2115	0.21	Q				
43+15	0.2113	0.21	Q				
43+20	0.2112	0.21	Q				
43+25	0.2110	0.21	Q				
43+30	0.2109	0.21	Q				
43+35	0.2107	0.21	Q				
43+40	0.2106	0.21	Q				
43+45	0.2104	0.21	Q				
43+50	0.2103	0.21	Q				
43+55	0.2101	0.21	Q				
44+ 0	0.2100	0.21	Q				
44+ 5	0.2098	0.21	Q				
44+10	0.2097	0.21	Q				
44+15	0.2095	0.21	Q				
44+20	0.2094	0.21	Q				
44+25	0.2092	0.21	Q				
44+30	0.2091	0.21	Q				
44+35	0.2089	0.21	Q				
44+40	0.2088	0.21	Q				
44+45	0.2086	0.21	Q				
44+50	0.2085	0.21	Q				
44+55	0.2083	0.21	Q				
45+ 0	0.2082	0.21	Q				
45+ 5	0.2080	0.21	Q				
45+10	0.2079	0.21	Q				
45+15	0.2077	0.21	Q				
45+20	0.2076	0.21	Q				
45+25	0.2074	0.21	Q				
45+30	0.2073	0.21	Q				
45+35	0.2071	0.21	Q				
45+40	0.2070	0.21	Q				
45+45	0.2069	0.21	Q				
45+50	0.2067	0.21	Q				
45+55	0.2066	0.21	Q				
46+ 0	0.2064	0.21	Q				
46+ 5	0.2063	0.21	Q				
46+10	0.2061	0.21	Q				
46+15	0.2060	0.21	Q				
46+20	0.2058	0.21	Q				
46+25	0.2057	0.21	Q				
46+30	0.2055	0.21	Q				
46+35	0.2054	0.21	Q				
46+40	0.2052	0.21	Q				
46+45	0.2051	0.21	Q				
46+50	0.2049	0.20	Q				
46+55	0.2048	0.20	Q				
47+ 0	0.2046	0.20	Q				
47+ 5	0.2045	0.20	Q				
47+10	0.2044	0.20	Q				
47+15	0.2042	0.20	Q				
47+20	0.2041	0.20	Q				
47+25	0.2039	0.20	Q				
47+30	0.2038	0.20	Q				
47+35	0.2036	0.20	Q				
47+40	0.2035	0.20	Q				
47+45	0.2033	0.20	Q				
47+50	0.2032	0.20	Q				
47+55	0.2030	0.20	Q				
48+ 0	0.2029	0.20	Q				
48+ 5	0.2028	0.20	Q				
48+10	0.2026	0.20	Q				
48+15	0.2025	0.20	Q				
48+20	0.2023	0.20	Q				
48+25	0.2022	0.20	Q				
48+30	0.2020	0.20	Q				
48+35	0.2019	0.20	Q				
48+40	0.2017	0.20	Q				
48+45	0.2016	0.20	Q				
48+50	0.2015	0.20	Q				
48+55	0.2013	0.20	Q				
49+ 0	0.2012	0.20	Q				

49+ 5	0.2010	0.20	Q				
49+10	0.2009	0.20	Q				
49+15	0.2007	0.20	Q				
49+20	0.2006	0.20	Q				
49+25	0.2004	0.20	Q				
49+30	0.2003	0.20	Q				
49+35	0.2002	0.20	Q				
49+40	0.2000	0.20	Q				
49+45	0.1999	0.20	Q				
49+50	0.1997	0.20	Q				
49+55	0.1996	0.20	Q				
50+ 0	0.1994	0.20	Q				
50+ 5	0.1993	0.20	Q				
50+10	0.1992	0.20	Q				
50+15	0.1990	0.20	Q				
50+20	0.1989	0.20	Q				
50+25	0.1987	0.20	Q				
50+30	0.1986	0.20	Q				
50+35	0.1985	0.20	Q				
50+40	0.1983	0.20	Q				
50+45	0.1982	0.20	Q				
50+50	0.1980	0.20	Q				
50+55	0.1979	0.20	Q				
51+ 0	0.1977	0.20	Q				
51+ 5	0.1976	0.20	Q				
51+10	0.1975	0.20	Q				
51+15	0.1973	0.20	Q				
51+20	0.1972	0.20	Q				
51+25	0.1970	0.20	Q				
51+30	0.1969	0.20	Q				
51+35	0.1968	0.20	Q				
51+40	0.1966	0.20	Q				
51+45	0.1965	0.20	Q				
51+50	0.1963	0.20	Q				
51+55	0.1962	0.20	Q				
52+ 0	0.1961	0.20	Q				
52+ 5	0.1959	0.20	Q				
52+10	0.1958	0.20	Q				
52+15	0.1956	0.20	Q				
52+20	0.1955	0.20	Q				
52+25	0.1954	0.20	Q				
52+30	0.1952	0.20	Q				
52+35	0.1951	0.20	Q				
52+40	0.1949	0.19	Q				
52+45	0.1948	0.19	Q				
52+50	0.1947	0.19	Q				
52+55	0.1945	0.19	Q				
53+ 0	0.1944	0.19	Q				
53+ 5	0.1942	0.19	Q				
53+10	0.1941	0.19	Q				
53+15	0.1940	0.19	Q				
53+20	0.1938	0.19	Q				
53+25	0.1937	0.19	Q				
53+30	0.1936	0.19	Q				
53+35	0.1934	0.19	Q				
53+40	0.1933	0.19	Q				
53+45	0.1931	0.19	Q				
53+50	0.1930	0.19	Q				
53+55	0.1929	0.19	Q				
54+ 0	0.1927	0.19	Q				
54+ 5	0.1926	0.19	Q				
54+10	0.1924	0.19	Q				
54+15	0.1923	0.19	Q				
54+20	0.1922	0.19	Q				
54+25	0.1920	0.19	Q				
54+30	0.1919	0.19	Q				
54+35	0.1918	0.19	Q				
54+40	0.1916	0.19	Q				
54+45	0.1915	0.19	Q				
54+50	0.1913	0.19	Q				
54+55	0.1912	0.19	Q				

55+ 0	0.1911	0.19	Q				
55+ 5	0.1909	0.19	Q				
55+10	0.1908	0.19	Q				
55+15	0.1907	0.19	Q				
55+20	0.1905	0.19	Q				
55+25	0.1904	0.19	Q				
55+30	0.1903	0.19	Q				
55+35	0.1901	0.19	Q				
55+40	0.1900	0.19	Q				
55+45	0.1899	0.19	Q				
55+50	0.1897	0.19	Q				
55+55	0.1896	0.19	Q				
56+ 0	0.1894	0.19	Q				
56+ 5	0.1893	0.19	Q				
56+10	0.1892	0.19	Q				
56+15	0.1890	0.19	Q				
56+20	0.1889	0.19	Q				
56+25	0.1888	0.19	Q				
56+30	0.1886	0.19	Q				
56+35	0.1885	0.19	Q				
56+40	0.1884	0.19	Q				
56+45	0.1882	0.19	Q				
56+50	0.1881	0.19	Q				
56+55	0.1880	0.19	Q				
57+ 0	0.1878	0.19	Q				
57+ 5	0.1877	0.19	Q				
57+10	0.1876	0.19	Q				
57+15	0.1874	0.19	Q				
57+20	0.1873	0.19	Q				
57+25	0.1872	0.19	Q				
57+30	0.1870	0.19	Q				
57+35	0.1869	0.19	Q				
57+40	0.1868	0.19	Q				
57+45	0.1866	0.19	Q				
57+50	0.1865	0.19	Q				
57+55	0.1864	0.19	Q				
58+ 0	0.1862	0.19	Q				
58+ 5	0.1861	0.19	Q				
58+10	0.1860	0.19	Q				
58+15	0.1858	0.19	Q				
58+20	0.1857	0.19	Q				
58+25	0.1856	0.19	Q				
58+30	0.1854	0.19	Q				
58+35	0.1853	0.19	Q				
58+40	0.1852	0.19	Q				
58+45	0.1850	0.19	Q				
58+50	0.1849	0.18	Q				
58+55	0.1848	0.18	Q				
59+ 0	0.1846	0.18	Q				
59+ 5	0.1845	0.18	Q				
59+10	0.1844	0.18	Q				
59+15	0.1842	0.18	Q				
59+20	0.1841	0.18	Q				
59+25	0.1840	0.18	Q				
59+30	0.1838	0.18	Q				
59+35	0.1837	0.18	Q				
59+40	0.1836	0.18	Q				
59+45	0.1834	0.18	Q				
59+50	0.1833	0.18	Q				
59+55	0.1832	0.18	Q				
60+ 0	0.1831	0.18	Q				
60+ 5	0.1829	0.18	Q				
60+10	0.1828	0.18	Q				
60+15	0.1827	0.18	Q				
60+20	0.1825	0.18	Q				
60+25	0.1824	0.18	Q				
60+30	0.1823	0.18	Q				
60+35	0.1821	0.18	Q				
60+40	0.1820	0.18	Q				
60+45	0.1819	0.18	Q				
60+50	0.1818	0.18	Q				

60+55	0.1816	0.18	Q				
61+ 0	0.1815	0.18	Q				
61+ 5	0.1814	0.18	Q				
61+10	0.1812	0.18	Q				
61+15	0.1811	0.18	Q				
61+20	0.1810	0.18	Q				
61+25	0.1808	0.18	Q				
61+30	0.1807	0.18	Q				
61+35	0.1806	0.18	Q				
61+40	0.1805	0.18	Q				
61+45	0.1803	0.18	Q				
61+50	0.1802	0.18	Q				
61+55	0.1801	0.18	Q				
62+ 0	0.1799	0.18	Q				
62+ 5	0.1798	0.18	Q				
62+10	0.1797	0.18	Q				
62+15	0.1796	0.18	Q				
62+20	0.1794	0.18	Q				
62+25	0.1793	0.18	Q				
62+30	0.1792	0.18	Q				
62+35	0.1790	0.18	Q				
62+40	0.1789	0.18	Q				
62+45	0.1788	0.18	Q				
62+50	0.1787	0.18	Q				
62+55	0.1785	0.18	Q				
63+ 0	0.1784	0.18	Q				
63+ 5	0.1783	0.18	Q				
63+10	0.1782	0.18	Q				
63+15	0.1780	0.18	Q				
63+20	0.1779	0.18	Q				
63+25	0.1778	0.18	Q				
63+30	0.1776	0.18	Q				
63+35	0.1775	0.18	Q				
63+40	0.1774	0.18	Q				
63+45	0.1773	0.18	Q				
63+50	0.1771	0.18	Q				
63+55	0.1770	0.18	Q				
64+ 0	0.1769	0.18	Q				
64+ 5	0.1768	0.18	Q				
64+10	0.1766	0.18	Q				
64+15	0.1765	0.18	Q				
64+20	0.1764	0.18	Q				
64+25	0.1763	0.18	Q				
64+30	0.1761	0.18	Q				
64+35	0.1760	0.18	Q				
64+40	0.1759	0.18	Q				
64+45	0.1757	0.18	Q				
64+50	0.1756	0.18	Q				
64+55	0.1755	0.18	Q				
65+ 0	0.1754	0.18	Q				
65+ 5	0.1752	0.18	Q				
65+10	0.1751	0.18	Q				
65+15	0.1750	0.17	Q				
65+20	0.1749	0.17	Q				
65+25	0.1747	0.17	Q				
65+30	0.1746	0.17	Q				
65+35	0.1745	0.17	Q				
65+40	0.1744	0.17	Q				
65+45	0.1742	0.17	Q				
65+50	0.1741	0.17	Q				
65+55	0.1740	0.17	Q				
66+ 0	0.1739	0.17	Q				
66+ 5	0.1737	0.17	Q				
66+10	0.1736	0.17	Q				
66+15	0.1735	0.17	Q				
66+20	0.1734	0.17	Q				
66+25	0.1733	0.17	Q				
66+30	0.1731	0.17	Q				
66+35	0.1730	0.17	Q				
66+40	0.1729	0.17	Q				
66+45	0.1728	0.17	Q				

66+50	0.1726	0.17	Q				
66+55	0.1725	0.17	Q				
67+ 0	0.1724	0.17	Q				
67+ 5	0.1723	0.17	Q				
67+10	0.1721	0.17	Q				
67+15	0.1720	0.17	Q				
67+20	0.1717	0.17	Q				
67+25	0.1714	0.17	Q				
67+30	0.1711	0.17	Q				
67+35	0.1707	0.17	Q				
67+40	0.1704	0.17	Q				
67+45	0.1701	0.17	Q				
67+50	0.1698	0.17	Q				
67+55	0.1694	0.17	Q				
68+ 0	0.1691	0.17	Q				
68+ 5	0.1688	0.17	Q				
68+10	0.1685	0.17	Q				
68+15	0.1681	0.17	Q				
68+20	0.1678	0.17	Q				
68+25	0.1675	0.17	Q				
68+30	0.1672	0.17	Q				
68+35	0.1668	0.17	Q				
68+40	0.1665	0.17	Q				
68+45	0.1662	0.17	Q				
68+50	0.1659	0.17	Q				
68+55	0.1656	0.17	Q				
69+ 0	0.1652	0.17	Q				
69+ 5	0.1649	0.16	Q				
69+10	0.1646	0.16	Q				
69+15	0.1643	0.16	Q				
69+20	0.1640	0.16	Q				
69+25	0.1637	0.16	Q				
69+30	0.1633	0.16	Q				
69+35	0.1630	0.16	Q				
69+40	0.1627	0.16	Q				
69+45	0.1624	0.16	Q				
69+50	0.1621	0.16	Q				
69+55	0.1618	0.16	Q				
70+ 0	0.1615	0.16	Q				
70+ 5	0.1612	0.16	Q				
70+10	0.1609	0.16	Q				
70+15	0.1605	0.16	Q				
70+20	0.1602	0.16	Q				
70+25	0.1599	0.16	Q				
70+30	0.1596	0.16	Q				
70+35	0.1593	0.16	Q				
70+40	0.1590	0.16	Q				
70+45	0.1587	0.16	Q				
70+50	0.1584	0.16	Q				
70+55	0.1581	0.16	Q				
71+ 0	0.1578	0.16	Q				
71+ 5	0.1575	0.16	Q				
71+10	0.1572	0.16	Q				
71+15	0.1569	0.16	Q				
71+20	0.1566	0.16	Q				
71+25	0.1563	0.16	Q				
71+30	0.1560	0.16	Q				
71+35	0.1557	0.16	Q				
71+40	0.1554	0.16	Q				
71+45	0.1551	0.16	Q				
71+50	0.1548	0.15	Q				
71+55	0.1545	0.15	Q				
72+ 0	0.1542	0.15	Q				
72+ 5	0.1539	0.15	Q				
72+10	0.1536	0.15	Q				
72+15	0.1533	0.15	Q				
72+20	0.1530	0.15	Q				
72+25	0.1527	0.15	Q				
72+30	0.1524	0.15	Q				
72+35	0.1521	0.15	Q				
72+40	0.1518	0.15	Q				

72+45	0.1515	0.15	Q				
72+50	0.1513	0.15	Q				
72+55	0.1510	0.15	Q				
73+ 0	0.1507	0.15	Q				
73+ 5	0.1504	0.15	Q				
73+10	0.1501	0.15	Q				
73+15	0.1498	0.15	Q				
73+20	0.1495	0.15	Q				
73+25	0.1492	0.15	Q				
73+30	0.1489	0.15	Q				
73+35	0.1487	0.15	Q				
73+40	0.1484	0.15	Q				
73+45	0.1481	0.15	Q				
73+50	0.1478	0.15	Q				
73+55	0.1475	0.15	Q				
74+ 0	0.1472	0.15	Q				
74+ 5	0.1470	0.15	Q				
74+10	0.1467	0.15	Q				
74+15	0.1464	0.15	Q				
74+20	0.1461	0.15	Q				
74+25	0.1458	0.15	Q				
74+30	0.1455	0.15	Q				
74+35	0.1453	0.15	Q				
74+40	0.1450	0.14	Q				
74+45	0.1447	0.14	Q				
74+50	0.1444	0.14	Q				
74+55	0.1442	0.14	Q				
75+ 0	0.1439	0.14	Q				
75+ 5	0.1436	0.14	Q				
75+10	0.1433	0.14	Q				
75+15	0.1430	0.14	Q				
75+20	0.1428	0.14	Q				
75+25	0.1425	0.14	Q				
75+30	0.1422	0.14	Q				
75+35	0.1420	0.14	Q				
75+40	0.1417	0.14	Q				
75+45	0.1414	0.14	Q				
75+50	0.1411	0.14	Q				
75+55	0.1409	0.14	Q				
76+ 0	0.1406	0.14	Q				
76+ 5	0.1403	0.14	Q				
76+10	0.1401	0.14	Q				
76+15	0.1398	0.14	Q				
76+20	0.1395	0.14	Q				
76+25	0.1392	0.14	Q				
76+30	0.1390	0.14	Q				
76+35	0.1387	0.14	Q				
76+40	0.1384	0.14	Q				
76+45	0.1382	0.14	Q				
76+50	0.1379	0.14	Q				
76+55	0.1377	0.14	Q				
77+ 0	0.1374	0.14	Q				
77+ 5	0.1371	0.14	Q				
77+10	0.1369	0.14	Q				
77+15	0.1366	0.14	Q				
77+20	0.1363	0.14	Q				
77+25	0.1361	0.14	Q				
77+30	0.1358	0.14	Q				
77+35	0.1356	0.14	Q				
77+40	0.1353	0.14	Q				
77+45	0.1350	0.14	Q				
77+50	0.1348	0.13	Q				
77+55	0.1345	0.13	Q				
78+ 0	0.1343	0.13	Q				
78+ 5	0.1340	0.13	Q				
78+10	0.1337	0.13	Q				
78+15	0.1335	0.13	Q				
78+20	0.1332	0.13	Q				
78+25	0.1330	0.13	Q				
78+30	0.1327	0.13	Q				
78+35	0.1325	0.13	Q				

78+40	0.1322	0.13	Q				
78+45	0.1319	0.13	Q				
78+50	0.1317	0.13	Q				
78+55	0.1314	0.13	Q				
79+ 0	0.1312	0.13	Q				
79+ 5	0.1309	0.13	Q				
79+10	0.1307	0.13	Q				
79+15	0.1304	0.13	Q				
79+20	0.1302	0.13	Q				
79+25	0.1299	0.13	Q				
79+30	0.1297	0.13	Q				
79+35	0.1294	0.13	Q				
79+40	0.1292	0.13	Q				
79+45	0.1289	0.13	Q				
79+50	0.1287	0.13	Q				
79+55	0.1284	0.13	Q				
80+ 0	0.1282	0.13	Q				
80+ 5	0.1280	0.13	Q				
80+10	0.1277	0.13	Q				
80+15	0.1275	0.13	Q				
80+20	0.1272	0.13	Q				
80+25	0.1270	0.13	Q				
80+30	0.1267	0.13	Q				
80+35	0.1265	0.13	Q				
80+40	0.1262	0.13	Q				
80+45	0.1260	0.13	Q				
80+50	0.1258	0.13	Q				
80+55	0.1255	0.13	Q				
81+ 0	0.1253	0.13	Q				
81+ 5	0.1250	0.13	Q				
81+10	0.1248	0.12	Q				
81+15	0.1246	0.12	Q				
81+20	0.1243	0.12	Q				
81+25	0.1241	0.12	Q				
81+30	0.1238	0.12	Q				
81+35	0.1236	0.12	Q				
81+40	0.1234	0.12	Q				
81+45	0.1231	0.12	Q				
81+50	0.1229	0.12	Q				
81+55	0.1227	0.12	Q				
82+ 0	0.1224	0.12	Q				
82+ 5	0.1222	0.12	Q				
82+10	0.1219	0.12	Q				
82+15	0.1217	0.12	Q				
82+20	0.1215	0.12	Q				
82+25	0.1212	0.12	Q				
82+30	0.1210	0.12	Q				
82+35	0.1208	0.12	Q				
82+40	0.1205	0.12	Q				
82+45	0.1203	0.12	Q				
82+50	0.1201	0.12	Q				
82+55	0.1199	0.12	Q				
83+ 0	0.1196	0.12	Q				
83+ 5	0.1194	0.12	Q				
83+10	0.1192	0.12	Q				
83+15	0.1189	0.12	Q				
83+20	0.1187	0.12	Q				
83+25	0.1185	0.12	Q				
83+30	0.1183	0.12	Q				
83+35	0.1180	0.12	Q				
83+40	0.1178	0.12	Q				
83+45	0.1176	0.12	Q				
83+50	0.1173	0.12	Q				
83+55	0.1171	0.12	Q				
84+ 0	0.1169	0.12	Q				
84+ 5	0.1167	0.12	Q				
84+10	0.1164	0.12	Q				
84+15	0.1162	0.12	Q				
84+20	0.1160	0.12	Q				
84+25	0.1158	0.12	Q				
84+30	0.1156	0.12	Q				

84+35	0.1153	0.12	Q				
84+40	0.1151	0.12	Q				
84+45	0.1149	0.11	Q				
84+50	0.1147	0.11	Q				
84+55	0.1144	0.11	Q				
85+ 0	0.1142	0.11	Q				
85+ 5	0.1140	0.11	Q				
85+10	0.1138	0.11	Q				
85+15	0.1136	0.11	Q				
85+20	0.1134	0.11	Q				
85+25	0.1131	0.11	Q				
85+30	0.1129	0.11	Q				
85+35	0.1127	0.11	Q				
85+40	0.1125	0.11	Q				
85+45	0.1123	0.11	Q				
85+50	0.1121	0.11	Q				
85+55	0.1118	0.11	Q				
86+ 0	0.1116	0.11	Q				
86+ 5	0.1114	0.11	Q				
86+10	0.1112	0.11	Q				
86+15	0.1110	0.11	Q				
86+20	0.1108	0.11	Q				
86+25	0.1106	0.11	Q				
86+30	0.1103	0.11	Q				
86+35	0.1101	0.11	Q				
86+40	0.1099	0.11	Q				
86+45	0.1097	0.11	Q				
86+50	0.1095	0.11	Q				
86+55	0.1093	0.11	Q				
87+ 0	0.1091	0.11	Q				
87+ 5	0.1089	0.11	Q				
87+10	0.1087	0.11	Q				
87+15	0.1084	0.11	Q				
87+20	0.1082	0.11	Q				
87+25	0.1080	0.11	Q				
87+30	0.1078	0.11	Q				
87+35	0.1076	0.11	Q				
87+40	0.1074	0.11	Q				
87+45	0.1072	0.11	Q				
87+50	0.1070	0.11	Q				
87+55	0.1068	0.11	Q				
88+ 0	0.1066	0.11	Q				
88+ 5	0.1064	0.11	Q				
88+10	0.1062	0.11	Q				
88+15	0.1060	0.11	Q				
88+20	0.1058	0.11	Q				
88+25	0.1056	0.11	Q				
88+30	0.1054	0.11	Q				
88+35	0.1052	0.11	Q				
88+40	0.1050	0.10	Q				
88+45	0.1048	0.10	Q				
88+50	0.1046	0.10	Q				
88+55	0.1044	0.10	Q				
89+ 0	0.1042	0.10	Q				
89+ 5	0.1040	0.10	Q				
89+10	0.1038	0.10	Q				
89+15	0.1036	0.10	Q				
89+20	0.1034	0.10	Q				
89+25	0.1032	0.10	Q				
89+30	0.1030	0.10	Q				
89+35	0.1028	0.10	Q				
89+40	0.1026	0.10	Q				
89+45	0.1024	0.10	Q				
89+50	0.1022	0.10	Q				
89+55	0.1020	0.10	Q				
90+ 0	0.1018	0.10	Q				
90+ 5	0.1016	0.10	Q				
90+10	0.1014	0.10	Q				
90+15	0.1012	0.10	Q				
90+20	0.1010	0.10	Q				
90+25	0.1008	0.10	Q				

90+30	0.1006	0.10	Q				
90+35	0.1004	0.10	Q				
90+40	0.1002	0.10	Q				
90+45	0.1000	0.10	Q				
90+50	0.0998	0.10	Q				
90+55	0.0996	0.10	Q				
91+ 0	0.0995	0.10	Q				
91+ 5	0.0993	0.10	Q				
91+10	0.0991	0.10	Q				
91+15	0.0989	0.10	Q				
91+20	0.0987	0.10	Q				
91+25	0.0985	0.10	Q				
91+30	0.0983	0.10	Q				
91+35	0.0981	0.10	Q				
91+40	0.0979	0.10	Q				
91+45	0.0978	0.10	Q				
91+50	0.0976	0.10	Q				
91+55	0.0974	0.10	Q				
92+ 0	0.0972	0.10	Q				
92+ 5	0.0970	0.10	Q				
92+10	0.0968	0.10	Q				
92+15	0.0966	0.10	Q				
92+20	0.0964	0.10	Q				
92+25	0.0963	0.10	Q				
92+30	0.0961	0.10	Q				
92+35	0.0959	0.10	Q				
92+40	0.0957	0.10	Q				
92+45	0.0955	0.10	Q				
92+50	0.0953	0.10	Q				
92+55	0.0952	0.10	Q				
93+ 0	0.0950	0.09	Q				
93+ 5	0.0948	0.09	Q				
93+10	0.0946	0.09	Q				
93+15	0.0944	0.09	Q				
93+20	0.0942	0.09	Q				
93+25	0.0941	0.09	Q				
93+30	0.0939	0.09	Q				
93+35	0.0937	0.09	Q				
93+40	0.0935	0.09	Q				
93+45	0.0933	0.09	Q				
93+50	0.0932	0.09	Q				
93+55	0.0930	0.09	Q				
94+ 0	0.0928	0.09	Q				
94+ 5	0.0926	0.09	Q				
94+10	0.0924	0.09	Q				
94+15	0.0923	0.09	Q				
94+20	0.0921	0.09	Q				
94+25	0.0919	0.09	Q				
94+30	0.0917	0.09	Q				
94+35	0.0916	0.09	Q				
94+40	0.0914	0.09	Q				
94+45	0.0912	0.09	Q				
94+50	0.0910	0.09	Q				
94+55	0.0909	0.09	Q				
95+ 0	0.0907	0.09	Q				
95+ 5	0.0905	0.09	Q				
95+10	0.0903	0.09	Q				
95+15	0.0902	0.09	Q				
95+20	0.0900	0.09	Q				
95+25	0.0898	0.09	Q				
95+30	0.0896	0.09	Q				
95+35	0.0895	0.09	Q				
95+40	0.0893	0.09	Q				
95+45	0.0891	0.09	Q				
95+50	0.0890	0.09	Q				
95+55	0.0888	0.09	Q				
96+ 0	0.0886	0.09	Q				
96+ 5	0.0884	0.09	Q				
96+10	0.0883	0.09	Q				
96+15	0.0881	0.09	Q				
96+20	0.0879	0.09	Q				

96+25	0.0878	0.09	Q				
96+30	0.0876	0.09	Q				
96+35	0.0874	0.09	Q				
96+40	0.0873	0.09	Q				
96+45	0.0871	0.09	Q				
96+50	0.0869	0.09	Q				
96+55	0.0868	0.09	Q				
97+ 0	0.0866	0.09	Q				
97+ 5	0.0864	0.09	Q				
97+10	0.0863	0.09	Q				
97+15	0.0861	0.09	Q				
97+20	0.0859	0.09	Q				
97+25	0.0858	0.09	Q				
97+30	0.0856	0.09	Q				
97+35	0.0854	0.09	Q				
97+40	0.0853	0.09	Q				
97+45	0.0851	0.09	Q				
97+50	0.0849	0.08	Q				
97+55	0.0848	0.08	Q				
98+ 0	0.0846	0.08	Q				
98+ 5	0.0845	0.08	Q				
98+10	0.0843	0.08	Q				
98+15	0.0841	0.08	Q				
98+20	0.0840	0.08	Q				
98+25	0.0838	0.08	Q				
98+30	0.0837	0.08	Q				
98+35	0.0835	0.08	Q				
98+40	0.0833	0.08	Q				
98+45	0.0832	0.08	Q				
98+50	0.0830	0.08	Q				
98+55	0.0829	0.08	Q				
99+ 0	0.0827	0.08	Q				
99+ 5	0.0825	0.08	Q				
99+10	0.0824	0.08	Q				
99+15	0.0822	0.08	Q				
99+20	0.0821	0.08	Q				
99+25	0.0819	0.08	Q				
99+30	0.0817	0.08	Q				
99+35	0.0816	0.08	Q				
99+40	0.0814	0.08	Q				
99+45	0.0813	0.08	Q				
99+50	0.0811	0.08	Q				
99+55	0.0810	0.08	Q				
100+ 0	0.0808	0.08	Q				
100+ 5	0.0807	0.08	Q				
100+10	0.0805	0.08	Q				
100+15	0.0803	0.08	Q				
100+20	0.0802	0.08	Q				
100+25	0.0800	0.08	Q				
100+30	0.0799	0.08	Q				
100+35	0.0797	0.08	Q				
100+40	0.0796	0.08	Q				
100+45	0.0794	0.08	Q				
100+50	0.0793	0.08	Q				
100+55	0.0791	0.08	Q				
101+ 0	0.0790	0.08	Q				
101+ 5	0.0788	0.08	Q				
101+10	0.0787	0.08	Q				
101+15	0.0785	0.08	Q				
101+20	0.0784	0.08	Q				
101+25	0.0782	0.08	Q				
101+30	0.0781	0.08	Q				
101+35	0.0779	0.08	Q				
101+40	0.0778	0.08	Q				
101+45	0.0776	0.08	Q				
101+50	0.0775	0.08	Q				
101+55	0.0773	0.08	Q				
102+ 0	0.0772	0.08	Q				
102+ 5	0.0770	0.08	Q				
102+10	0.0769	0.08	Q				
102+15	0.0767	0.08	Q				

102+20	0.0766	0.08	Q				
102+25	0.0764	0.08	Q				
102+30	0.0763	0.08	Q				
102+35	0.0761	0.08	Q				
102+40	0.0760	0.08	Q				
102+45	0.0758	0.08	Q				
102+50	0.0757	0.08	Q				
102+55	0.0755	0.08	Q				
103+ 0	0.0754	0.08	Q				
103+ 5	0.0753	0.08	Q				
103+10	0.0751	0.08	Q				
103+15	0.0750	0.07	Q				
103+20	0.0748	0.07	Q				
103+25	0.0747	0.07	Q				
103+30	0.0745	0.07	Q				
103+35	0.0744	0.07	Q				
103+40	0.0743	0.07	Q				
103+45	0.0741	0.07	Q				
103+50	0.0740	0.07	Q				
103+55	0.0738	0.07	Q				
104+ 0	0.0737	0.07	Q				
104+ 5	0.0735	0.07	Q				
104+10	0.0734	0.07	Q				
104+15	0.0733	0.07	Q				
104+20	0.0731	0.07	Q				
104+25	0.0730	0.07	Q				
104+30	0.0728	0.07	Q				
104+35	0.0727	0.07	Q				
104+40	0.0726	0.07	Q				
104+45	0.0724	0.07	Q				
104+50	0.0723	0.07	Q				
104+55	0.0721	0.07	Q				
105+ 0	0.0720	0.07	Q				
105+ 5	0.0719	0.07	Q				
105+10	0.0717	0.07	Q				
105+15	0.0716	0.07	Q				
105+20	0.0714	0.07	Q				
105+25	0.0713	0.07	Q				
105+30	0.0712	0.07	Q				
105+35	0.0710	0.07	Q				
105+40	0.0709	0.07	Q				
105+45	0.0708	0.07	Q				
105+50	0.0706	0.07	Q				
105+55	0.0705	0.07	Q				
106+ 0	0.0704	0.07	Q				
106+ 5	0.0702	0.07	Q				
106+10	0.0701	0.07	Q				
106+15	0.0700	0.07	Q				
106+20	0.0698	0.07	Q				
106+25	0.0697	0.07	Q				
106+30	0.0696	0.07	Q				
106+35	0.0694	0.07	Q				
106+40	0.0693	0.07	Q				
106+45	0.0692	0.07	Q				
106+50	0.0690	0.07	Q				
106+55	0.0689	0.07	Q				
107+ 0	0.0688	0.07	Q				
107+ 5	0.0686	0.07	Q				
107+10	0.0685	0.07	Q				
107+15	0.0684	0.07	Q				
107+20	0.0682	0.07	Q				
107+25	0.0681	0.07	Q				
107+30	0.0680	0.07	Q				
107+35	0.0678	0.07	Q				
107+40	0.0677	0.07	Q				
107+45	0.0676	0.07	Q				
107+50	0.0674	0.07	Q				
107+55	0.0673	0.07	Q				
108+ 0	0.0672	0.07	Q				
108+ 5	0.0671	0.07	Q				
108+10	0.0669	0.07	Q				

108+15	0.0668	0.07	Q				
108+20	0.0667	0.07	Q				
108+25	0.0665	0.07	Q				
108+30	0.0664	0.07	Q				
108+35	0.0663	0.07	Q				
108+40	0.0662	0.07	Q				
108+45	0.0660	0.07	Q				
108+50	0.0659	0.07	Q				
108+55	0.0658	0.07	Q				
109+ 0	0.0657	0.07	Q				
109+ 5	0.0655	0.07	Q				
109+10	0.0654	0.07	Q				
109+15	0.0653	0.07	Q				
109+20	0.0651	0.07	Q				
109+25	0.0650	0.07	Q				
109+30	0.0649	0.06	Q				
109+35	0.0648	0.06	Q				
109+40	0.0646	0.06	Q				
109+45	0.0645	0.06	Q				
109+50	0.0644	0.06	Q				
109+55	0.0643	0.06	Q				
110+ 0	0.0642	0.06	Q				
110+ 5	0.0640	0.06	Q				
110+10	0.0639	0.06	Q				
110+15	0.0638	0.06	Q				
110+20	0.0637	0.06	Q				
110+25	0.0635	0.06	Q				
110+30	0.0634	0.06	Q				
110+35	0.0633	0.06	Q				
110+40	0.0632	0.06	Q				
110+45	0.0631	0.06	Q				
110+50	0.0629	0.06	Q				
110+55	0.0628	0.06	Q				
111+ 0	0.0627	0.06	Q				
111+ 5	0.0626	0.06	Q				
111+10	0.0625	0.06	Q				
111+15	0.0623	0.06	Q				
111+20	0.0622	0.06	Q				
111+25	0.0621	0.06	Q				
111+30	0.0620	0.06	Q				
111+35	0.0619	0.06	Q				
111+40	0.0617	0.06	Q				
111+45	0.0616	0.06	Q				
111+50	0.0615	0.06	Q				
111+55	0.0614	0.06	Q				
112+ 0	0.0613	0.06	Q				
112+ 5	0.0611	0.06	Q				
112+10	0.0610	0.06	Q				
112+15	0.0609	0.06	Q				
112+20	0.0608	0.06	Q				
112+25	0.0607	0.06	Q				
112+30	0.0606	0.06	Q				
112+35	0.0604	0.06	Q				
112+40	0.0603	0.06	Q				
112+45	0.0602	0.06	Q				
112+50	0.0601	0.06	Q				
112+55	0.0600	0.06	Q				
113+ 0	0.0599	0.06	Q				
113+ 5	0.0597	0.06	Q				
113+10	0.0596	0.06	Q				
113+15	0.0595	0.06	Q				
113+20	0.0594	0.06	Q				
113+25	0.0593	0.06	Q				
113+30	0.0592	0.06	Q				
113+35	0.0591	0.06	Q				
113+40	0.0589	0.06	Q				
113+45	0.0588	0.06	Q				
113+50	0.0587	0.06	Q				
113+55	0.0586	0.06	Q				
114+ 0	0.0585	0.06	Q				
114+ 5	0.0584	0.06	Q				

114+10	0.0583	0.06	Q				
114+15	0.0582	0.06	Q				
114+20	0.0580	0.06	Q				
114+25	0.0579	0.06	Q				
114+30	0.0578	0.06	Q				
114+35	0.0577	0.06	Q				
114+40	0.0576	0.06	Q				
114+45	0.0575	0.06	Q				
114+50	0.0574	0.06	Q				
114+55	0.0573	0.06	Q				
115+ 0	0.0572	0.06	Q				
115+ 5	0.0571	0.06	Q				
115+10	0.0569	0.06	Q				
115+15	0.0568	0.06	Q				
115+20	0.0567	0.06	Q				
115+25	0.0566	0.06	Q				
115+30	0.0565	0.06	Q				
115+35	0.0564	0.06	Q				
115+40	0.0563	0.06	Q				
115+45	0.0562	0.06	Q				
115+50	0.0561	0.06	Q				
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116+ 0	0.0559	0.06	Q				
116+ 5	0.0558	0.06	Q				
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116+15	0.0555	0.06	Q				
116+20	0.0554	0.06	Q				
116+25	0.0553	0.06	Q				
116+30	0.0552	0.06	Q				
116+35	0.0551	0.06	Q				
116+40	0.0550	0.06	Q				
116+45	0.0549	0.05	Q				
116+50	0.0548	0.05	Q				
116+55	0.0547	0.05	Q				
117+ 0	0.0546	0.05	Q				
117+ 5	0.0545	0.05	Q				
117+10	0.0544	0.05	Q				
117+15	0.0543	0.05	Q				
117+20	0.0542	0.05	Q				
117+25	0.0541	0.05	Q				
117+30	0.0540	0.05	Q				
117+35	0.0539	0.05	Q				
117+40	0.0538	0.05	Q				
117+45	0.0536	0.05	Q				
117+50	0.0535	0.05	Q				
117+55	0.0534	0.05	Q				
118+ 0	0.0533	0.05	Q				
118+ 5	0.0532	0.05	Q				
118+10	0.0531	0.05	Q				
118+15	0.0530	0.05	Q				
118+20	0.0529	0.05	Q				
118+25	0.0528	0.05	Q				
118+30	0.0527	0.05	Q				
118+35	0.0526	0.05	Q				
118+40	0.0525	0.05	Q				
118+45	0.0524	0.05	Q				
118+50	0.0523	0.05	Q				
118+55	0.0522	0.05	Q				
119+ 0	0.0521	0.05	Q				
119+ 5	0.0520	0.05	Q				
119+10	0.0519	0.05	Q				
119+15	0.0518	0.05	Q				
119+20	0.0517	0.05	Q				
119+25	0.0516	0.05	Q				
119+30	0.0515	0.05	Q				
119+35	0.0514	0.05	Q				
119+40	0.0513	0.05	Q				
119+45	0.0512	0.05	Q				
119+50	0.0511	0.05	Q				
119+55	0.0510	0.05	Q				
120+ 0	0.0509	0.05	Q				

120+ 5	0.0508	0.05	Q				
120+10	0.0507	0.05	Q				
120+15	0.0506	0.05	Q				
120+20	0.0505	0.05	Q				
120+25	0.0504	0.05	Q				
120+30	0.0503	0.05	Q				
120+35	0.0503	0.05	Q				
120+40	0.0502	0.05	Q				
120+45	0.0501	0.05	Q				
120+50	0.0500	0.05	Q				
120+55	0.0499	0.05	Q				
121+ 0	0.0498	0.05	Q				
121+ 5	0.0497	0.05	Q				
121+10	0.0496	0.05	Q				
121+15	0.0495	0.05	Q				
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121+25	0.0493	0.05	Q				
121+30	0.0492	0.05	Q				
121+35	0.0491	0.05	Q				
121+40	0.0490	0.05	Q				
121+45	0.0489	0.05	Q				
121+50	0.0488	0.05	Q				
121+55	0.0487	0.05	Q				
122+ 0	0.0486	0.05	Q				
122+ 5	0.0485	0.05	Q				
122+10	0.0484	0.05	Q				
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122+20	0.0483	0.05	Q				
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122+35	0.0480	0.05	Q				
122+40	0.0479	0.05	Q				
122+45	0.0478	0.05	Q				
122+50	0.0477	0.05	Q				
122+55	0.0476	0.05	Q				
123+ 0	0.0475	0.05	Q				
123+ 5	0.0474	0.05	Q				
123+10	0.0473	0.05	Q				
123+15	0.0473	0.05	Q				
123+20	0.0472	0.05	Q				
123+25	0.0471	0.05	Q				
123+30	0.0470	0.05	Q				
123+35	0.0469	0.05	Q				
123+40	0.0468	0.05	Q				
123+45	0.0467	0.05	Q				
123+50	0.0466	0.05	Q				
123+55	0.0465	0.05	Q				
124+ 0	0.0464	0.05	Q				
124+ 5	0.0464	0.05	Q				
124+10	0.0463	0.05	Q				
124+15	0.0462	0.05	Q				
124+20	0.0461	0.05	Q				
124+25	0.0460	0.05	Q				
124+30	0.0459	0.05	Q				
124+35	0.0458	0.05	Q				
124+40	0.0457	0.05	Q				
124+45	0.0456	0.05	Q				
124+50	0.0456	0.05	Q				
124+55	0.0455	0.05	Q				
125+ 0	0.0454	0.05	Q				
125+ 5	0.0453	0.05	Q				
125+10	0.0452	0.05	Q				
125+15	0.0451	0.05	Q				
125+20	0.0450	0.05	Q				
125+25	0.0449	0.04	Q				
125+30	0.0449	0.04	Q				
125+35	0.0448	0.04	Q				
125+40	0.0447	0.04	Q				
125+45	0.0446	0.04	Q				
125+50	0.0445	0.04	Q				
125+55	0.0444	0.04	Q				

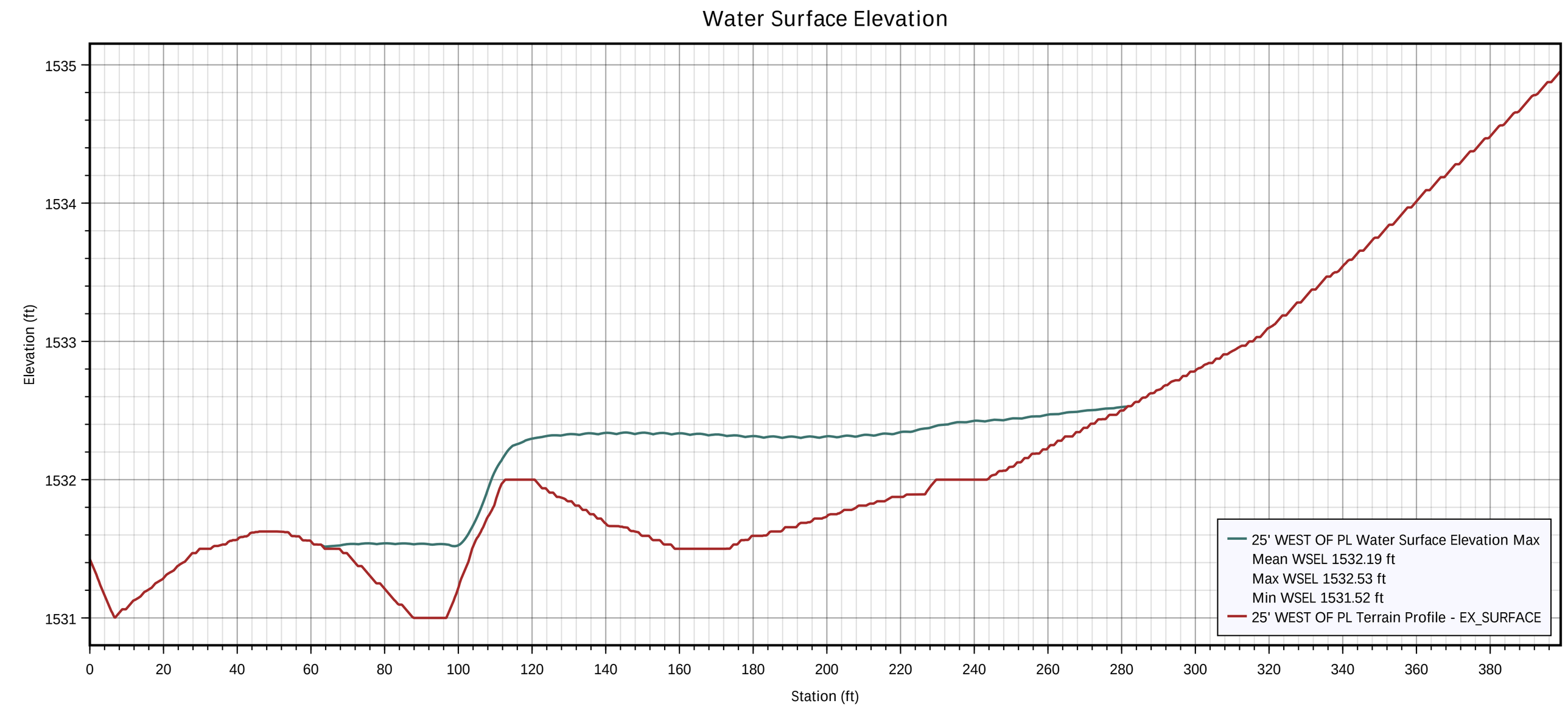
126+ 0	0.0443	0.04	Q				
126+ 5	0.0443	0.04	Q				
126+10	0.0442	0.04	Q				
126+15	0.0441	0.04	Q				
126+20	0.0440	0.04	Q				
126+25	0.0439	0.04	Q				
126+30	0.0438	0.04	Q				
126+35	0.0438	0.04	Q				
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126+45	0.0436	0.04	Q				
126+50	0.0435	0.04	Q				
126+55	0.0434	0.04	Q				
127+ 0	0.0433	0.04	Q				
127+ 5	0.0433	0.04	Q				
127+10	0.0432	0.04	Q				
127+15	0.0431	0.04	Q				
127+20	0.0430	0.04	Q				
127+25	0.0429	0.04	Q				
127+30	0.0428	0.04	Q				
127+35	0.0428	0.04	Q				
127+40	0.0427	0.04	Q				
127+45	0.0426	0.04	Q				
127+50	0.0425	0.04	Q				
127+55	0.0424	0.04	Q				
128+ 0	0.0423	0.04	Q				
128+ 5	0.0423	0.04	Q				
128+10	0.0422	0.04	Q				
128+15	0.0421	0.04	Q				
128+20	0.0420	0.04	Q				
128+25	0.0419	0.04	Q				
128+30	0.0419	0.04	Q				
128+35	0.0418	0.04	Q				
128+40	0.0417	0.04	Q				
128+45	0.0416	0.04	Q				
128+50	0.0415	0.04	Q				
128+55	0.0415	0.04	Q				
129+ 0	0.0414	0.04	Q				
129+ 5	0.0413	0.04	Q				
129+10	0.0412	0.04	Q				
129+15	0.0411	0.04	Q				
129+20	0.0411	0.04	Q				
129+25	0.0410	0.04	Q				
129+30	0.0409	0.04	Q				
129+35	0.0408	0.04	Q				
129+40	0.0408	0.04	Q				
129+45	0.0407	0.04	Q				
129+50	0.0406	0.04	Q				
129+55	0.0405	0.04	Q				
130+ 0	0.0404	0.04	Q				
130+ 5	0.0404	0.04	Q				
130+10	0.0403	0.04	Q				
130+15	0.0402	0.04	Q				
130+20	0.0401	0.04	Q				
130+25	0.0401	0.04	Q				
130+30	0.0400	0.04	Q				
130+35	0.0399	0.04	Q				
130+40	0.0398	0.04	Q				
130+45	0.0397	0.04	Q				
130+50	0.0397	0.04	Q				
130+55	0.0396	0.04	Q				
131+ 0	0.0395	0.04	Q				
131+ 5	0.0394	0.04	Q				
131+10	0.0394	0.04	Q				
131+15	0.0393	0.04	Q				
131+20	0.0392	0.04	Q				
131+25	0.0391	0.04	Q				
131+30	0.0391	0.04	Q				
131+35	0.0390	0.04	Q				
131+40	0.0389	0.04	Q				
131+45	0.0388	0.04	Q				
131+50	0.0388	0.04	Q				

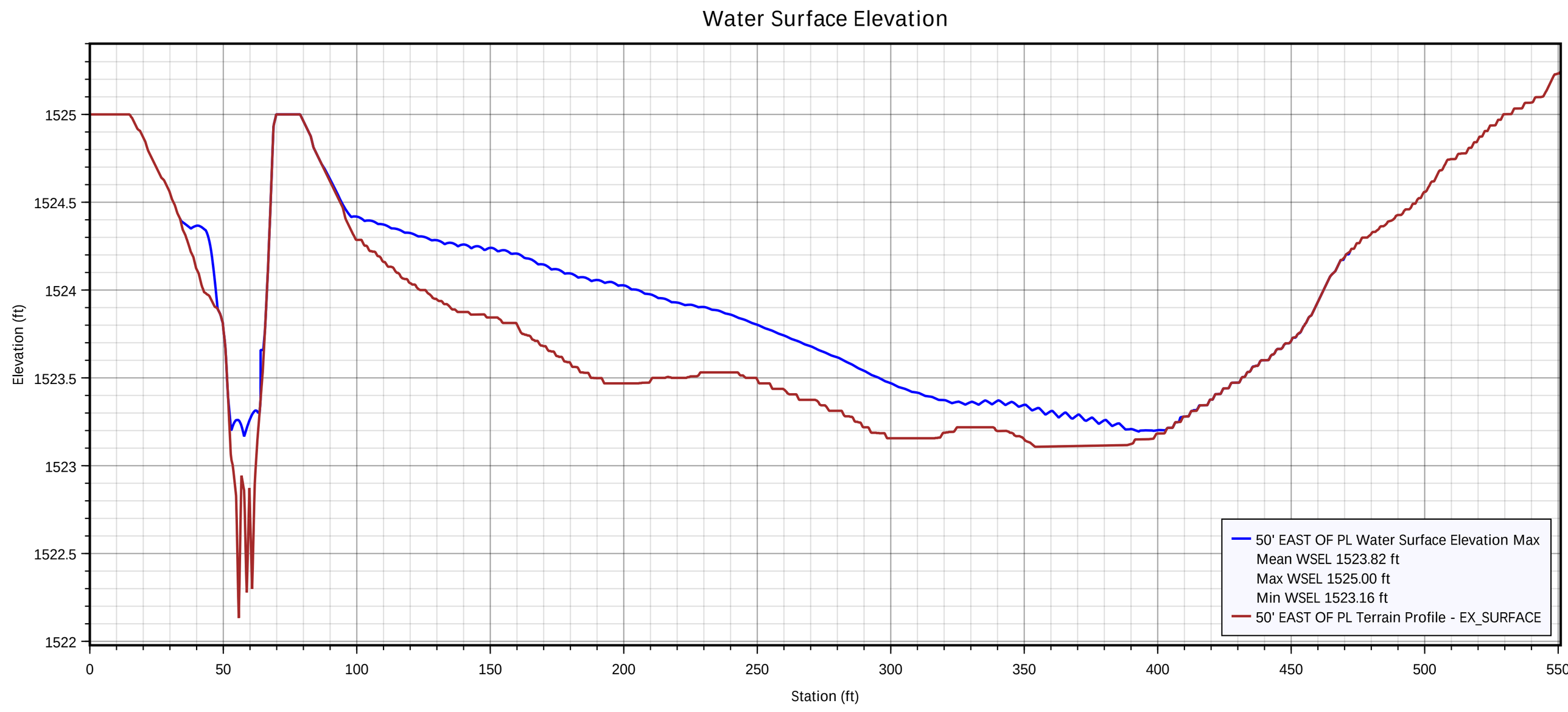
131+55	0.0387	0.04	Q	|	|	|	|
132+ 0	0.0386	0.04	Q	|	|	|	|
132+ 5	0.0385	0.04	Q	|	|	|	|
132+10	0.0385	0.04	Q	|	|	|	|
132+15	0.0384	0.04	Q	|	|	|	|
132+20	0.0383	0.04	Q	|	|	|	|
132+25	0.0382	0.04	Q	|	|	|	|
132+30	0.0382	0.04	Q	|	|	|	|
132+35	0.0381	0.04	Q	|	|	|	|
132+40	0.0380	0.04	Q	|	|	|	|
132+45	0.0380	0.04	Q	|	|	|	|
132+50	0.0379	0.04	Q	|	|	|	|
132+55	0.0378	0.04	Q	|	|	|	|
133+ 0	0.0377	0.04	Q	|	|	|	|
133+ 5	0.0377	0.04	Q	|	|	|	|
133+10	0.0376	0.04	Q	|	|	|	|
133+15	0.0375	0.04	Q	|	|	|	|
133+20	0.0374	0.04	Q	|	|	|	|
133+25	0.0374	0.04	Q	|	|	|	|
133+30	0.0373	0.04	Q	|	|	|	|
133+35	0.0372	0.04	Q	|	|	|	|
133+40	0.0372	0.04	Q	|	|	|	|
133+45	0.0371	0.04	Q	|	|	|	|
133+50	0.0370	0.04	Q	|	|	|	|
133+55	0.0369	0.04	Q	|	|	|	|
134+ 0	0.0369	0.04	Q	|	|	|	|
134+ 5	0.0368	0.04	Q	|	|	|	|
134+10	0.0367	0.04	Q	|	|	|	|
134+15	0.0367	0.04	Q	|	|	|	|
134+20	0.0366	0.04	Q	|	|	|	|
134+25	0.0365	0.04	Q	|	|	|	|
134+30	0.0364	0.04	Q	|	|	|	|
134+35	0.0364	0.04	Q	|	|	|	|
134+40	0.0363	0.04	Q	|	|	|	|
134+45	0.0362	0.04	Q	|	|	|	|
134+50	0.0362	0.04	Q	|	|	|	|
134+55	0.0361	0.04	Q	|	|	|	|
135+ 0	0.0360	0.04	Q	|	|	|	|
135+ 5	0.0360	0.04	Q	|	|	|	|
135+10	0.0359	0.04	Q	|	|	|	|
135+15	0.0358	0.04	Q	|	|	|	|
135+20	0.0358	0.04	Q	|	|	|	|
135+25	0.0357	0.04	Q	|	|	|	|
135+30	0.0356	0.04	Q	|	|	|	|
135+35	0.0355	0.04	Q	|	|	|	|
135+40	0.0355	0.04	Q	|	|	|	|
135+45	0.0354	0.04	Q	|	|	|	|
135+50	0.0353	0.04	Q	|	|	|	|
135+55	0.0353	0.04	Q	|	|	|	|
136+ 0	0.0352	0.04	Q	|	|	|	|
136+ 5	0.0351	0.04	Q	|	|	|	|
136+10	0.0351	0.04	Q	|	|	|	|
136+15	0.0350	0.04	Q	|	|	|	|
136+20	0.0349	0.03	Q	|	|	|	|
136+25	0.0349	0.03	Q	|	|	|	|
136+30	0.0348	0.03	Q	|	|	|	|
136+35	0.0347	0.03	Q	|	|	|	|
136+40	0.0347	0.03	Q	|	|	|	|
136+45	0.0346	0.03	Q	|	|	|	|
136+50	0.0345	0.03	Q	|	|	|	|
136+55	0.0345	0.03	Q	|	|	|	|
137+ 0	0.0344	0.03	Q	|	|	|	|
137+ 5	0.0343	0.03	Q	|	|	|	|
137+10	0.0343	0.03	Q	|	|	|	|
137+15	0.0342	0.03	Q	|	|	|	|
137+20	0.0341	0.03	Q	|	|	|	|
137+25	0.0341	0.03	Q	|	|	|	|
137+30	0.0340	0.03	Q	|	|	|	|
137+35	0.0339	0.03	Q	|	|	|	|
137+40	0.0339	0.03	Q	|	|	|	|
137+45	0.0338	0.03	Q	|	|	|	|

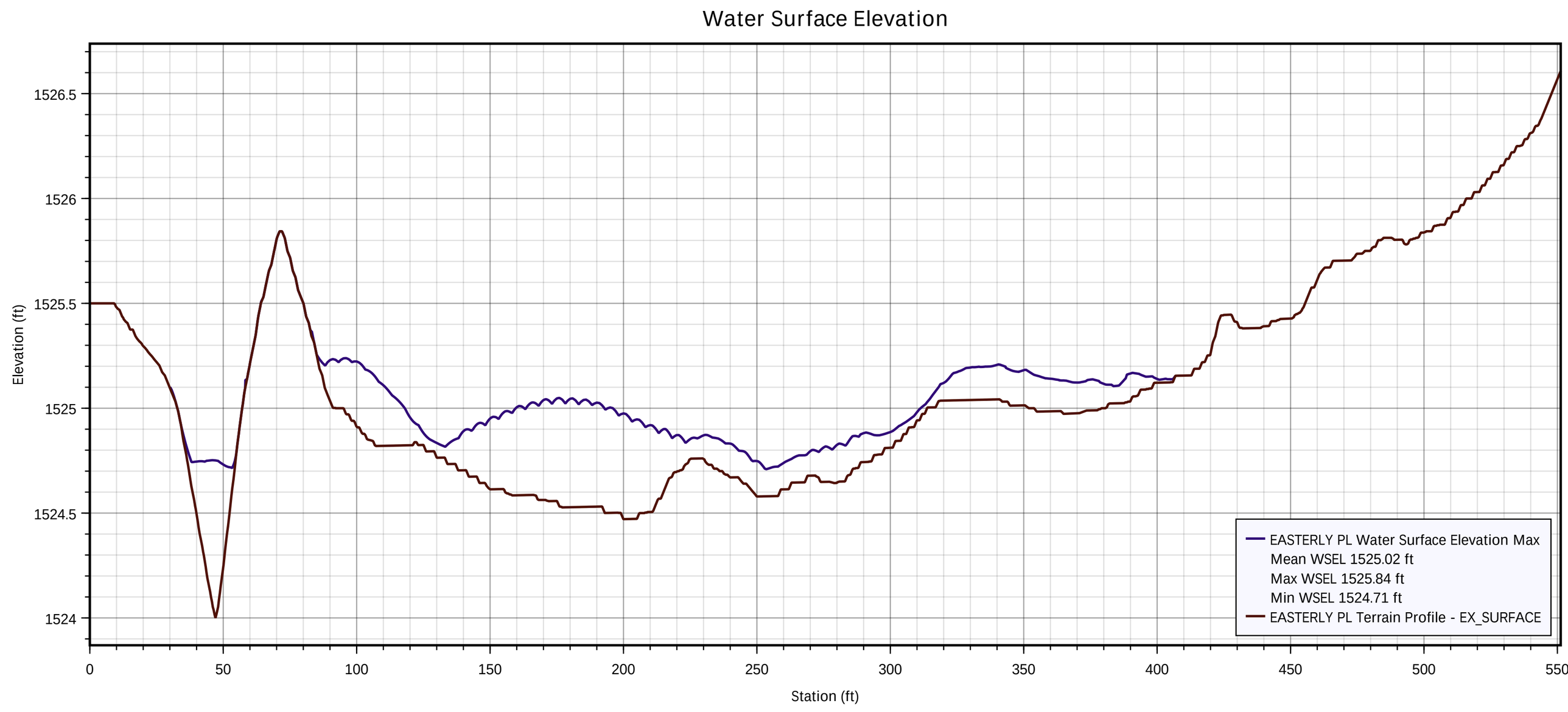
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  137+50       0.0338      0.03  Q          |          |          |          |
  137+55       0.0337      0.03  Q          |          |          |          |
  138+ 0       0.0336      0.03  Q          |          |          |          |
  138+ 5       0.0336      0.03  Q          |          |          |          |
  138+10       0.0335      0.03  Q          |          |          |          |
  138+15       0.0334      0.03  Q          |          |          |          |
  138+20       0.0334      0.03  Q          |          |          |          |
  138+25       0.0333      0.03  Q          |          |          |          |
  138+30       0.0332      0.03  Q          |          |          |          |
  138+35       0.0332      0.03  Q          |          |          |          |
  138+40       0.0331      0.03  Q          |          |          |          |
  138+45       0.0330      0.03  Q          |          |          |          |
  138+50       0.0330      0.03  Q          |          |          |          |
  138+55       0.0329      0.03  Q          |          |          |          |
  139+ 0       0.0329      0.03  Q          |          |          |          |
  139+ 5       0.0328      0.03  Q          |          |          |          |
  139+10       0.0327      0.03  Q          |          |          |          |
  139+15       0.0327      0.03  Q          |          |          |          |
  139+20       0.0326      0.03  Q          |          |          |          |
  139+25       0.0325      0.03  Q          |          |          |          |
  139+30       0.0325      0.03  Q          |          |          |          |
  139+35       0.0324      0.03  Q          |          |          |          |
  139+40       0.0324      0.03  Q          |          |          |          |
  139+45       0.0323      0.03  Q          |          |          |          |
  139+50       0.0322      0.03  Q          |          |          |          |
  139+55       0.0322      0.03  Q          |          |          |          |
-------------------------------------------------------------------------
       ****************************HYDROGRAPH DATA****************************
                    Number of intervals =  3485
                    Time interval =    5.0 (Min.)
                    Maximum/Peak flow rate =      279.025 (CFS)
                    Total volume =      14.746 (Ac.Ft)
              Status of hydrographs being held in storage
                         Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
              Peak (CFS)      0.000     0.000     0.000     0.000     0.000
              Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
       *************************************************************************

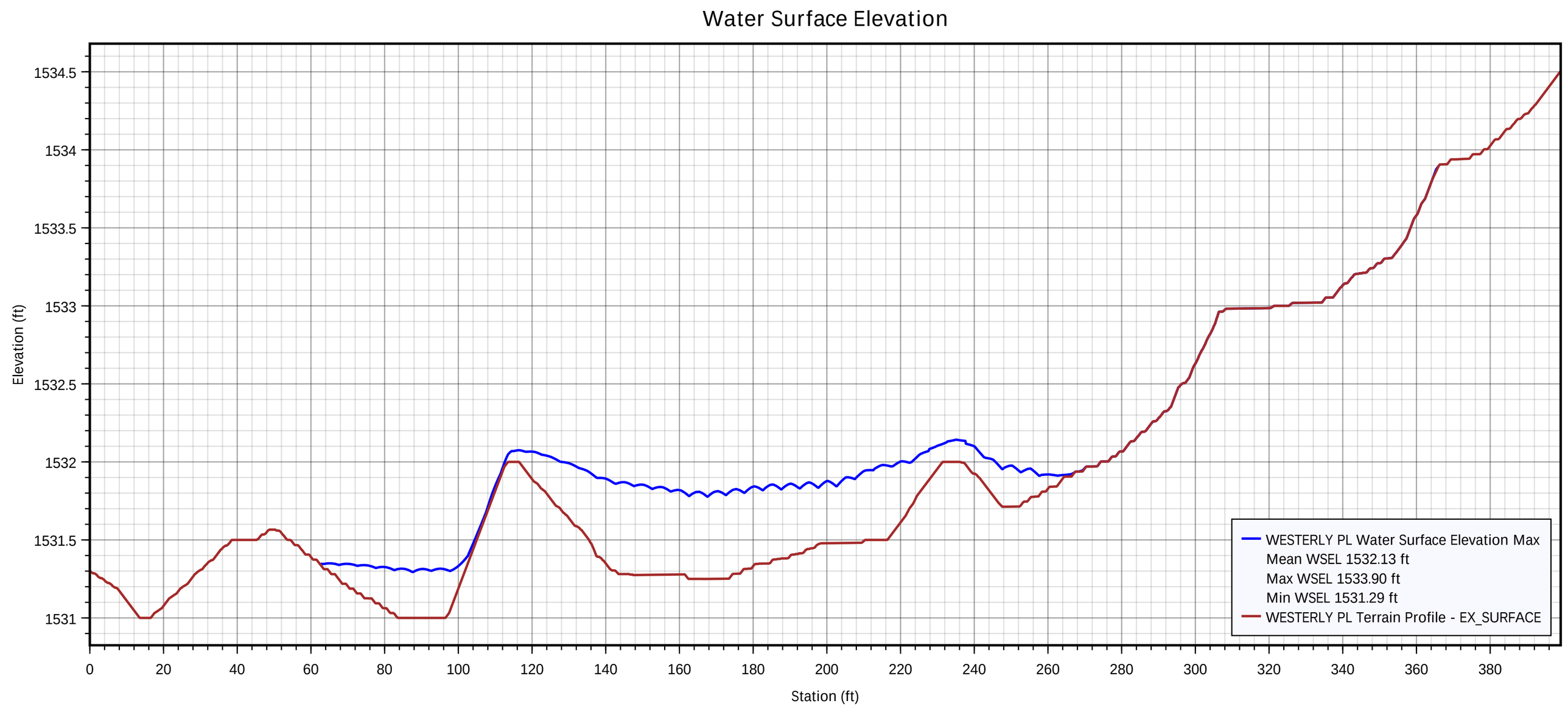
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```

APPENDIX H.2: PRE-PROJECT TWO DIMENSIONAL HEC-RAS WATER SURFACE ELEVATION PROFILE LINES


Water Surface Elevation
Elevation (ft)
1535
1534
1533
1532
1531
0
20
40
60
80
100
120
140
160
180
200
220
240
260
280
300
320
340
360
380
Station (ft)
25' WEST OF PL Water Surface Elevation Max
Mean WSEL 1532.19 ft
Max WSEL 1532.53 ft
Min WSEL 1531.52 ft
25' WEST OF PL Terrain Profile - EX_SURFACE

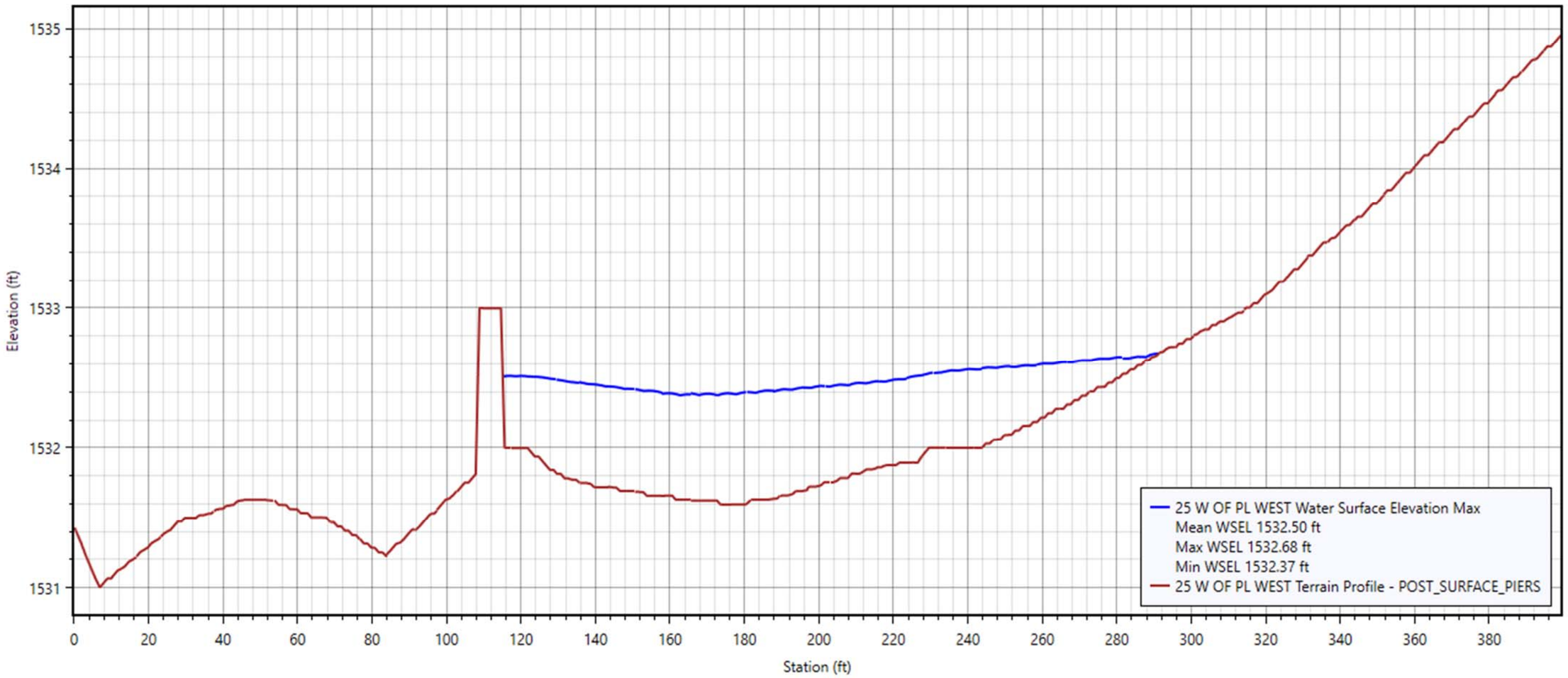

Water Surface Elevation
Elevation (ft)
1525
1524.5
1524
1523.5
1523
1522.5
1522
0
50
100
150
200
250
300
350
400
450
500
550
Station (ft)
50' EAST OF PL Water Surface Elevation Max
Mean WSEL 1523.82 ft
Max WSEL 1525.00 ft
Min WSEL 1523.16 ft
50' EAST OF PL Terrain Profile - EX_SURFACE

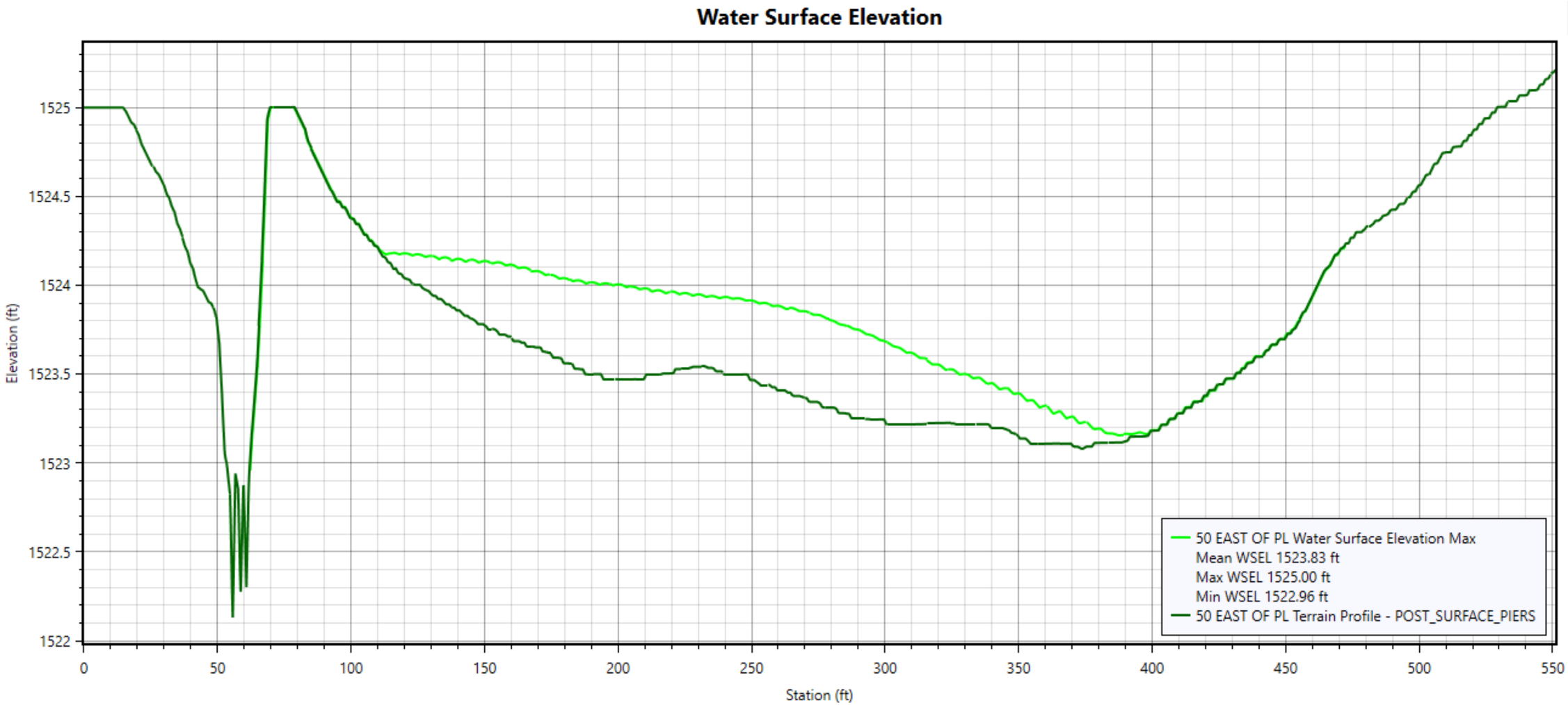

Water Surface Elevation
Elevation (ft)
1526.5
1526
1525.5
1525
1524.5
1524
0
50
100
150
200
250
300
350
400
450
500
550
Station (ft)
EASTERLY PL Water Surface Elevation Max
Mean WSEL 1525.02 ft
Max WSEL 1525.84 ft
Min WSEL 1524.71 ft
EASTERLY PL Terrain Profile - EX_SURFACE

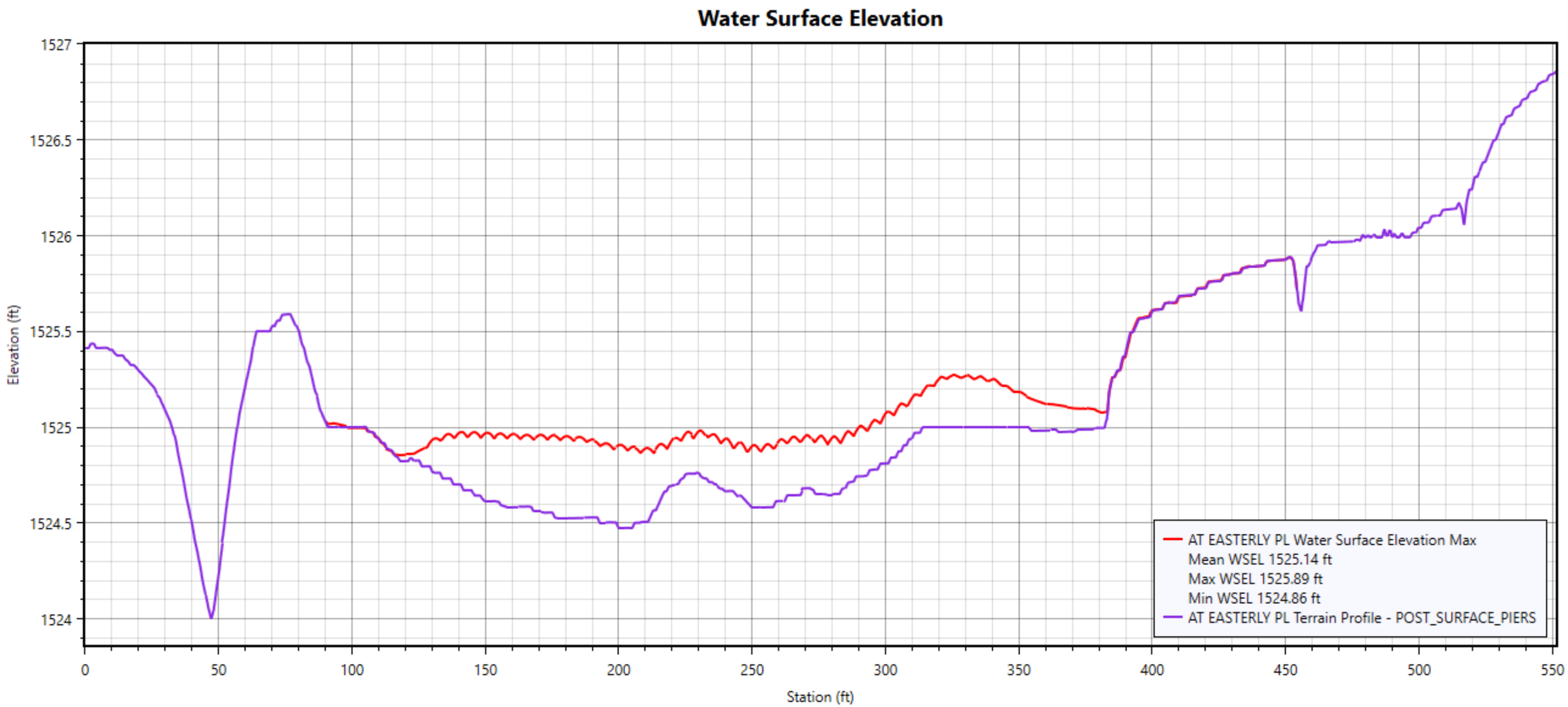

Water Surface Elevation
Elevation (ft)
1534.5
1534
1533.5
1533
1532.5
1532
1531.5
1531
0
20
40
60
80
100
120
140
160
180
200
220
240
260
280
300
320
340
360
380
Station (ft)
WESTERLY PL Water Surface Elevation Max
Mean WSEL 1532.13 ft
Max WSEL 1533.90 ft
Min WSEL 1531.29 ft
WESTERLY PL Terrain Profile - EX_SURFACE

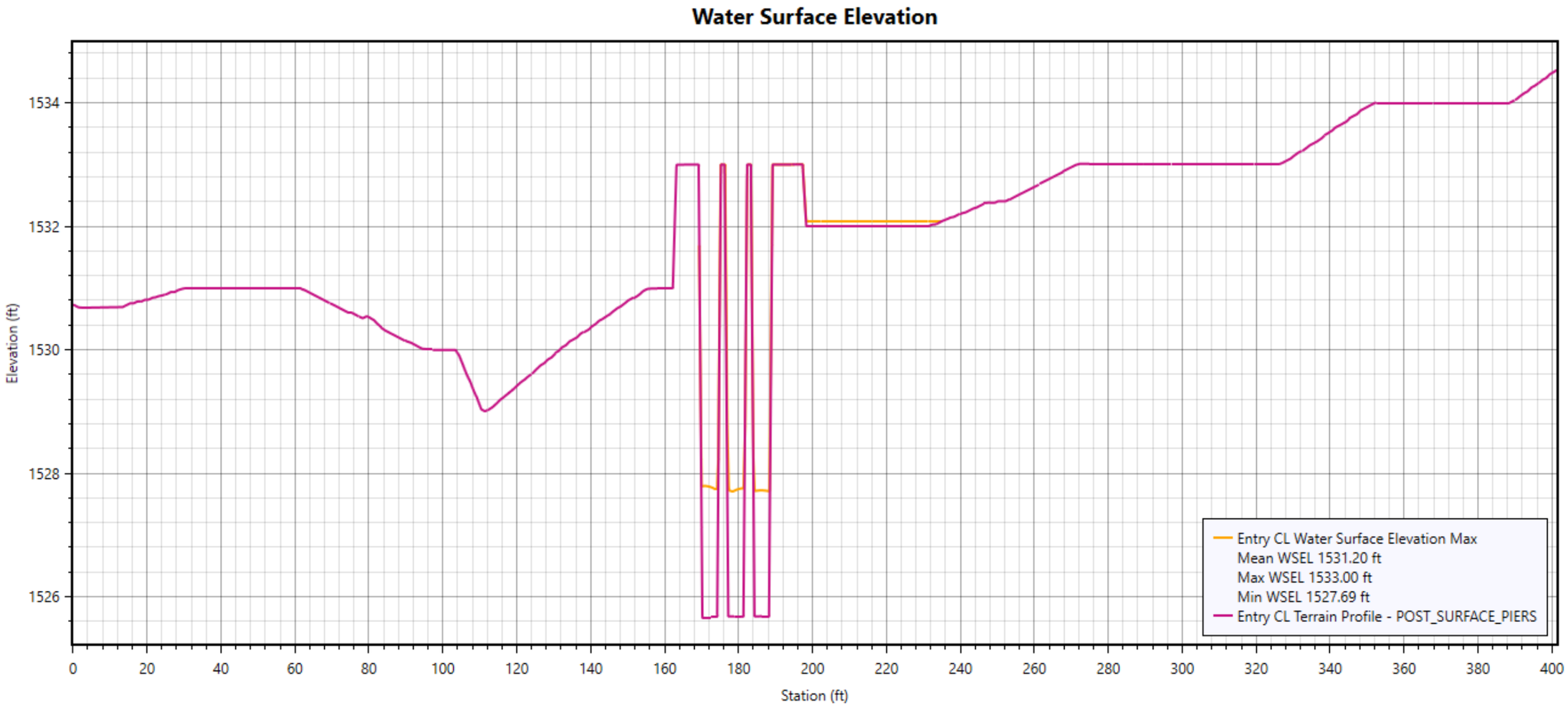
APPENDIX H.3: POST-PROJECT TWO DIMENSIONAL HEC-RAS WATER SURFACE ELEVATION PROFILE LINES

Water Surface Elevation

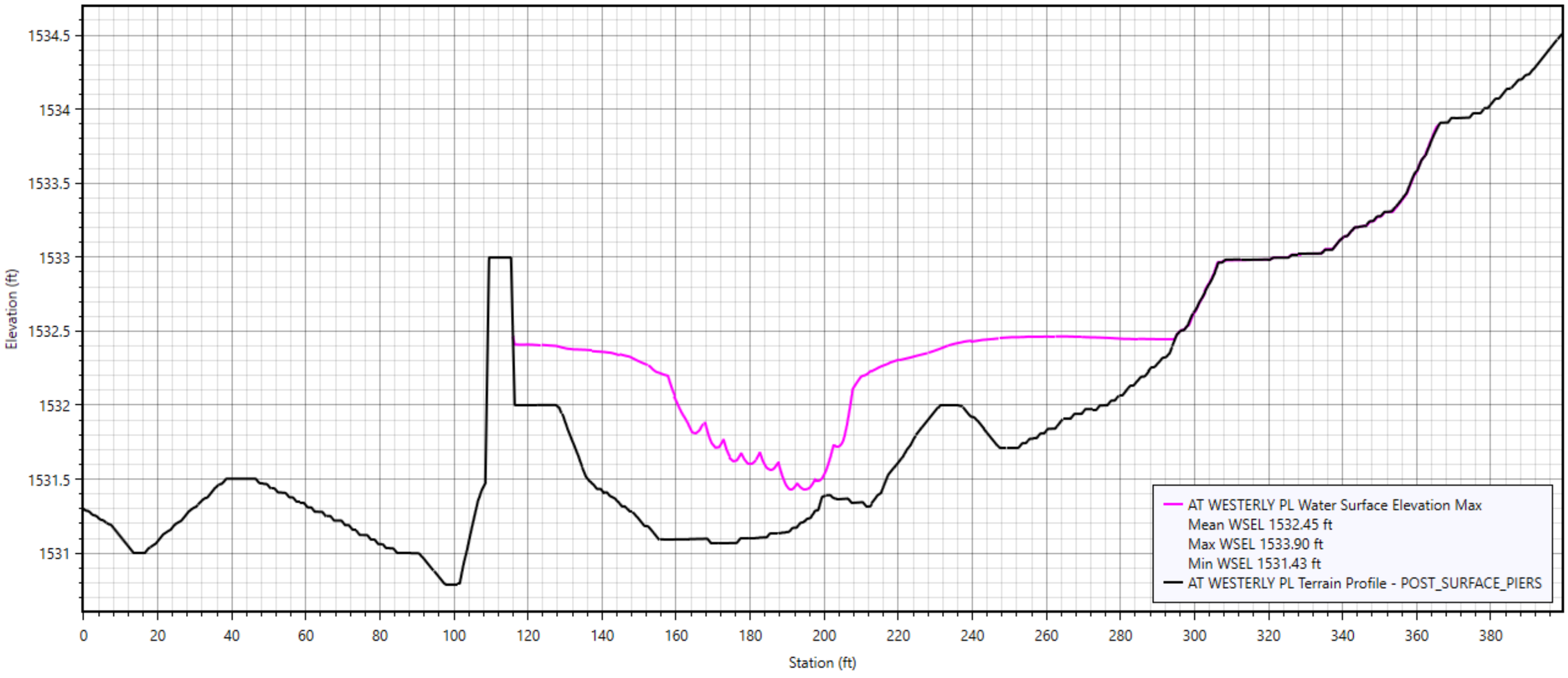



Water Surface Elevation
Elevation (ft)
1525
1524.5
1524
1523.5
1523
1522.5
1522
0
50
100
150
200
250
300
350
400
450
500
550
Station (ft)
50 EAST OF PL Water Surface Elevation Max
Mean WSEL 1523.83 ft
Max WSEL 1525.00 ft
Min WSEL 1522.96 ft
50 EAST OF PL Terrain Profile - POST_SURFACE_PIERS


Water Surface Elevation
Elevation (ft)
1527
1526.5
1526
1525.5
1525
1524.5
1524
0
50
100
150
200
250
300
350
400
450
500
550
Station (ft)
AT EASTERLY PL Water Surface Elevation Max
Mean WSEL 1525.14 ft
Max WSEL 1525.89 ft
Min WSEL 1524.86 ft
AT EASTERLY PL Terrain Profile - POST_SURFACE_PIERS


Water Surface Elevation
Elevation (ft)
1534
1532
1530
1528
1526
0
20
40
60
80
100
120
140
160
180
200
220
240
260
280
300
320
340
360
380
400
Station (ft)
Entry CL Water Surface Elevation Max
Mean WSEL 1531.20 ft
Max WSEL 1533.00 ft
Min WSEL 1527.69 ft
Entry CL Terrain Profile - POST_SURFACE_PIERS

Water Surface Elevation



APPENDIX H.4: INTERIM CHANNEL STORAGE VOLUME CALCULATIONS

OFFSITE CHANNEL

Contour Elevation	Contour Area (sf)	Contour Area (ac)	Contour Interval Volume (ac-ft)	Total Basin Volume (ac-ft)	Total Basin Volume (ft^3)
1523.00	15800.75	0.363		0.0000	
1.00			0.616		
1524.00	39642.00	0.910		0.6158	26823.40
2.00			1.204		
1525.00	66386.59	1.524		1.8197	79266.29

APPENDIX H.5: DRAWDOWN CALCULATIONS

DRAWDOWN CALCULATIONS

Diameter of Drywell	5	ft
Depth of Infiltrating Surfac area	20	ft
Circumference	15.70796	ft
Infiltrating Surface Area	314.1593	sq. ft.
Infiltrating Flow Rate	0.51	cfs
Volume	79266.29	cu. ft.
Drawdown Time	43.17	hours

EXCERPTS

EXCERPT A DRYWELL PERCOLATION TESTING – WILL BE PROVIDED

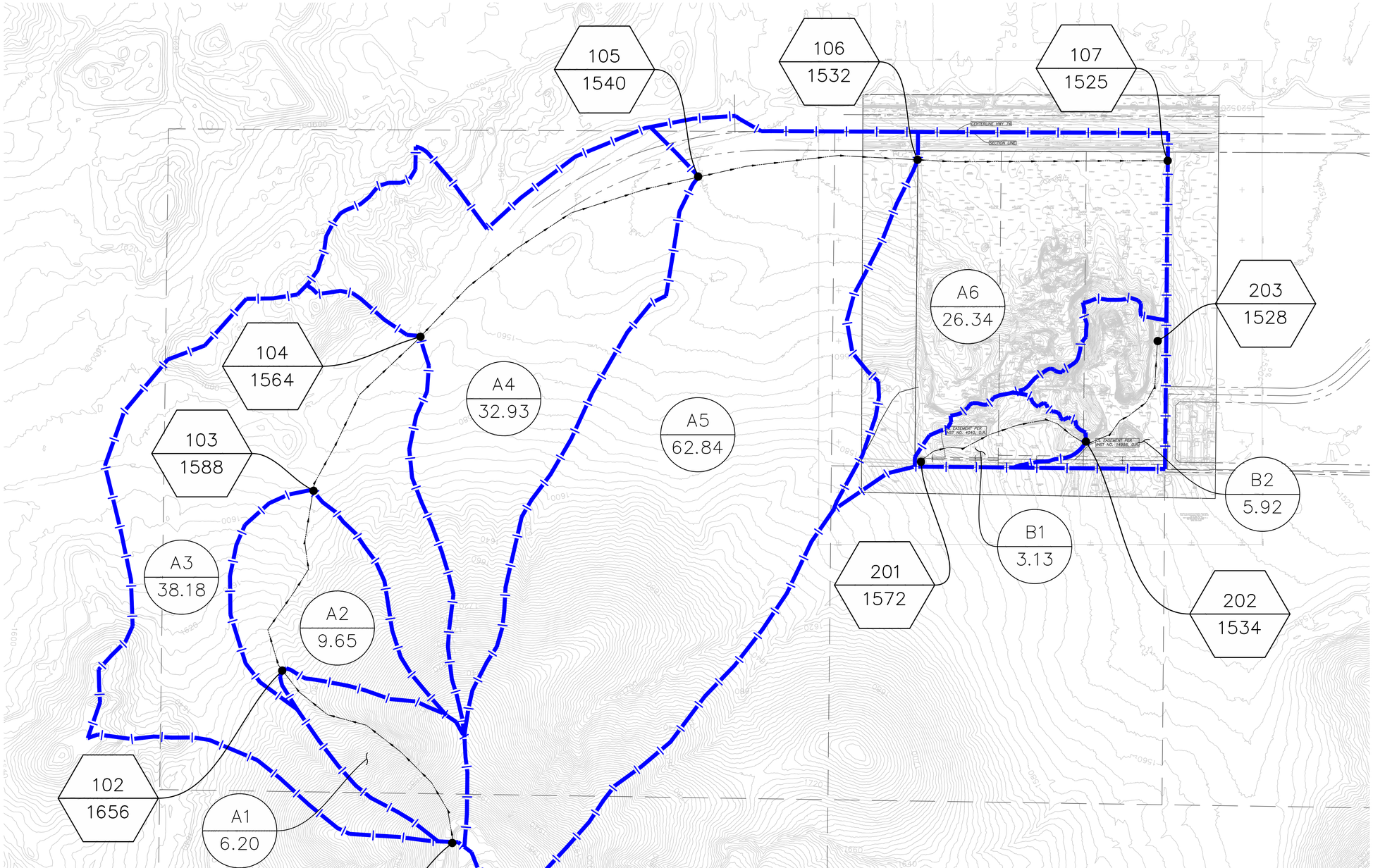
EXHIBITS

EXHIBIT A: EXISTING CONDITION RATIONAL METHOD HYDROLOGY MAP

HEMET 30

COUNTY OF RIVERSIDE, STATE OF CALIFORNIA

EXISTING CONDITION HYDROLOGY MAP



LEGEND:

- X.X / X.X — NODE/CONCENTRATION POINT; FLOWLINE ELEVATION
- XXXX.X — APPROXIMATE INVERT ELEVATION
- XXX / X.X — SUB AREA; ACRES
- L=XXX' — FLOW DISTANCE
- FLOW PATH
- WATERSHED BOUNDARY

N

GRAPHIC SCALE
200' 0 100' 200' 400'
1" = 200'

EXHIBIT "A"

HEMET 30

EXISTING CONDITION HYDROLOGY MAP

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41660 IVY STREET, SUITE A
MURRIETA, CA 92562
PH. 951.304.9552 FAX 951.304.3568

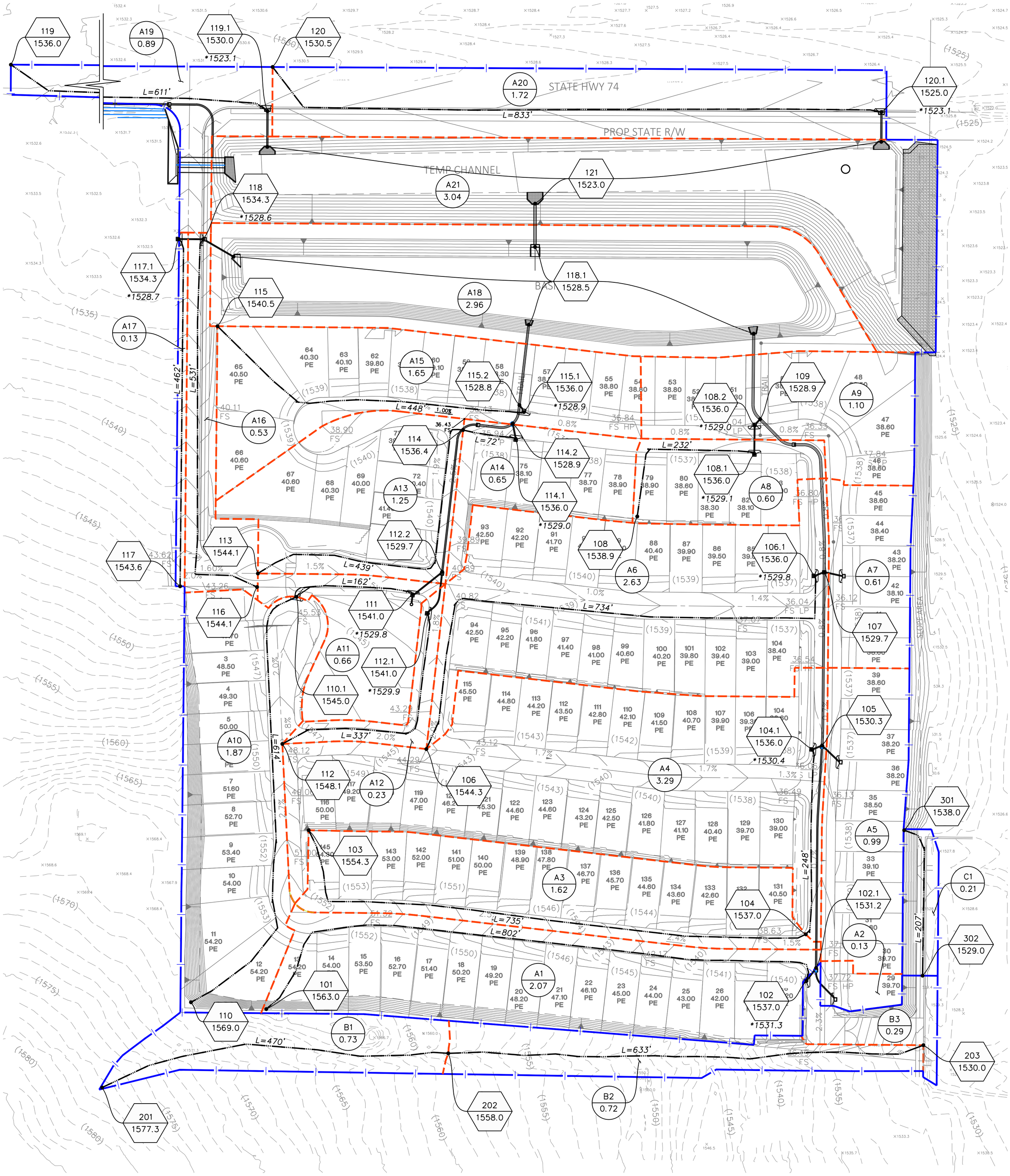
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EXHIBIT B: **POST-PROJECT CONDITION RATIONAL METHOD HYDROLOGY MAP**

HEMET 30

COUNTY OF RIVERSIDE, STATE OF CALIFORNIA

POST-PROJECT CONDITION SITE HYDROLOGY MAP



LEGEND:

X.X / X.X	NODE/CONCENTRATION POINT / FLOWLINE ELEVATION
XXXX.X	APPROXIMATE INVERT ELEVATION
XXX / X.X	SUB AREA / ACRES
L=XXX'	FLOW DISTANCE
	FLOW PATH
	WATERSHED SUB-BOUNDARY

GRAPHIC SCALE
60' 0 30' 60' 120'
1" = 60'

JLC Engineering & Consulting, Inc.
41660 IVY STREET, SUITE A
MURRIETA, CA 92562
PH. 951.304.9552 FAX 951.304.3568

EXHIBIT "B-1"

HEMET 30

POST-PROJECT CONDITION SITE HYDROLOGY MAP

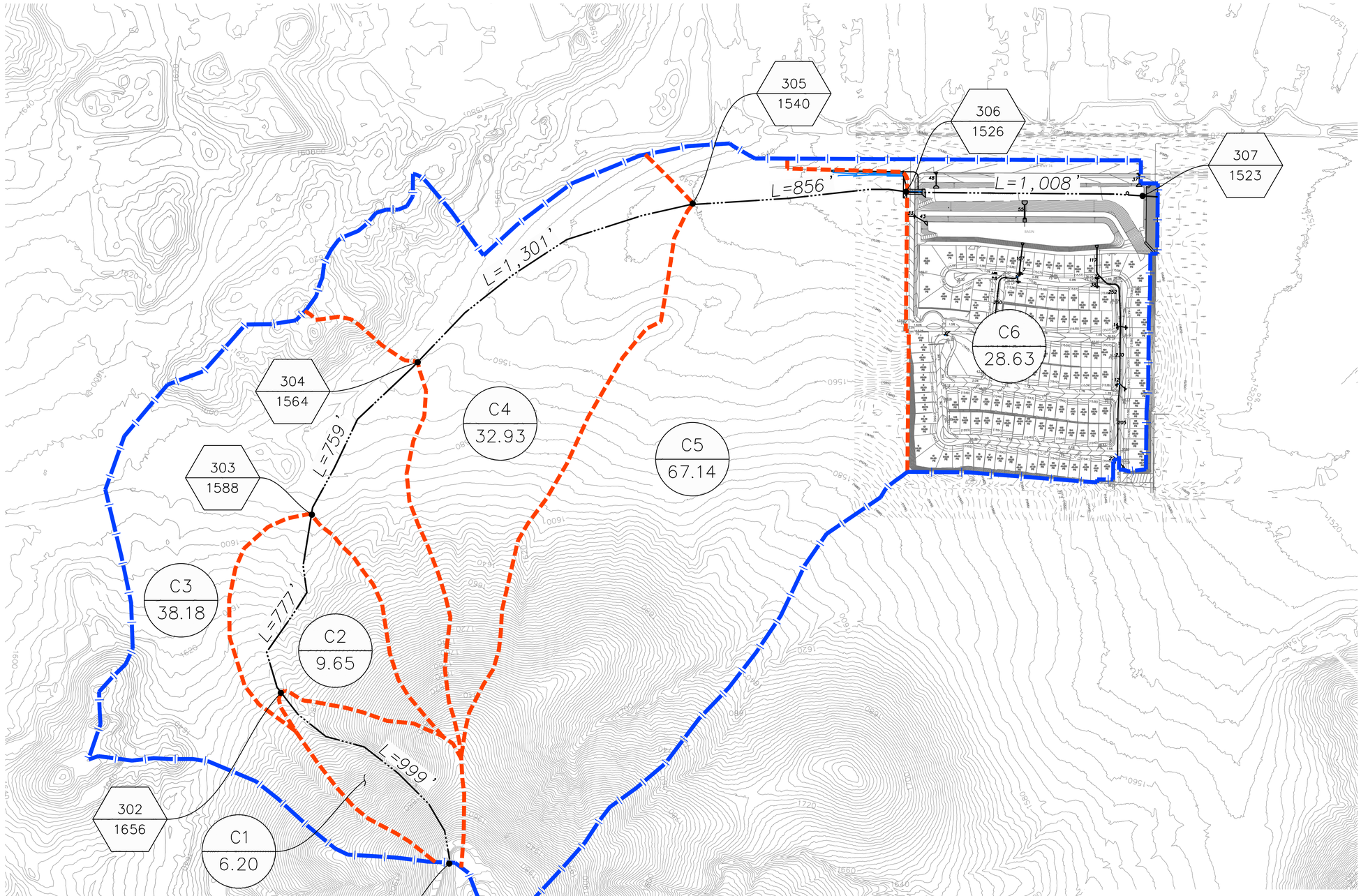
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SHEET 1 OF 1

TENTATIVE TRACT MAP 37737

COUNTY OF RIVERSIDE, STATE OF CALIFORNIA

POST-PROJECT CONDITION OFFSITE HYDROLOGY MAP



LEGEND:

- X.X / X.X — NODE/CONCENTRATION POINT / FLOWLINE ELEVATION
- XXXX.X — APPROXIMATE INVERT ELEVATION
- XXX / X.X — SUB AREA / ACRES
- L=XXX' — FLOW DISTANCE
- FLOW PATH
- WATERSHED BOUNDARY

N

GRAPHIC SCALE
200' 0 100' 200' 400'
1" = 200'

EXHIBIT "B-2"

TTM 37737

POST-PROJECT CONDITION OFFSITE HYDROLOGY MAP

JLC Engineering & Consulting, Inc.
41660 IVY STREET, SUITE A
MURRIETA, CA 92562
PH. 951.304.9552 FAX 951.304.3568

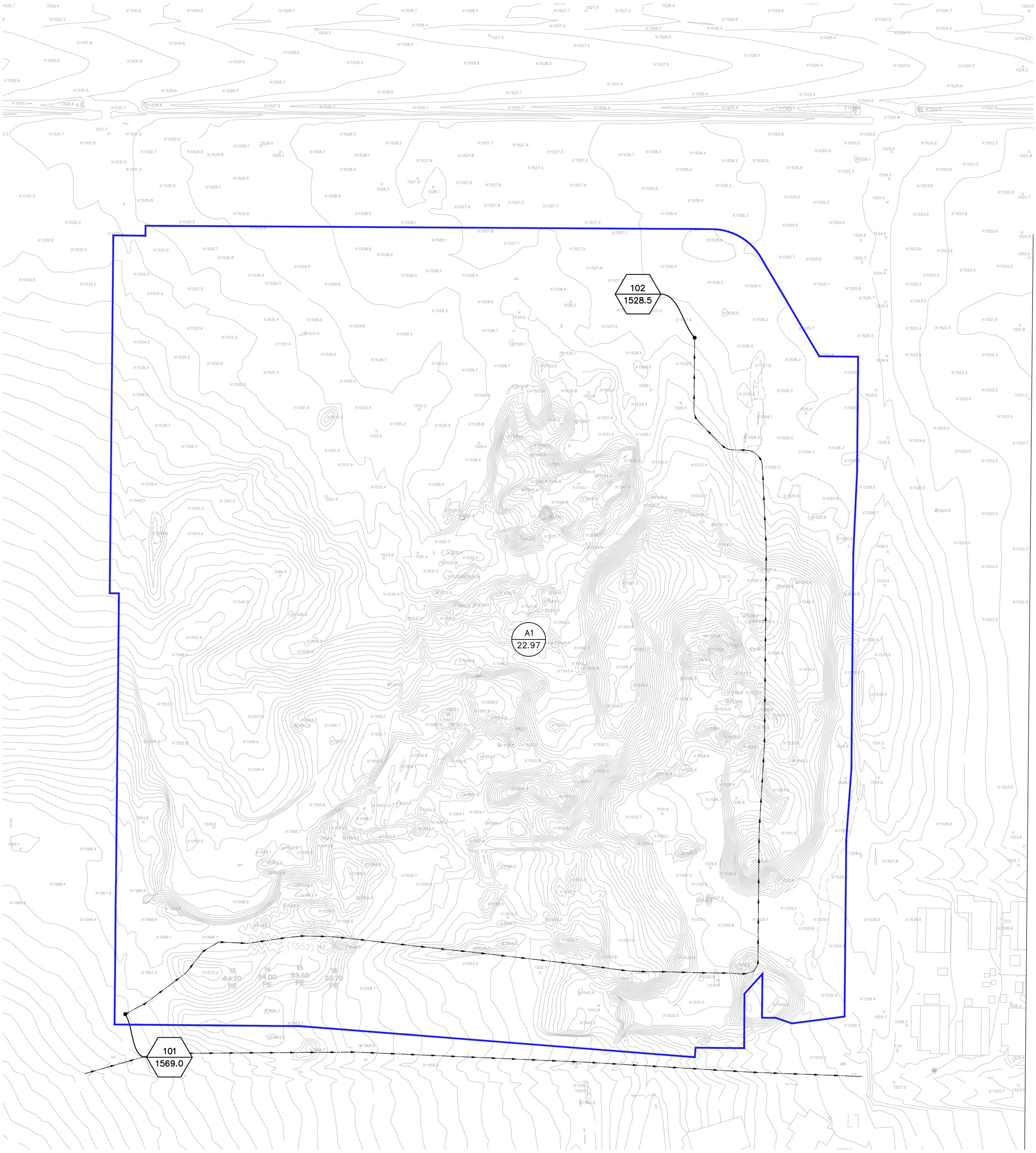
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EXHIBIT C: EXISTING CONDITION UNIT HYDROGRAPH HYDROLOGY MAP

TENTATIVE TRACT MAP 37737

COUNTY OF RIVERSIDE, STATE OF CALIFORNIA

EXISTING CONDITION UNIT HYDROGRAPH MAP



LEGEND:

X.X / X.X	NODE/CONCENTRATION POINT / FLOWLINE ELEVATION
XXXX.X	APPROXIMATE INVERT ELEVATION
XXX / X.X	SUB AREA / ACRES
L=XXX'	FLOW DISTANCE
	FLOW PATH
	WATERSHED BOUNDARY

N

GRAPHIC SCALE

60' 0 30' 60' 120'

1" = 60'

EXHIBIT "C"

TTM 37737

EXISTING CONDITION
UNIT HYDROGRAPH MAP

JLC Engineering & Consulting, Inc.

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MURRIETA, CA 92562
PH. 951.304.9552 FAX 951.304.3568

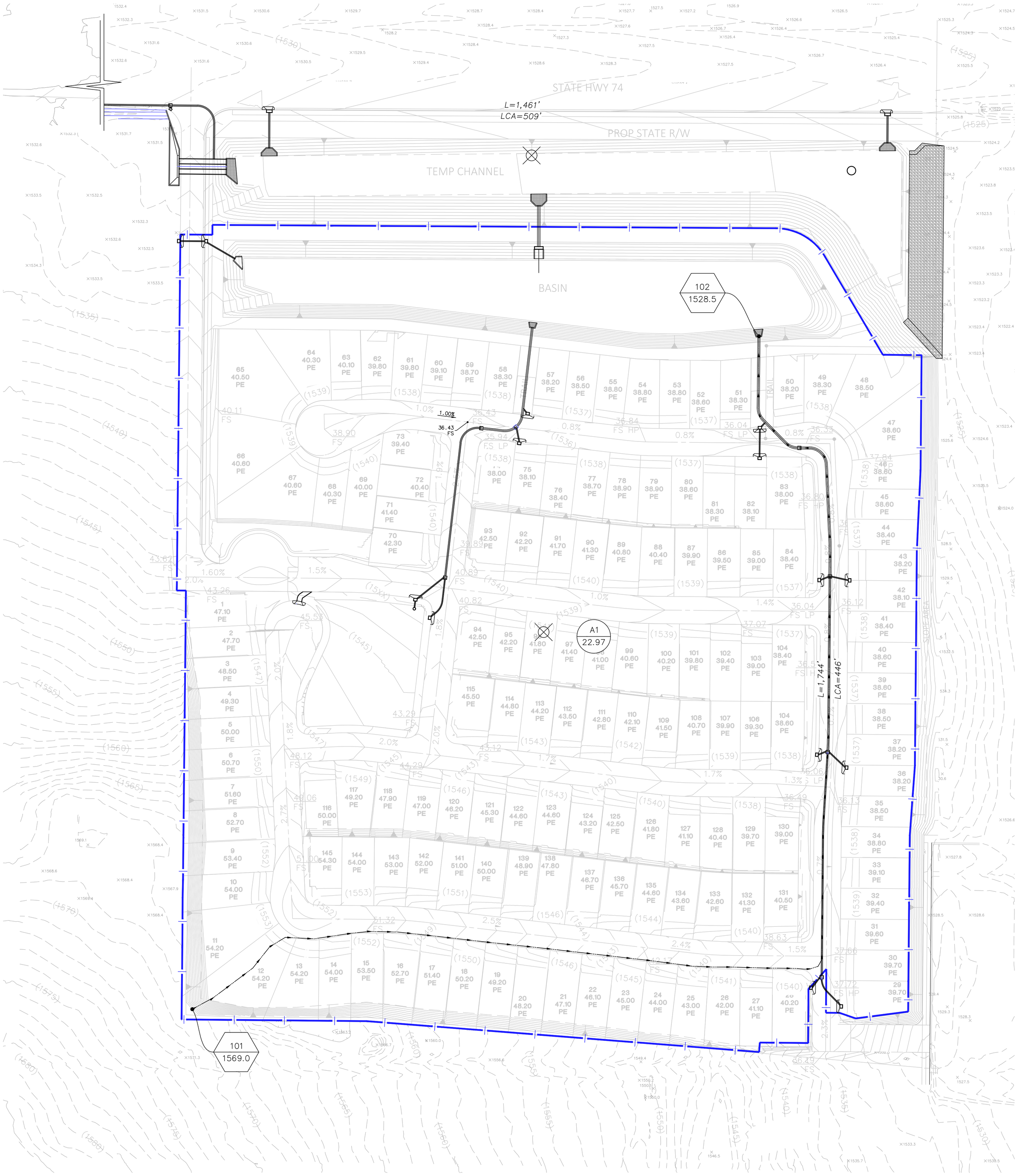
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EXHIBIT D: **POST-PROJECT CONDITION UNIT HYDROGRAPH HYDROLOGY MAP**

TENTATIVE TRACT MAP 37737

COUNTY OF RIVERSIDE, STATE OF CALIFORNIA

POST-PROJECT CONDITION SITE HYDROLOGY MAP



LEGEND:

- X.X / X.X — NODE/CONCENTRATION POINT / FLOWLINE ELEVATION
- XXXX.X — APPROXIMATE INVERT ELEVATION
- XXX / X.X — SUB AREA / ACRES
- L=XXX' — FLOW DISTANCE
- FLOW PATH
- WATERSHED SUB-BOUNDARY
- AREA CENTROID

N

GRAPHIC SCALE
60' 0 30' 60' 120'
1" = 60'

JLC Engineering & Consulting, Inc.
41660 IVY STREET, SUITE A
MURRIETA, CA 92562
PH. 951.304.9552 FAX 951.304.3568

EXHIBIT "D"

TTM 37737

POST-PROJECT CONDITION SITE HYDROLOGY MAP

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Last Opened: Nov 03, 2021 - 9:05am by jcarver

EXHIBIT E: DRAINAGE FACILITIES MAP

HEMET 30

COUNTY OF RIVERSIDE, STATE OF CALIFORNIA

DRAINAGE FACILITIES MAP

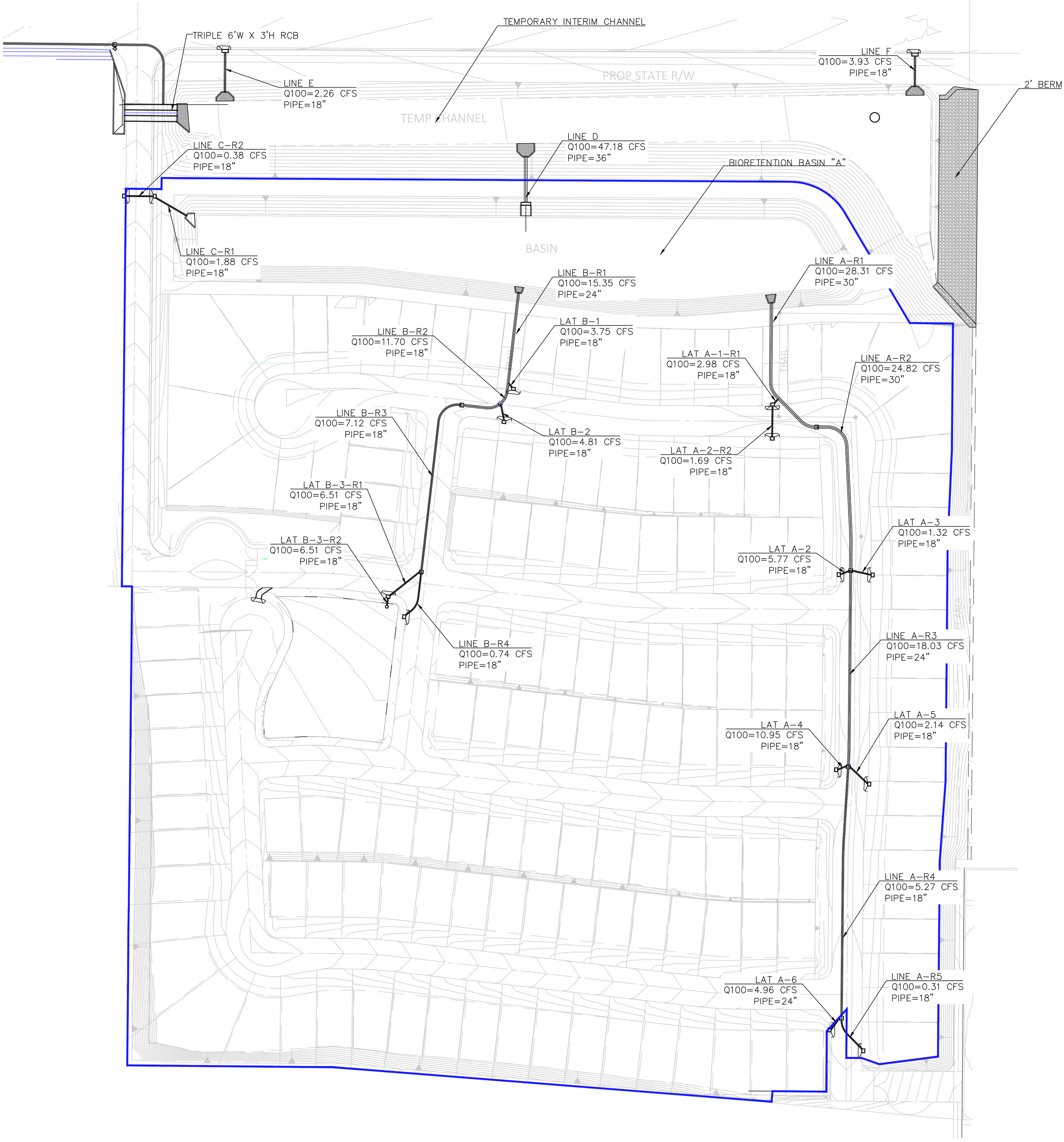


EXHIBIT "E"

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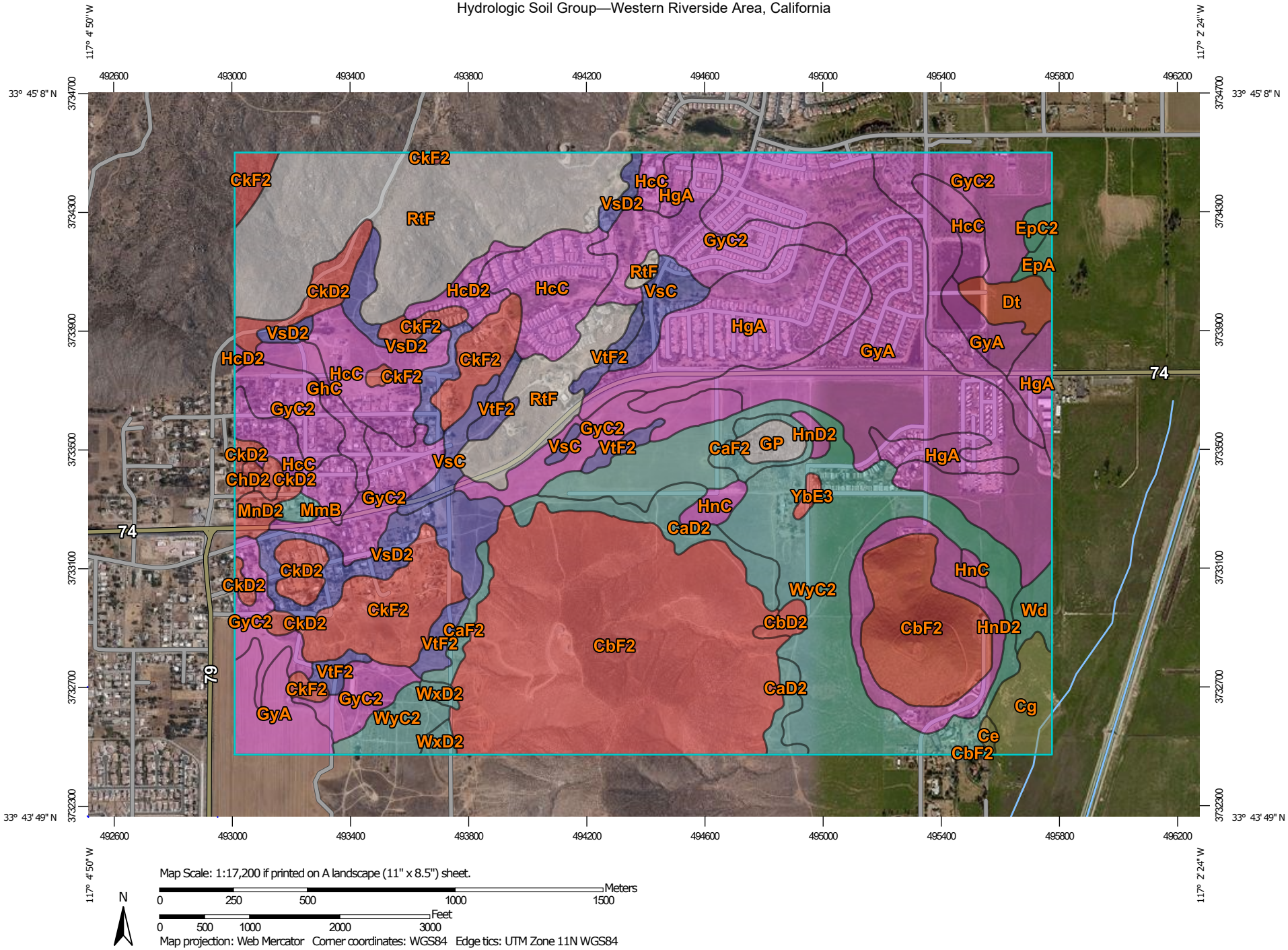
DRAINAGE FACILITIES MAP

JLC Engineering & Consulting, Inc.

41660 IVY STREET, SUITE A
MURRIETA, CA 92562
PH. 951.304.9552 FAX 951.304.3568

Drawing Name: O:\150.10.19\Engineering\Hydrology Plan\Exhibits\Drainage Facilities Map.dwg
Last Opened: Nov 03, 2021 - 8:26am by jcarver

EXHIBIT F: HYDROLOGIC SOILS MAP


117° 4' 50" W
117° 2' 24" W
33° 45' 8" N
33° 43' 49" N
492600
493000
493400
493800
494200
494600
495000
495400
495800
496200
3734700
3734300
3733900
3733500
3733100
3732700
3732300
CkF2
HcC
HgA
VsD2
GyC2
RtF
HcC
EpC2
EpA
Dt
CkD2
HcD2
HcC
VsC
RtF
HgA
GyA
VsD2
CkF2
VtF2
HcD2
HcC
GhC
CkF2
GyC2
VtF2
RtF
HgA
74
GyC2
VsC
VtF2
CaF2
GP
HnD2
CkD2
HcC
VsC
HgA
ChD2
CkD2
GyC2
YbE3
MnD2
MmB
HnC
CaD2
74
VsD2
HnC
CkD2
CkD2
WyC2
CkF2
Wd
GyC2
CkD2
CbD2
CbF2
HnD2
CaF2
VtF2
CbF2
79
VtF2
CkF2
GyC2
WxD2
CaD2
Cg
GyA
WyC2
Ce
WxD2
CbF2
Map Scale: 1:17,200 if printed on A landscape (11" x 8.5") sheet.
N
0
250
500
1000
1500
Meters
0
500
1000
2000
3000
Feet
Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 11N WGS84

MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Rating Polygons

A

A/D

B

B/D

C

C/D

D

Not rated or not available

Soil Rating Lines

A

A/D

B

B/D

C

C/D

D

Not rated or not available

Soil Rating Points

A

A/D

B

B/D

C

C/D

D

Not rated or not available

Water Features

Streams and Canals

Transportation

Rails

Interstate Highways

US Routes

Major Roads

Local Roads

Background

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15,800.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL:
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Western Riverside Area, California
Survey Area Data: Version 11, Sep 12, 2018

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jan 5, 2015—Jun 25, 2019

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
CaD2	Cajalco fine sandy loam, 8 to 15 percent slopes, eroded	C	23.5	1.7%
CaF2	Cajalco fine sandy loam, 15 to 35 percent slopes, erode d	C	11.8	0.8%
CbD2	Cajalco rocky fine sandy loam, 5 to 15 percent slopes, eroded	D	3.4	0.2%
CbF2	Cajalco rocky fine sandy loam, 15 to 50 percent slopes, eroded	D	236.6	17.0%
Ce	Chino silt loam, drained	C/D	1.3	0.1%
Cg	Chino silt loam, drained, strongly saline-alkali	C/D	16.0	1.2%
ChD2	Cieneba sandy loam, 8 to 15 percent slopes, eroded	D	1.9	0.1%
CkD2	Cieneba rocky sandy loam, 8 to 15 percent slopes, eroded	D	26.1	1.9%
CkF2	Cieneba rocky sandy loam, 15 to 50 percent slopes, eroded	D	62.4	4.5%
Dt	Domino fine sandy loam, saline-alkali	D	10.4	0.7%
EpA	Exeter sandy loam, deep, 0 to 2 percent slopes	C	3.2	0.2%
EpC2	Exeter sandy loam, deep, 2 to 8 percent slopes, eroded	C	2.9	0.2%
GhC	Gorgonio loamy sand, 0 to 8 percent slopes	A	10.7	0.8%
GP	Gravel pits		6.4	0.5%
GyA	Greenfield sandy loam, 0 to 2 percent slopes	A	179.5	12.9%
GyC2	Greenfield sandy loam, 2 to 8 percent slopes, eroded	A	174.0	12.5%
HcC	Hanford coarse sandy loam, 2 to 8 percent slopes	A	85.7	6.2%

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
HcD2	Hanford coarse sandy loam, 8 to 15 percent slopes, eroded	A	9.4	0.7%
HgA	Hanford fine sandy loam, 0 to 2 percent slopes	A	82.5	5.9%
HnC	Honcut sandy loam, 2 to 8 percent slopes	A	6.8	0.5%
HnD2	Honcut sandy loam, 8 to 15 percent slopes, eroded	A	27.0	1.9%
MmB	Monserate sandy loam, 0 to 5 percent slopes	C	2.9	0.2%
MnD2	Monserate sandy loam, shallow, 5 to 15 percent slopes, eroded	D	5.4	0.4%
RtF	Rockland		154.4	11.1%
VsC	Vista coarse sandy loam, 2 to 8 percent slopes	B	20.8	1.5%
VsD2	Vista coarse sandy loam, 8 to 15 percent slopes, eroded	B	49.6	3.6%
VtF2	Vista rocky coarse sandy loam, 2 to 35 percent slopes, eroded	B	20.7	1.5%
Wd	Waukena loam, saline-alkali	C	6.6	0.5%
WxD2	Wyman fine sandy loam, 8 to 15 percent slopes, eroded	C	4.4	0.3%
WyC2	Wyman loam, 2 to 8 percent slopes, eroded	C	144.1	10.3%
YbE3	Yokohl loam, 8 to 25 percent slopes, severely eroded	D	1.8	0.1%
Totals for Area of Interest			**1,392.4**	**100.0%**

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

EXHIBIT G: RAINFALL MAPS

2 YEAR, 1 HOUR

HEMET 30
RAINFALL VALUE = 0.50

JLC Engineering & Consulting, Inc.

40040 COLISEUM WAY
MURRIETA, CA 92562
PH. 951.304.9552 FAX 951.304.3568

NOTES:
1. Isohyetals based on NOAA Atlas 2, Volume XI - California, 1973.

RCFC & WCD
HYDROLOGY MANUAL

RIVERSIDE COUNTY FLOOD CONTROL
AND
WATER CONSERVATION DISTRICT

2-YEAR — 1-HOUR
PRECIPITATION

APPROVED CHIEF ENGINEER R.E. NO. 8823
DATE
DRAWN BY R.L.S.
PLATE D-4.3
SHEET NO
DR NO
REVISED

2 YEAR, 24 HOUR

HEMET 30
RAINFALL VALUE = 1.80

JLC Engineering & Consulting, Inc.

40040 COLISEUM WAY
MURRIETA, CA 92562
PH. 951.304.9552 FAX 951.304.3568

NOTES:
1. Isohyetals from NOAA Atlas 2,
Volume XI - California, 1973.

RCFC & WCD
HYDROLOGY MANUAL

RIVERSIDE COUNTY FLOOD CON
AND
WATER CONSERVATION DISTR

2-YEAR — 24-HOU
PRECIPITATION

DRAWN BY: R.A.S.
APPROVED

100 YEAR, 1 HOUR

HEMET 30
RAINFALL VALUE = 1.20

JLC Engineering & Consulting, Inc.

40040 COLISEUM WAY
MURRIETA, CA 92562
PH. 951.304.9552 FAX 951.304.3568

Notes:
Isohyetals based on NOAA Atlas 2, Volume XI - California, 1973

RCFC & WCD

RIVERSIDE COUNTY FLOOD CONTROL AND WATER CONSERVATION DISTRICT

100-YEAR — 1-HOUR PRECIPITATION

DRAWN BY:

SHEET No.

100 YEAR, 24 HOUR

HEMET 30
RAINFALL VALUE = 4.50

JLC Engineering & Consulting, Inc.

40040 COLISEUM WAY
MURRIETA, CA 92562
PH. 951.304.9552 FAX 951.304.3568

Isohyetals from NOAA Atlas 2
Volume XI - California, 1973

RCFC & WCD

RIVERSIDE COUNTY FLOOD CONT
AND
WATER CONSERVATION DISTRI

100-YEAR — 24-HOU
PRECIPITATION

APPROVED CHIEF ENGINEER R.C.F.C. NO. 8823

DRAWN BY

EXHIBIT H: SLOPE OF INTENSITY DURATION CURVES

SLOPE INTENSITY CURVE

HEMET 30
SLOPE = 0.50

JLC Engineering & Consulting, Inc.

40040 COLISEUM WAY
MURRIETA, CA 92562
PH. 951.304.9552 FAX 951.304.3568

1. Slope of Intensity-Duration Curve based on district analysis of automatic recording rain gage records

RIVERSIDE COUNTY FLOOD CONTROL AND WATER CONSERVATION DISTRICT

SLOPE OF INTENSITY DURATION CURVE

DRAWN BY R.A.S. SHEET No

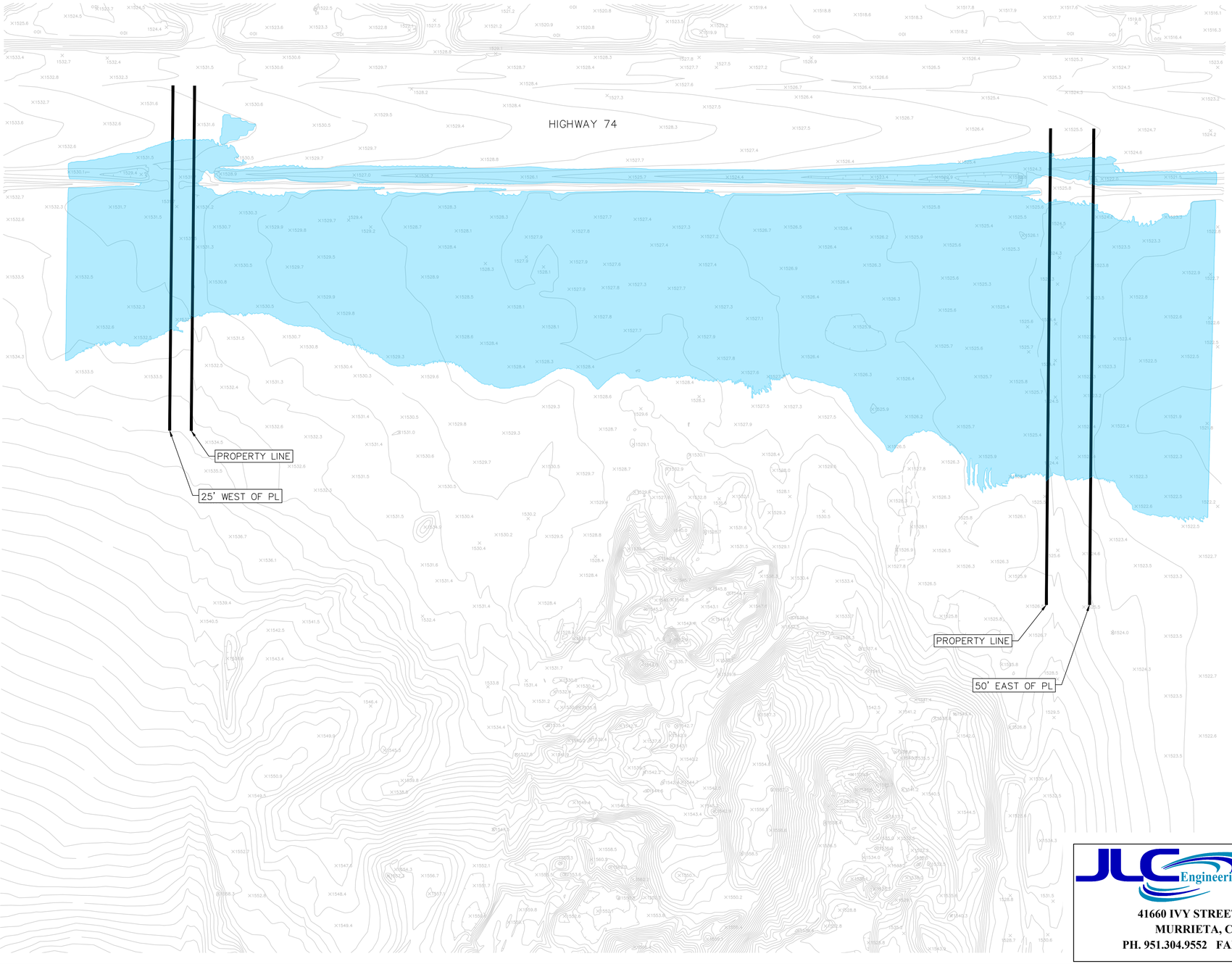
APPROVED

EXHIBIT I: PRE-PROJECT TWO DIMENSIONAL HEC-RAS MAP

HEMET 30

COUNTY OF RIVERSIDE, STATE OF CALIFORNIA

PRE-PROJECT CONDITION TWO DIMENSIONAL HEC-RAS MAP



LEGEND:

PROFILE LINE

MAXIMUM FLOOD EXTENTS

N

GRAPHIC SCALE

60' 0 30' 60' 120'

1" = 60'

EXHIBIT "I"

HEMET 30

PRE-PROJECT 2D HEC-RAS MAP

JLC Engineering & Consulting, Inc.

41660 IVY STREET, SUITE A
MURRIETA, CA 92562
PH. 951.304.9552 FAX 951.304.3568

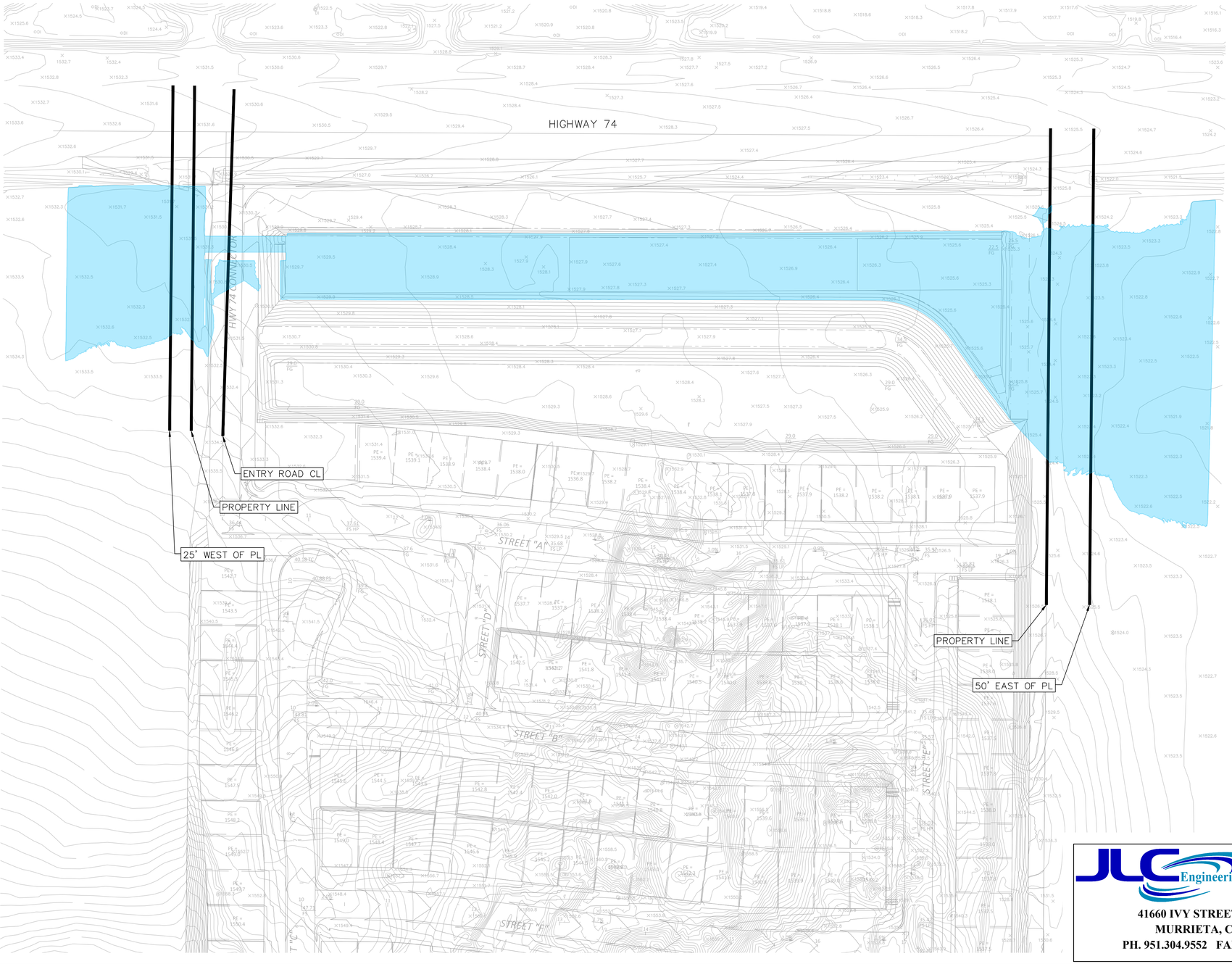
Drawing Name: Q:\150.10.19\Engineering\HEC-RAS\Exhibits\2D Pre-Project Map.dwg
Last Opened: Mar 08, 2021 - 2:21pm By Javier

EXHIBIT J: POST-PROJECT TWO DIMENSIONAL HEC-RAS MAP

HEMET 30

COUNTY OF RIVERSIDE, STATE OF CALIFORNIA

PRE-PROJECT CONDITION TWO DIMENSIONAL HEC-RAS MAP



LEGEND:

PROFILE LINE

MAXIMUM FLOOD EXTENTS

N

GRAPHIC SCALE

60' 0 30' 60' 120'

1" = 60'

EXHIBIT "J"

HEMET 30

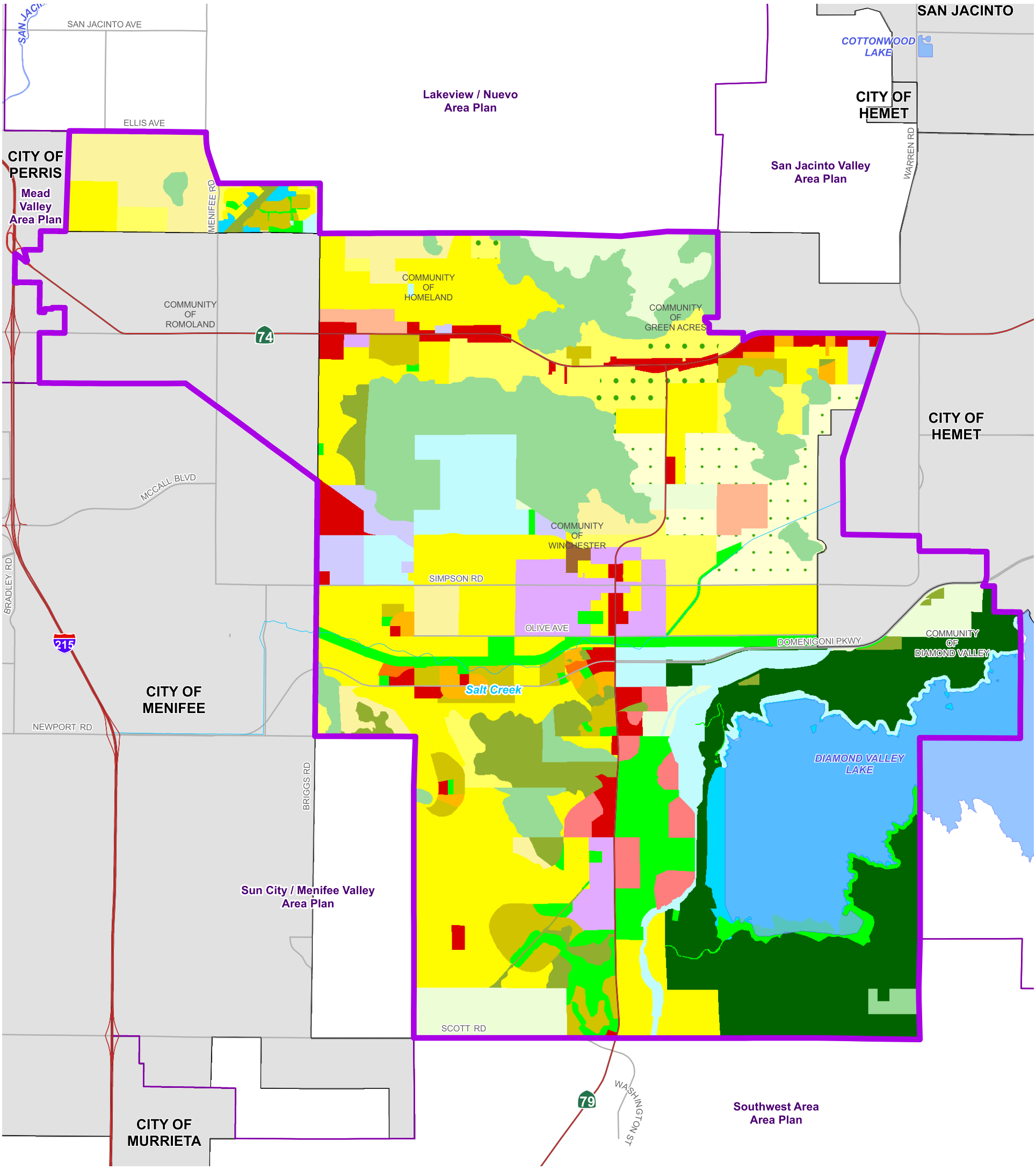
PRE-PROJECT 2D HEC-RAS MAP

JLC Engineering & Consulting, Inc.

41660 IVY STREET, SUITE A
MURRIETA, CA 92562
PH. 951.304.9552 FAX 951.304.3568

Drawing Name: G:\150.10.01\Engineering\HEC-RAS\Exhibits\2D Post-Project Map.dwg
Last Opened: Mar 08, 2021 - 2:20pm by Javier

EXHIBIT K: ULTIMATE CONDITION LAND USE MAP



Data Source: Riverside County Planning

COMMUNITY DEVELOPMENT

- Estate Density Residential
- Very Low Density Residential
- Low Density Residential
- Medium Density Residential
- Medium High Density Residential
- High Density Residential
- Very High Density Residential
- Highest Density Residential
- Commercial Retail
- Commercial Tourist
- Light Industrial
- Business Park
- Public Facilities
- Mixed-Use Area

RURAL COMMUNITY

- Rural Community - Estate Density Residential
- Rural Community - Very Low Density Residential
- Rural Community - Low Density Residential

RURAL

- Rural Residential
- Rural Mountainous

AGRICULTURE

- Agriculture

OPEN SPACE

- Conservation
- Conservation Habitat
- Open Space Recreation
- Mineral Resources
- Water

- Highways
- Area Plan Boundary
- Waterbodies
- City Boundary

Figure 3

December 6, 2016

0 0.75 1.5 Miles

Disclaimer: Maps and data are to be used for reference purposes only. Map features are approximate, and are not necessarily accurate to surveying or engineering standards. The County of Riverside makes no warranty or guarantee as to the content (the source is often third party), accuracy, timeliness, or completeness of any of the data provided, and assumes no legal responsibility for the information contained on this map. Any use of this product with respect to accuracy and precision shall be the sole responsibility of the user.

RIVERSIDE COUNTY PLANNING DEPARTMENT

HARVEST VALLEY/ WINCHESTER AREA PLAN LAND USE PLAN

Path: Y:\GP_Exhibits\HVWAP-landuse.mxd